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Cohesive strength of nanocrystalline ZnO:Ga thin films deposited at room temperature

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Abstract

In this study, transparent conducting nanocrystalline ZnO:Ga (GZO) films were deposited by dc magnetron sputtering at room temperature on polymers (and glass for comparison). Electrical resistivities of 8.8×10^{-4} and $2.2 \times 10^{-3} \Omega \text{ cm}$ were obtained for films deposited on glass and polymers, respectively. The crack onset strain (COS) and the cohesive strength of the coatings were investigated by means of tensile testing. The COS is similar for different GZO coatings and occurs for nominal strains approx. 1%. The cohesive strength of coatings, which was evaluated from the initial part of the crack density evolution, was found to be between 1.3 and 1.4 GPa. For these calculations, a Young's modulus of 112 GPa was used, evaluated by nanoindentation.

Introduction

Doped ZnO thin films are widely used as transparent electrodes in optoelectronic and electro-optic devices such as solar cells and flat panel displays [1-3], because of their unique properties, specifically low electrical resistivity and high transmittance in the visible spectral region [4]. These properties are obtained using substrate temperatures higher than 200°C, but growing interest in flexible substrates has led to the use of polymeric alternatives, which require the deposition of films at low temperature [5]. Furthermore, the deposition on polymeric substrates decreases the quality of the film properties [6]; therefore, the pursuit toward an understanding of the structural, electromechanical and electro-optical properties of nanocrystalline (nc) thin films is crucial for device applications.

Experimental details

ZnO:Ga (GZO) thin films were deposited by dc-magnetron sputtering on glass and polyethylene naphthalate (PEN) substrates, under an Ar atmosphere with a base pressure of 2×10^{-4} Pa, from a GZO target (zinc oxide/gallium oxide, 95.5/4.5 wt.%) of 2" diameter. A target current density of 0.6 mA/cm² was applied, and a deposition rate of 21 nm/min was obtained. No bias was applied to

the substrate holder during the depositions, which took place at room temperature. The working pressure (P_w) was varied from 0.41 to 0.86 Pa, with the target-to-substrate distance kept at a constant 8 cm. The crystallinity and crystal orientation was studied using a Bruker AXS Discover D8 (Madison, USA) for X-ray diffraction (XRD). Glass substrates were used to avoid the presence of polymer substrate peaks. The electrical resistivity, carrier concentration and Hall mobility of the coatings on glass substrates were all measured using Van der Pauw geometry under a magnetic field of 1 Tesla. The electro-mechanical tests were carried out on $10 \times 40 \text{ mm}^2$ samples using a computer-controlled tensile testing machine (Minimat, Polymer Labs, Loughborough, UK), which was mounted on an optical microscope stage (Nikon Optiphot-100, Tokyo, Japan). One of the grips of the instrument was displaced at a constant speed of 0.2 mm/min. The applied load and stage displacement values were recorded at 1-s intervals. Crack development was recorded through a CCD camera connected to the microscope, with the evolution of the crack density obtained by the subsequent video analysis. The thickness of the polymer substrates was measured using a Fischer Dualscope MPOR instrument (Sindelfingen, Germany).

Results and discussion

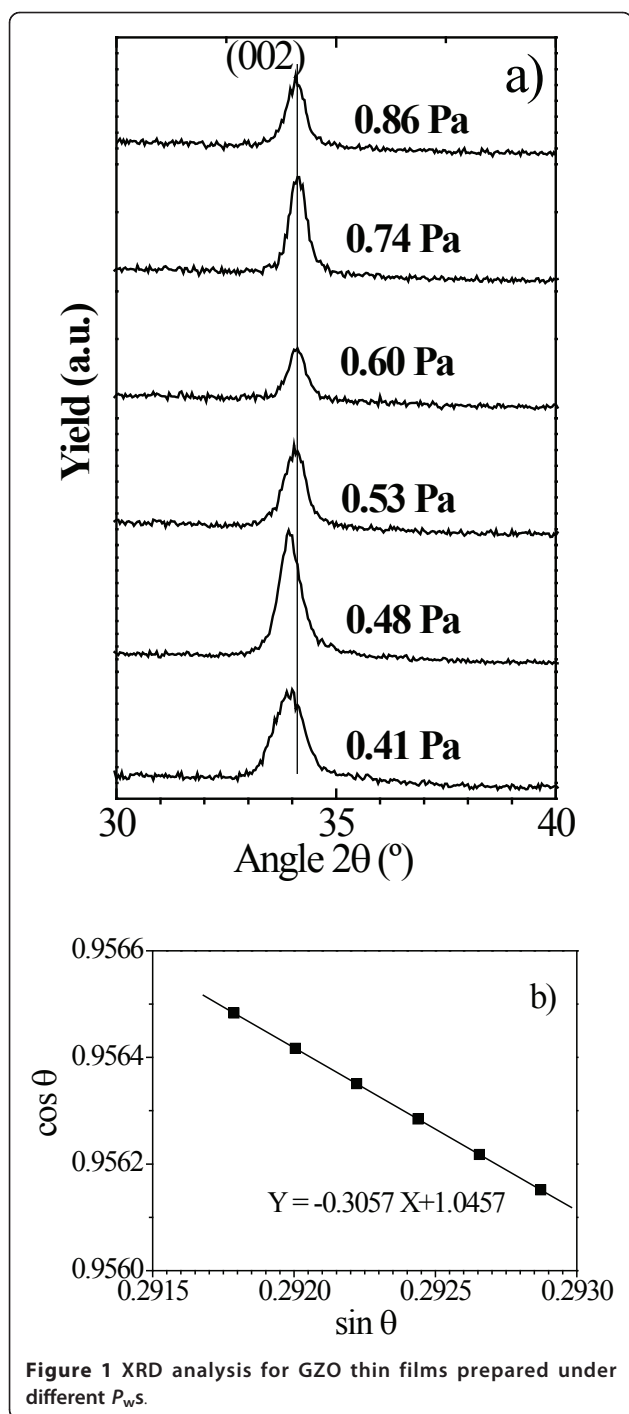
Structural characterization

Figure 1a shows the XRD spectra obtained for nc GZO thin films (approx. 100-nm thick) as a function of the

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P_w , where only the ZnO (002) peak, at approx. 34° , is observed. The spectra reveal a highly textured hexagonal phase with a wurtzite structure. A lower P_w resulted in samples with a higher c -lattice parameter. In the thin films prepared with a P_w , between 0.41 and 0.86 Pa, the (002) peak position shifted from $2\theta = 33.93^\circ$ ($c = 0.528$ nm) to $2\theta = 34.06^\circ$ ($c = 0.525$ nm). The full-width at half-maximum (FWHM) can be expressed as a linear

combination of the lattice strain and crystalline size. The effects of strain and particle size on the FWHM can be expressed as [7]

$$\beta \cos \theta / \lambda = (1/\varepsilon) + (\tau \sin \theta / \lambda) \quad (1)$$

where β is the measured FWHM, θ is the Bragg angle of the peak, λ is the X-ray wavelength (1.5418 Å), ε is the effective particle size and τ is the effective strain. The average particle size, calculated from the plot $\cos \theta$ versus $\sin \theta$ shown in Figure 1b, was 8.7 nm. The particle size (D_v) calculated from Scherrer's formula ($D_v = 0.94\lambda / (\beta \cos \theta)$), was 8.9 nm, which is very close to that calculated from Equation 1 [8]). The presence of strain in the ZnO crystal lattice, caused indirectly by P_w , can be expected to exert significant influence on the mechanical properties of the nc-GZO thin film.

Optical properties

The nc nature of the thin films influences both optical and electrical performance. Figure 2 shows optical transmittance as a function of wavelength for thick GZO films (approx. 700 nm) prepared on glass at various P_w , using air as a reference. The near infra-red transmittance is lower for P_w values of 0.41 and 0.53 Pa and increases with higher P_w , which is consistent with the changes observed in the electrical resistivity (discussed in the next section). The optical band gap for GZO films was calculated by plotting $(\alpha h\nu)^2$ as a function of photon energy ($h\nu$) and extrapolating the linear region of $(\alpha h\nu)^2$ to energy axis where $(\alpha h\nu)^2$ corresponds to zero. Figure 2b shows the plot of $(\alpha h\nu)^2$ as a function of photon energy ($h\nu$) for GZO films. From these plots, it can be seen that the value of the bandgap of GZO decreased from 3.73 eV (0.41 Pa) to 3.48 eV (0.86 Pa), which can be understood in the context of the Burstein Moss shift [9].

Electrical properties

The electrical resistivity, charge carrier concentration and Hall mobility as a function of the P_w , for GZO films deposited on glass, are shown in Figure 3. The resistivity of GZO samples decreased initially, and then increased with the P_w . In general, the average resistivity was low (approx. $10^{-4} \Omega \text{ cm}$), which can be attributed to high carrier concentration. Considering the similarity in the conduction mechanism of electrons in GZO and ITO, the grain boundary (GB) and ionized impurity scattering processes can be considered the two dominant mechanisms, limiting electron transport in nc-GZO films, as in the case of ITO, where other scattering mechanisms such as lattice vibrations and neutral impurity scattering may typically be neglected [10]. The relative importance of the scattering mechanism is dependent on film

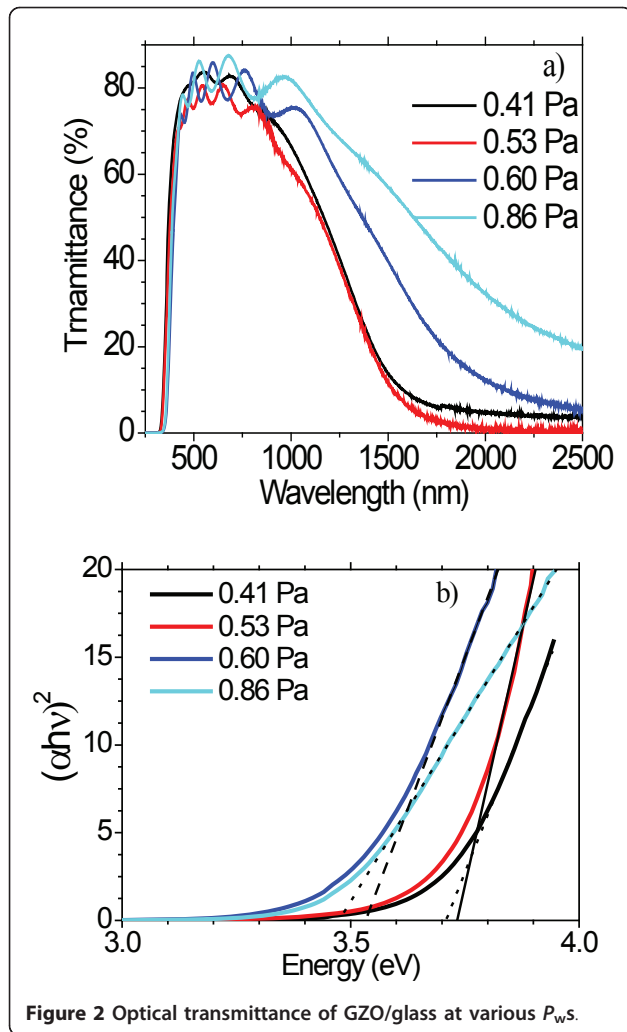


Figure 2 Optical transmittance of GZO/glass at various P_w s.

quality and carrier concentration. Unlike intrinsic ZnO, where the conduction is generally controlled by GB-scattering, in doped ZnO at high electron density ($>10^{20} \text{ cm}^{-3}$), the ionized impurity scattering can be expected to dominate, which explains the low values of electron mobility ($<10 \text{ cm}^2\text{V/s}$) [11].

Tensile tests

Tensile tests were performed at a constant strain rate on PEN substrates ($82 \mu\text{m}$) coated with GZO films (approx. 100 nm) prepared under two different P_w s to increase nominal strains. The PEN substrate is isotropic, and the elastic modulus was 4.23 GPa , as measured through the tensile test on uncoated substrate. The cracking densities as a function of the substrate nominal strain for two different GZO coatings (0.53 and 0.86 Pa) are shown in Figure 4a. The crack densities at saturation of these two PEN/GZO films were 0.316 and $0.515 \mu\text{m}^{-1}$, respectively. The coatings have similar properties and thicknesses, with small differences causing variations wholly within

acceptable margins of error. Using the weakest link model, the coating's cohesive strength was evaluated from the early stages of the fragmentation process, assuming a Weibull-type, size-dependent probability of failure for the coating fragments of length ℓ under a stress σ [12,13]:

$$F(\sigma) = 1 - \exp \left[-\frac{\ell}{\ell_0} \left(\frac{\sigma}{\beta} \right)^\alpha \right] \quad (2)$$

Assuming that the residual stresses were negligible, in the initial stage of fragmentation, the average fragment length was related to the stress acting in the coating. The average fragment length (ℓ) is $\ell_0(\sigma/\beta)^\alpha$, where a normalizing factor (ℓ_0) of $1 \mu\text{m}$ was chosen. In addition, σ is the axial stress acting in the coating, and α and β are the Weibull shape and scale parameters, respectively. These parameters were derived from a plot of $\ln(\ell)$ versus $\ln(\sigma)$, shown in Figure 4b, using the initial part of the crack density evolution of the PEN/GZO coatings, displayed in Figure 4a.

The cohesive strength of the coating at critical length (ℓ_c) can be expressed as

$$\sigma_{\max}(\ell_c) = \beta \left(\frac{\ell_c}{\ell_0} \right)^{-1/\alpha} \Gamma(1 + 1/\alpha) \quad (3)$$

where Γ is the gamma function, $\ell_c = (3/2)\ell_{\text{sat}}$ is the critical length and ℓ_{sat} is the experimental mean fragment length at saturation, which is also the inverse of the crack density at saturation [14]. As shown in Figure 4a, the GZO coatings prepared at P_w of 0.53 and 0.86 Pa revealed mean fragment lengths at saturation of 3.11 and $1.94 \mu\text{m}$, respectively.

In order to take into account its influence, the internal stress was evaluated, and the COS and the coating strength obtained with this method were corrected.

$$\text{COS}^{\text{cor}} = \text{COS} + \varepsilon_i \quad (4)$$

where σ_i is the internal stress and $\varepsilon_i = \sigma_i(1 - \nu_c)/E_c$, the internal strain, with E_c and ν_c being the Young's modulus and Poisson ratio, respectively, of the coating. Young's modulus of GZO was measured by nanoindentation at 113 and 112 GPa from samples prepared at 0.60 and 0.86 Pa , respectively. Young's modulus of the PEN substrate was determined from tensile testing (4.23 GPa). The cohesive strength of the coatings, which was evaluated from the initial part of the crack density evolution, was found to be between 1.3 and 1.4 GPa . The crack onset strains (COS^{cor}) occurs for nominal strains of 1.1 and 1.0% , respectively. The COS and cohesive strength of GZO are relatively similar to those reported in the literature for other polycrystalline conducting films [15].

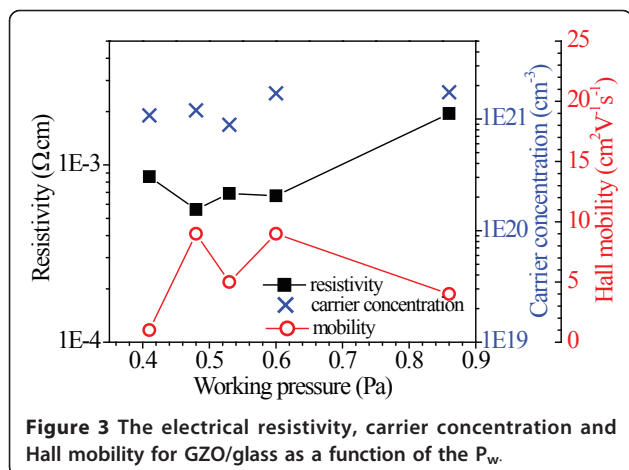


Figure 3 The electrical resistivity, carrier concentration and Hall mobility for GZO/glass as a function of the P_w .

Summary

The material, opto-electrical properties, COS, the coating cohesive strength, as well as the influence of mechanical strain on the electrical properties of nc

GZO thin films were investigated. The estimated average crystalline size of nc-GZO films was approx. 8.7 nm, and the bandgap shifted from 3.73 eV (0.41 Pa) to 3.48 eV (0.86 Pa), where the low resistivity (approx. $10^{-4} \Omega \text{ cm}$) and the high electron density ($>10^{20} \text{ cm}^{-3}$) explain the dominating scattering process as the ionized impurity scattering. The COS is similar for different GZO coatings and occurs for nominal strains approx. 1%. The cohesive strength of coatings, which was evaluated from the initial part of the crack density evolution, was found to be between 1.3 and 1.4 GPa, while the Young's modulus was evaluated by nanoindentation.

Abbreviations

COS: crack onset strains; FWHM: full-width at half-maximum; GB: grain boundary; nc: nanocrystalline; PEN: polyethylene naphthalate; XRD: X-ray diffraction.

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Authors' contributions

LR and SLM proposed the research work, and with APS coordinated the collaborations and carried out the analysis and interpretation of the experimental results. VG and LRP participated in sample processing, electromechanical experimental measurements, and analysis and interpretation of the results. PA, AVK and YAD carried out electrical measurements and SC performed the nanoindentation measurements. All authors read and approved the final manuscript.

Competing interests

The authors declare that they have no competing interests.

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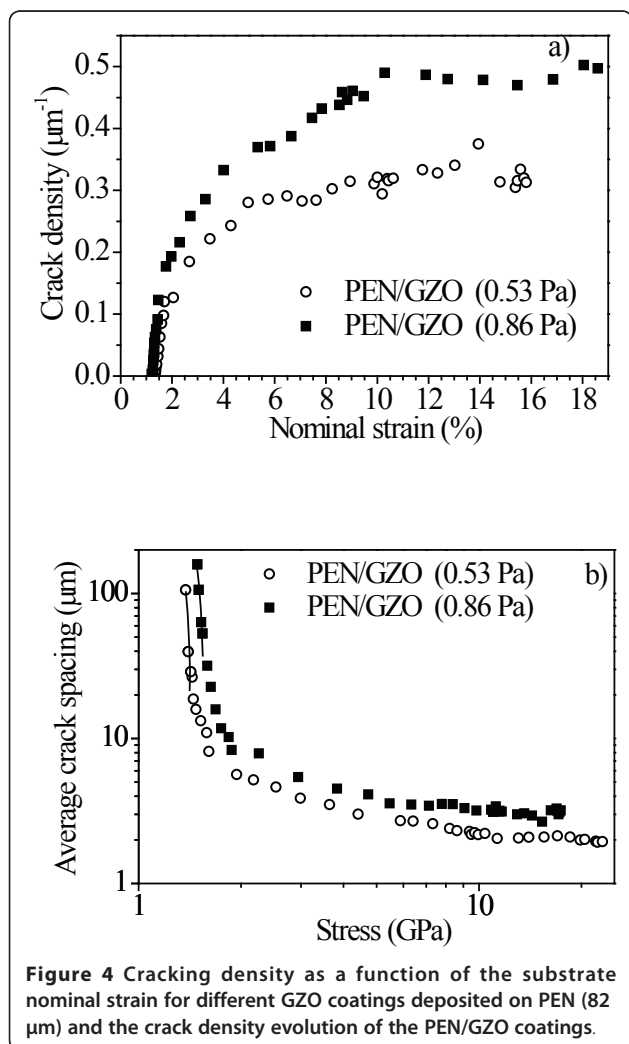


Figure 4 Cracking density as a function of the substrate nominal strain for different GZO coatings deposited on PEN (82 μm) and the crack density evolution of the PEN/GZO coatings.

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