

Regular Article - Experimental Physics

# The cryogenic RWELL: a stable charge multiplier for dual-phase liquid argon detectors

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**Abstract** The operation of a cryogenic Resistive WELL (RWELL) in liquid argon vapor is reported for the first time. It comprises a Thick Gas Electron Multiplier (THGEM) structure coupled to a resistive Diamond-Like Carbon (DLC) anode deposited on an insulating substrate. The multiplier was operated at cryogenic temperature (90 K, 1.2 bar) in saturated argon vapor and characterized in terms of charge gain and electrical stability. A comparative study with standard, non-resistive THGEM (a.k.a LEM) and WELL multipliers confirmed the RWELL advantages in terms of discharge quenching – i.e. superior gain and stability.

#### **Contents**

1	Intro	oduction				
2	Exp	erimental setup				
	2.1	Detector assembly and readout				
	2.2	Cryostat				
3	Methodology					
	3.1	Physics of the detector				
	3.2	Gas purity				
	3.3	Liquefaction and thermal stabilization				
	3.4	Gain stabilization and voltage scan				
4	Results					
	4.1	Collection signals, spectra, and efficiency 5				
	4.2 20GΩ-RWELL at 90 K: amplification signals					
		and spectra				
	4.3	Comparative study				
	4.4	Discharge probability				
5	Sun	nmary and discussion				
R	efere	nces				

# 1 Introduction

In recent years, the Thick Gaseous Electron Multiplier (THGEM) [1,2] and its derivatives have become a leading technology in the field of particle and radiation detection. Thanks to their robustness and relatively low cost, these detectors have been proposed and are currently employed in numerous fields, as reviewed in [3]. Amongst its derivatives, several attempts were conducted to couple the THGEM to resistive materials in order to enhance the detector's immunity against electrical discharges. Closed, WELL-like configurations [4] were proposed with a single-sided THGEM structure attached to a resistive anode, decoupling the multiplier from the readout electrode. Amongst them, the Resistive WELL (RWELL) [5] can be found, having a thin resistive layer anode decoupled from the readout by an insulator; another one is the Resistive Plate WELL (RPWELL) [6], with the resistive-plate anode directly in contact with the readout electrode. Others include the Segmented RWELL (SRWELL) [7], a variant of the RWELL featuring a metallic grid under the resistive film (for faster charge evacuation), that, together with the RPWELL, were proposed as potential sampling elements for Digital Hadronic Calorimetry (DHCAL) [8–10]. All these THGEM and THGEM-like concepts were extensively investigated at room temperature. THGEM detectors (LEM, Large Electron Multipliers) were investigated very intensively in dual-phase liquid argon TPCs [11], as potential candidates for the DUNE neutrino experiment [12]. Results of extensive systematic studies of THGEM-based detectors in noble-liquid vapors are reported in [13,14]. Others were studied at liquid-xenon temperatures in counting gases, e.g. Ne/CH<sub>4</sub>; among them in Gas Photo-Multipliers (GPM) [15,16]. The RPWELL was successfully investigated in Ne/CH<sub>4</sub> down to 163 K [17] and resistive materials have been explored also for large-volume experiments as a possible solution to electrical discharges [18,19].



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979 Page 2 of 11 Eur. Phys. J. C (2023) 83:979

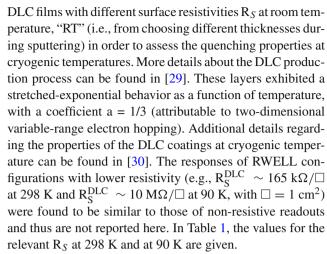
Notwithstanding, the charge readout in dual-phase detectors has been practically abandoned, at least in pure Ar vapors, due to instabilities even at very low gains [20]. A successful concept for attaining robust operation at higher charge gains could permit, e.g. in neutrino experiments, lowering detection thresholds thus reaching sensitivities superior to those of current single-phase devices [21]. A small increase of the charge gain, though, would likely remain insufficient for dark-matter experiments, dealing with very low WIMP-deposited energies [22]. The possibility of integrating resistive materials into detector assemblies, to mitigate the disruptive effects of sparks, turned out to be less straightforward than expected – due to the insulating behavior of resistive materials at low temperatures. So far, only the operation of an RPWELL equipped with a Fe<sub>2</sub>O<sub>3</sub>/YSZ ceramic plate was reported in Ne/CH4 at liquid xenon temperature (163 K) [17]. A game-changing solution that made possible the operation of resistive detectors at liquid argon temperature (90 K) was provided by Diamond-Like-Carbon (DLC) layers [23]. This material has been employed lately for spark protection in various other gas-avalanche detectors at room temperature [24–28]. By adjusting the thickness of the DLC layer, it was possible to cover a broad range of resistivities suitable for spark protection, down to the liquid-vapor coexistence point of argon (87.5 K at 1 bar). In this work, the results of the successful operation of a cryogenic RWELL are summarized and an overview of the detector properties in comparison to its non-protected counterparts (THGEM, THWELL) is provided.

# 2 Experimental setup

# 2.1 Detector assembly and readout

During this study, three detector concepts were investigated: THGEM, THWELL, and RWELL; they are schematically presented in Fig. 1.

The first investigated configuration consisted of a double-sided  $3 \times 3$  cm<sup>2</sup>, 0.8 mm thick THGEM (0.5 mm diameter holes distributed in a hexagonal pattern with 1 mm pitch, and  $\sim 0.1$  mm hole rim) followed by an induction gap of 2 mm and an induction field  $E_i = 5$  kV/cm (see Fig. 1a). In all the cases, the drift field was  $E_d = 0.5$  kV/cm. The second structure was a 0.8 mm thick THWELL detector: a  $3 \times 3$  cm<sup>2</sup>, 0.8 mm thick single-sided THGEM structure (0.5 mm diameter holes distributed in a hexagonal pattern with 1 mm pitch and  $\sim 0.1$  mm hole rim) directly coupled to a metallic anode (see Fig. 1b). The RWELL was realized with a  $3 \times 3$  cm<sup>2</sup>, 0.8 mm thick single-sided THGEM electrode (with the same geometry of the THWELL) pressed onto a metallic anode via a resistive layer deposited on a 0.1 mm thick Kapton insulating foil (see Fig. 1c). Experiments were conducted using



To create electrical contacts, the DLC-coated Kapton foil was fixed onto a PCB, and the DLC layer was connected to two sides of copper lines using cryogenic conductive epoxy.<sup>1</sup> An electrically-insulating cryogenic epoxy,<sup>2</sup> was subsequently used to encapsulate the components (see Fig. 2).

All the electrodes (i.e. cathode, THWELL, resistive layer and readout electrode) were biased by an HV power supply<sup>3</sup> or via a charge-sensitive preamplifier.<sup>4</sup> The latter was equipped with a protection circuit composed of surge arresters<sup>5</sup> in parallel and a series resistor of 220  $\Omega$ . The time evolution of the detector gain was studied in order to establish stable operation conditions. For gain stabilization studies, the signals from the preamplifier were fed to an amplifier<sup>6</sup>; the amplified signals were digitized by a multi-channel analyzer. For all the other measurements, waveforms from the preamplifier were acquired using a digital oscilloscope<sup>8</sup> and post-processed using dedicated Matlab scripts. Histograms of the preamplifier signal amplitude were also acquired using the oscilloscope. Currents from the electrodes were read out by a digitizer<sup>9</sup> and monitored using LabVIEW SignalExpress [31].

# 2.2 Cryostat

The measurements were performed in a dedicated LAr cryostat, WISArD (Weizmann Institute of Science liquid Argon



<sup>&</sup>lt;sup>1</sup> Master Bond EP21TDCS-LO.

<sup>&</sup>lt;sup>2</sup> Stycast 2850FT.

<sup>&</sup>lt;sup>3</sup> CAEN N1471H.

<sup>&</sup>lt;sup>4</sup> Cremat: Model CR-110 with CR-150-R5 evaluation board.

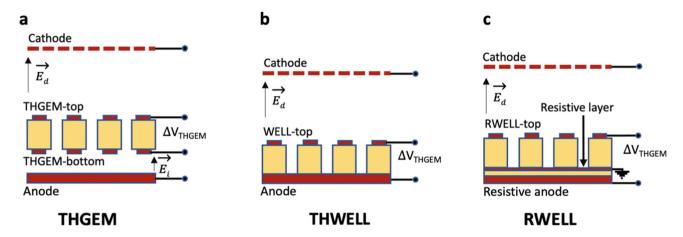
<sup>&</sup>lt;sup>5</sup> 8EC 90, EPCOS-TDK Electronics.

<sup>&</sup>lt;sup>6</sup> Ortec Model 450.

<sup>&</sup>lt;sup>7</sup> Amptek MCA 8000D.

<sup>&</sup>lt;sup>8</sup> Tektronix MSO 5204B.

<sup>9</sup> NI USB-6008.



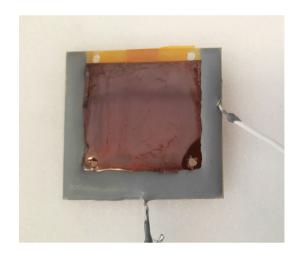
**Fig. 1** Scheme of **a** a THGEM (LEM) detector followed by an induction gap and a readout anode; **b** a THWELL detector, with a metallic anode at its bottom; **c** a RWELL detector, with a thin-film resistive

anode decoupled from the metallic anode by an insulating plate. In all three cases, the drift gap was equal to 15 mm and the THGEM structure (double-sided in  $\bf a$  and single-sided in  $\bf b$ ,  $\bf c$ ) was 0.8 mm thick

Detector) described in detail in [32]. In all the experiments, an <sup>241</sup>Am source emitting 5.5 MeV alpha particles with a rate of about 10 Hz was installed on a metallic plate cathode at a distance of 15 mm from the multiplying electrode. The source emission was opportunely confined using a metallic collimator of 4 mm thickness and 5 mm diameter. A 12 µm Mylar foil was installed at the collimator's emitting face to attenuate the alpha energy to about 4 MeV. This granted full containment of the alpha-particles in the drift volume ( $\approx$  7 mm range in gaseous argon at 90 K, 1.2 bar calculated with SRIM [33] assuming a gas density of 6.65 kg/m<sup>3</sup> [34]. Uncertainties related to the longitudinal and lateral straggling accounted for  $\approx 280 \, \mu \text{m}$  and  $\approx 300 \, \mu \text{m}$ , respectively.). Each detector configuration was operated in the saturated vapor phase of argon at 90 K. This was realized by inserting the detector assembly inside a Teflon cup, as depicted in Fig. 3. Argon was liquefied into the cryostat using a cryocooler, 10 till the upper edge of the cup. The level of the liquid was monitored using temperature sensors located in the proximity of the cup edges, inside the cup adjacent to the detector anode, and in other parts of the system. This prevented the liquid from penetrating into the detector region. The chosen operation within the vapor enclosed in the cup rather than in the liquid phase minimized losses due to electron recombination and extraction (see Fig. 3 in [35]), thus yielding a higher number of ionization electrons and facilitating the measurements. The temperature inside the system was constantly monitored using a temperature controller. 11 A conceptual scheme of the cryogenic setup is depicted in Fig. 3.

Table 1 Surface resistivity at 298 K and at 90 K for two different DLC samples

DLC layer	R <sub>S</sub> <sup>DLC</sup> at 298 K	R <sub>S</sub> <sup>DLC</sup> at 90 K
Sample 1	$\sim$ 14 M $\Omega/\Box$	$\sim 20~\mathrm{G}\Omega/\Box$
Sample 2	$\sim 1~M\Omega/\Box$	$\sim 200~\text{M}\Omega/\Box$



**Fig. 2** Resistive anode composed by a DLC layer fixed on a PCB board with electrically-insulating cryogenic epoxy. The electric connections, realized with cryogenic conductive epoxy, are encapsulated and connected with coaxial wires

#### 3 Methodology

#### 3.1 Physics of the detector

The 4 MeV alpha particles (attenuated  $^{241}$ Am source) generate  $\sim 10^5$  primary electrons in the drift region along a track forming an angle of at least  $60^\circ$  with the detector surface

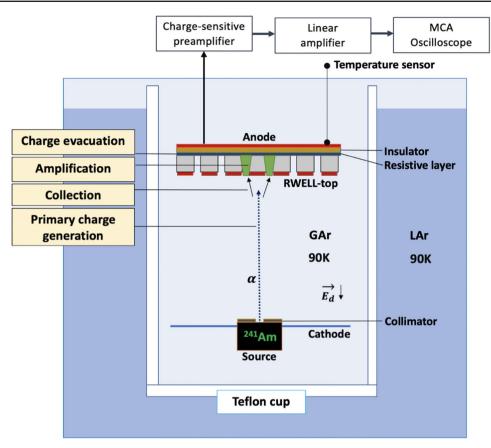


<sup>&</sup>lt;sup>10</sup> Cryomec PT90.

<sup>&</sup>lt;sup>11</sup> CryoCon model 24.

979 Page 4 of 11 Eur. Phys. J. C (2023) 83:979

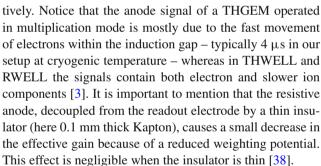
Fig. 3 Scheme of the cryogenic setup for investigating the detectors (here an RWELL). The assembly and the involved physical processes are detailed. The detector was operated at 90 K. 1.2 bar



(W-value of 26.3 eV in Ar [36]). These are drifted towards the THGEM holes under a field  $E_d=0.5\,\mathrm{kV/cm}$ . Increasing the bias across the multiplier electrode, defined as  $\Delta V_{THGEM}$ results in a high electric field within the holes, allowing for the onset of avalanche multiplication of the primary charges. The amplification factor (i.e. detector gain) increases exponentially with  $\Delta V_{THGEM}$ , typically in the range of 2.7–3.2 kV in our configuration. Charge from avalanche electrons is evacuated to the ground through the anode in the THGEM and THWELL multipliers and along the resistive-anode surface in the RWELL (see Fig. 1). An electrical signal is induced onto all the electrodes by the movement of charges (electrons and ions) during the entire process, as described by the Shockley–Ramo theorem [37]. We refer to the collection signal as the one induced by the movement of the primary charges in the drift gap. This was recorded from the cathode in specific measurements where  $\Delta V_{THGEM} = 0$  kV. We refer to the amplification signal as the one induced by the movement of the avalanche charges. It was recorded from the anode with  $\Delta V_{THGEM}$  in the range of detector operation. The effective detector gain can be estimated by the following normalization:

$$G_{Eff} = \frac{P_{Amplif}}{P_{Coll}} \tag{1}$$

where  $P_{Amplif}$  and  $P_{Coll}$  are the Gaussian mean values of the spectra of amplification and collection signals, respec-



#### 3.2 Gas purity

Gas purity plays a crucial role in LAr-TPCs, where a sub-ppb level of electronegative impurities is targeted [39] in order to minimize electron capture during the drift in the liquid or gas. The maximum achievable gain of gaseous multipliers in Ar is strongly affected by the presence of impurities, quenching for instance avalanche-induced VUV photons that are responsible for secondary avalanche feedback [40]. Therefore, for a realistic comparison of the multipliers, they should be investigated in very pure Ar vapor. For this reason, prior to any measurement, the system was vacuum-pumped for at least 12 h reaching a pressure of  $\sim 1 \times 10^{-4}$  mbar. A residual gas analyzer was used to measure the level and composition



<sup>&</sup>lt;sup>12</sup> SRS RGA200.

of residual impurities. It was found that the main sources of contamination were  $H_2O$ , Ne, HF,  $N_2$ , CO. When filling the system with  $\sim 1$  bar of Ar, the residual impurities got diluted to a concentration of 0.1 ppm. This should be compared with the level of impurities in the Ar gas bottle: 99.999% with  $H_2O \le 2$  ppm,  $O_2 \le 2$  ppm,  $C_nH_m \le 0.5$  ppm and  $N_2 \le 5$  ppm, as specified by the producer. During operation, the gas was recirculated and purified with a hot getter<sup>13</sup> in order to grant a nominal impurity content of the order of 1 ppb.

#### 3.3 Liquefaction and thermal stabilization

The cryostat was filled up with liquid argon until a temperature of 90 K was measured in the gaseous phase at the level of the assembly (temperature sensor in Fig. 3). The pressure inside the cryostat throughout all the operations corresponded to the saturation pressure  $P_s = 1.2$  bar at 90 K. In order to grant thermal stability, according to our experience, the detector was not operated during the first six hours following liquefaction. During this period, the gas was purified at 2 L per hour for at least 24 h.

## 3.4 Gain stabilization and voltage scan

The gain of each detector configuration was characterized by scanning the voltage across the RWELL,  $\Delta V_{RWELL}$ , in the operational range while  $E_d = 0.5 \text{ kV/cm}$  was kept constant. An increase of  $\Delta V_{RWELL}$  corresponded to an increase of the detector gain followed by a small reduction (about 20%), up to stabilization after several hours. This effect is due to the accumulation of charges on the THGEM's insulating substrate (holes' walls and rims) [41]. For each voltage configuration, a minimum of 100 spectra of 120 s each were acquired. In Fig. 4, the gain stabilization for the RWELL detector operated at 90 K, 1.2 bar is shown as an example.  $\Delta V_{RWELL}$  was set to 2.7 kV, sufficient to obtain well-defined spectra above noise, and it was subsequently increased up to 3.175 kV in steps of 50 V or 100 V. After a certain value of  $\Delta V_{RWELL}$ , the detector entered a region of electrical instability. This was different for each detector configuration. For the THGEM and THWELL, a single discharge made the detector unstable by removing the charging-up, and a power cycle was required. For the RWELL, discharges were quenched by the resistive layer and the detector could be operated stably despite a loss in energy resolution due to small gain fluctuations (e.g.  $\Delta V_{RWELL} = 3.15$  and 3.175 kV in Fig. 4).

For the RWELL, three regions of operation were identified: (i) discharge-free behavior up to 3 kV, (ii) stable operation in the presence of quenched discharges for 3 kV  $<\Delta V_{RWELL}<3.175$  kV and (iii) presence of constant

currents above 3.175 kV. The measurement was stopped when the detector entered the latter region. For the THGEM and THWELL, two regions of operation were identified: discharge-free behavior up to  $\Delta V_{THGEM} = 3.2$  kV and  $\Delta V_{THWELL} = 2.9$  kV, and an unstable region of intense discharges above it; there the measurements were stopped.

#### 4 Results

#### 4.1 Collection signals, spectra, and efficiency

The process of primary charge drift and collection is independent of the adopted detector configuration. An average collection signal from a dataset of 1000 waveforms is shown in Fig. 5, left. Its risetime provides a good estimate of the cathode-anode transit time of the ionization electrons, given that any alpha track orientation would induce signals of different shape yet with the same total duration. Thus all signals peak at about the same time when recorded through a charge amplifier. For our typical drift field of  $E_d=0.5~\rm kV/cm$ , the average risetime (from 10 to 90% of the signal maximum) corresponds to 5.5  $\mu$ s, yielding a drift velocity estimate of  $v_e=2.7~\rm mm/\mu s$ , which is in approximate agreement with the simulated value at 90 K and 1.2 bar (from Magboltz [42]).

In Fig. 5, right, a typical spectrum of collection-signal amplitudes recorded for a sample of  $4.5 \times 10^3$  waveforms is shown. The spectrum is normalized to the count value of the most probable amplitude. It was calibrated by injecting a known amount of charge through a 2 pF capacitor. The mean value of the distribution corresponds to  $\sim 1.5 \times 10^5$  primary electrons.

In Fig. 6, left, a scan of the WELL detector operated at 90 K, 1.2 bar was carried out in terms of the anode-signal amplitude from the preamplifier as a function of  $\Delta V_{\rm WELL}$ , with E<sub>d</sub> = 0.5 kV/cm. The cathode-signal amplitude recorded at  $\Delta V_{\rm WELL}$  = 0 kV and E<sub>d</sub> = 0.5 kV/cm, is also reported for comparison; it is the same for the RWELL (Fig. 5, left). Each point was recorded using the digital oscilloscope and represents the mean value of the distribution of signal amplitudes, each one containing  $10^3$  entries. The uncertainties were extrapolated as the  $\sigma$  of the charge distributions. One can observe in Fig. 6, right, a rise of the collection efficiency reaching a plateau at about  $\Delta V_{\rm WELL} = 1.2$  kV, remaining constant until the onset of charge multiplication at about  $\Delta V_{\rm WELL} = 1.5$  kV. A charge gain  $\sim$  8 can be derived from Fig. 6, left, at  $\Delta V_{\rm WELL} = 2.9$  kV.

Thus, for  $\Delta V_{\rm WELL} \geq 1.5$  kV, the detector operates with full collection efficiency and, consequently,  $G_{\rm Eff}$  (defined in Eq. 1) is equivalent to the absolute detector gain  $G_{\rm Abs}$ . These conclusions apply to the RWELL case as well.



<sup>&</sup>lt;sup>13</sup> Entegris HotGetter PS3-MT3-R-2.

**979** Page 6 of 11 Eur. Phys. J. C (2023) 83:979

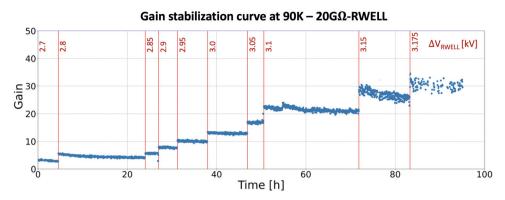
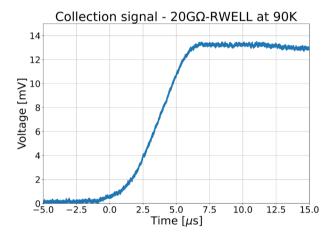


Fig. 4 Gain stabilization for the  $20G\Omega$ -RWELL detector operated with alpha-particles at 90 K, 1.2 bar. The voltage configurations are indicated by red vertical bars and the corresponding values in kV are reported above them. The gain decreased over time (20% gain reduction) until

stabilization. For 3 kV  $<\Delta V_{RWELL}<3.175$  kV, the detector operated in the presence of quenched discharges. Gain fluctuations are also visible at  $\Delta V_{RWELL}=3.15$  and 3.175 kV



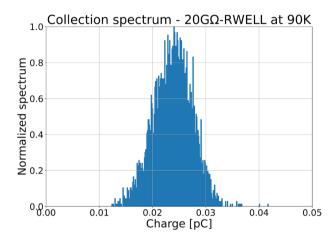


Fig. 5 Left: Average charge-collection waveform from the preamplifier, for an RWELL detector operated with alpha-particles at 90 K, 1.2 bar; Right: Signal amplitude spectrum calibrated to charge

# 4.2 20GΩ-RWELL at 90 K: amplification signals and spectra

The detector voltage was scanned in the range  $\Delta V_{RWELL} = 2.7-3.2$  kV. In Fig. 7 left, the calibrated charge spectra are shown. Histograms were recorded using the MCA and each one contained  $\sim 5 \times 10^3$  entries. All spectra were normalized to their area and to the maximum at  $\Delta V_{RWELL} = 2.7$  kV. The lowenergy tail is attributed to the partial energy deposition of alpha particles exiting the collimator at large angles.

For detailed risetime studies, a waveform-by-waveform analysis was made and the most probable value (mpv) was taken from a Gaussian fit to the risetime distributions. Exemplary histograms are shown in Fig. 7 right. An increase of the risetime as a function of  $\Delta V_{RWELL}$  was observed in Fig. 8 (orange circles), from around 4 to 8  $\mu$ s. Despite the limited

signal/noise, a drift velocity analysis was carried out using the technique introduced for  $\alpha$ -particles in [43] and a constant value of  $v_e \sim 1.8$  mm/ $\mu$ s was found (about 30% less than the simulated value quoted in the previous section). This indicates that the main contribution to the spread of the risetime distributions comes from the different orientations of the  $\alpha$ particles, while the increase of the mpv with  $\Delta V_{RWELL}$  stems from the detector response. A quadratic subtraction of the low-field risetimes, performed in order to isolate the effect, is superimposed in Fig. 8 (blue circles). The time constant associated with photon feedback [44,45] is shown for illustration (magenta dashed line). Even if a good match is visible, the observed agreement might be coincidental. Field modifications due to ion space charge or charge accumulation at the plate may induce a similar effect given that the contribution from the ion-drift across the THGEM structure amounts



Eur. Phys. J. C (2023) 83:979 Page 7 of 11 97

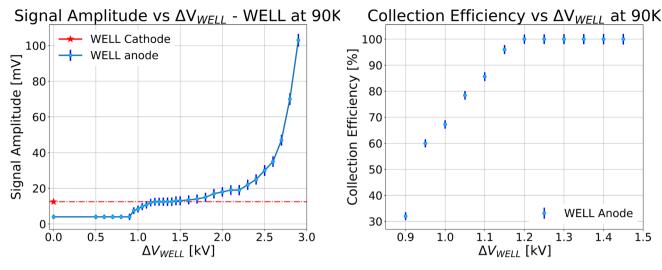


Fig. 6 Left: Scan of the WELL detector operated at 90 K, 1.2 bar in terms of the anode signals' amplitudes from the preamplifier as a function of  $\Delta V_{WELL}$ , with  $E_{\rm d}=0.5$  kV/cm. The cathode signal amplitude

is also reported for comparison (see red star); right: WELL collection efficiency as a function of  $\Delta V_{WELL}$ , with  $E_d=0.5~kV/cm$ 

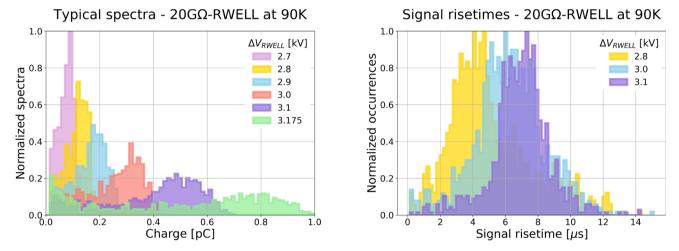


Fig. 7 Left: Reconstructed  $\alpha$ -spectra obtained from an RWELL detector irradiated with  $\alpha$ -particles at 90 K, 1.2 bar; right: risetime distributions obtained in the same thermodynamic conditions

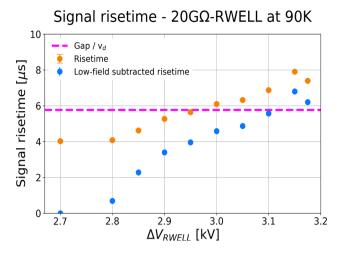
to  $\approx 1~\mu s$ : a field reduction down to 20%, even if a priori very extreme, would cause a similar increasing trend with  $\Delta V_{RWELL}.$  On the other hand, ion feedback from the cathode, at the timescale of ms, would lead to well-separated spurious signals that were only present at  $\Delta V_{RWELL}=3.175~kV$  (up to 40% of the events, with a discharge rate of  $\approx 1\%$ ). Perhaps the best indication that breakdown is slow (either photon or ion-driven), in contrast to a conventional streamer mechanism, is the fact that the surface resistance required in present conditions is considerably larger than that required in VUV-quenched gases at room temperature.

Figure 9 depicts the RWELL gain as a function of  $\Delta V_{RWELL}$  at different temperatures (presented in Fig. 2a of [46]). Gain uncertainties represent the gain variations of the stabilization curve.

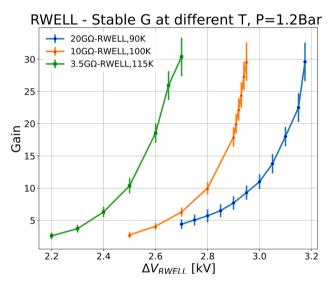
Since the gas pressure was kept constant along the experiments, in first approximation the gas density is only temperature-dependent,  $\rho_g \sim T^{-1}$ . The DLC resistivity decreased with increasing temperature, from  $20~\text{G}\Omega/\square$  at 90~K to  $10~\text{G}\Omega/\square$  at 100~K and  $3.5~\text{G}\Omega/\square$  at 115~K [30]. The detector characterization was performed first at 90~K, then the LAr level was reduced by warming up the system and extracting gas until the temperature reached the levels of 100~K and 115~K. The maximal achievable stable gain in the presence of quenched discharges was approximately 30~regardless of the temperature and DLC resistivity. The three curves manifest the same exponential trend, which is a feature of avalanche multiplication. Above a detector gain close to 18, the presence of quenched discharges was observed ( $\approx 0.25~\text{µC}$ ); they did not prevent the RWELL operation



979 Page 8 of 11 Eur. Phys. J. C (2023) 83:979



**Fig. 8** Most probable signal risetime as a function of the applied voltage for the RWELL detector operated at 90 K, 1.2 bar, with  $\rm E_{\it d} = 0.5~kV/cm$  (orange circles). The low-subtracted risetime (blue circles) and the photon feedback time constant (magenta dashed line) are also reported

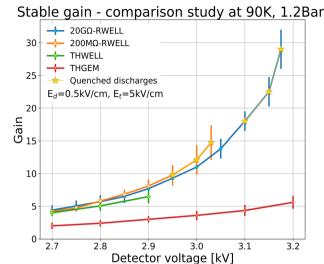


**Fig. 9** RWELL gain, measured in stable operation conditions, as a function of the applied voltage at different temperatures. The resistivity of the DLC layer at each temperature is also reported. Reprinted from [46]

and did not affect its performance. Above a gain of 30, the appearance of constant currents led to the detector tripping.

#### 4.3 Comparative study

Past studies with LEM structures in dual-phase argon TPCs were carried out in different conditions: 87 K, 0.98 bar, cosmic muons, and unknown argon purity [47]. Thus, such results in terms of maximum achievable gain can not be directly compared to the ones obtained in this study. In order to demonstrate the potential advantages of the resistive configuration, the RWELL detector response was compared with



**Fig. 10** Comparison study showing the stable gain for a THGEM+2mm induction gap, a THWELL, a 200M $\Omega$ -RWELL and a 20G $\Omega$ -RWELL, at 90 K and 1.2 bar. In all cases, the THGEM structure was 0.8 mm thick (see text)

Table 2 Maximal stable-gain values for the investigated structures

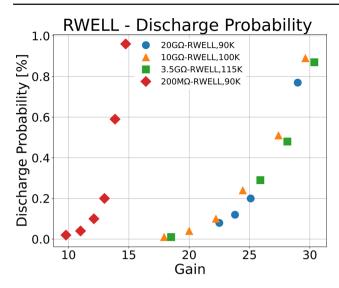
Detector	THGEM	THWELL	200MΩ-RWELL	20GΩ-RWELL
Max stable	6	8	15	30
gain				

that of THWELL and THGEM (LEM) in the same experimental system, irradiation source and conditions, at 90 K and 1.2 bar. Note that the RWELL was operated with DLC anodes of 200  $M\Omega/\square$  and 20  $G\Omega/\square$ . The data were recorded after a gain stabilization cycle in purified Ar (see above). In all cases,  $E_d$  was kept at 0.5 kV/cm and the induction field in the THGEM configuration was set to 5 kV/cm.

Gain curves for all the tested detectors are shown in Fig. 10. The uncertainties on the gain were extracted from the gain stabilization measurements as the  $\sigma$  of the distribution. It is possible to observe that both RWELL detectors outperform their non-protective counterparts. The maximal stable-gain values achieved are summarized in Table 2:

The respective 2- and 4-fold gain increase of the RWELL configuration compared to the THWELL can be explained by the discharge quenching features of the resistive layer. Discharges occurring in the two non-protected detectors, WELL and THGEM, generally led to the tripping of the detector and often damaged the preamplifier. In both RWELL configurations, the presence of quenched discharges was observed: at 10 < G < 15 for the  $200 \text{M}\Omega\text{-RWELL}$  and 18 < G < 30 for the  $20 \text{G}\Omega\text{-RWELL}$ . Discharges could be sustained throughout the detector operation without affecting the stable gain, the discharge charge ( $\approx 0.25~\mu\text{C}$ ) was  $\sim 15\text{-fold}$  lower than the one of unprotected detectors ( $\geq 3.75~\mu\text{C}$ ), and





**Fig. 11** Discharge probability as a function of the RWELL gain for four different configurations:  $200M\Omega/\Box$  at 90 K and  $20~G\Omega/\Box$  at 90 K,  $10~G\Omega/\Box$  at 100 K,  $3.5~G\Omega/\Box$  at 115 K. Irradiation done with 4 MeV alpha particles, pressure: 1.2 bar

destructive effects to the electronics were strongly mitigated. Beyond  $\Delta V_{RWELL}$  = 3.05 kV for the 200M $\Omega$ -RWELL and  $\Delta V_{RWELL}$  = 3.175 kV for the 20G $\Omega$ -RWELL, both RWELL configurations were not operable due to the presence of constant currents.

#### 4.4 Discharge probability

We define the discharge probability  $P_d$  as the number of discharges occurring per detected alpha particle per unit of time:

$$P_d = \frac{N_d}{E_r \times t}$$

where  $N_d$  represents the number of discharges recorded,  $E_r$  is the rate of detected events and t is the measurement time.  $E_r$  was measured using a surface-barrier silicon detector<sup>14</sup> and was found to be  $\approx 10$  Hz.

In Fig. 11, the discharge probability of the RWELL is depicted as a function of gain at different temperatures (90 K–200 M $\Omega$ / $\square$ , 90 K–20 G $\Omega$ / $\square$ , 100 K–10 G $\Omega$ / $\square$ , 115 K–3.5 G $\Omega$ / $\square$ ).

Note the fast rise in discharge probability with the lowest resistivity RWELL, while the other three behave similarly. This is related to the fact that, for a higher  $R_{\rm S}$ , the charge evacuation process is slower and consequently, the effective electric field at the bottom of the hole is reduced during the development of the avalanche, leading to quenching. In all cases, at maximal gain values, the discharge probability reaches  $\sim 1\%$ .

#### 5 Summary and discussion

The availability of DLC films with tunable surface resistivity has permitted, for the first time, the implementation of the cryogenic RWELL. It was operated under 4 MeV alpha particles in purified Ar at 90 K and 1.2 bar. With resistive anodes of 200 M $\Omega$ / $\square$  and 20G  $\Omega$ / $\square$ , the RWELL exhibited discharge-quenching capabilities and could reach gains of  $\sim$  15 and  $\sim$  30, respectively. Relative to RWELL detectors operated at room temperature, much higher R<sub>S</sub> values were needed to reach lower discharge quenching factors [5,38]. A comparison with a THWELL and with a THGEM (LEM) + 2 mm induction gap demonstrated the superiority of the resistive configurations in terms of stability and gain (the latter was 6 and 8 for the THGEM and THWELL, respectively, with alpha particles).

The RWELL was operated also in the presence of moderate discharges, the latter being  $\sim$  15-fold smaller than those in THWELL. In general, non-resistive configurations could not be operated in the presence of discharges, which also happened to damage the electronic readout. For all the configurations with  $R_S > 3.5 \text{ G}\Omega/\square$ , it was possible to operate the detector with  $P_d \le 0.01\%$  (upper bound estimation limited by the source rate and measurement time) up to a gain  $\sim$  18, after which the discharge probability sharply increased to  $\approx 1\%$  at a gain of  $\sim 30$ . The dependence of the discharge probability on R<sub>S</sub> cannot be explained by simple considerations based on the streamer mechanism, which would lead to quenching resistances lower than the ones employed here (in line with observations in quenched mixtures at RT). For this reason, the process of discharge quenching at cryogenic conditions requires further investigation.

A factor 2.5–5 higher stable gain values was reached with the RWELL compared to a bare THGEM/THWELL in our current setup under the same conditions. This demonstrates the potential advantage of coupling a resistive anode to the multiplier, also in noble gas at cryogenic conditions. A direct comparison with the results presented in literature obtained with LEM detectors [48] was not possible due to the different conditions of operation (e.g. gas density and purity, type of primary ionization, different electrode parameters, etc.).

To conclude, the successful operation of the RWELL detector at cryogenic temperature represents an important milestone. Though requiring further investigations, it has the potential for improved scalable readout in future large-volume dual-phase detectors. The scaling up depends on industrial THGEM-electrode production limits and DLC-coating facilities. Electrode sizes reaching  $50 \times 50 \text{ cm}^2$  were already reported [49]; DLC-film coating currently reaches  $20 \times 100 \text{ cm}^2$  [50]. DLC films proved to be robust, minimally affected by aging, and cheap to produce [51].



<sup>&</sup>lt;sup>14</sup> Ortec F Series Partially Depleted Silicon Surface Barrier Radiation Detector.

**979** Page 10 of 11 Eur. Phys. J. C (2023) 83:979

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