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Removal of Cr (III) and Ni (II) from tannery effluent using calcium carbonate coated bacterial magnetosomes

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Heavy metal contamination of surface water bodies and ground water has been a major problem around the world. Calcium-based adsorbents are effective but cannot be separated easily after the treatment. Magnetosomes are biogenic magnetite synthesised as highly ordered chain-like structures by magnetotactic bacteria. In this study, we have prepared magnetically controlled calcite microcrystals using magnetosomes for the adsorption experiment. The ability of magnetic calcite as adsorbent was investigated for the removal of Cr (III) and Ni (II) ions from synthetic solution. Critical parameters, such as the effect of pH, temperature, contact time, initial ion concentration, and adsorbent dose, were optimised in comparison with calcite, magnetosomes, and activated carbon for maximum metal ion removal. The study showed that equilibrium was established in 1 h for both Cr (III) and Ni (II) at a pH of 6.0 and 8.0, respectively. The adsorption process follows pseudo-second-order reaction kinetics, along with Langmuir and Freundlich adsorption isotherms. The thermodynamics of adsorption of both metal ions on magnetic calcite showed that the adsorption was spontaneous and endothermic in nature. Magnetically controlled calcite crystals successfully removed Cr (III) and Ni (II) from collected tannery effluent and separated from the solution by applying magnetic field. Maximum removal of chromium and nickel (94 and 84%) by magnetic calcite is similar to calcite crystals but higher than magnetosomes and activated carbon. The results indicated that magnetic calcite could be used as an alternative adsorbent for removing heavy metals from tannery

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INTRODUCTION

Heavy metal contamination is a cause of serious concern for the environment, aquatic life, animals and humans. The unplanned industrialisation and urbanisation caused severe threat to water bodies worldwide.² In developing countries, the industries are located along the water bodies, and it discharges untreated toxic waste to the surface water.³ The presence of heavy metal ions in water bodies has been a major concern as it can induce toxicity at low-level exposure. The sources of heavy metals in the water bodies are anthropogenic activities, industrial, agricultural, domestic effluents and natural sources.4

The tanning industry that occupies a place of prominence in developing countries produce large amount of wastewater containing toxic heavy metals (Cr, Pb, Zn, Cu, Cd, As, Se).5 Discharge of untreated effluents into the waterbodies causes surface and ground water pollution, endangering biodiversity and lowering agriculture production.⁶ Some of the heavy metals are toxic, carcinogenic or mutagenic, even in very low concentrations. For example, chromium alum and chromium (III) sulphate used during the tanning process produce two forms of chrome; hexavalent chromium and trivalent chromium in which the hexavalent form is toxic. Heavy metals tend to bio-accumulate in the human body and increase the concentration of a chemical in biological organism overtime. A recent report by Roy et al. showed heavy metals present in tannery effluent are toxic to microorganisms, algae, plants and red blood cells (RBC).8

Treatment of metal-contaminated wastewater prior to its discharge to the environment is crucial for the reduction of toxicity. Conventional treatment processes for heavy metal removal from wastewater include chemical precipitation, preoxidation or post-oxidation, coagulation, activated carbon adsorption, reduction, ion exchanges, etc.⁹ These processes have many drawbacks, such as high inputs, toxic by-products and incomplete metal removal. Over the last few decades, cheaper and more effective technologies have been developed for the removal of low levels of trace metals from wastewater and water supplies. 10 Calcium carbonate is an economically efficient and eco-friendly adsorbent for the removal of heavy metals from water. CaCO₃ has been used to remove manganese, 11 cadmium, lead, zinc, nickel and chromium.¹² However, the serious problem of treating metalcontaminated water using calcium carbonate was the drop in the quality of water after treatment.13

The difficulty in separating calcium carbonate from the treated water can be resolved by a secondary separation based on a magnetically enhanced separation technology.¹⁴ Magnetic nanoparticles (MNPs)-based adsorbents are widely used in bioremediation due to the large surface area and easy separation by an external magnetic field.¹⁵ However, the toxicity of chemically synthesised MNPs hindered further development of MNPs-based heavy metal removal filters.¹⁶ Magnetosomes extracted from magnetotactic bacteria (MTB) could be a feasible alternative to resolve such problems. Magnetosomes mineral consists of single crystals of either the ferrimagnetic iron oxide, magnetite (Fe₃O₄), or the iron sulphide, greigite (Fe₃S₄) enveloped by a bilayer lipid membrane.¹⁷ Magnetic properties of MTB have been a subject of growing interest in recent years due to a high level of

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biocompatibility, low toxicity, narrow size distribution and excellent dispersion. In this study, we have fabricated calcium carbonate coated magnetosomes and critical adsorption parameters have been analysed. The possibilities of using magnetically responsive calcium carbonate microcrystals as an alternative method for the removal of heavy metals (Cr (III), Ni (II)) from tannery effluent have been studied briefly.

RESULTS AND DISCUSSION

Characterisation of magnetosomes, calcite and calcite coated magnetosomes

The yield of magnetosomes from Magnetospirillum sp. VITRJS2 was found to be 10 ± 0.7 mg/L of bacterial culture. The cultivation yield of magnetosomes was found to be less than the amount obtained elsewhere. This could be because the hungate standard technique is less efficient than the chemostat culturing method. Modifications of growth media and culturing conditions have

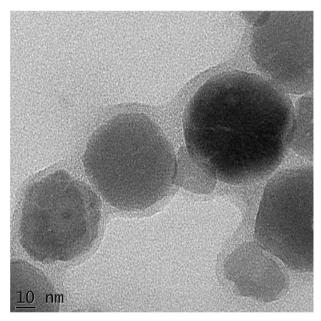


Fig. 1 Transmission electron microscopy (TEM) image of a chain of cubo-octahedral magnetite magnetosomes isolated from the strain VITRJS-2. Individual magnetosome crystals were surrounded by a membrane. The extracted magnetosomes were applied to copper grids and negatively stained with 2.5% (w/v) ammonium molybdate

yielded overproduction of magnetosomes in which a maximum yield of 83.23 ± 5.36 mg/L was obtained. ¹⁸

The shape and size of magnetosomes were determined by transmission electron microscopy (TEM) analysis. The extracted magnetosomes were cubo-octahedral shaped and arranged in chains (Fig. 1). The surface morphology and chemical purity of extracted magnetosome, calcite and calcite-coated magnetosomes were visualised by SEM/EDS analysis (Fig. 2). The synthesised calcite and magnetic calcite showed cubic crystalline structure. EDS analysis of calcite indicated 48.1% carbon, 39.5% oxygen and 12.4% calcium, whereas magnetosome coupled calcite showed 1.6% iron which confirms the coupling of calcite and magnetosomes.¹⁹

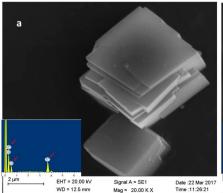
FTIR analysis of magnetosomes, calcite and magnetic calcite showed the absorption peaks from 500 to 4000 cm⁻¹ (Fig. 3). The presence of Fe–O bonds which confirms the magnetite elemental composition of magnetosome. Magnetosomes showed characteristic Fe–O peaks at 524.64 cm⁻¹ (Fig. 3a).²⁰ Calcite showed peaks of calcium at the absorption, 700–900 cm⁻¹ and bands of carbonate were found at 1082 and 1381 cm⁻¹. The magnetic-calcite possesses both magnetite (513/487 cm⁻¹) and calcite (709/869 cm⁻¹) peaks.(Fig. 3c). The presence of peaks from magnetite and calcite represents the coupling of both thus forming magnetic-calcite.

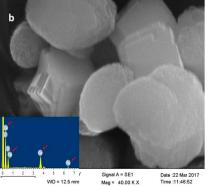
Adsorption of Cr (III) and Ni (II) from aqueous solution

Effect of different factors on adsorption of Cr (III) and Ni (II) by magnetosome, activated carbon, calcite and magnetic calcite was optimised through batch experiments. Critical parameters such as the effect of pH, temperature, contact time, initial ion concentration and adsorbent dose were analysed.

Effect of pH on adsorption of Cr (III) and Ni (II) from aqueous solution

The initial pH of the sorption medium is a critical parameter for adsorption experiments. Change in pH influences the surface charge and the degree of ionisation of the adsorbent surface and thereby affects the sorption capacity. Hence the effect of pH on adsorption of Cr (III) and Ni (II) ions were studied in the range of 2.0–8.0 (Fig. 4). Maximum biosorption capacities were attained at pH 6.0 and 8.0 for Cr (III) and Ni (II), respectively. The amount of Cr (III) and Ni (II) adsorbed per unit of adsorbent increased from pH 2.0 to 6.0 for all four adsorbents. At low pH (2.0) H⁺ ions compete with the metal ions to bind on the adsorbent surface and when the pH increased the negatively charged adsorbent surface was available for the metal ions. However, Cr (III) and Ni (III) precipitate at pH values above 8.0 and hinder the adsorption





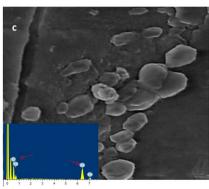


Fig. 2 SEM/EDS analysis of (**a**) calcite microcrystals are of typical rhombohedron/cubic. Crystalline structure and EDS analysis of calcite indicated 48.1% carbon, 39.5% oxygen and 12.4% calcium. (**b**) Magnetic calcite shows the cubic shaped calcite microcrystals and octahedron shaped magnetosome crystals. EDS spectrum of magnetosome coupled calcite showed 1.6% iron which confirms the coupling of calcite and magnetosomes. (**c**) Magnetosomes shows the cubo-octahedral shaped nano crystals arranged as chains

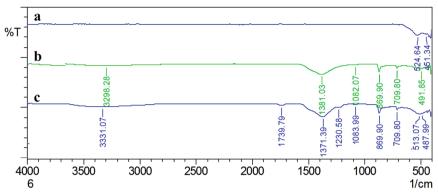


Fig. 3 FTIR analysis of (**a**) magnetosomes shows characteristic Fe–O peaks at 524.64 cm⁻¹. (**b**) Calcite shows peaks of calcium at the absorption, 700–900 cm⁻¹ and bands of carbonate were found at 1082 and 1381 cm⁻¹. (**c**) Magnetic calcite possesses both magnetite (513/487 cm⁻¹) and calcite (709/869 cm⁻¹) peaks

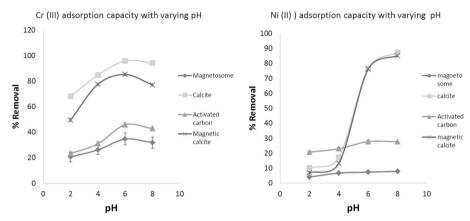


Fig. 4 Effect of pH on equilibrium Cr (III) and Ni (II) adsorption capacity of magnetosome, activated carbon, magnetic calcite and activated calcite (biosorbent dose = 0.5 g/L; $C_0 = 10 \text{ g/L}$; contact time = 12 h; T = 30 °C)

process. Among the four adsorbents used calcite and magnetic calcite showed maximum removal efficiency for Cr (III) (95 and 85%, respectively) followed by activated carbon (45%) and magnetosomes (34%). Adsorption of Ni (III) followed a similar pattern with maximum removal efficiency of 87 and 85% by calcite and magnetic calcite.

Effect of temperature on adsorption of Cr (III) and Ni (II) from aqueous solution

The adsorption of Cr (III) and Ni (II) onto the adsorbents was studied as a function of temperature at different time intervals (Fig. 5). It was observed that the removal of both metals increased with increase in temperature from 20 to 40 °C. Although the rise in % removal efficiency while increasing the temperature is slight, the highest % removal efficiency was observed at temperature 40 °C for both calcite and magnetic calcite. Calcite and magnetic calcite recorded the highest % removal efficiency of 99% for Cr (III) adsorption and 86% for Ni (II) adsorption. The adsorption process is endothermic, and availability of more active sites at a higher temperature may be one reason for the increase in adsorption.

Effect of initial metal concentration on adsorption of Cr (III) and Ni (II) from aqueous solution

Six different concentrations of Cr (III) and Ni (II) ions (50, 100, 250, 500, 1000, 2000 mg/L) were used to determine the effect of initial metal concentration on the adsorption capacity of four selected adsorbents at three different temperatures (Fig. 6). At all the measured temperature, the increase in initial metal concentration results in the increase in adsorption capacity. However, the %

removal efficiency (yield) decreased as the sorption sites get saturated by a higher amount of metal ions. At the lower concentration of metal ions, the available sites of adsorption are more hence higher adsorption yield is obtained.²⁵

Effect of adsorbent dose on adsorption of Cr (III) and Ni (II) from aqueous solution

The influence of adsorbent dose on adsorption of Cr (III) and Ni (II) is shown in Fig. 7. Different doses of adsorbent (100, 250, 500, 1000, 2000 mg/L) were used to find the optimum dosage to remove the maximum amount of Cr (III) and Ni (II) from aqueous solution. When the adsorbent dosage increased the yield of adsorption increased, but the adsorption capacity declined. The percentage of adsorption increased from 35.5 to 99% and from 35 to 82% respectively, for Cr (III) and Ni (II) when treated with calcite. Cr (III) and Ni (II) ions solution treated with magnetic calcite also followed a similar pattern of adsorption. The adsorption capacity of Cr (III) and Ni (II) adsorbed decreased from 3355 to 241.39 mg/g and from 3700 to 423 mg/g, respectively, when calcite/magnetic calcite was used as the adsorbate. The increase in percentage removal could be due to increase in available adsorption sites, whereas the availability of remaining unsaturated sites decreases the adsorption capacity.2

Effect of contact time on adsorption of Cr (III) and Ni (II) from aqueous solution

The equilibrium point of Cr (III) and Ni (II) adsorption from aqueous solution were determined. The adsorption capacity and adsorption yield were calculated at different time intervals to find the



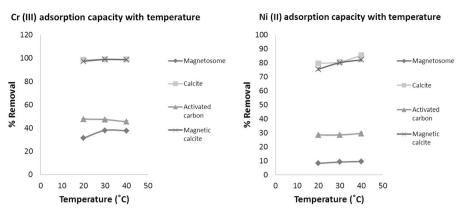


Fig. 5 Effect of temperature on equilibrium Cr (III) and Ni (II) adsorption capacity of magnetosome, activated carbon, magnetic calcite and activated calcite (biosorbent dose = $0.5 \, \text{g/L}$; $C_0 = 10 \, \text{g/L}$; contact time = $12 \, \text{h}$; pH = $6.0 \, \text{for Cr}$ (III) and $8.0 \, \text{for Ni}$ (II)

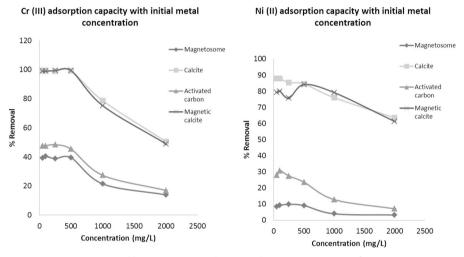


Fig. 6 Effect of initial ion concentration on equilibrium Cr (III) and Ni (II) adsorption capacity of magnetosome, activated carbon, magnetic calcite and activated calcite (biosorbent dose = 0.5 g/L; contact time = 12 h; $T = 40 \,^{\circ}\text{C}$; pH = 6.0 for Cr (III) and 8.0 for Ni (III)

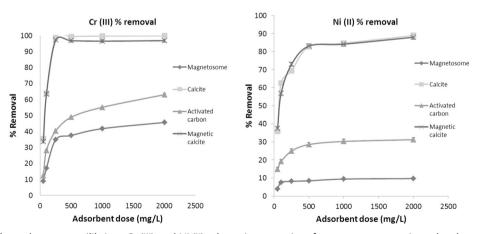
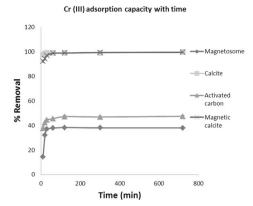


Fig. 7 Effect of adsorbent dose on equilibrium Cr (III) and Ni (II) adsorption capacity of magnetosome, activated carbon, magnetic calcite and activated calcite ($C_0 = 10 \text{ g/L}$; contact time = 12 h; $T = 40 \,^{\circ}\text{C}$; pH = 6.0 for Cr (III) and 8.0 for Ni (II))

equilibrium point (Fig. 8). The equilibrium for Cr (III) and Ni (II) was established after 30 min for all the four adsorbents. The adsorption capacity was found to be constant after the equilibrium point. High adsorption capacity in the initial stages is as a result of the availability of more active sites on the surface of the adsorbent which gets saturated further. ²⁶

Adsorption kinetics

The adsorption process could be dependent on different mechanisms, such as particle diffusion, mass transfer or chemical reactions. The pseudo-first-order kinetic model, pseudo-second-order kinetic model, and intra-particle diffusion model were used to determine the kinetic mechanism of the adsorption process.



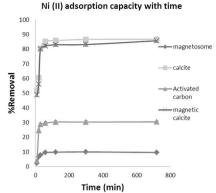


Fig. 8 Effect of contact time on equilibrium Cr (III) and Ni (II) adsorption capacity of magnetosome, activated carbon, magnetic calcite and activated calcite (biosorbent dose = 0.5 g/L; $C_0 = 10$ g/L; T = 40 °C; pH = 6.0 for Cr (III) and 8.0 for Ni (II))

The pseudo-first-order kinetic model of Lagergren describes the rate of occupied adsorbed sites is proportional to the rate of unoccupied sites. The linear form of the pseudo-first-order equation (1) is given as follows:²⁷

$$\log(q_{\rm e} - q_{\rm t}) = \log q_{\rm e} - k_1 t / 2.303 \tag{1}$$

where $q_{\rm t}$ and $q_{\rm e}$ are adsorption capacities at equilibrium (mg/g) and time t and k_1 is the pseudo-first-order rate constant (min⁻¹). A linear plot of log $(q_{\rm e}-q_{\rm t})$ vs. t provided the values of k_1 and $q_{\rm e}$ from the slope and intercept, respectively. The validity of the adsorption mechanism is based on the values of the regression coefficient, R^2 , and the predicted $q_{\rm e}$ values obtained. The R^2 value for all four adsorbents does not fit to the adsorption process, and the predicted $q_{\rm e}$ were different from calculated $q_{\rm e}$. Hence the adsorption process does not show good agreement with the pseudo-first-order kinetic model.

The pseudo-second-order kinetic model implies chemisorption during the adsorption process.²⁸ It is expressed as

$$\frac{t}{q_{\rm t}} = \frac{1}{k_2 q_{\rm e}^2} + \frac{1}{q_{\rm e}} t \tag{2}$$

where $q_{\rm t}$ and $q_{\rm e}$ are adsorption capacities at equilibrium (mg/g) and time t and k_2 is the pseudo-second-order rate constant (g/mL min). The linear plot of $t/q_{\rm t}$ vs. t provided the values of k_2 and $q_{\rm e}$ from the slope and intercept as recorded in Table 1. The experimental and calculated $q_{\rm e}$ values are comparable, and the values of R^2 for the pseudo-second-order kinetic model are high (all greater than 0.9). Hence adsorption of Cr (III) and Ni (II) by all four adsorbents showed good fit into pseudo-second order equation, and chemisorption is one possible mechanism of adsorption for both Cr (III) and Ni (II).

To elucidate the mechanism of adsorption process, the intraparticle diffusion model was applied, and the model equation is expressed as follows:²⁹

$$q_{\rm t} = K_{\rm d}t^{1/2} + C \tag{3}$$

where q_t is adsorption capacities at time t and K_d represents the intraparticle diffusion rate constant, and C is the intercept. A linear plot of q_t vs. $t^{1/2}$ is linear and passes through the origin. The R^2 values for intra-particle diffusion model are high in both the intervals (linear and equilibrium). Therefore adsorption of Cr (III) and Ni (II) by all the four adsorbents follows a possible mechanism of intra-particle diffusion. However, the C value is greater than 0, hence intra-particle diffusion is not the rate determining step in the adsorption process.

Adsorption isotherms

Adsorption isotherm explains the equilibrium between metal ions adsorbed by the adsorbent to the metal ion present in the

solution. The adsorbent capacity of the adsorbent was calculated to design the adsorption system to remove maximum pollutant (metal ions). The Langmuir, Freundlich isotherm models have been used to investigate the effect of initial metal concentrations on adsorbent capacity at different temperatures.

The Langmuir isotherm is used to describe a monolayer adsorption onto the surface of an adsorbent, and the linear form is expressed as follows:³⁰

$$\frac{C_e}{q_e} = \frac{1}{q_o K_L} + \frac{1}{q_0} C_e \tag{4}$$

where $C_{\rm e}$ (mg/L) is the equilibrium concentration, $q_{\rm e}$ (mg/g) is the adsorption capacity at equilibrium, q_0 are the Langmuir constants related to the adsorption capacity and $K_{\rm L}$ is the rate of adsorption. To find the Langmuir constants $C_{\rm e}/q_{\rm e}$ was plotted against $C_{\rm e}$, a straight line with a slope of $1/q_0$ was obtained. The isotherm parameters are computed in Table 2. The correlation coefficient (R^2) is high (all greater than 0.9). Hence good agreement of the Langmuir isotherm was observed based on the experimental data for all the four adsorbents.

The Freundlich isotherm determines the ability of adsorbents in non-ideal sorption on heterogeneous surfaces. The linear form is expressed as³¹

$$\ln q_{\rm e} = \ln K_{\rm F} + \frac{1}{n} \ln C_{\rm e} \tag{5}$$

where $q_{\rm e}$ is the amount of adsorption capacity at equilibrium (mg/g) and $C_{\rm e}$ is the equilibrium concentration of metal ions. $K_{\rm F}$ and n are Freundlich constants, where $K_{\rm F}$ and 1/n are the adsorption capacity of the adsorbent. The plot of $\ln q_{\rm e}$ vs. $\ln C_{\rm e}$ gives linear plot with slope 1/n. Freundlich constants ($K_{\rm F}$ and n) were calculated and are shown in Table 2. High R^2 values show good agreement with the Freundlich model and the value of n gives an indication of how favourable the adsorption process is. Since all the values of n are between 1 and 10, favourable adsorption has been carried out by the selected adsorbents.

Adsorption thermodynamics

The Gibbs free energy changes were calculated by using the equilibrium constants obtained from Langmuir isotherm. The integrated form of this equation is expressed as

$$InK_{L} = \frac{\Delta S^{\circ}}{R} - \frac{\Delta H^{\circ}}{R} \frac{1}{T}$$
 (6)

Gibbs free energy $\Delta \emph{G}^{\circ}$ for each temperature is obtained from the equation

$$\Delta G^{\circ} = \Delta H^{\circ} - T \Delta S^{\circ} \tag{7}$$



Table 1. (a) Coefficients of pseudo-first-order and pseudo-second-order adsorption kinetic models and intraparticle diffusion model (Cr (III) metal ion = 500 mg/L). (b) Coefficients of pseudo-first-order and pseudo-second-order adsorption kinetic models and intraparticle diffusion model (Ni (II) metal ion = 500 mg/L)

Orders model	Parameters	Adsorbents				
		Magnetosome	Activated carbon	Calcite	Magnetic calcite	
a)						
Pseudo-first-order model	$q_{\rm e}$ Cal. (mg/g)	286.83	158.87	220.038	271.05	
	$q_{\rm e}$ Exp. (mg/g)	502.94	652.08	1453.26	1439.38	
	$K_1 (\text{min}^{-1})$	0.009	0.016	0.020	0.015	
	R^2	0.641	0.575	0.514	0.511	
Pseudo-second-order model	$q_{\rm e}$ Cal. (mg/g)	588.24	750	1666.7	1666.7	
	$q_{\rm e}$ Exp. (mg/g)	502.94	652.08	1453.3	1439.4	
	K_2 (min ⁻¹)	0.043	0.399	0.051	0.077	
	R^2	0.992	0.903	0.969	0.968	
Intraparticle diffusion model	K_{I}	70.08	97.12	243.2	236.84	
	K _{II}	2.835	0.378	0.288	0.752	
	$R_{\rm l}^{2}$	0.834	0.741	0.958	0.942	
	$R_{\rm II}^{2}$	0.995	0.756	0.785	0.989	
b)						
Pseudo-first-order model	$q_{\rm e}$ Cal. (mg/g)	55.12	210.82	328.69	227.47	
Pseudo-first-order model	$q_{\rm e}$ Exp. (mg/g)	90.02	312.76	1259.78	1196.68	
	$K_1 (\text{min}^{-1})$	0.0096	0.013	0.055	0.02	
	R^2	0.69	0.901	0.901	0.67	
Pseudo-second-order model	$q_{\rm e}$ Cal. (mg/g)	111.11	290.59	1250	1250	
	$q_{\rm e}$ Exp. (mg/g)	90.02	312.76	1259.78	1196.68	
	$K_2 (\text{min}^{-1})$	0.331	0.034	0.002	0.002	
	R^2	0.973	0.999	0.999	0.999	
Intraparticle diffusion model	K_{I}	13.91	50.21	220.39	155.98	
	K _{II}	0.79	3.09	0.095	0.174	
	R_{l}^{2}	0.676	0.933	0.958	0.883	
	$R_{\rm H}^{2}$	0.956	0.758	0.168	0.997	

Isotherms	Parameters	Adsorbents					
		Magnetosome	Activated carbon	Calcite	Magnetic calcite		
a)							
Langmuir	q_0 (mg/g)	4.762	5.88	20	20		
	K_{L} (L/mg)	0.274	0.274	0.132	0.136		
	R^2	0.961	0.951	0.964	0.947		
Freundlich	$K_{\rm F}$ (mg/g (L/mg)1/n)	4.617	5.338	6.099	6.21		
	n	1.565	1.539	1.28	1.29		
	R^2	0.867	0.862	0.929	0.923		
b)							
Langmuir	q_0 (mg/g)	2.083	3.704	100	100		
	K_{L} (L/mg)	0.072	0.189	0.0143	0.016		
	R^2	0.982	0.976	0.878	0.938		
Freundlich	$K_{\rm F}$ (mg/g (L/mg)1/n)	1.869	2.550	2.054	1.614		
	n	1.323	1.485	1.049	1.015		
	R^2	0.926	0.885	0.994	0.989		

The calculated Gibbs free energy changes, standard enthalpy and entropy changes were determined from the ln K_b vs. 1/T plot and values are shown in Table 3. The positive ΔH° endothermic nature of biosorption and the positive value of ΔS° confirm the increased randomness at the solid–solution interface during biosorption.

Adsorption of Cr (III) and Ni (II) from tannery effluent

Sample analysis. The chromium and nickel content were estimated by atomic absorption (http://www.epa.gov). The concentration of Cr (III) was found to be 12.8 μg/mL, and concentration of nickel in water sample was found to be 1.69 μg/mL. The maximum permissible concentration in water as defined by USEPA (2003) was 0.05 and 0.02 μg/mL for Cr (III) and Ni (II), respectively.

Adsorption. Adsorption of Cr (III) and Ni (II) from tannery effluent was carried out in previously standardised optimum conditions. The synthesised magnetic crystal removed 94% of Cr (III) and 84% of Ni (II) from the effluent (Table 4). The % removal is identical to calcite crystals and higher than bacterial magnetosomes and

Table 3. Adsorption thermodynamic parameters: (a) Cr (III) and (b) Ni (II)

(11)			
Adsorbent	ΔG°	ΔS°	ΔH°
a)			
Magnetosome	Negative	0.096	36.51
Activated carbon	Negative	0.049	19.11
Calcite	Negative	0.0659	30.97
Magnetic calcite	Negative	0.1075	42.92
b)			
Magnetosome	Negative	0.0108	6.7194
Activated carbon	Negative	0.0105	6.39
Calcite	Negative	0.103	35.26
Magnetic calcite	Negative	0.0195	9.96

activated carbon. EDS and FTIR analyses of tannery effluent treated adsorbent confirmed the absorbance of Cr (III) and Ni (II). EDS analysis of treated magnetic calcite showed 2.79% of Cr (III) and 1.6% Ni (II) in weight percentage. Calcite microcrystals showed 2.84 and 1.47% of Cr (III) and Ni (II), respectively (Fig. 9). FTIR analysis of treated calcite and magnetic calcite showed the presence of Cr (III) and Ni (II) in absorption peaks from 400 to 500 cm⁻¹ (Fig. 10). The removal efficiency of Cr (III) and Ni (II) by magnetic calcite was compared with other adsorbents (Table 5).

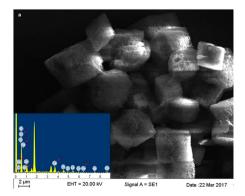
The usage of magnetic calcite crystal as an alternate method for the removal of heavy metals (Cr (III) and Ni (II)) from tannery effluent water is promising. The produced magnetic calcite crystal was characterised and batch adsorption experiments for the removal of Cr (III) and Ni (II) have been carried out. The magnetic property of magnetosomes can be used for the separation of heavy metal ions after treatment. The adsorption experiment results followed second-order kinetic model and the values fit in with the Langmuir and Freundlich isotherms. Future work should consider the dynamic flow column experiments to assess the feasibility and to design a removal system for field operation. Parameters such as the effectiveness, capacity, and longevity of reactive materials should be assessed. Certain factors such as precipitate formation and loss of porosity cannot be accurately determined by batch experiments. The current results suggest that exploration of new, efficient, inexpensive materials as heavy metal removal system improve the existing system.

METHODS

Cultivation of MTB

Magnetospirillum sp. VITRJS2 strain was isolated from sediment in Thenpennai Lake, Cuddalore, located in India. The strain RJS2 was phylogenetically affiliated with the Alphaproteobacteria and biomineralize cubo-octahedral magnetosomes.³² For cultivation, the strain was subcultured in Magnetospirillum growth medium (MSGM) as described by Blakemore et al.³³ Hungate anaerobic technique was followed for the culturing of the bacteria.³⁴ About 50 mL of the media was transferred to 100 mL serum bottles and sparged with sterile nitrogen gas to create redox condition. The culture bottles were closed with butyl rubber stoppers and sealed with aluminium caps and sterilised by autoclaving. Before

Table 4. Percentage adsorption of Cr (III) and Ni (II) from tannery effluent						
Metal ions	Initial concentration, C_i (mg/L)	Final concentration, C_o (mg/L)	Volume (L)	Adsorbent dose (g)	Adsorption capacity (mg/g)	% removal
Cr (III)	12.8	0.7	0.1	0.05	24.2	94
Ni (II)	1.69	0.27	0.1	0.05	2.84	84



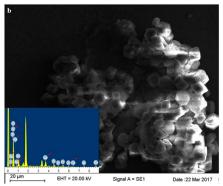


Fig. 9 SEM/EDS analysis of tannery effluent treated (a) calcite microcrystals showed 2.84% and 1.47% of Cr (III) and Ni (II) in weight percentage, respectively. (b) Magnetic calcite shows 2.79% of Cr (III) and 1.6% Ni (II) in weight percentage

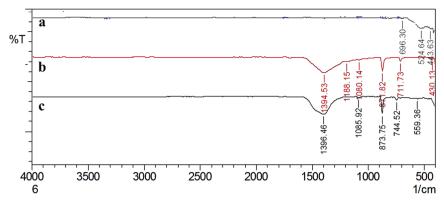


Fig. 10 FTIR analysis of tannery effluent treated (**a**) magnetosomes shows characteristic Fe–O peaks at 443 and 524 cm⁻¹, (**b**) calcite shows peaks of calcium at the absorption, 711 and 871 cm⁻¹ and bands of carbonate were found at 1080 cm⁻¹ and (**c**) magnetic calcite possesses both magnetite (443/524 cm⁻¹) and calcite (711/871 cm⁻¹) peaks. The new peak that appear after the treatment at 1396 cm⁻¹ corresponds to the adsorbed Cr (III) and Ni (II). The appearance of new peak may be due to the interaction between the functional groups and metal ions

 Table 5.
 Comparison of adsorption capacities of Cr (III) and Ni (II) with other adsorbants

Materials	Adsorption capacity (mg/g)		References	
	Cr (III)	Ni (II)		
Rice husk	0.79	_	39,40	
sRaw rice bran	0.8	0.78	41	
Sawdust	_	0.229	42,43	
Orange peel	_	158	44	
Cococut shell charcoal	3.65	-	45	
Modified rice hull	23.4	-	46	
Red mud	_	160	47	
Soya cake	_	0.7	48	
Activated alumina	1.6	-	49	
Activated charcoal	0.9614	-		
Wheat bran	0.942	-	50	
Activated rice husk carbon	0.8	-	39	
Pine leaves	0.277	-	43	
Modified oak sawdust	1.7	3.29	51	
CETYL-amended zeolite	0.65	-	52	
Cornelian cherry	59.4	-	53	
Apricot stone	58.86	-		
Almond shells	59.64	-		
Sodium carboxy methyl cellulose stabilised iron nanoparticles	255	-	54	
Scrap Iron	19	-	55	
Fe@SiO ₂	467	-	56	
Ion exchange resin	-	138	57	
Wool	41.2	-	58	
Olive cake	33.4	-		
Chemical precipitation (NaOH)	-	9.6	59	
Magnetic calcite	24.2	2.84	This study	

inoculation, sterile vitamin and ferric quinate solution was added using hypodermic syringe through the rubber closure without disturbing the anoxic environment inside the culture bottle. The media was then inoculated with *Magnetospirillum* sp. culture and incubated in the shaker incubator for 3 days at room temperature (28 °C).

Magnetosome extraction and characterisation

Extraction of the magnetosomes from MTB was carried out according to the modified method described by Alphandery et al. The bacterial cells in logarithmic phase were separated from the culture medium by centrifugation (4000×g for 20 min). The pellet was re-suspended in PBS (0.01 M, pH 7.4) and washed repeatedly by centrifugation. Further the cell pellet was re-suspended in Tris–HCl buffer (0.1 M, pH 7.0) and the cell membranes were disrupted by ultrasonication (Sonics Vibracell, USA) at 30 W for 2 h. The magnetosomes extract was repeatedly purified by magnetic separation and the extracted magnetosomes were freeze dried (Lark, Penguin Classic Plus, India) and stored for further use.

Preparation of calcite and calcite-coated bacterial magnetosomes The stable form of calcium carbonate microcrystals (CaCO₃) was prepared

by mixing an equal volume of 100 mM $CaCl_2$ solution and Na_2CO_3 solution under vigorous mixing. The precipitated solid was collected and immediately filtered through cellulose nitrate membrane (0.2 μ m) and dried under vacuum.³⁶

The $CaCO_3$ coated magnetosomes were fabricated by mixing equal volume of $0.33 \, M \, CaCl_2$ solution and Na_2CO_3 in the presence of vigorously stirred magnetosome (50 mg/mL). The precipitate was filtered through cellulose nitrate membrane ($0.2 \, \mu m$) and dried at 70 °C for 30 min.³⁷ The magnetic calcite crystals were further purified by magnetic separation, and excess $CaCO_3$ was removed by several washing.

Characterisation of adsorbent

Magnetosomes, calcite and calcium carbonate coated magnetosomes were characterised by scanning electron microscopy (SEM/EDS; ZEISS EV018, Germany) and Fourier transforms infrared (FTIR; Shimadzu, Japan) spectral measurements.

Adsorption experiments

All adsorption parameters were measured in batch system. Different metal ion concentrations were prepared in deionized water. The effect of various factors, such as contact time (10–720 min), pH (2–8), temperature (20–40° C), adsorbent dosage (0–2000 mg/L) and initial metal concentration (0–2000 mg/L) on adsorption capacity were examined. Batch experiments were carried out in 250 mL Erlenmeyer flasks containing 50 mL metal solution and agitated on an orbital shaker at 150 rpm. Unless otherwise conditions specified adsorption experiments were conducted at pH (7), temperature (30°C), adsorbent dosage (500 mg/L) and initial metal concentration (500 mg/L). Samples were withdrawn at predetermined time intervals and centrifuged at 5000 rpm for 10 min. The residual metal concentration of the supernatant was determined by atomic absorption analysis (AAS Varian AA240). All the experiments were carried out in triplicates, and average values were used in the data analysis.

The amount of heavy metal adsorbed was calculated using the following equation:

$$q = \frac{(C_0 - C_e)V}{M}$$

where q is the amount of metal adsorbed per gram of adsorbent, C_0 is the initial concentration of metal ion (mg/L), Ce is the final concentration of metal ion (mg/L), V is the initial volume of the adsorption medium (L), and M is the mass of the adsorbent (a).

The removal efficiency (%) and equilibrium adsorbed concentration, q (mg/g) of metal ions were calculated as follows:

Removal efficiency (%) =
$$\frac{C_0 - C_t}{C_0} X 100$$

Kinetic parameters

To explain the mechanism of adsorption kinetic equation for pseudo-firstorder, pseudo-second order and intra-particle diffusion model have been used to test experimental data.

Equilibrium parameters

Langmuir and Freundlich adsorption isotherm studies were conducted to explain the equilibrium between metal ions adsorbed and metal ions in solution.

Thermodynamic parameters

Gibbs free energy change of adsorption (ΔG^0), enthalpy (ΔH^0) and entropy (ΔS^0) changes of the adsorption process have been calculated.

Adsorption of Cr (III) and Ni (II) from tannery effluent

Study area and sample collection. The effluent sample was collected from highly contaminated tannery effluent discharge site in Palar River basin with the geographical location of 12.78°N latitude 78.7°E longitude. The discharged effluent was found to have polluted the Puliathengal, Vanapadi, Pinji and Thandalam lakes in the Palar River basin.³⁸ The physical appearance, pH and temperature of the samples were recorded onsite after sample collection. The presence of Cr (III) and Ni (II) in the samples were estimated by atomic absorption spectrophotometer (Varian Spectra AA240). Total chromium and nickel were measured with the respective working standard. The results are presented as means and standard deviation of each mean (n = 3).

Adsorption capacity of Cr (III) and Ni (II)

Adsorption experiments were performed in triplicates in optimal operational parameters such as pH, contact time, temperature and adsorbent dosage. Adsorption experiment for the removal of Cr (III) was conducted at pH (6.0), temperature (40 °C), contact time (60 min) and adsorbent dosage (500 mg/L). The recovery of Ni (II) from the tannery effluent was conducted in similar parameters except for the pH (8.0). After the adsorption experiment, the solution was filtered, and residual concentration of metal ions was measured using AAS (Varian Spectra AA240). Removal efficiency (%) and adsorption capacity were calculated. The adsorption capacity of calcite and magnetic calcite was analysed using EDS and FTIR analyses.

Data availability statement

Sequences of the 16S rRNA gene determined in this study were assigned the GenBank accession numbers. The newly determined sequences of Magnetospirillum strains VITRJS2, has been deposited under the accession numbers KJ570852.

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AUTHOR CONTRIBUTIONS

K.S. gave the concept about the work. J.J.J. designed the work and analysed the data. R.V. and S.G. helped in data collection. J.J.J. interpreted the data and drafted the

article. M.A.J. and K.S. have done the critical revision of the article. K.S. has done the final correction of the manuscript and approved the version to be published.

ADDITIONAL INFORMATION

Competing interests: The authors declare no competing interests.

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