

Appendix A

Contributions to Ontology for Ground Vehicles

A.1 General Environmental Conditions

A.1.1. *Distribution of ground on Earth to drive on (global map)*

Continents and Islands on the globe

- Geodetic reference system, databases
- Specially prepared roadways: road maps
- Cross-country driving, types of ground
 - Geometric description (3-D)
 - Support qualities for tires and tracks
- Ferries linking continents and islands

National Traffic Rules and Regulations

Global navigation system availability

A.1.2. *Lighting conditions as a function of time*

Natural lighting by sun (and moon)

- Sun angle relative to the ground for a given location and time
- Moon angle relative to the ground for a given location and time

Headlights of vehicles

- Lights for signaling intentions/special conditions
- Urban lighting conditions
- Special lights at construction sites (incl. flashes)
- Blinking blue lights

A.1.3 *Weather conditions*

- Temperatures (Effects on friction of tires)
- Winds
- Bright sunshine/Fully overcast/Partially cloudy
- Rain/Hail/Snow
- Fog (visibility ranges)
- Combinations of items above
- Road surface conditions (weather dependent)
- Dry/Wet/Slush/Snow (thin, heavy, deep tracks) /Ice
- Leaf cover (dry – wet)/Dirt cover (partial – full)

A.2 Roadways

A.2.1. *Freeways, Motorways, Autobahnen etc.*

- Defining parameters, lane markings
- Limited access parameters
- Behavioral rules for specific vehicle types
- Traffic and navigation signs
- Special environmental conditions

A.2.2. *Highways (State-), high-speed roads*

- Defining parameters, lane markings (like above)

A.2.3. *Ordinary state roads (two-way traffic) (like above)*

A.2.4. *Unmarked country roads (sealed)*

A.2.5. *Unsealed roads*

A.2.6. *Tracks*

A.2.7. *Infrastructure along roadways*

Line markers on the ground, Parking strip, Arrows,

Pedestrian crossings

Road shoulder, Guide rails

Regular poles (reflecting, ~1 m high) and markers for snow conditions

A.3 Vehicles

(as objects without driver/autonomous system; wheeled vehicles, vehicles with tracks, mixed wheels and tracks)

A.3.1. *Wheeled vehicles*

Bicycle: Motorbike, Scooter;

Bicycle without a motor: Different sizes for grown-ups and children

Tricycle

Multiple (even) number of wheels

Cars, Vans/microbuses, Pickups/Sports utility vehicles, Trucks,

Buses, Recreation vehicles, Tractors, Trailers

A.3.2. *Vehicles with tracks*

A.3.3. *Vehicles with mixed tracks and wheels*

A.4 Form, Appearance, and Function of Vehicles

(shown here for cars as one example; similar for all classes of vehicles)

A.4.1. *Geometric size and 3-D shape (generic with parameters)*

A.4.2. *Subpart hierarchy*

Lower body, Wheels, Upper body part, Windshields (front and rear)

Doors (side and rear), Motor hood, Lighting groups (front and rear)

Outside mirrors

A.4.3. *Variability over time, shape boundaries (aspect conditions)*

A.4.4. *Photometric appearance (function of aspect and lighting conditions)*

Edges and shading, Color, Texture

A.4.5. *Functionality (performance with human or autonomous driver)*

Factors determining size and shape

Performance parameters (as in test reports of automotive journals; engine power, power train)

Controls available [throttle, brakes, steering (*e.g.*, “Ackermann”)]

Tank size and maximum range

Range of capabilities for standard locomotion:

Acceleration from standstill

Moving into lane with flowing traffic

Lane keeping (accuracy)

Observing traffic regulations (max. speed, passing interdiction)

Distance keeping from vehicle ahead
 (standard, average values, fluctuations)
 Lane changing [range of maneuver times as $f(\text{speed})$]
 Overtaking behavior [safety margins as $f(\text{speed})$]
 Braking behavior (moderate, reasonably early onset)
 Proper setting of turn lights before start of maneuver
 Turning off onto crossroad
 Entering and leaving a circle
 Handling of road forks
 Observing right of way at intersections
 Negotiating “hair-pin” curves (switchbacks)
 Proper reaction to static obstacle detected in your lane
 Proper reaction to animals detected on or near the driveway
 Emergency stops
 Parking alongside the road
 Parking in bay
 U-turns
 Safety features (ABS, ESP ...)
 Self-check capabilities
 Tire pressure
 Engine performance (a few easy standard tests like “gas pulses”)
 Brake performance

A.4.6. *Visually observable behaviors of others* (driven by a human or autonomously)

Standard behavioral modes (like list of capabilities above)

Unusual behavioral modes

Reckless entrance into your lane from parking position or neighboring lane at much lower speed
 Oscillations over entire lane width (even passing lane markings)
 Unusually slow speeds with no noticeable external reason
 Disregarding traffic regulations [max. speed (average amount), passing interdiction, traffic lights]
 Very short distance to vehicle ahead
 Hectic lane change behavior, high acceleration levels (very short maneuver times, large vehicle pitch and bank angles, “slalom” driving)
 Overtaking behavior (daring, frequent attempts, questionable safety margins, cutting into your lane at short distance)
 Braking behavior (sudden and harsh?)
 Start of lateral maneuvers before or without proper setting of turn lights.
 Speed not adapted to actual environmental conditions (uncertainties and likely fluctuations taken into account)
 Disregarding right of way at intersections.
 Pedestrians disregarding standard traffic regulations
 Bicyclists disregarding standard traffic regulations

Recognizing unusual behavior of other traffic participants due to unexpected or sudden malfunctions (perturbations).

Reaction to animals on the driveway (f(type of animal))

Other vehicles slipping due to local environmental conditions (like ice)

A.4.7. Perceptual capabilities

A.4.8. Planning and decision making capabilities

A.5 Form, Appearance, and Function of Humans

(Similar structure as above for cars plus modes of locomotion)

A.6 Form, Appearance, and Likely Behavior of Animals

(relevant in road traffic: Four-legged, birds, snakes)

A.7 General Terms for Acting “Subjects” in Traffic

Subjects: Contrary to “objects” (proper), having passive bodies and no capability of self-controlled acting, “subjects” are defined as objects with the capability of sensing and self-decided control actuation. Between sensing and control actuation, there may be rather simple or quite complicated data processing available taking stored data up to large knowledge bases into account. From a vehicle guidance point of view, both human drivers and autonomous perception and control systems are subsumed under this term. It designates a superclass encompassing all living beings and corresponding technical systems (*e.g.*, robots) as members.

These systems can be characterized by their type of equipment and performance levels achieved in different categories. Table 3.1 shows an example for road vehicles.

The capabilities in the shaded last three rows are barely available in today’s experimental intelligent road vehicles. Most of the terms are used for humans in common language. The terms “behavior” and “learning” should be defined more precisely since they are used with different meanings in different professional areas (*e.g.*, in biology, psychology, artificial intelligence, engineering).

Behavior (as proposed here) is an all-encompassing class term subsuming any kind and type of ‘action over time’ by subjects.

Action means using any kind of control variable available to the subject, leading to changes in the state variables of the problem domain.

State variables are the set of variables allowing decoupling future developments of a dynamic system from the past (all the history of the system with respect to body motion is stored in the present state); state variables cannot be changed at one moment. (Note two things: (1) This is quite the opposite of the definition of “state” in computer science; (2) accelerations are in general not (direct) state variables in this systems-dynamics sense since changes in control variables will affect them directly.)

Control variables are the leverage points for influencing the future development of dynamic systems. In general, there are two components of control activation involved in intelligent systems. If a payoff function is to be optimized by a “*maneuver*”, previous experience will have shown that certain control time

histories perform better than others. It is essential knowledge for good or even optimal control of dynamic systems, to know in which situations to perform what type of maneuver with which set of parameters; usually, the maneuver is defined by certain time histories of (coordinated) control input. The unperturbed trajectory corresponding to this nominal feed-forward control is also known, either stored or computed in parallel by numerical integration of the dynamic model exploiting the given initial conditions and the nominal control input. If perturbations occur, another important knowledge component is knowing how to link additional control inputs to the deviations from the nominal (optimal) trajectory to counteract the perturbations effectively. This has led to the classes of feed-forward and feedback control in systems dynamics and control engineering:

Feed-forward control components \underline{U}_{ff} are derived from a deeper understanding of the process controlled and the maneuver to be performed. They are part of the knowledge base of autonomous dynamic systems (derived from systems engineering and optimal control theory). They are stored in generic form for classes of ‘maneuvers’. Actual application is triggered from an instance for behavior decision and implemented by an embedded processor close to the actuator, taking the parameters recommended and the actual initial and desired final conditions (states) into account.

Feedback control components \underline{u}_{fb} link actual (additional) control output to system state or (easily measurable) output variables to force the trajectory toward the desired one despite perturbations or poor models underlying step 1. The technical field of ‘control engineering’ has developed a host of methods also for automotive applications. For linear (linearized) systems, linking the control output to the entire set of state variables allows specifying the “eigenmodes” ‘at will’ (in the range of validity of the linear models). In output feedback, adding components proportional to the derivative (D) and/or integral (I) of the signal allows improving speed of response (PD) and long-term accuracy (PI, PID).

Combined feed-forward and feedback control: For counteracting at least small perturbations during maneuvers, an additional feedback control component \underline{u}_{fb} may be superimposed on the feed-forward one (\underline{U}_{ff}) yielding a robust implementation of maneuvers.

Longitudinal control: In relatively simple, but very often sufficiently precise models of vehicle dynamics, a set of state variables affected by throttle and (homogeneous) braking actions with all wheels forms an (almost) isolated subsystem. It consists of the translational degrees of freedom in the vertical plane containing the plane of symmetry of the vehicle and the rotational motion in pitch, normal to this plane. The effects of gravity on sloping surfaces and the resulting performance limits are included.

Lateral control: Lateral translation (y direction), rotations around the vertical (z) and the longitudinal (x) axes form the lateral degrees of freedom, controlled essentially by the steer angle. Lateral motion of larger amplitude does have an influence also on longitudinal forces and pitching moment.

Maneuvers are stereotypical control output time histories (feed-forward control) known to transform (in the nominal case) the initial system state $\underline{x}(t_0)$ into a fi-

nal one $\underline{x}(t_i)$ in a given time (range) with boundary conditions (limits) on state variables observed. Certain ranges of perturbations during the maneuver can be counteracted by superimposed feedback control.

Maneuvers may be triggered by higher level decisions for implementing strategic ‘*mission elements*’ (e.g., turning off onto a crossroad) or in the context of a behavioral mission element running, due to the actual *situation* encountered (e.g., lane change for passing slower traffic or an evasive maneuver with respect to a static obstacle during ‘roadrunning’).

Table 3.3 gives a collection of road vehicle behavioral capabilities realized by feed-forward (left column) and feedback control (right column).

Mission elements are those parts of an entire mission that can be performed with the same subset of behavioral capabilities and parameters. Note that mission elements are defined by sets of compatible behavioral capabilities of the subject *actually performing* the mission.

Situation is the collection of environmental and all other facts that have an influence on making proper (if possible ‘optimal’) behavior decisions in the mission context. This also includes the state within a maneuver being performed (percentage of total maneuver performed, actual dynamic loads, *etc.*) and all safety aspects.

General comment:

Dimension: There are only four dimensions in our (mesoscale) physical world: Three space components and time. Rotational rates and velocities are components of the physical state, due to the nature of mechanical motion described by second-order differential equations (Newton’s law). These velocity components are additional degrees of freedom (d.o.f.), but not dimensions as claimed in some recent publications. Recursive estimation with physically meaningful models delivers these variables together with the pose variables.

Dimensions from discretization: In search problems it is a habit to call the possible states of a variable the dimension of the search space; this has nothing to do with physical dimensions.

Appendix B

Lateral Dynamics

B.1 Transition Matrix for Fourth-Order Lateral Dynamics

The linear process model for lateral road vehicle guidance derived in Chapters 3 and 7 (see Table 9.1) can be written as a seventh order system in analogue form [Mysliwetz 1990]:

$$\dot{x}(t) = Fx + g'u + v'(t) \quad (\text{Equation 3.6 with one control variable}) \quad (\text{B.1})$$

$$\begin{pmatrix} \dot{\lambda} \\ \dot{\beta} \\ \dot{\Psi}_{rel} \\ \dot{y}_V \\ \dot{C}_{0hm} \\ \dot{C}_{lhm} \\ \dot{C}_{lh} \end{pmatrix} = \begin{pmatrix} 0 & 0 & 0 & 0 & | & 0 & 0 & 0 \\ f_{12} & -1/T_\beta & 0 & 0 & | & 0 & 0 & 0 \\ V/a & 0 & 0 & 0 & | & -V & 0 & 0 \\ 0 & V & V & 0 & | & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & | & 0 & V & 0 \\ 0 & 0 & 0 & 0 & | & 0 & -3 \cdot V/L & 3 \cdot V/L \\ 0 & 0 & 0 & 0 & | & 0 & 0 & 0 \end{pmatrix} \begin{pmatrix} \lambda \\ \beta \\ \Psi_{rel} \\ y_V \\ C_{0hm} \\ C_{lhm} \\ C_{lh} \end{pmatrix} + \begin{pmatrix} k_\lambda \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix} \cdot u(t) + \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ n_{C_{lh}} \end{pmatrix}$$

$$\text{with } f_{12} = 1/(2T_\beta) - V/a; \quad T_\beta = V/k_{luf}; \quad \text{Equation 3.30.}$$

With T as cycle time for sampling (video frequency), the Laplace transform for the transition matrix is (see, e.g., [Kailath 1980]):

$$A(T) = L^{-1}\{(sI - F)^{-1}\}. \quad (\text{B.2})$$

For the discrete input gain vector g , one obtains from F and g'

$$g = \int_0^T A(\tau)g' d\tau. \quad (\text{B.3})$$

The noise term also has to be adjusted properly in correspondence with T . The resulting difference equation is B.4. The matrix A and the input gain vector g have the entries given below (note that g has many more entries than g' ; this is due to the buildup of state components from constant control input over one cycle!):

$$x(k+1) = A \cdot x(k) + g \cdot u(k) + v(k). \quad (\text{B.4})$$

$$A = \begin{pmatrix} 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ a_{21} & a_{22} & 0 & 0 & 0 & 0 & 0 \\ a_{31} & 0 & 1 & a_{34} & a_{35} & a_{36} & a_{37} \\ a_{41} & a_{42} & a_{43} & 1 & a_{45} & a_{46} & a_{47} \\ 0 & 0 & 0 & 0 & 1 & a_{56} & a_{57} \\ 0 & 0 & 0 & 0 & 0 & a_{66} & a_{67} \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 \end{pmatrix} \quad \text{and } g = \begin{pmatrix} g_1 \\ g_2 \\ g_3 \\ g_4 \\ 0 \\ 0 \\ 0 \end{pmatrix}. \quad (\text{a})$$

With the following abbreviations:

$$\begin{aligned} c_F &= V/a; & a_F &= -2k_{\text{lf}}/V; \\ b_F &= -k_{\text{lf}}/V + c_F; & a_c &= -3V/L; \end{aligned}$$

the non-vanishing elements a_{ij} of the transition matrix are

$$\begin{aligned} a_{21} &= b_F/a_F \cdot (e^{a_F T} - 1); & a_{22} &= e^{a_F T} \\ a_{31} &= c_F T; & a_{35} &= -VT; & a_{36} &= V^2/a_c^2 \cdot (a_c T + 1 - e^{a_c T}); \\ a_{37} &= -V^2[(1 - e^{a_c T})/a_c^2 + T/a_c + T/2]; \\ a_{41} &= (b_F V/a_F) \cdot [(e^{a_F T} - 1)/a_F - T] + c_F VT^2/2; \\ a_{42} &= (e^{a_F T} - 1)V/a_F; & a_{43} &= VT; & a_{45} &= -V^2 T^2/2; \\ a_{46} &= V^3[(1 - e^{a_c T})/a_c^2 + T/a_c + T/2]/a_c; \\ a_{47} &= -V^3[-(1 - e^{a_c T})/a_c^3 + T/a_c^2 + T/(2a_c) + T^3/6]; \\ a_{56} &= -V(1 - e^{a_c T})/a_c; & a_{57} &= V(a_c T + 1 - e^{a_c T})/a_c; \\ a_{66} &= e^{a_c T}; & a_{67} &= 1 - e^{a_c T}. \end{aligned}$$

The entries in the input gain vector are

$$\begin{aligned} g_1 &= T; & g_2 &= b_F/a_F \cdot \{(e^{a_F T} - 1)/a_F - T\}; & g_3 &= c_F T^2/2; \\ g_4 &= -b_F V/a_c^2 \cdot [T + a_F T^2/2 - (e^{a_F T} - 1)/a_F] - c_F VT^3/6. \end{aligned}$$

The rows in matrix A are given by the first index; this corresponds to the sequential innovation scheme in square root filtering using row vectors of A . Note that out of the 49 elements of A , 26 are zero (53%); explicit use of this structure can help making vector multiplication very economical: for rows 1 and 7 (first and last), the result has the same value as the multiplicand. For row index 2, multiplication of elements can stop at this row index 2, while for indices 5 and 6, starting multiplication at these indices is sufficient. Efficiently coded, many multiplications may be saved in this inner loop that is always running. Since several multiplications with these vectors occur in recursive computation of the expected error covariance (step 7.2 in Table 6.1), being efficient here really pays off in real-time vision.

B.2 Transfer Functions and Time Responses to an Idealized Doublet in Fifth-order Lateral Dynamics

From Equations 3.38 and 3.45, the analytical solution for the state vector in the ‘Laplace s -realm’ is obtained. The former equation yields for the ‘system matrix’

$$sI - \Phi = \begin{pmatrix} s & 0 & 0 & 0 & 0 \\ -V/(aT_\psi) & s+1/T_\psi & 0 & 0 & 0 \\ -1/(2T_\beta) & 1 & s+1/T_\beta & 0 & 0 \\ 0 & -1 & 0 & s & 0 \\ 0 & 0 & -V & -V & s \end{pmatrix}. \quad (\text{B.5})$$

By multiplication of Equation 3.45 from the left by $(sI - \Phi)^{-1}$, there follows

$$\underline{x}_{La}(s) = (sI - \Phi)^{-1} \cdot \underline{b} \cdot u(s) + (sI - \Phi)^{-1} \cdot \underline{x}_{La}(0). \quad (\text{B.6})$$

The first term defines the five transfer functions of a control input $u(s)$ while the second term gives the response to initial values in the state variables. All these expressions have a common denominator, the characteristic polynomial $D(s)$ of the determinant $\det(sI - \Phi)$

$$D = s^3(s + 1/T_\psi)(s + 1/T_\beta). \quad (\text{B.7})$$

The numerator polynomials of the transfer functions are obtained by the determinants in which the column corresponding to the state variable of interest has been replaced by the coefficient vector \underline{b} for control input. This yields the numerator terms for the heading angle ψ and the lateral position y

$$\begin{aligned} N_\psi &= [V/(a \cdot T_\psi)] \cdot s \cdot (s + 1/T_\beta) \\ N_y &= Va/(2T_\beta) \cdot [s^2 + s/T_\psi + 2V/(a \cdot T_\psi)]. \end{aligned} \quad (\text{B.8})$$

With the doublet input of Equation 3.44, $u_{\text{idd}}(s) = A \cdot s$, the resulting state variables yaw angle $\psi(s)$ and the lateral acceleration in the y direction $s^2 \cdot y(s)$ are in the Laplace-domain

$$\begin{aligned} \psi(s) &= [N_\psi / D] \cdot A \cdot s \\ &= A \cdot s [V/(a T_\psi)] \cdot s (s + 1/T_\beta) / [s^3 \cdot (s + 1/T_\beta)(s + 1/T_\psi)] \\ &= A V/(a T_\psi) / [s (s + 1/T_\psi)] \\ &= A V/(a T_\psi) \cdot [1/s - 1/(s + 1/T_\psi)]. \end{aligned} \quad (\text{B.9})$$

$$\begin{aligned} a_y(s) &= s^2 \cdot y(s) = N_y \cdot A \cdot s^3 / D \\ &= A V / T_\beta \cdot s^3 \cdot [s^2 + s/T_\psi + 2V/(a \cdot T_\psi)] / D \\ &= Va/(2T_\beta) \cdot [1(s) + B/(s + 1/T_\psi) - (B + 1/T_\beta)/(s + 1/T_\beta)], \\ &\quad \text{with } B = 2V/[a \cdot (T_\psi/T_\beta - 1)]. \end{aligned} \quad (\text{B.10})$$

The expression $1/s$ in Equation B.9 corresponds in the time domain to a unit step function, and the second term in Equation B.9: $c/(s + 1/T_i)$ to: $c \cdot \exp[-(t/T_i)]$. This yields with Equation 3.36 after back-transformation into the time domain

$$\psi(t)_{\text{doublet}} = A \cdot k_{\text{tff}} / (a \cdot i_{zB}^2) \cdot [1 - \exp(-t/T_\psi)]. \quad (\text{B.11})$$

$1(s)$ in Equation B.10 corresponds to a ‘Dirac impulse’ $\delta(0)$ at time 0 with an integral value of 1 (a step function in the integrated variable, the lateral velocity $v_y = \int a_y dt$ experiences a jump from 0 to 1 at $t = 0$). Introducing this and the relations given in Equation 3.37 into Equation B.10 yields for the time functions

$$\begin{aligned} a_y(t) &= A \cdot k_{\text{tff}} \cdot \left\{ 0.5 \cdot \delta(0) + \frac{V}{a(1 - i_{zB}^2)} \cdot [e^{-t/T_\beta} - e^{-t/T_\psi}] - \frac{0.5 \cdot k_{\text{tff}}}{V} e^{-t/T_\beta} \right\} \quad (\text{a}) \\ &= \frac{A}{2} \cdot k_{\text{tff}} \cdot \delta(0) + e^{-t/T_\beta} \cdot \left\{ \frac{VA k_{\text{tff}}}{a(1 - i_{zB}^2)} \cdot [1 - e^{-t/T_{\beta\text{mod}}}] - \frac{A k_{\text{tff}}^2}{2V} \right\}, \quad (\text{b}) \end{aligned} \quad (\text{B.12})$$

where $T_{\beta\text{mod}} = T_\beta \cdot i_{zB}^2 / (1 - i_{zB}^2)$.

The value $T_{\beta\text{mod}}/T_\beta = i_{zB}^2 / (1 - i_{zB}^2)$ is 2.77 for VaMoRs and 5.67 for VaMP. Figure B.1 shows the principal time histories of the exponential functions in scaled form

for VaMoRs. The yaw angle goes from zero to $[A \cdot k_{lf} / (a \cdot i_{zB}^2)]$ with time constant T_ψ . According to Equation 3.37, T_ψ increases linearly with speed.

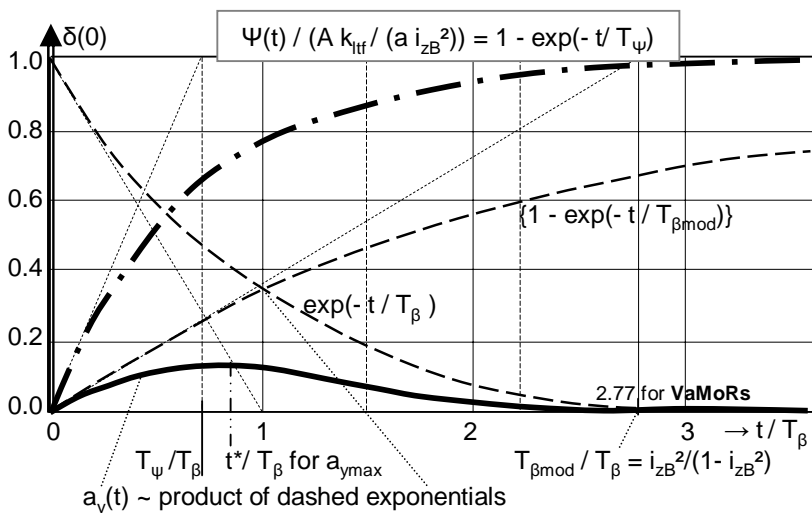


Figure B.1. Scaled dynamic response in yaw angle (*dash-dotted*) and lateral acceleration (*solid curve*) to doublet input in steering rate (see Equations B.11/B.12); the time axis is scaled by T_β

Appendix C

Recursive Least-squares Line Fit

Through a set of measurement points ($y_{m1} \dots y_{mN}$), equidistantly spaced on the abscissa ($x_1 = 0.5, 1.5 \dots N-0.5$), a straight line shall be fit recursively with interpolated measurement points ($y_1 \dots y_N$), if the standard deviation remains below a threshold value $\sigma_{\max th}$ and the new measurement point to be added is within a 3σ band around the existing fit. The resulting set of smoothed measurement data will be called a segment or a 1-D blob. The result shall be represented by the average value y_c in the segment, with the origin at the segment center x_c , and the (linear) slope ‘ a ’ around this center (see Figure C.1). A deviation from the usual terminology occurs because image evaluation with symmetric masks has its origin right between pixel boundaries; the reference pixel for mask evaluation has been selected at position (0.5, 0.5) of the mask (see Figure 5.19).

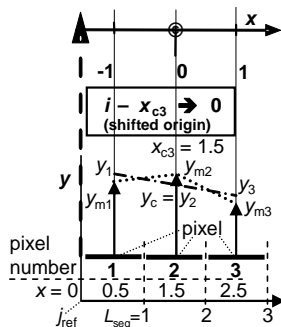


Figure C.1. Nomenclature used with integer basic scale for pixels; origin of centered scale at $N/2$

This definition leads to the fact that x_c is either an integer or lies exactly at the center between two integers ($i - 0.5$). Due to the integer values for the pixels and because a new segment is always started with the *reference coordinate* j_{ref} for $x_0 = 0$, the center of N values is located at

$$x_{c,abs} = j_{ref} + N/2 = j_{ref} + x_c. \quad (C.1)$$

C.1 Basic Approach

Since two measurement points can always be connected by a straight line, interpolation starts at the third point into a new segment. The general form of the interpolating straight line with x_c as the center of all x_i is

$$y_i = y_c + a \cdot \Delta x_i \quad (C.2)$$

$$\text{with } \Delta x_i = x_i - x_c.$$

y_c is always taken at the center of the data set, and ‘ a ’ is the slope of the line. This yields for the residues $e_i = y_i - y_{mi}$ (see Figure C.1) the set of equations:

$$\begin{aligned} e_1 &= y_c + (x_1 - x_c) \cdot a - y_{m1}, \\ e_2 &= y_c + (x_2 - x_c) \cdot a - y_{m2}, \\ e_3 &= y_c + (x_3 - x_c) \cdot a - y_{m3}. \end{aligned} \quad (C.3)$$

For easy generalization, this is written in matrix form with the two unknown variables: average value y_c of the interpolating straight line and slope a . The measurement vector y_m has length N , with the original running index i linearly increasing

from 1 to N ; measurement values of the pixels then are located at x -position [(pixel index i) $- 0.5$]; the initial value for N is 3 (Figure C.1). The running index for the shifted scale with $x_c = 0$ then goes from $-N/2$ to $+N/2$. With the model of Equation C.2, the errors are

$$[e] = \begin{bmatrix} 1 & x_1 - x_c \\ \cdot & \cdot \\ 1 & x_i - x_c \\ \cdot & \cdot \\ 1 & x_N - x_c \end{bmatrix} \cdot \begin{bmatrix} y_c \\ a \end{bmatrix} - [y_m]_N = A \cdot p - [y_m]_N. \quad (\text{C.3a})$$

The sum J of the squared errors can now be written

$$J = \sum_{i=1}^n e_i^2 = e^T e = (A \cdot p - y_m)^T (A \cdot p - y_m). \quad (\text{C.4})$$

The same procedure as in Section 5.3.2.1, setting the derivative $dJ/dp = 0$, leads to the optimal parameters p_{extr} for minimal J :

$$\begin{pmatrix} y_c \\ a \end{pmatrix}_{LS} = p_{extr} = (A^T A)^{-1} A^T y_m. \quad (\text{C.5})$$

With $x_i = i - 0.5$ from 0.5 to $N - 0.5$, and with Equation C.3a the product $A^T A$ can be written

$$A^T A = \begin{bmatrix} 1 & \cdot & \cdot & \cdot & \cdot \\ 0.5 - x_c & \cdot & i - 0.5 - x_c & \cdot & N - 0.5 - x_c \end{bmatrix} \cdot \begin{bmatrix} 1 & 0.5 - x_c \\ \cdot & \cdot \\ 1 & i - 0.5 - x_c \\ \cdot & \cdot \\ 1 & N - 0.5 - x_c \end{bmatrix} \quad (\text{C.6})$$

$$= \begin{bmatrix} N & a_{12} \\ a_{21} & a_{22} \end{bmatrix}.$$

By always choosing the center of gravity of the abscissa values x_c as reference and by shifting the indices correspondingly (see lower part of Figures C.1 and C.2), there follows

$$a_{21} = a_{12} = \sum_{i=1}^N (i - 0.5 - x_c) = 0. \quad (\text{C.7})$$

For each positive index in the shifted coordinates (lower part of figures), there is a corresponding negative one, yielding Equation C.7. This means that $A^T A$ is zero off the main diagonal. For a_{22} in Equation C.6 one obtains

$$a_{22} = \sum_{i=1}^N (i - 0.5 - x_c)^2 = \sum_{i=1}^N (i^2 - 2 \cdot i \cdot x_c + x_c^2 + 0.25 + x_c - i). \quad (\text{C.8})$$

Introducing the well-known relations

$$\sum_{i=1}^N i = N(N+1)/2, \quad (\text{C.9})$$

$$\sum_{i=1}^N i^2 = N(N+1)(2N+1)/6, \quad (\text{C.10})$$

the following result for a_{22} is obtained with $x_c = N/2$ after several steps

$$a_{22} = N(N^2 - 1)/12. \quad (\text{C.11})$$

With Equations C.7 and C.11 the inverse of $A^T A$ (Equation C.6) becomes

$$(A^T A)^{-1} = \begin{pmatrix} 1/N & 0 \\ 0 & 1/a_{22} \end{pmatrix}. \quad (\text{C.12})$$

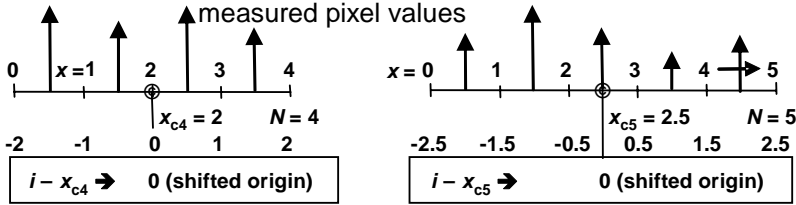


Figure C.2. Centered coordinates for even and odd numbers of equidistant grid points; this choice reduces the numerical workload

To obtain the optimal parameters for a least squares fit according to Equation C.6, the factor $A^T y_m$ has yet to be determined:

$$A^T y_m = \begin{bmatrix} 1 & \dots & 1 & \dots & 1 \\ 1-0.5-x_c & \dots & i-0.5-x_c & \dots & N-0.5-x_c \end{bmatrix} \cdot \begin{bmatrix} y_{m1} \\ \vdots \\ y_{mi} \\ \vdots \\ y_{mN} \end{bmatrix} \quad (\text{C.13})$$

$$= \begin{bmatrix} \text{Sym} \\ \text{Siym} - 0.5 \cdot \text{Sym} - x_c \cdot \text{Sym} \end{bmatrix},$$

$$\text{with } \text{Sym} = \sum_{i=1}^N y_{mi} \quad \text{and} \quad \text{Siym} = \sum_{i=1}^N (i \cdot y_{mi}). \quad (\text{a})$$

Inserting this, the relation $x_c = N/2$, and Equation C.11 into C.5, the following optimal parameters y_c and a are finally obtained:

$$\begin{pmatrix} y_c \\ a \end{pmatrix}_{LS} = \begin{pmatrix} 1/N & 0 \\ 0 & 1/a_{22} \end{pmatrix} \cdot \begin{pmatrix} \text{Sym} \\ \text{Siym} - \frac{N+1}{2} \text{Sym} \end{pmatrix} \quad (\text{C.14})$$

or

$$\begin{pmatrix} y_c \\ a \end{pmatrix}_{LS} = \begin{bmatrix} \text{Sym}/N \\ \left(\text{Siym} - \frac{N+1}{2} \text{Sym} \right) / a_{22} \end{bmatrix} = \begin{bmatrix} \text{Sym}/N \\ \frac{6}{N-1} \left(\frac{2}{N+1} \cdot \frac{\text{Siym}}{N} - \frac{\text{Sym}}{N} \right) \end{bmatrix}. \quad (\text{C.14}) \quad (\text{a})$$

y_c is nothing but the average value of all measurements y_{mi} ; to obtain the optimal slope a , the product $i \cdot y_{mi}$ has to be summed, too (Equation C.13a). It is seen

that for this least-squares fit with a cg-centered coordinate system ($y(0) = y_c$), where this origin moves in steps by 0.5 with N increasing by 1, just four numbers have to be stored: The number of data points N , the averaged sum of all measured values $y_c = Sym/N$, the averaged sum of all products ($i \cdot y_{mi}$): $Siym/N$, and, of course, the reference for $i = 1$ where the data set started; this yields the optimal parameters: ‘ $y_c = \text{average value at the segment center}$ ’ and ‘ $a = \text{slope}$ ’ for the best interpolating straight line by just a few mathematical operations independent of segment length n .

C.2 Extension of Segment by One Data Point

Let the existing segment have length N ; the averaged sums Sym/N and $Siym/N$ (Equation C.13) have been stored. If one new measurement value arrives, its expected magnitude according to the existing model can be computed. The number of measurements increases by 1, and the new segment center x_{ce} shifts to

$$N_e = N + 1; \quad x_{ce} = N_e / 2 = x_c + 0.5. \tag{C.15}$$

The predicted measurement value according to the linear model is

$$y_{mpr} = y_c + a \cdot (N + 1 - x_c) = y_{cpr} + a(N_e - x_{ce}). \tag{C.16}$$

Since the new origin x_{ce} is shifted to the right by 0.5, the expected average value y_{cpr} will be shifted by $a/2$, yielding the rightmost part of Equation C.16. The new measurement value y_{mNe} will be accepted as extension of the segment only if

$$|y_{mNe} - y_{mpr}| \leq 3 \cdot \sigma, \tag{C.17}$$

or $(y_{mNe} - y_{mpr})^2 \leq 9 \cdot \sigma^2,$

with σ^2 as variance of all previous measurements; otherwise, the segment is concluded with the original value for N .

If the segment is extended, the new parameters for best fit are, according to Equation C.14a

$$\begin{aligned} y_{ce} &= \frac{Sym_e}{N_e} = \left[\left(\frac{Sym}{N} \right) \cdot \frac{N}{N_e} + \frac{y_{mNe}}{N_e} \right]; \\ a_e &= \frac{6}{N_e - 1} \cdot \left(\frac{Siym_e / N_e}{x_{ce}} - y_{ce} \right) \\ &= \frac{6}{N_e - 1} \left\{ \frac{1}{x_{ce}} \cdot \left[\left(\frac{Siym}{N} \right) \cdot \frac{N}{N_e} + y_{mNe} \right] - y_{ce} \right\}. \end{aligned} \tag{C.18}$$

The terms in rounded brackets are the stored (original) values, while the terms in squared brackets are the new values for $N_e = N + 1$ to be stored. The definition of the variance is

$$Var(e)_N := \frac{1}{N - 1} \sum_{i=1}^N e_i^2 = J / N \quad (\text{with Equation C.4}). \tag{C.19}$$

Inserting the result C.14a for p in J , and exploiting the relations C.1 and C.6 to C.13, one obtains, with $y_m^T y_m = \sum_{i=1}^N y_{mi}^2 = Sy2m$ as shorthand notation,

$$\text{Var}(e)_N = \frac{\text{Sy}2m}{N-1} - f(\text{Siym}, N, a, x_c, y_c). \quad (\text{C.19a})$$

To be able to compute the variance recursively, the sum of the squared measurement values $\text{Sy}2m$ (divided by $N-1$) also has to be stored as an entry into Equation C.19a. The recursive update from N to $N+1$ is given below (on the right side)

$$\frac{\text{Sy}2m}{N} = \frac{1}{N} \sum_{i=1}^N y_{mi}^2 \quad \text{or} \quad \frac{\text{Sy}2m_e}{N_e} = \left[\frac{N}{N_e} \cdot \left(\frac{\text{Sy}2m}{N} \right) + \frac{y_{mNe}^2}{N_e} \right]. \quad (\text{C.20})$$

This shows that the new stored value (in square brackets) results from the old one (in rounded brackets) weighted by the factor N/N_e and the squared new measurement value weighted by $1/N_e$. Since the rather complex expressions for the variance are not used in the real-time algorithm, they are not discussed in detail here (see next section).

C.3 Stripe Segmentation with Linear Homogeneity Model

Instead of comparing the magnitude of the prediction error with the 3σ -value of the existing fit, as a criterion for acceptance of the next measurement point, the less computer-intensive criterion in the lower part of Equation C.17 is used:

$$(y_{mpr} - y_{mNe})^2 \leq 9 \cdot \sigma_N^2 = 9 \cdot (\text{Var}(e)|_N), \quad (\text{C.21})$$

or even

$$(y_{mpr} - y_{mNe})^2 \leq \text{variance limit (VarLim)}.$$

VarLim is a fixed threshold parameter of the method; for typical intensity values of video signals (8 to 10 bit, 256 to 1k levels) and the sensitivity of the human eye (~60 levels), threshold values $4 \leq \text{VarLim} \leq 225$ seem reasonable. With Equation C.21, acceptance can be decided without computing the new fit and the new variance. The influence of the new measurement point on the parameters for optimal fit is neglected.

The second method is to compute all new parameters including the new variance and to compare the residue

$$e_{Ne} = y_{cNe} + a_{Ne} \cdot (N_e - x_{ce}) - y_{mNe} \quad (\text{C.22})$$

squared of the new measurement point N_e with the newly determined variance

$$e_{Ne}^2 \leq 9 \cdot \sigma_{Ne}^2 = 9 \cdot (\text{Var}(e)|_{Ne}). \quad (\text{C.23})$$

When the new value is accepted, store all updated values:

$$N = N_e; \quad \frac{\text{Sym}}{N} = \frac{\text{Sym}_e}{N_e}; \quad \frac{\text{Siym}}{N} = \frac{\text{Siym}_e}{N_e}; \quad \frac{\text{Sy}2m}{N} = \frac{\text{Sy}2m_e}{N_e}; \quad (\text{C.24})$$

$$y_c = y_{ce}; \quad x_c = x_c + 0.5; \quad a = a_e; \quad \text{Var}(e)|_N = \text{Var}(e)|_{Ne}.$$

Now the next value can be tested with the same procedure.

C.4 Dropping Initial Data Point

This segment reduction at the start may sometimes have beneficial effects on the quality of the linear fit. After several data points have been interpolated by a straight line, the variance of the whole set may be reduced by dropping the first point or a few initial points from the segment. An indication for this situation is given when the first residue on the left side is larger than the standard deviation of the segment. To check this, the interpolated value at location $i = 1$ has to be computed with the parameter set $(y_{cN}$ and $a_N)$ after N data points

$$e_{1N} = y_{cN} + a_N \cdot (1 - x_{cN}) - y_{m1}. \quad (\text{C.25})$$

For computational efficiency again the variance is taken as a base for decision: If

$$(e_1)_N^2 \geq \text{Var}(e)|_N, \quad (\text{C.26})$$

dropping the first data point will decrease the variance of the remaining data set. The even simpler check with a fixed threshold

$$(e_1)_N^2 \geq \text{VarLim} \quad (\text{C.26a})$$

has proven well suited for efficient real-time computation.

With the stored values of Equation C.24 and always working with locally centered representations, the reduction at the left is directly analogous to the extension at the right-hand side. The problematic point is the sum Siy_m of the products (local index times measurement value) (Equation C.13a and C.18). The new starting point of the segment will become $(x_{\text{ref}} + 1)$, but the length N_{red} of the segment will be reduced by 1, while the position of its center is reduced by -0.5 for symmetry; i in Siy_m has to be decremented

$$\begin{aligned} x_{\text{ref}} &:= x_{\text{ref}} + 1; & N_{\text{red}} &= N - 1; & x_{\text{cred}} &= x_c - 0.5; \\ Siym_{\text{red}} &= N \sum_{j=2}^N (j-1) \cdot y_{mj} = \sum_{i_{\text{red}}=1}^{N_{\text{red}}} i_{\text{red}} \cdot y_{mi_{\text{red}}} = \sum_{j=2}^N j \cdot y_{mj} - \sum_{j=2}^N y_{mj}. \end{aligned} \quad (\text{C.27})$$

By noting that

$$Siy_m_N = y_{m1} + \sum_{i=2}^N i \cdot y_{mi}; \quad Sym_N = y_{m1} + \sum_{i=2}^N y_{mi}, \quad (\text{C.28})$$

adding $0 = (y_{m1} - y_{m1})$ to the lower Equation C.27 immediately yields

$$Siy_{\text{red}} = y_{m1} + \sum_{j=2}^N j \cdot y_{mj} - (y_{m1} + \sum_{j=2}^N y_{mj}) = Siym_N - Sym_N; \quad (\text{C.29})$$

$$Sym_{\text{red}} = Sym_N - y_{m1}.$$

This leads to the *recursive procedure* that is to be executed as long as the initial residue squared is larger than the threshold ‘variance limit’:

$$\begin{aligned} N_{\text{red}} &= N - 1; & x_{\text{ref}} &:= x_{\text{ref}} + 1; & x_{\text{cred}} &= x_c - 0.5; \\ Siym_{\text{red}} &= Siym_N - Sym_N; & Sy2m_{\text{red}} &= Sy2m_N - y_{m1}^2; \\ Sym_{\text{red}} &= Sym_N - y_{m1}; & y_{\text{cred}} &= Sym_{\text{red}}/N_{\text{red}}; \end{aligned} \quad (\text{C.30})$$

$$a_{\text{red}} = \frac{6}{N_{\text{red}} - 1} \left(\frac{2}{N_{\text{red}} + 1} \cdot \frac{Siym_{\text{red}}}{N_{\text{red}}} - y_{\text{cred}} \right).$$

The maximum number k of points to be dropped will not be large, in general, since otherwise the segment would have been ended during normal extension.

After reducing the segment length at the side of low indices i , increasing the segment at the other end should be tried again. Figure 5.32 has been interpolated without dropping terms at the left side of the segment, from which the line fit was started. The first longer segment from \sim row = 90 to 115 (upper left center in the figure, designated as ‘blob 1’) could profit from dropping the leftmost data point since a steeper negative value for a_{red} can fit several following data points better. (dotted line, Figure C.3 shows a blown up view of blob 1 of Figure 5.32. The solid line is the least-squares line fit resulting without a check of the residue of the ‘first’ data point after each update; interpolation is stopped at the solid black dots (lower right) because the variance exceeds the threshold set.

Dropping the ‘first’ data point (top left) allows a much better fit to the remaining points; it even allows an extension of the segment to larger values L_{seg} (two more data points) The dotted line in Figure C.3 shows an improved fit with reduced total variance.

Figure 5.35 shows several cases of this type of blob data fit, with the method described here, for a number of columns of a video field. In the top left subfigure, the white lines mark the cross sections selected. Some correspondences between object regions in the scene and blob parameters are given. The task of hypothesis generation in vision is to come up with most reasonable object hypotheses given a collection of features (blobs, edges and corners); homogeneous areas with center of gravity, shape as well as shading parameters are a big step forward compared to just edge features with adjacent average gray values available in real-time evaluation about fifteen years ago.

Figure C.4 (next page) shows the flowchart of the segmentation algorithm including size adaptation at both ends for an optimal fit of shaded stripe segments.

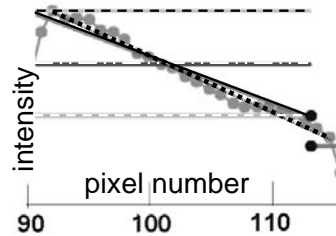


Figure C.3. Large threshold values for starting a line fit (upper left corner) may lead to suboptimal results (see text)

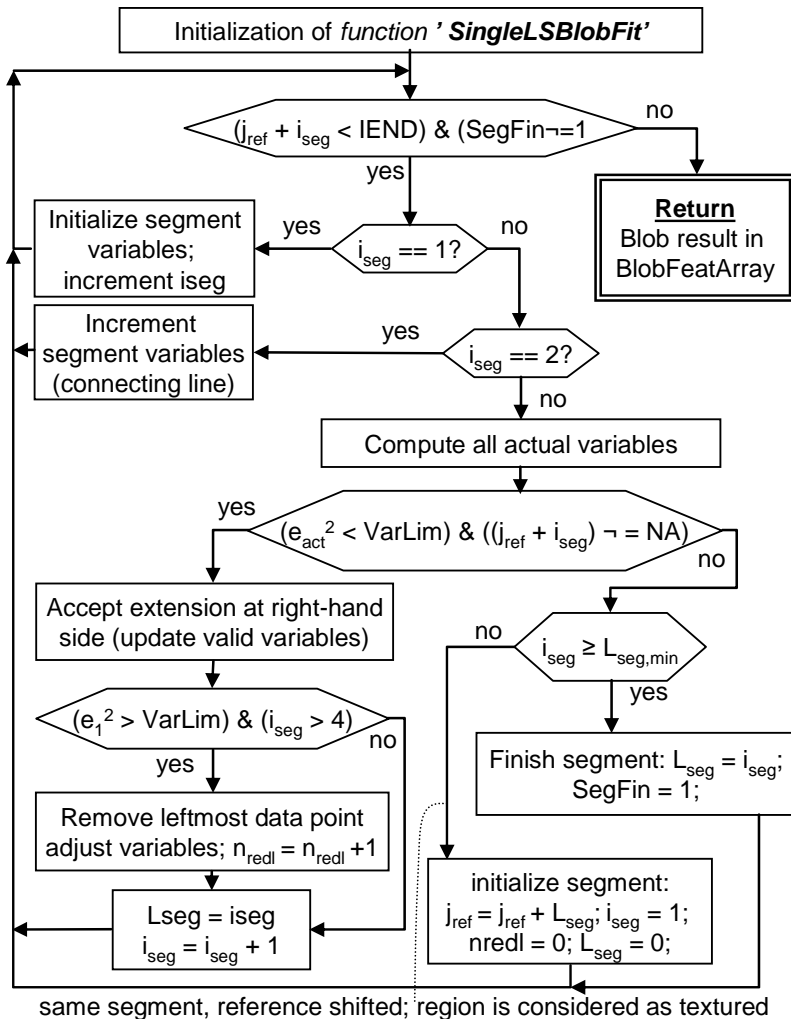


Figure C.4. Flowchart of segmentation method for linearly shaded regions including boundary adaptation at both ends (Matlab®-terminology)

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