

# Appendix A

## Useful Formulas and Equations

### Ohm's Law

$$V = IR \quad I = \frac{V}{R} \quad R = \frac{V}{I}$$

$$P = IV \quad P = I^2R \quad P = \frac{V^2}{R}$$

### *n* Series Resistances

$$R_{eq} = R_1 + R_2 + \dots + R_n$$

### *n* Parallel Resistances

$$R_{eq} = \frac{1}{\frac{1}{R_1} + \frac{1}{R_2} + \dots + \frac{1}{R_n}}$$

### Frequency and Period

$$f = \frac{1}{T} \quad T = \frac{1}{f} \quad \omega = 2\pi f = \frac{2\pi}{T} \quad f = \frac{\omega}{2\pi}$$

### Inductive and Capacitive Reactance ( $\mathbf{j} = \sqrt{-1}$ )

$$X_C = \frac{1}{2\pi f C} \angle -90^\circ \quad X_C = \frac{-j}{2\pi f C} \quad X_C = \frac{1}{j2\pi f C} \quad |X_C| = \frac{1}{2\pi f C}$$

$$X_L = 2\pi f L \angle 90^\circ \quad X_L = j2\pi f L \quad |X_L| = 2\pi f L$$

**Bipolar Transistor Relationships**

$$I_C = \beta I_B \quad I_E = I_C + I_B \quad r_e = \frac{V_T}{I_{CQ}} \quad I_C \cong I_S e^{\frac{V_{BE}}{V_T}}$$

**Triode Relationships**

$$g_m = \mu r_P \quad \mu = \frac{g_m}{r_P} \quad r_P = \frac{\mu}{g_m} \quad I_P = k(V_P + \mu V_G)^{\frac{3}{2}}$$

**JFET Relationships**

$$g_{m0} = \frac{2I_{DSS}}{V_P} \quad I_D = I_{DSS} \left( 1 - \frac{|V_{GS}|}{V_P} \right)^2$$

# Appendix B

## Selected Tube Characteristic Curves

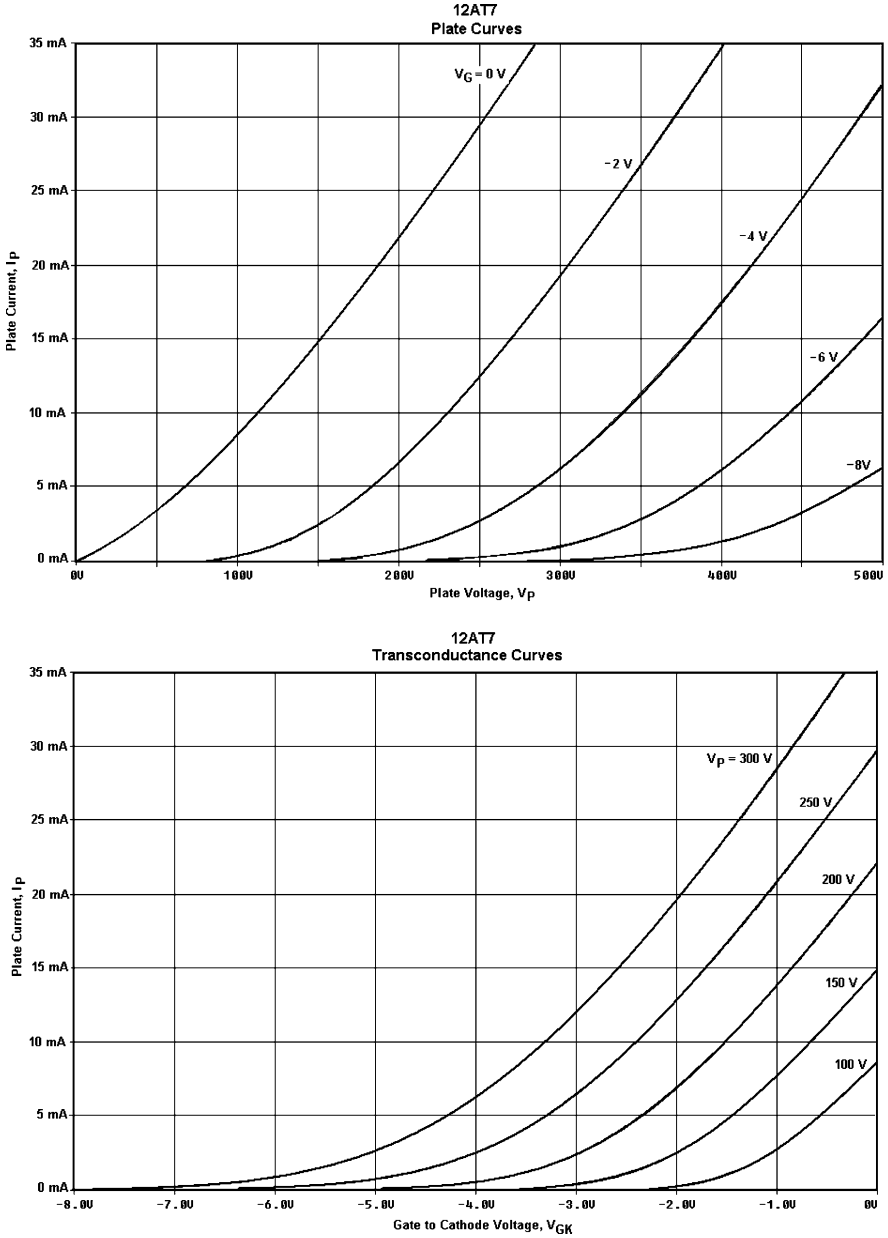


Fig. B.1 12AT7 plate and transconductance curves

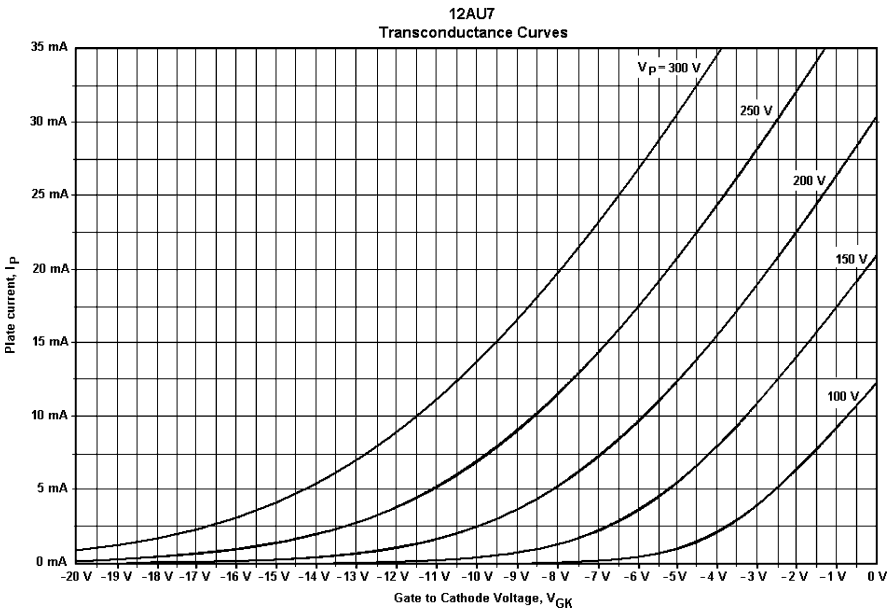
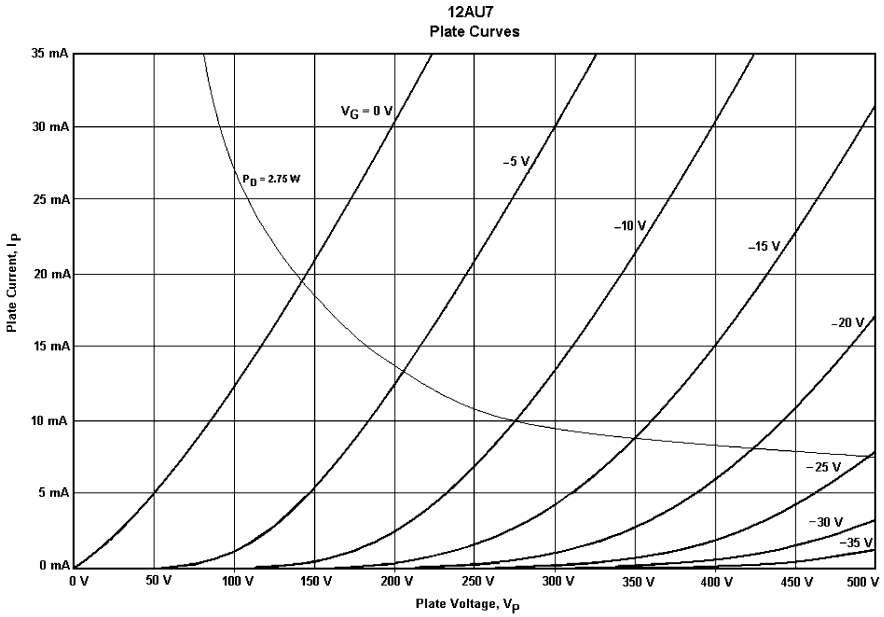


Fig. B.2 12AU7 plate and transconductance curves

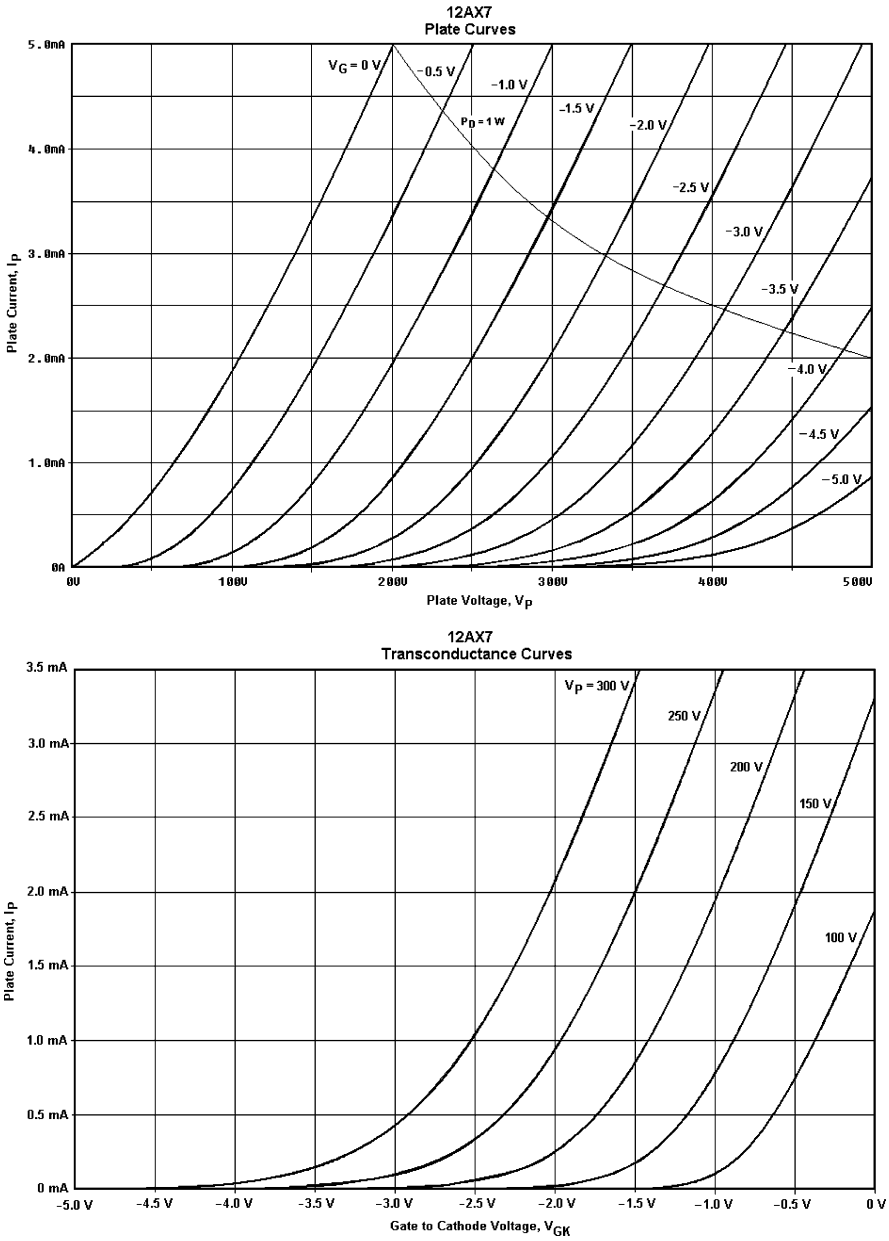


Fig. B.3 12AX7 plate and transconductance curves

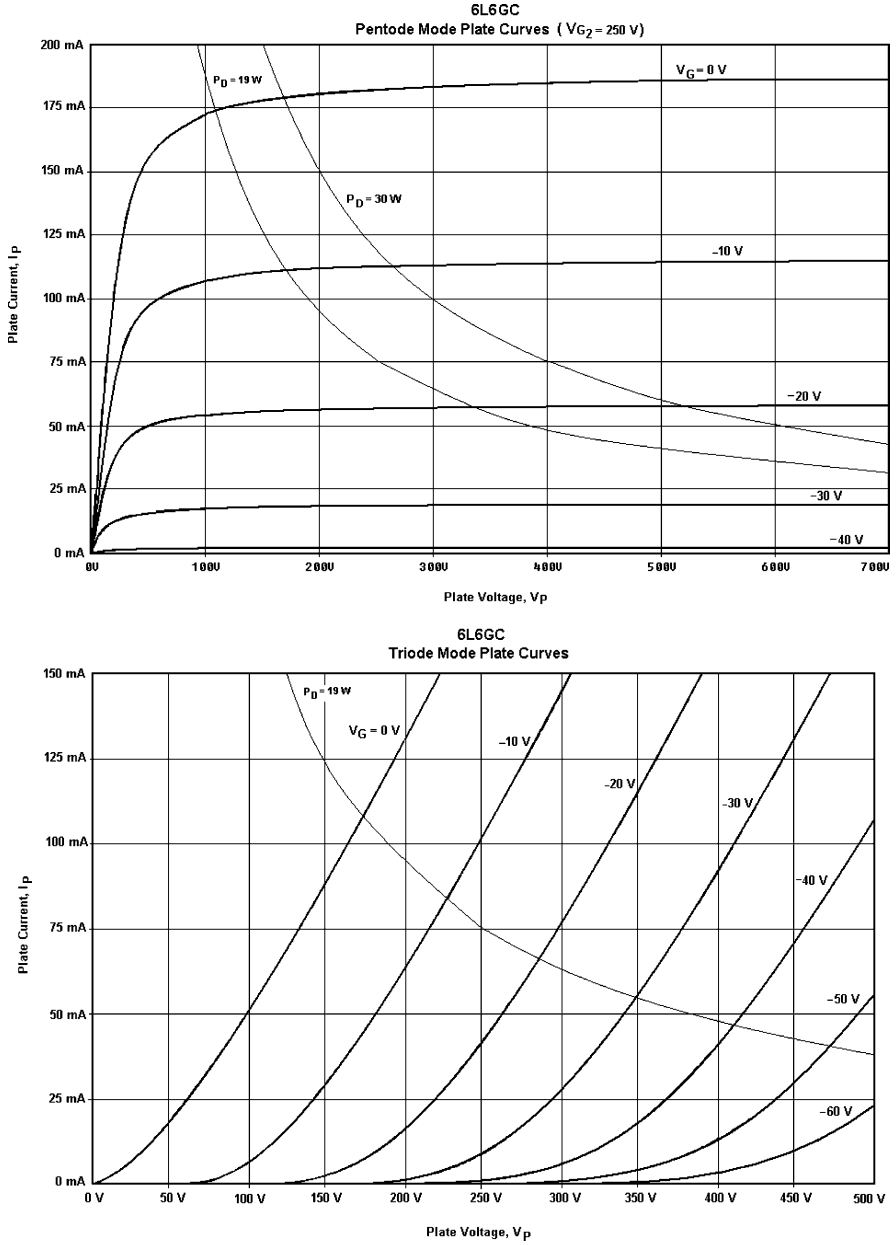


Fig. B.4 6L6GC pentode and triode mode plate curves

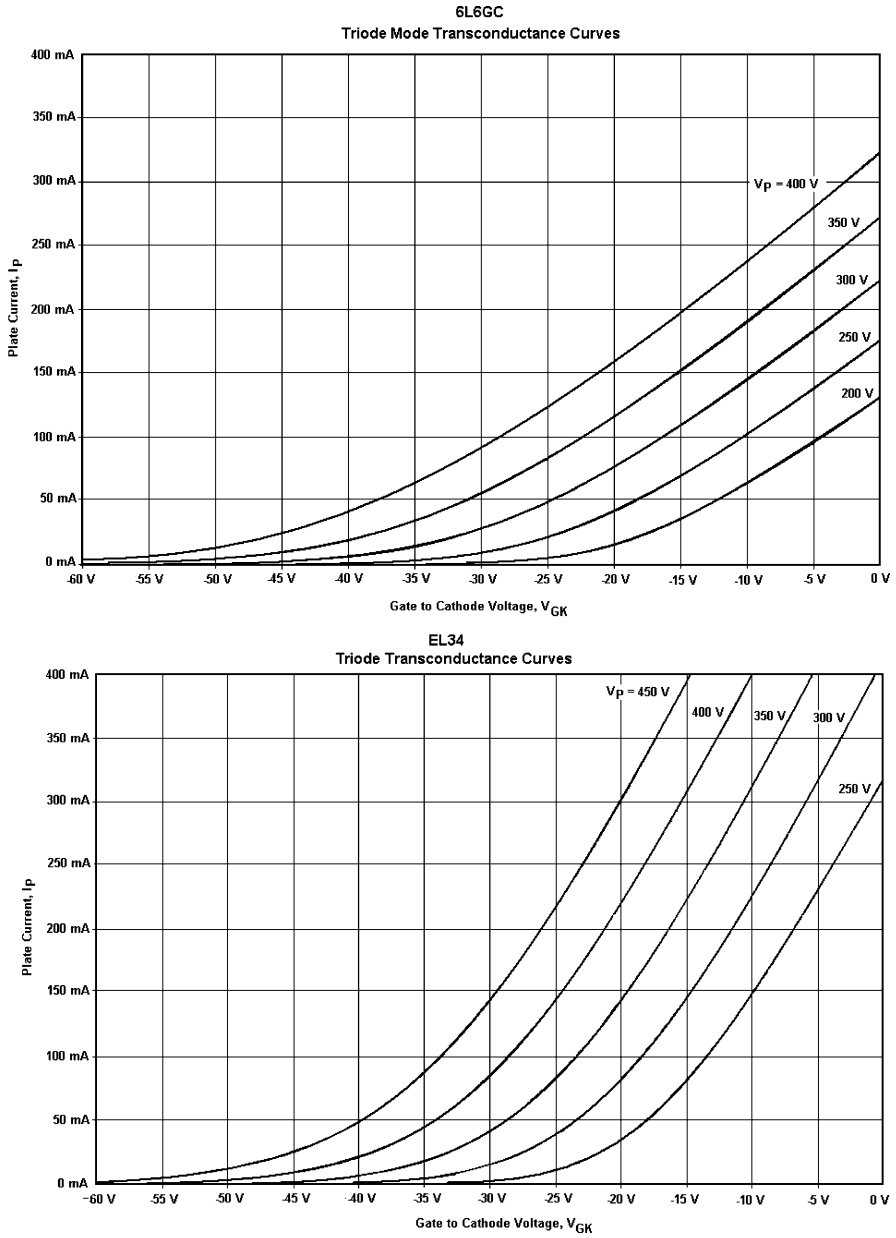


Fig. B.5 6L6GC and EL34 triode mode transconductance curves

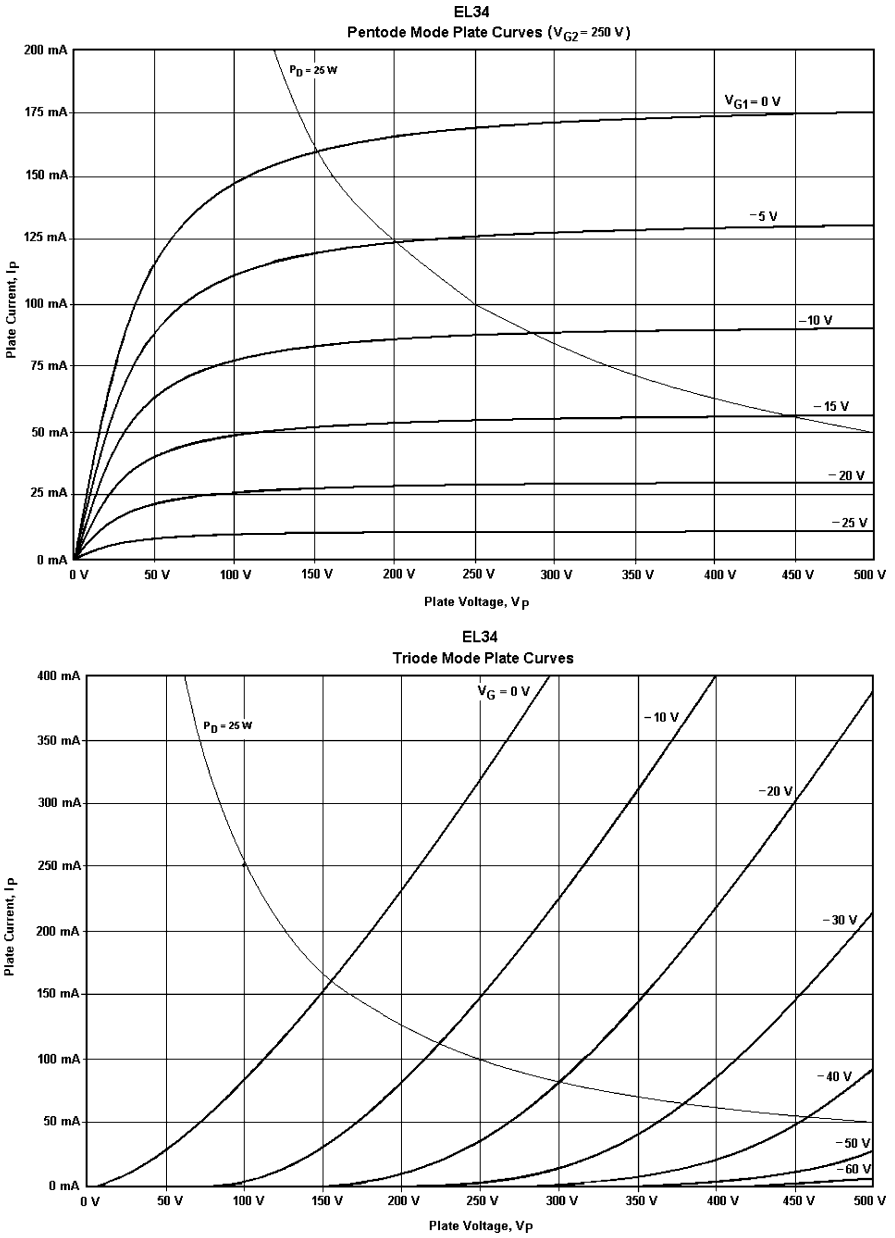


Fig. B.6 EL34 pentode and triode mode plate curves



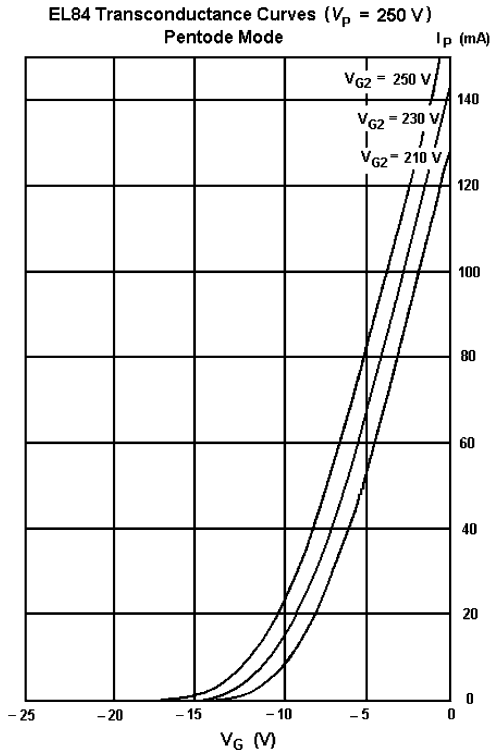
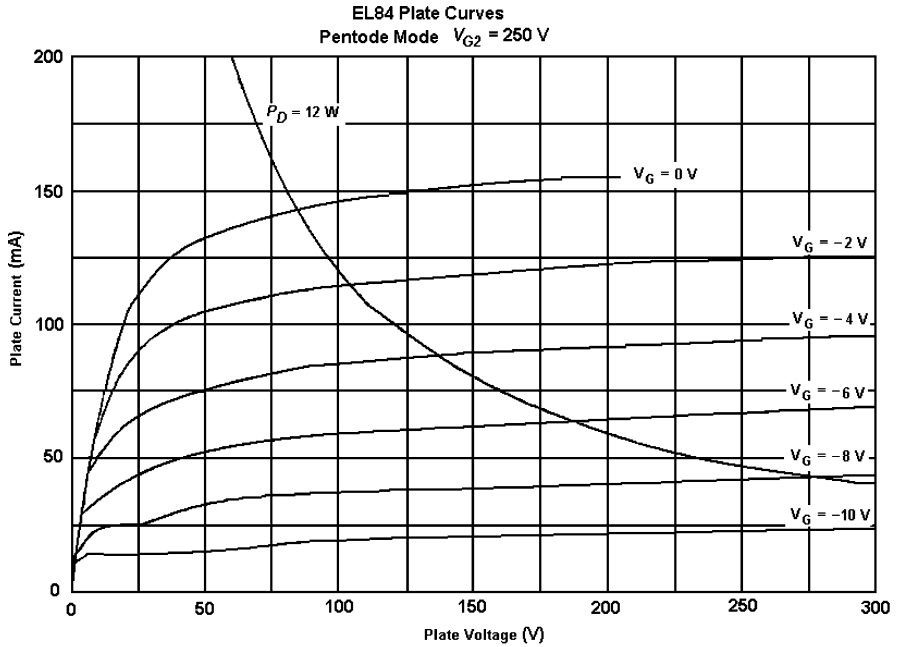


Fig. B.7 EL84 pentode mode plate and transconductance curves

# Appendix C

## Basic Vacuum Tube Operating Principles

### Diodes

The diode is the simplest vacuum tube. Recall that the vacuum tube diode operates by thermionic emission of electrons from a heated cathode within the evacuated glass envelope of the tube, as shown in Fig. C.1.

#### *Reverse Bias*

When the anode is at a negative potential with respect to the cathode  $V_{AK} \leq 0$  V, the diode is said to be reverse biased, and the current flow through the tube is approximately zero. This occurs because the free electrons around the cathode are repelled by the negative potential at the anode, as shown in Fig. C.1a.

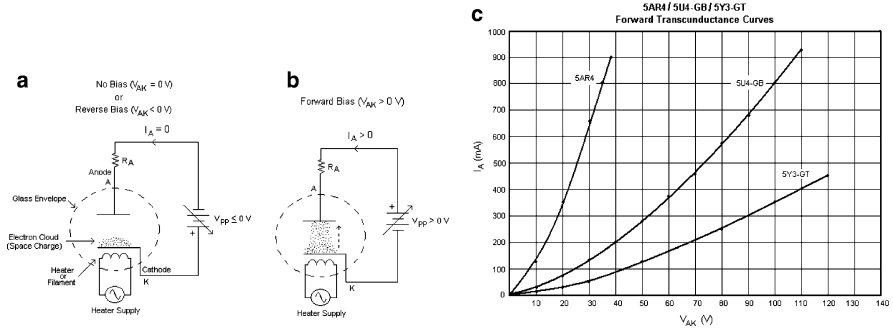
#### *Forward Bias*

If the anode terminal is made positive with respect to the cathode  $V_{AK} > 0$  V, electrons that are attracted from the cathode are free to travel through the vacuum to the anode, as shown in Fig. C.1b. This condition is referred to as forward bias.

The current that flows in a forward biased vacuum tube diode is not a linear function of the applied voltage, but rather obeys what is called the Child–Langmuir law, which is

$$I_A = k V_P^{\frac{3}{2}} \tag{C.1}$$

The constant  $k$  is the *perveance* of the diode. A high value of perveance results in a diode that drops less voltage at a given forward current. For typical vacuum tube diodes,  $k$  ranges from approximately 0.003 to 0.00035. The forward bias current vs. voltage relationships for three common vacuum tube diodes, the 5AR4, 5U4-GB,



**Fig. C.1** Vacuum tube diode operation

and the 5Y3-GT, are shown in Fig. C.1c. All three diodes closely follow the Child–Langmuir law, with the value of  $k$  varying from 0.003 for the 5AR4, to 0.00035 for the 5Y3-GT.

### Triodes

If we take a vacuum tube diode and place a fine wire *grid*, often called the *control grid*, in between the cathode and the anode (which we will now refer to as the *plate*), a triode may be represented as shown in Fig. C.2. The function of the grid is to allow control of the flow of electrons from the cathode to the plate.

Examine Fig. C.2a. In this case, there is no bias applied to the grid of the triode. That is, the grid and cathode are at the same potential, which in this case is ground, and  $V_{GK} = 0$  V. Physically, the grid has very little cross-sectional area. This, plus the fact that the grid is at the same potential as the cathode means that nearly all of the electrons that leave the cathode make it across to the plate. The grid leakage current is quite small, on the order of 1 nA or less, and so may be ignored in this discussion. With no bias, the plate current  $I_P$  will increase with plate voltage  $V_P$  just as it would for a normal vacuum tube diode.

In Fig. C.2b, the grid is biased to a more negative potential than the cathode. Now, the positive potential of the plate exerts less attractive force on the electrons surrounding the cathode, and the plate current will be reduced relative to that which would flow with no bias on the grid. If we step the grid bias voltage from zero to some maximum value, a family of plate characteristic curves is generated. Figure C.3 shows the plate characteristic curves for the 12AU7 triode. The equation that describes these curves is

$$i_P = k(V_P + \mu v_G)^{\frac{3}{2}} \tag{C.2}$$

When there is no bias applied to the triode, the term  $\mu v_G$  is zero, and (C.2) reduces to the standard Child–Langmuir equation for a diode, (C.1).

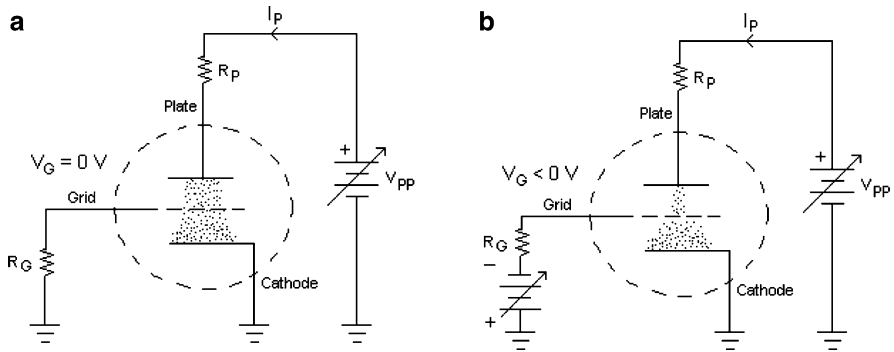


Fig. C.2 The addition of the grid creates a triode

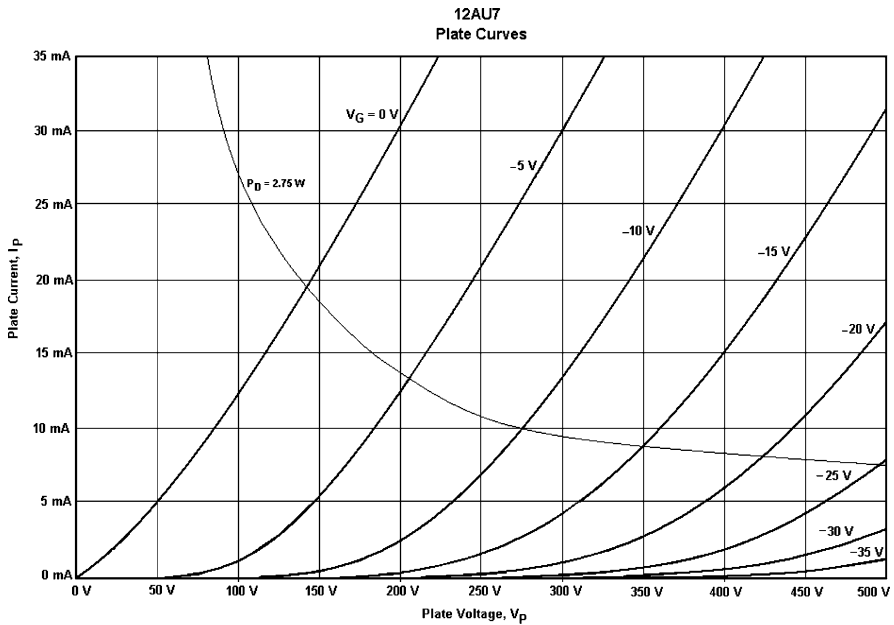


Fig. C.3 Plate characteristic curves for the 12AU7

### Amplification Factor

The parameter  $\mu$  (Greek mu) is called the amplification factor. The value of  $\mu$  depends on the construction of the tube. For example the 6AS7-G is a low- $\mu$  triode with  $\mu = 2$ , while the 12AX7 is a high- $\mu$  triode with  $\mu = 100$ . The actual value of  $\mu$  varies somewhat from one tube to another of the same type, but it is generally close enough to the published value that in many cases we can consider it to be the same for

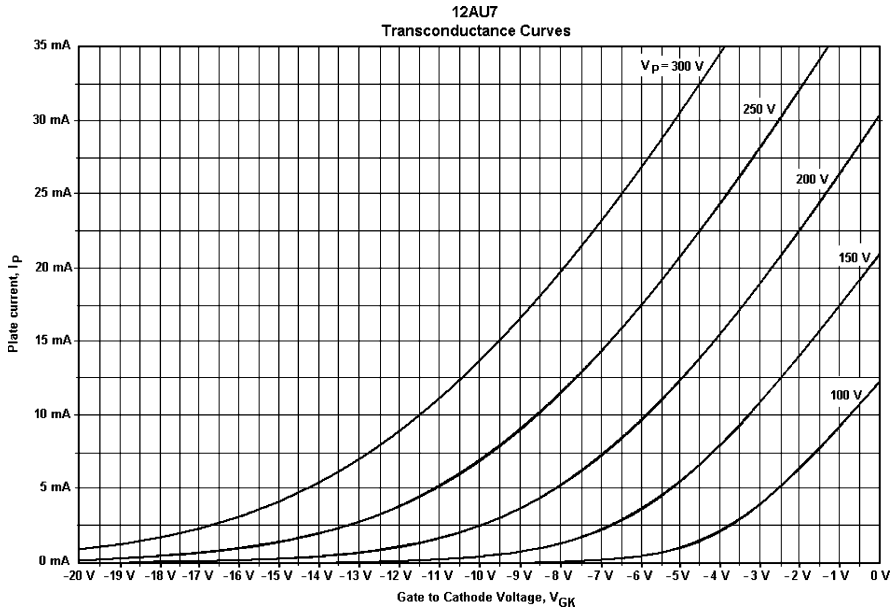


Fig. C.4 Transconductance curves for the 12AU7

every tube of the same type. This is in sharp contrast to bipolar transistors where, for example, beta may vary wildly from one device to another with the same part number.

### Transconductance

The parameter that relates plate current  $I_p$  to gate bias voltage  $V_{GK}$  is called *transconductance*, which is designated as  $g_m$ . We can plot plate current as a function of grid voltage at various plate voltage levels. This produces a family of transconductance curves, such as those shown for the 12AU7 in Fig. C.4.

Transconductance allows us to view the triode as a voltage-controlled current-source. Looking at the triode from an AC signal standpoint, we have

$$i_p = g_m v_G \tag{C.3}$$

Where the AC plate current  $i_p$  is controlled by the AC grid voltage  $v_G$ . We are taking some liberties here, assuming that  $v_G = v_{GK}$ , which is true when there is no cathode resistance in the AC equivalent circuit.

### Plate Resistance

The effective internal resistance of the plate  $r_p$  is another basic tube parameter that is very important. For example, maximum power transfer from the tube to a load

that is driven by the plate occurs when  $r_p = R_L$ . Although it is generally not necessary to have a precise match between  $r_p$  and  $R_L$ , triodes with low plate resistance are better suited for driving low resistance loads than triodes with high plate resistance.

Plate resistance, amplification factor, and transconductance are related by the following equation.

$$\mu = g_m r_p \quad (\text{C.4})$$

## Tetrodes

A tetrode is a four-terminal tube that is created with the addition of a *screen grid* between the plate and the control grid. The function of the screen grid is to shield the control grid from the plate, which reduces the effective input capacitance of the tube. The screen grid is typically held at a slightly less positive voltage than the plate, and is often bypassed to ground to enhance the shielding effect and reduce input capacitance to a minimum. The schematic symbol for a tetrode is shown in Fig. C.5.

The presence of the screen grid has some negative effects on tube characteristics as well. For example, since the screen grid is held at a relatively high positive potential, it will accelerate electrons as they move from the cathode toward the plate. The increased energy of the electrons striking the plate causes secondary electrons to be emitted from the plate back toward the screen grid. Many of these secondary electrons are captured by the screen grid, resulting in significant screen grid current which is undesirable. The creation of secondary emission current can also cause undesirable nonlinear behavior of the tetrode, even causing negative resistance under some conditions.

## Pentodes

The undesirable characteristics of the tetrode are improved by the addition of a fifth element, called a *suppressor grid*. This forms a *pentode*. The schematic symbol for a pentode is shown in Fig. C.6. The suppressor grid is located between the screen

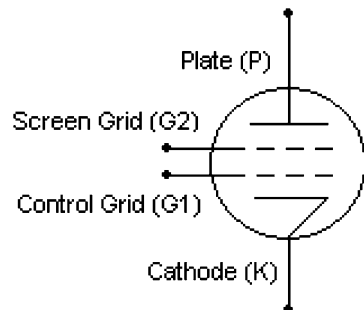


Fig. C.5 Schematic symbol for a tetrode

Fig. C.6 Schematic symbol for the pentode

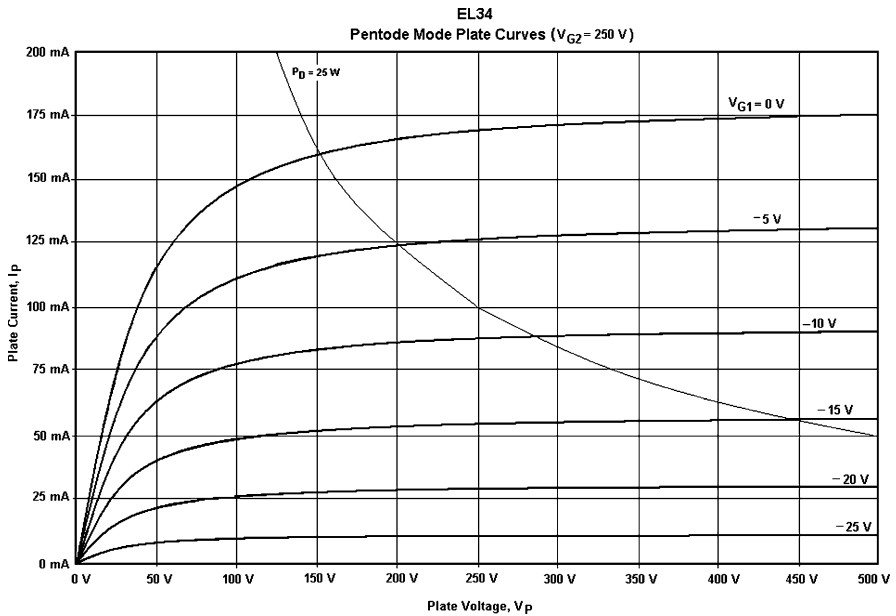
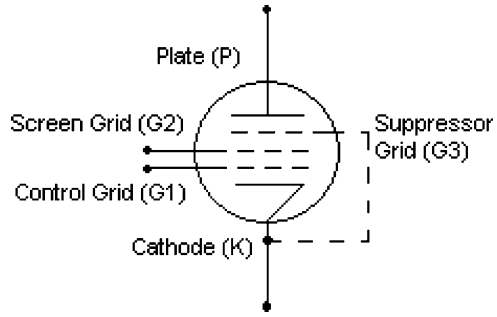


Fig. C.7 Plate characteristic curves for the EL34 pentode

grid and the plate inside the tube. Most often the suppressor grid is tied directly to the cathode, which holds it at a very negative potential relative to the plate. The function of the suppressor grid is to repel secondary emission electrons back to the plate, preventing them from causing excessive current flow and power dissipation in the screen grid.

Pentodes generally have much higher effective plate resistance  $r_p$ , and amplification factor  $\mu$ , than triodes. The plate characteristic curves for pentodes are very similar to those of bipolar transistors and field effect transistors. The plate curves for the EL34 pentode are shown in Fig. C.7.

The pentode can also be configured to operate as a triode simply by connecting the screen grid directly to the plate. Operation as a triode significantly reduces  $r_p$ ,  $\mu$ , and maximum power output, but is often used to obtain particularly desirable overdrive and distortion characteristics.

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