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# Monitoring the instrument response of the high-sensitivity seismograph network in Japan (Hi-net): effects of response changes on seismic interferometry analysis

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## Abstract

More than 10 years have passed since observations began to be recorded by Hi-net, a network of high-sensitivity seismometers located in Japan. Several large earthquakes, including the 2011 Tohoku-Oki earthquake, have been recorded by the network during this period. Age-related degradation and the strong ground motion of large earthquakes may change the instrument response of the high-sensitivity seismometers of Hi-net. Thus, we checked the natural frequency  $f$  and damping constant  $h$  for each Hi-net sensor and monitored the instrument response for 10 years from 2003 to 2013. Most of the sensors showed a stable instrument response over this period. More than 95 % of the sensors whose responses we could well estimate showed small fluctuations in their natural frequencies and damping constants of within 0.05 Hz and 0.05, respectively. We also found that many Hi-net sensors in northeastern Japan showed slight changes in the instrument response as a result of the 2011 Tohoku-Oki earthquake. Based on the assumption that the instrument responses remained unchanged, the fractional velocity reduction in the subsurface structure was reported by seismic interferometry analysis. To investigate how changes in the instrument response can cause errors in seismic interferometry analysis, we conducted a synthetic test. The results indicate that the instrument response did not result in systematic variation in the time delay observed in the interferometry analysis. This confirmed that the velocity decrease observed as a result of the 2011 Tohoku-Oki earthquake was not due to artificial instrument error.

**Keywords:** Hi-net sensor; Test coil; Instrument response; Seismic interferometry

## Background

The National Research Institute for Earth Science and Disaster Prevention (NIED) has operated three nationwide seismic networks since the 1990s. The networks consist of approximately 80 broadband seismographs, 1700 strong-motion seismographs, and 800 high-sensitivity seismographs and are referred to as F-net, KiK-net/K-NET, and Hi-net, respectively. These three seismic networks observe seismic motions for short to long periods and detect earthquakes of small to large magnitudes (Okada et al. 2004).

Hi-net is designed for the detection of small earthquakes and very weak signals from the deep crust. At a Hi-net station, a sensor characterized by a natural frequency of 1 Hz is installed at the bottom of a borehole of 100 m or more in depth to reduce background noise (Obara et al. 2005). The performance and limitations of the sensor dynamic range were investigated by Shiomi et al. (2005). The sensor orientation at the bottom of the borehole cannot be observed by the naked eye but may be accurately estimated by analyzing the long-wavelength waveforms and ambient seismic signals (Shiomi 2013). The Hi-net records have been used to determine the accurate hypocenter locations and mechanisms of small earthquakes (e.g., Yukutake et al. 2008) and have contributed to the new finding of a non-volcanic seismic tremor in southwestern Japan (Obara 2002). Additionally, the records have been

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used for the construction of subsurface structure models by seismic travel-time tomography (e.g., Matsubara et al. 2009), receiver function analysis (e.g., Shiomi et al. 2004; Ueno et al. 2008), and scattering-wave analysis (e.g., Takahashi et al. 2009). Although the Hi-net sensors were originally designed for regional or small earthquakes, high-quality observations can be successfully achieved using a simulation filter from the Hi-net sensors to the F-net broadband sensors for far-field large earthquakes (Maeda et al. 2011). The waveforms recorded by the Hi-net stations are available on the NIED Hi-net website (<http://www.hinet.bosai.go.jp/?LANG=en>).

Wegler and Sens-Schönfelder (2007) proposed a method referred to as passive image interferometry (PII), in which fractional changes in the background seismic velocity structure (less than approximately 1 %) can be identified by monitoring a correlation function of the ambient seismic noise. This method has successfully detected temporal changes in the subsurface structure associated with a large earthquake (e.g., Brenguier et al. 2008a), a volcanic eruption (e.g., Brenguier et al. 2008b), and Earth tides (Takano et al. 2014). Since Hi-net provides continuous high-quality seismograms, Hi-net records are suitable for the PII. For example, the PII of the Hi-net records revealed a significant velocity decrease of more than 0.3 % for the 2004 Mw 6.6 mid-Niigata earthquake (Wegler et al. 2009), the 2007 Mw 6.6 Noto Hanto earthquake (Ohmi et al. 2008), and the seismic swarm activity by magma intrusions in the Izu Peninsula, Japan (Ueno et al. 2012). Additionally, for the 2011 Tohoku-Oki earthquake, a significant velocity decrease of approximately 1.5 % was reported based on monitoring by the autocorrelation function (ACF) using Hi-net records (Minato et al. 2012).

These PII results implicitly presumed stable instrument responses of the Hi-net sensors during the analysis period. However, stability is not always assured, because some sensors suffer from ground motions larger than the stroke limitation. This can damage the sensor and change the instrument response. Figure 1 shows records of the 2011 Tohoku-Oki earthquake at the N.KMIH station. The KiK-net waveform indicates strong motions larger than the stroke limitation of the Hi-net sensor which is 2 mm (Fig. 1b). Thus, although it appears to work correctly, the Hi-net sensor cannot accurately record large ground motions, because of the stroke limitation (Fig. 1c). Such large signals may cause significant changes in the instrument response for PII because PII is sensitive to very small velocity structure changes (approximately 1 %). To maintain a satisfactorily high performance of a seismograph and guarantee accurate PII results, it is necessary to carefully monitor the changes in the instrument response and examine the effects of these changes on the PII.

This study thoroughly investigates the instrument responses of approximately 800 Hi-net sensors using a

daily test coil signal over a period of 10 years that includes the 2011 Tohoku-Oki earthquake. Analyzing the test coil signal, we estimated the natural frequency and damping constant as the instrument responses for each sensor of Hi-net. Additionally, we examined how changes in the instrument response can affect the subsurface structure changes detected by PII for the 2011 Tohoku-Oki earthquake.

## Methods

### Evaluation of instrument response

We estimated the natural frequency  $f$  and damping constant  $h$  for each Hi-net sensor by using a daily test signal. Figure 2a shows a schematic of a Hi-net seismometer. A coil bobbin, which works as a pendulum in the seismometer, includes a signal coil and a test coil. The signal coil is for the detection of ground motion, which induces a current in the coil. The coil bobbin is displaced by an electrical voltage applied to the test coil. When we apply a voltage  $e_i$  to a test coil with length  $l$  and resistance  $R$  in a magnetic flux density  $B$ , the weight of the coil bobbin  $M$ , the generated Lorentz force per unit mass  $f$ , given by

$$f = \frac{Bl}{MR} e_i, \quad (1)$$

displaces the coil bobbin in the vertical direction. The values of  $B$ ,  $l$ ,  $M$ , and  $R$  are constant. When an electrical voltage is applied suddenly as shown in Fig. 2b, the force is produced in a stepwise shape. The equation of motion for the coil bobbin is then given by

$$\ddot{z}(t) + 2h\omega_0\dot{z}(t) + \omega_0^2 z(t) = fH(t), \quad (2)$$

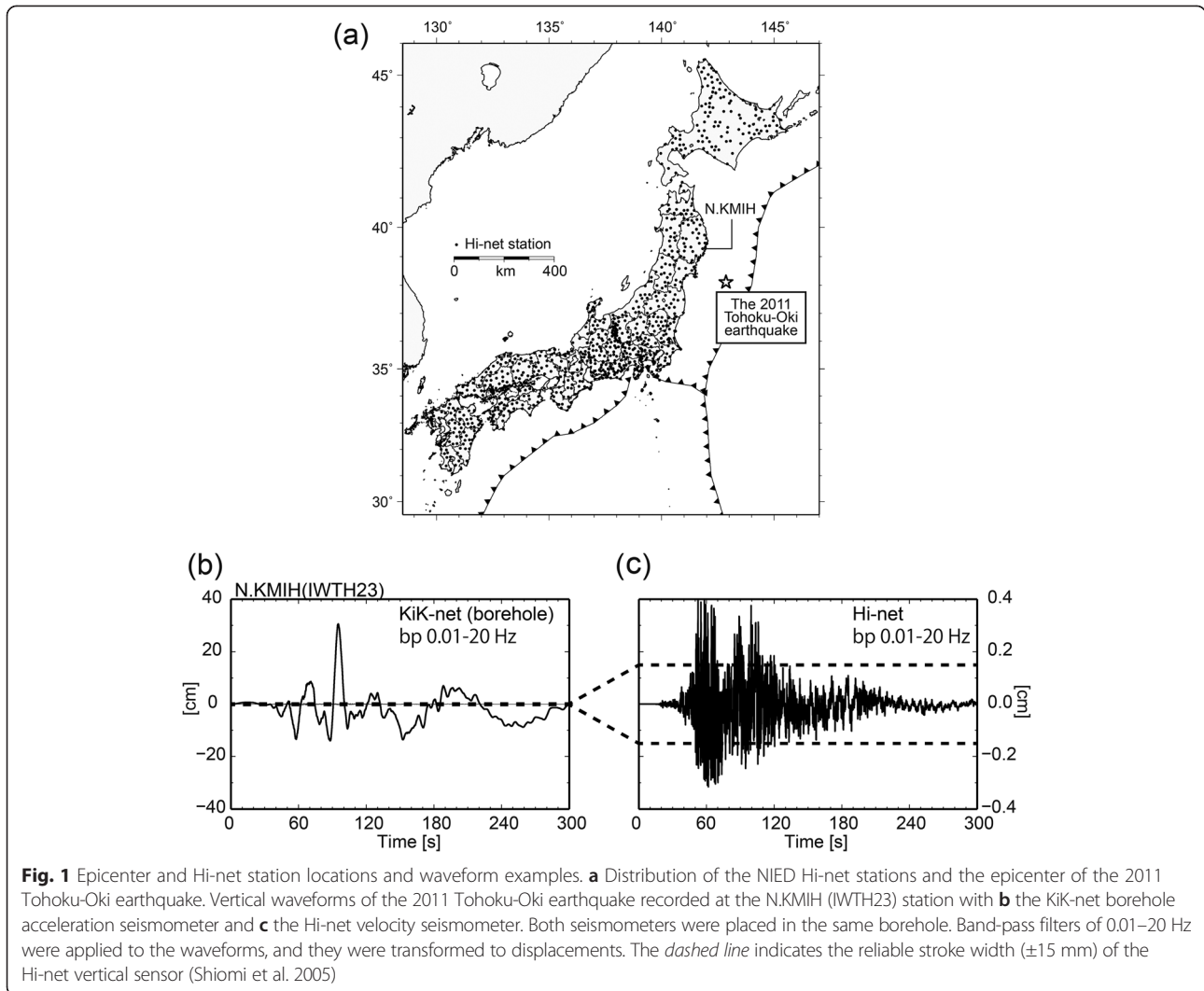
where  $z(t)$  is the displacement of the bobbin,  $\omega_0$  is the natural angular frequency,  $h$  is the damping resistance, and a function  $H(t)$  is defined as

$$H(t) = \begin{cases} 0, & t < 0 \\ 1, & t \geq 0 \end{cases}.$$

We then obtained  $Z(\omega)$  from the Fourier transform of  $z(t)$  as

$$Z(\omega) = \frac{C_0}{(\omega^2 - 2h\omega_0 i\omega - \omega_0^2) i\omega}, \quad (3)$$

where  $C_0$  is a constant which includes the constant values of  $B$ ,  $l$ ,  $M$ , and  $R$ . Equation (3) shows the displacement spectrum of the coil bobbin. The displacement of the coil bobbin induces the voltage  $e_0$  in the signal coil. The output voltage  $e_0$  produced by this bobbin motion is proportional to the velocity of the coil bobbin  $v(t) = dz(t)/dt$ , and the Fourier transform of the velocity is given by



$$V(\omega) = \frac{C_0}{\omega^2 - 2h\omega_0 i \omega - \omega_0^2}. \quad (4)$$

Therefore, we obtain the output voltage, in other words, an instrument response, with respect to the force given by the right-hand side of Eq. (2) by performing the inverse Fourier transform given by Eq. (4).

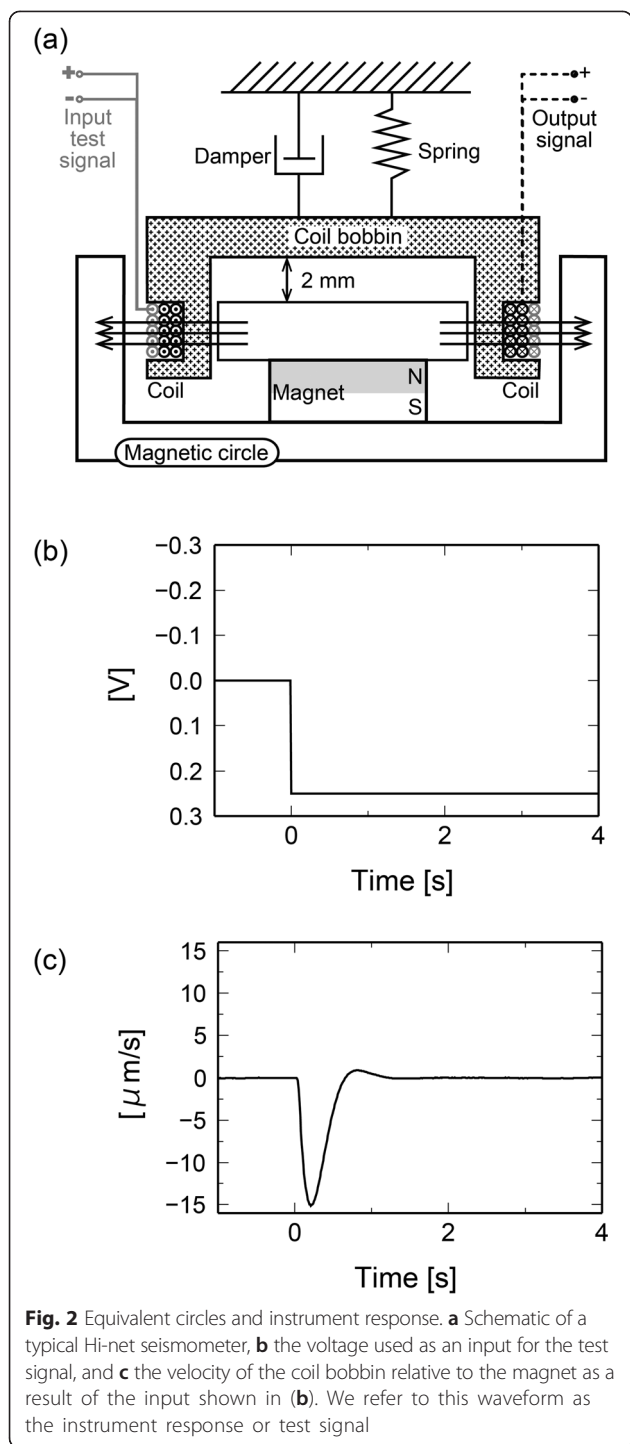
The electrical voltage was applied every morning at 9:00 AM, as shown in Fig. 2b, and a test signal was obtained for each Hi-net sensor, as shown in Fig. 2c. Figure 3 shows examples of the calculated instrument responses (test signals) for three difference sets of natural frequencies  $f$  and damping constants  $h$ :  $(f, h) = (1.0 \text{ Hz}, 0.7)$ ,  $(0.9 \text{ Hz}, 0.6)$ , and  $(0.5 \text{ Hz}, 0.3)$ . The standard Hi-net sensor is set to 1.0 Hz and 0.7. If the instrument response is characterized by  $f = 0.9 \text{ Hz}$  and  $h = 0.6$ , the difference from the standard instrument response is not very large, whereas a large difference is recognized for the case of  $f = 0.5 \text{ Hz}$  and  $h = 0.3$ .

#### Estimating the parameters of instrument response using a test coil record

We estimated the natural frequency  $f$  and damping constant  $h$  for the Hi-net sensors using a grid-search method. We calculated the root mean square reduction (rr), which is defined as

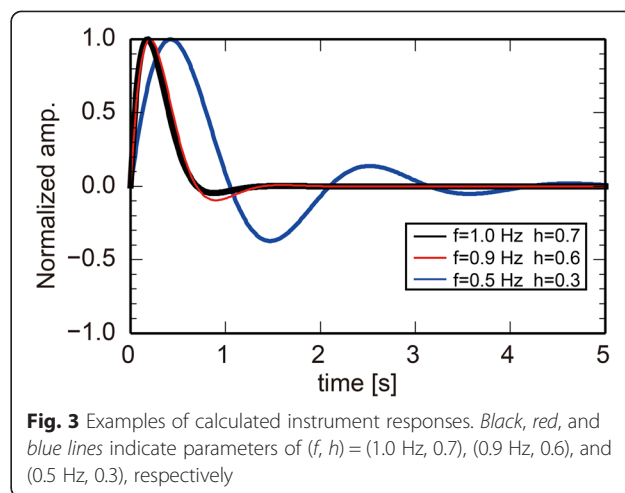
$$rr = 1 - \sqrt{\frac{\sum_i [S(t_i) - O(t_i)]^2}{\sum_i [O(t_i)]^2}}, \quad (5)$$

where  $S(t)$  and  $O(t)$  are the calculated and observed instrument responses, respectively. The rr is larger when the equation better reproduces the observation. It takes a maximum value of 1 when the calculation perfectly matches the observation. By changing  $f$  from 0.1 to 2.1 Hz with a step of 0.01 Hz and  $h$  from 0.1 to 2.1 with a step of 0.01, we investigated an



appropriate range of  $f$  and  $h$  values to maximize the value of  $rr$ .

Figure 4a shows the  $rr$  distribution as a function of  $f$  and  $h$  for the instrument response at the N.KMIH station (the station location is shown in Fig. 1a) recorded on 4 June 2010. The maximum  $rr$  value is 0.98 for a parameter set of  $f = 1.11$  Hz and  $h = 0.68$ . Figure 4b–e compares the observed and calculated

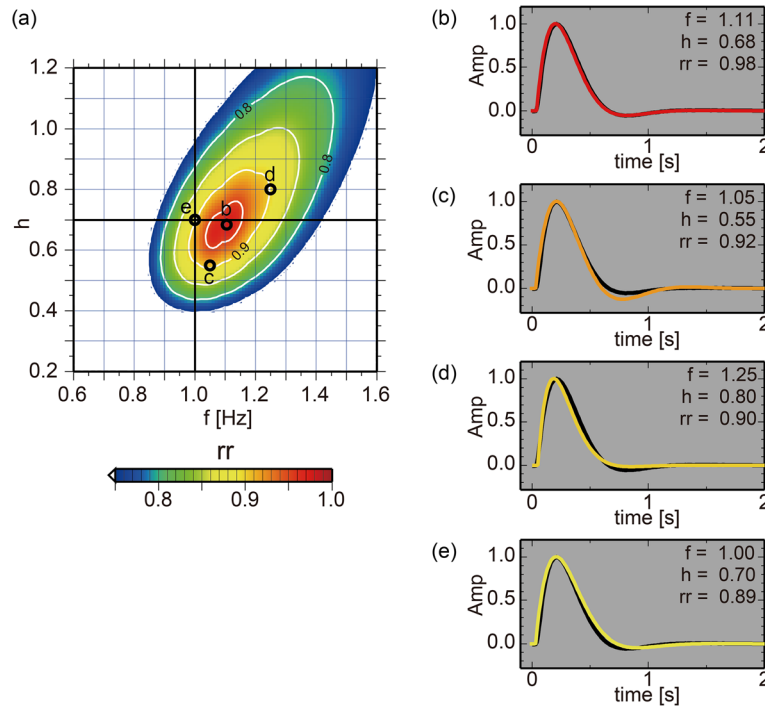


instrument responses for each  $f$  and  $h$  set. Very good agreement between the observed and calculated instrument responses is obtained when the  $rr$  value is larger than 0.95. This study assumes that the ranges of  $f$  and  $h$  that yield  $rr$  values larger than 0.95 are the estimated natural frequency and damping constant for an instrument response. We estimated these ranges to be  $f = 1.05\text{--}1.15$  Hz and  $h = 0.6\text{--}0.75$  for the instrument response at the N.KMIH station in Fig. 4a.

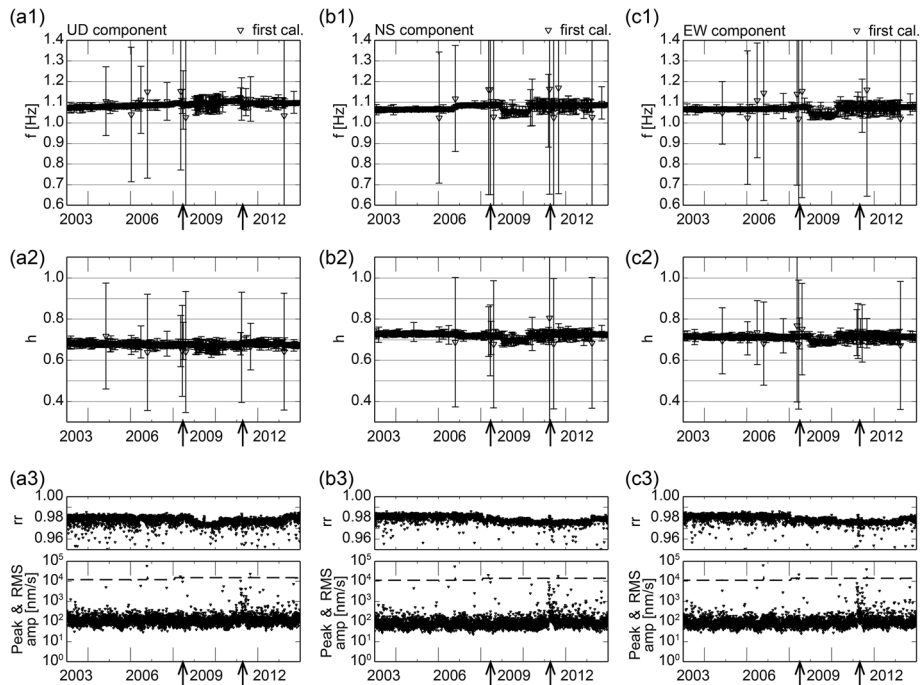
### Results and discussion

Figure 5 shows an example of the time series of  $f$ ,  $h$ ,  $rr$ , and the root mean square (RMS) amplitude of the waveform from 2003 to 2013 for three component seismographs at the N.KMIH station in the Tohoku region (the station location is shown in Fig. 1a). The  $rr$  value is an important index in the stability determination for parameter estimation, as shown in Fig. 4. For the vertical component time series in Fig. 5a, low  $rr$  values were estimated occasionally and the values of  $f$  and  $h$  were not always stable. It was usually because natural earthquakes such as aftershocks of the Iwate–Miyagi Nairiku earthquake (Mw 6.9) in 2008 and the 2011 Tohoku–Oki earthquake (Mw 9.1) contaminated the test signals. However, most  $rr$  values in the whole period were greater than 0.95, which indicates very good agreement between the observed and calculated instrument responses. The natural frequencies and damping constants during the analyzed period were estimated to be in the ranges of  $f = 1.05\text{--}1.10$  Hz and  $h = 0.65\text{--}0.75$ , respectively. The results of the north–south and east–west components were similar to those of the vertical component, as shown in Fig. 5b, c.

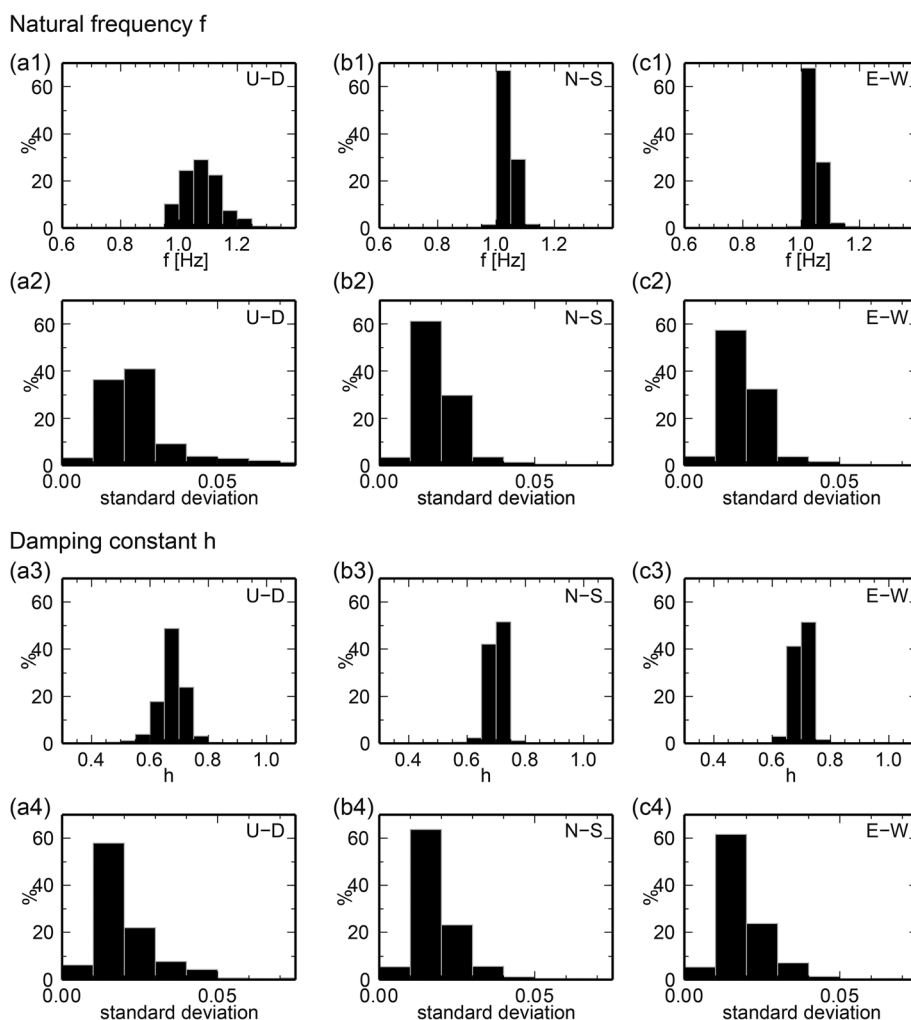
Figure 6 summarizes the distribution of the instrument responses for all Hi-net stations in this study, including a histogram of the average  $f$  (Fig. 6(a1)), the standard deviation of  $f$  (Fig. 6(a2)), the average  $h$



**Fig. 4** Results of a grid-search method for the determination of the natural frequency  $f$  and damping constant  $h$  of a Hi-net sensor. **a** Values of  $rr$  as a function of  $f$  and  $h$ . **b–e** Observed (black line) and calculated instrument responses for various parameter sets: **(b)**  $f = 1.11$  Hz and  $h = 0.68$ , **c**  $f = 1.05$  Hz and  $h = 0.55$ , **d**  $f = 1.25$  Hz and  $h = 0.80$ , and **e**  $f = 1.00$  Hz and  $h = 0.70$ . Each calculated waveform is colored according to the value of  $rr$



**Fig. 5** Temporal changes in the instrumental parameters from 2003 to 2013. **a** Vertical components of (a1) the natural frequency  $f$  Hz of the test signal at the N.KMIH station, (a2) the damping constant  $h$ , and (a3) the  $rr$  and the peak (broken line) and RMS (dot) amplitudes 3 s before the test signal. **b** North–south and **c** east–west components of the variables in (a). The arrows indicate the dates of the Iwate–Miyagi Nairiku Earthquake in 2008 and the 2011 Tohoku–Oki earthquake



**Fig. 6** Histograms of the natural frequency and damping constant distributions. **a** Distributions of the vertical components of (a1) the natural frequency  $f$ , (a2) the standard deviation of  $f$  over 10 years, (a3) the damping constant  $h$ , and (a4) the standard deviation of  $h$  over 10 years. The values were counted when the value of  $rr$  exceeded 0.95. **b** North–south and **c** east–west components of the variables in (a)

(Fig. 6(a3)), and the standard deviation of  $h$  (Fig. 6(a4)) for the vertical sensors for over 10 years for each station. Figure 6b, c indicate the same values for the north–south and east–west components of the seismometers, respectively. More than 95 % of the stations have natural frequencies and damping constants in the ranges of  $f=1.0$ – $1.2$  Hz and  $h=0.6$ – $0.75$ . The standard deviations of the  $f$  and  $h$  for each station are within 0.05 Hz and 0.05, respectively, indicating that there is no significant variation in the instrument response (see Fig. 4). Therefore, we conclude that the Hi-net sensors as a whole are well controlled, with small instrument-to-instrument variations. Additionally, the sensors are very stable over the analyzed 10 years, although slight fluctuations in the instrument response were sometimes recognized during large earthquakes.

### Influence of changes in instrument response on crustal monitoring by interferometry analysis

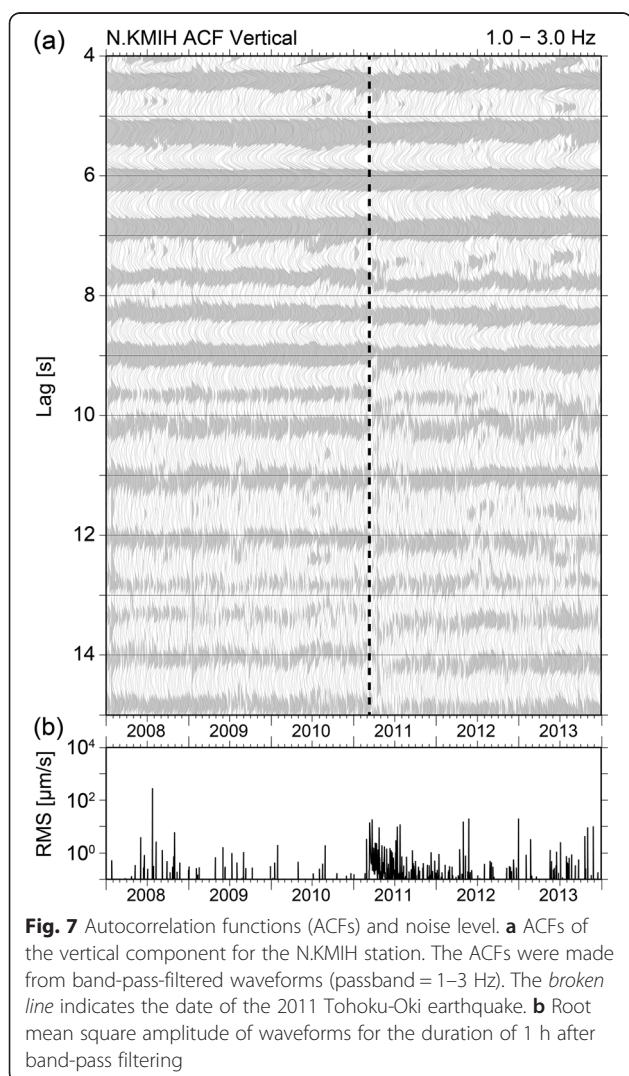
#### *Passive image interferometry of the 2011 Tohoku-Oki earthquake*

During the 2011 Mw 9.1 Tohoku-Oki earthquake, a large-amplitude seismic wave propagated through eastern Honshu (e.g., Suzuki et al. 2011). Fractional subsurface velocity change after the earthquake was reported associated with the strong motion and the large stress/strain change (e.g., Brenguier et al. 2014; Nakata and Snieder 2011). We conducted PII using the records of the vertical components of Hi-net. Following a stretching method proposed by Wegler et al. (2009), we estimated the time delay of the ACF from the reference ACF in the lag time of 4–15 s for the frequency range of 1–3 Hz and detected the changes in the subsurface

seismic velocity structure that occurred during the 2011 Tohoku-Oki earthquake.

Figure 7 shows the ACFs obtained from the continuous Hi-net records of the N.KMIH station during the period of 2008–2013. The ACE, which is considered as a Green's function of the source and receiver located at the station, does not vary significantly and shows high stability over each time period. However, looking carefully, a slight time delay from the lag time can be observed immediately following the occurrence of the 2011 Tohoku-Oki earthquake. For example, there is a time delay of approximately 0.1 s at a lag time of approximately 8.5 s.

The time delays between the reference ACF and the ACFs from 30 October 2010 and 30 October 2011 at each lag time are estimated in Fig. 8(a1, a2), respectively. The reference ACF is defined as the mean of the ACFs in 2009 and 2010. For comparison, we first estimated the time delay on 30 October 2010, a day without a large



event, as shown in Fig. 8(a1). No systematic variation of the time delay with the lag time is evident in the figure. Conversely, in Fig. 8(a2), which shows the time delay on 30 October 2011, a day roughly 5 months after the 2011 Tohoku-Oki earthquake, it is evident that the time delay increases with increasing lag time. The stretching method in the PII interprets the time delay of an ACF as being caused by a decrease in the background velocity structure; when the background seismic velocity decreases by  $\alpha\%$ , the time delay is given by  $dt = \alpha/100$  for a lag time of  $t$  (e.g., Sens-Schönfelder and Wegler 2006). We estimated that the velocity structure decreased by approximately 0.5 % at the N.KMIH station after the 2011 Tohoku-Oki earthquake (Fig. 8b).

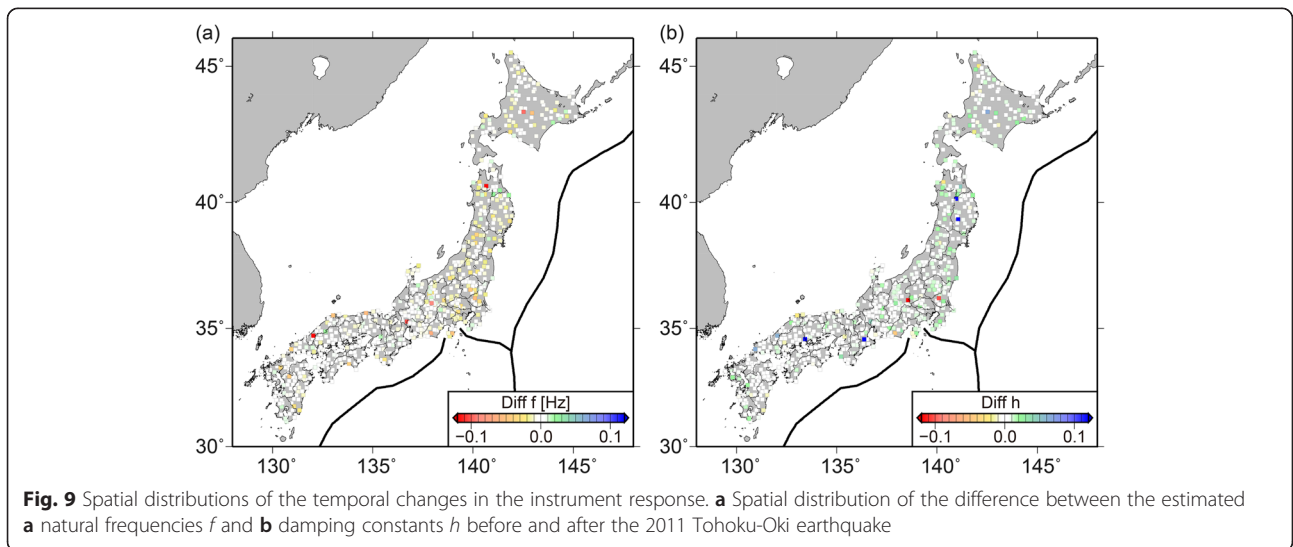
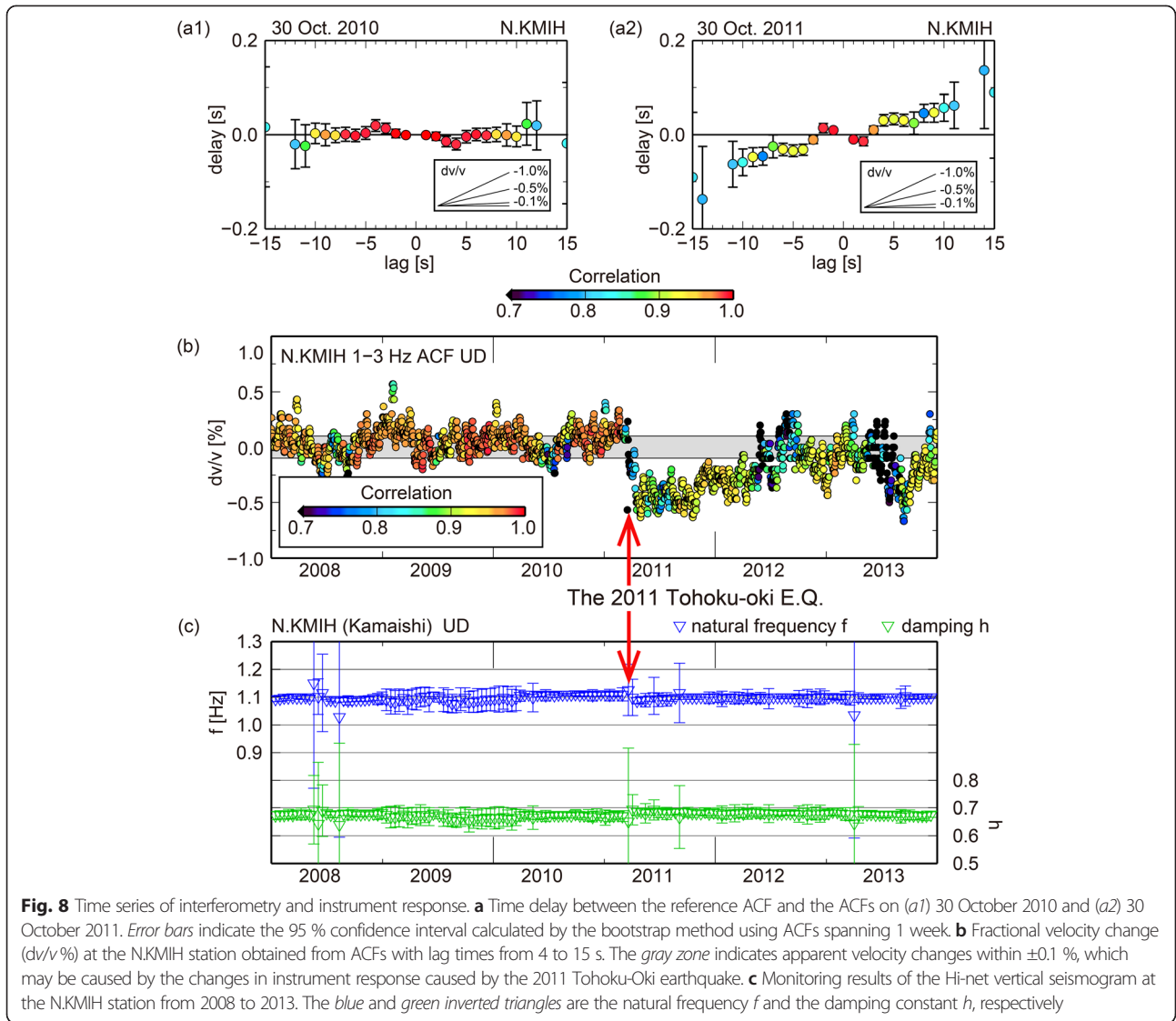
### Changes in instrument response

Since the ground shaking caused by the 2011 Tohoku-Oki earthquake was too strong for a high-sensitivity seismograph, an instrument response change must be considered. After the earthquake, in fact, a very small change of the  $f$  and the  $h$  seems to occur at N.KMIH as shown in Fig. 8c. We may have misidentified the change in the instrument response as corresponding to a change in the subsurface velocity structure resulting from the earthquake. Therefore, we investigate whether the change in the instrument response can misrepresent the subsurface velocity change.

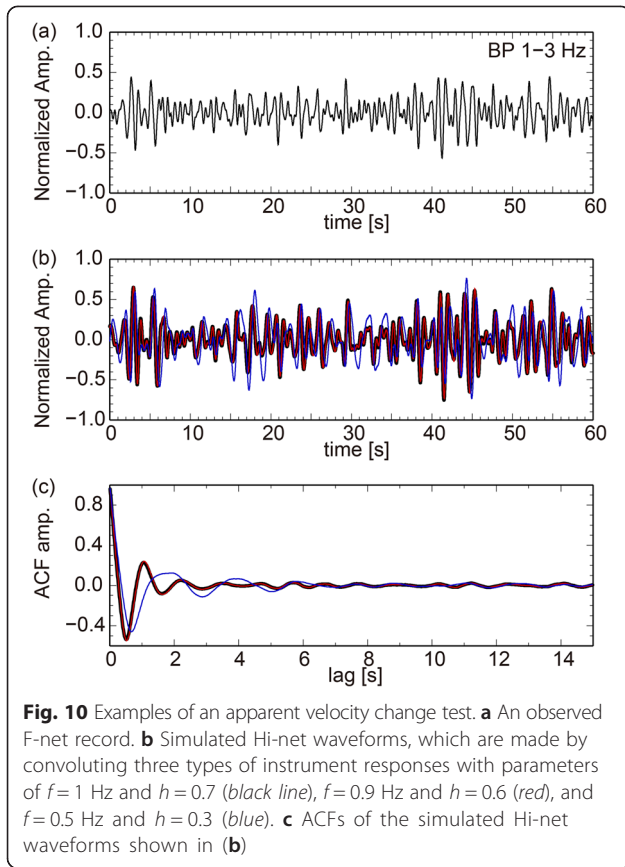
Figure 9 shows the distribution of the differences between the instrument responses before and after the earthquake. We found that many stations in northeastern Japan had small instrument response changes. This means that the instrument responses for the Hi-net sensors, especially those in northeastern Japan, were affected by the large shaking of the 2011 Tohoku-Oki earthquake. However, the changes in the natural frequencies and damping constants for the sensors were smaller than  $\pm 0.05$  Hz and  $\pm 0.05$ , respectively.

### Apparent temporal changes in subsurface structure due to changes in instrument response

We then examined the extent to which the change in the instrument response during the 2011 Tohoku-Oki earthquake could affect the velocity change estimated by PII. First, a band-pass filter with a passband of 1–3 Hz was applied to ambient noise recorded by a broadband F-net station (N.KSNF) as shown in Fig. 10a. We then convoluted instrument responses characterized by  $(f, h) = (1.0 \text{ Hz}, 0.7)$ ,  $(0.9 \text{ Hz}, 0.6)$ , and  $(0.5 \text{ Hz}, 0.3)$  to simulate a seismogram of a normal Hi-net sensor, a seismogram of a Hi-net sensor which was slightly damaged by age-related degradation or large earthquakes, and a seismogram in an extreme case, respectively (black, red, and blue lines, respectively, in Fig. 10b). Figure 10c shows the ACFs for the three types of simulated







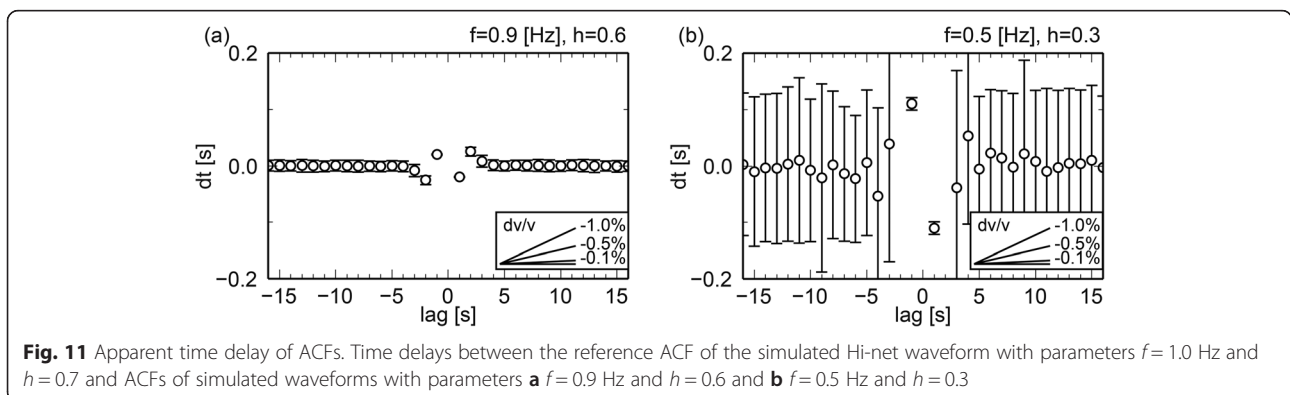
seismogram records which were calculated using the same method as in Fig. 4.

Figure 11 shows the estimated time delay from the reference ACF with  $f = 1.0$  Hz and  $h = 0.7$  for each lag time of ACFs with  $f = 0.9$  Hz and  $h = 0.6$ , which represents a possible change in the instrument responses after the 2011 Tohoku-Oki earthquake, and  $f = 0.5$  Hz and  $h = 0.3$ , which represents an unrealistically extreme case. We did not find a systematic time delay according to the change in the lag time. Additionally, a very small velocity change of less than 0.1 % may be obtained by the stretching method when a possible response change

occurs (Fig. 11a). However, the velocity reduction caused by the 2011 Tohoku-Oki earthquake was 0.5 %, as shown in Fig. 8(a2) and 8b. Since this velocity change is significantly larger than 0.1 %, the obtained velocity structure change is not an artifact caused by the instrument response change during the large earthquake. Figure 11b shows the result for an extremely large instrument response change, which shows unstable values of the lag time  $dt$  at each elapsed time. This extreme case of changes in the instrument response cannot reproduce a systematic change in the lag time, according to the lag time obtained by the PII (Fig. 8(a2)). Therefore, we conclude that the change of an instrument response caused by age-related degradation or large earthquakes is usually too small to affect the result of the PII.

### Conclusions

We monitored the instrument responses for Hi-net sensors for 10 years from 2003 to 2013 by estimating their natural frequencies  $f$  and damping constants  $h$  from the test signal. We found that the Hi-net sensors are well controlled with small instrument-to-instrument variation; more than 95 % of the sensors show natural frequencies in the range of  $f = 1.0$ – $1.2$  Hz and damping constants in the range of  $h = 0.6$ – $0.8$ . Furthermore, each Hi-net sensor is very stable against the temporal change over a decade. Their standard deviations of the natural frequency and damping constant were within 0.05 Hz and 0.05, respectively. During the 2011 Tohoku-Oki earthquake, large seismic waves exceeding the dynamic range of the Hi-net sensor were observed at the stations near the earthquake focal area. Small changes in the instrument response were also recognized in the Hi-net sensors after the earthquake. Thus, we conducted a synthetic test to investigate how changes in the instrument response can cause errors in seismic interferometry analysis. The test indicated that the instrument response change did not result in systematic variation in the time delay obtained from the PII of the 2011 Tohoku-Oki



earthquake. This supports the conclusion that the 0.5 % decrease in the velocity at the N.KMIH station after the 2011 Tohoku-Oki earthquake was not due to artificial error caused by the large ground shaking.

#### Competing interests

The authors declare that they have no competing interests.

#### Authors' contributions

TU analyzed data and drafted the manuscript. TS offered numerous comments about the analysis. KS offered numerous comments about the Hi-net record. YH observed and provided the seismic records of Hi-net. All authors read and approved the final manuscript.

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