



# Effects of high-temperature heating and cryogenic quenching on the physico-mechanical properties of limestone

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## Abstract

This paper is designed to investigate the influence of high-temperature heating and cryogenic quenching using liquid nitrogen (LIN) cooling on the physico-mechanical properties of limestone such as compressive strength, tensile strength, ultrasonic pulse velocity (UPV) and morphological characterization. The main aim is to provide a better understanding on influence of the temperature shock including high temperature pre-treatments and combined process with heating followed by LIN quenching on the physico-mechanical properties of rock. The samples were subjected to different thermal treatment using high-temperature of 100 °C, 200 °C, 400 °C and 600 °C for 4 h. In addition, the combined process of heating at 600 °C for 4 h and LIN quenching for 15 min, 30 min, 45 min and 60 min has also been explored. The obtained results indicate that pre-treatments in limestone depict decreasing trend in strength values. Limestone samples show 62% drop in uniaxial compressive strength (UCS) and 84% drop in Brazilian tensile strength (BTS) for 600 °C pre-treatment for 4 h, whereas the decrease in 70% of UCS and 89% of BTS are also observed for the combined process with 60 min of LIN quenching. The influence of pre-treatment on UPV and microstructure of rock has been investigated in detail. Due to thermal stress, very low UPV has been obtained for the pre-treated samples compared to untreated. SEM analysis has been carried out to understand the fracture morphology for both untreated and treated rock samples.

**Keywords** High temperature · Liquid nitrogen · Physico-mechanical properties · Limestone

## 1 Introduction

Globally, researchers attempted many thermal pre-treatments of rocks to estimate the effect of those treatments on the technical properties of rocks. The influence of high temperature on the properties of rocks is very much important for practical engineering applications. Due to high temperature treatment, the mechanical properties such as strength, Young modulus and Poisson's ratio are severely affected. The study on deviation in rock properties due to thermal cracking is relevant to various engineering applications. To overcome those limitations, the influence of high temperature on the different rocks is a key topic for research. The changes in rock properties

due to high temperature treatments have been noticed by various researchers [1–4]. It has been concluded that the effect of treatment depends on different properties of rock such as mineral composition, porosity, density etc. Darot and Reuschle had chosen granite as raw material and tested at a temperature of 510 °C under the different ranges of confining pressure [5]. They have concluded that the permeability of rock enhanced with the increased effective pressure. Chaki et al. noticed the influence of thermal treatment of rock for the temperatures up to 600 °C and got the good consistency between the results [6]. Liang et al. studied the effect of high temperature on the physico-mechanical parameters of rock, whereas the ultrasonic velocity of samples decreased and also the

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compressive strength decreased with increasing temperature [7]. David et al. investigated the thermal crack generation of granite due to increment in temperature [8]. Wang et al. choose red sandstone to understand the effect of thermal treatment on the mechanical properties [9]. Rock sample was heated to 200 °C and then immersed into water for the thermal shock and for this shock the mechanical properties of the sandstone decreased. Jason et al. investigated thermal cracking of rock and noticed the intergranular cracks occurred due to the temperature shock [10]. Hamand-Etienne et al. showed the transformation of mechanical behavior of rock due to high temperature up to 600 °C [11]. The tensile strength and elastic modulus decreased with increasing temperature. There are two important parameters *i.e.*, porosity and seismic velocity for evaluation of the influence of pores and cracks inside the rocks due the thermal treatment [12]. Brotons et al. exhibited the influence of thermal shock on Calcarenite rock sample [13]. They have investigated that UCS of Calcarenite reduces up to 35% followed by air-cooled and 50% followed by water-cooled condition at the temperature difference of 105–600 °C. Young's modulus has been reduced over 75% and 78% respectively. It was established that UCS of Calcarenite is the most sensitive parameter to cooling condition. Chakrabarti et al. reported that at the temperature above 250–300 °C, there are some changes in color for sandstone [14]. Sandstone, changes its color from brown to reddish brown but the change may not be clearly seen until the stone has been heated to the temperature above 400 °C. Wu et al. researched different types of sandstones and concluded that after 400 °C, strength was decreased and a sharp drop between 400 and 600 °C temperature, when strength is just fewer than 60% of the initial value [15]. Koca et al. tested nine intact marble samples under various temperatures to determine the strength of rock [16]. They had collected rock samples from building elements and they have also tested five samples from it. It was reported that material's UCS exposed to 500 °C and then drop in temperature shows very similar UCS values with the material which was tested at 500 °C. Variations in wave velocity and porosity of sandstone after high-temperature treatment have been investigated by Hu et al. When the temperature is higher than 400 °C, porosity quickly increases, and wave velocity sharply decreases [17]. Zhang et al. studied the thermal effect on physical and mechanical properties of rock at 25–500 °C. The physico-mechanical properties of rocks such as compressive strength, tensile strength and wave velocity changed apparently due to the high temperature treatment. The tensile strength, compressive strength and wave velocity decreased due to the increasing number of micro fracture inside the rock [18]. Peng et al. concluded that the thermal damage has a great effect on physical and

mechanical properties of the rock sample. With increasing temperature, the non-linearity in the initial deformation stage is gradually enhanced [19]. González-Gómez et al. tested four limestones and showed the effect of thermal degradation on the compression strength, ultimate compression strain, color and mass loss of rock sample [20]. High temperatures cause degradation of natural stones. Strength of the natural stones is adversely affected by the increase of temperature and started decreasing with 600 °C and above [21]. Ding et al. have studied the effects of temperature (200, 400, 600 and 800 °C) and confining pressure (20, 30 and 40 MPa) on the mechanical properties of sandstone. Decrease in peak effective loading stress was observed with enhanced temperature and varies accordingly with change in initial confining pressure [22].

According to the literature review, most of the researchers have given priority to the individual high temperature treatment or LIN treatment; but the effect of both combined treatments is more effective as the sudden temperature changing occurred during the quenching process. Bisai et al. conducted some experiment on treating granite and sandstone samples with LIN and concluded that granite sample shows more than 40% reduction in ultimate tensile strength and 28% in UCS, whereas sandstone samples depict drop in UCS of 33% [23, 24]. This present paper aims to provide a better understanding on influence of the temperature shock including high temperature pre-treatments and combined process with heating followed by LIN quenching on the physico-mechanical properties of rock. Limestone is considered as the raw material for this study to understand the physico-mechanical (UCS, BTS, UPV and SEM) behavior under different pre-treatment conditions.

## 2 Materials and methods

### 2.1 Specimen and preparation

In this study, limestone has been selected as appropriate rock samples for understanding the influence of pre-treatments and combined process of pre-treatment and sudden quenching. The cores were saw cut into uniaxial compression and Brazilian test specimen. The samples were prepared according to ISRM standards with the correct length to diameter ratio. The cylindrical samples were polished before testing. The samples were air dried to maintain the constant mass. Also, the chemical composition of the limestone which is used in the present studies has been identified. Energy dispersive X-ray (EDX) analysis using ZEISS EDS detector is used to solve the above purpose. Figure 1 and Table 1 show the elemental composition and their corresponding weight percentage in limestone sample. The samples dimensions of UCS and

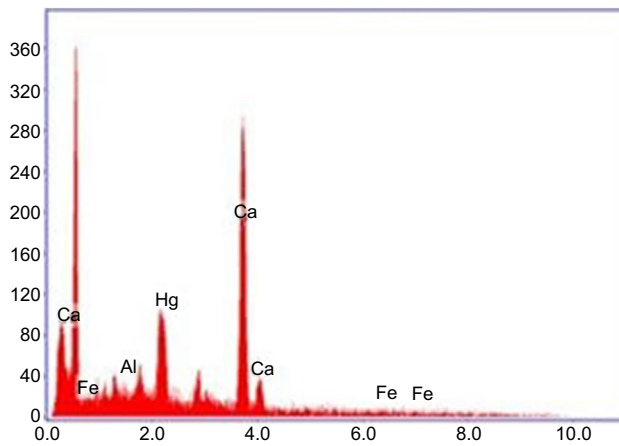


Fig. 1 EDX analysis of limestone

**Table 1** Elemental details of limestone samples

Element	Weight (%)	Atomic (%)
Al K	12.83	18.05
Ca K	85.26	80.75
Fe K	1.70	1.16
Hg L	0.21	0.04

BTS tests are illustrated in Tables 2 and 3 with the suitable pre-treatments and their corresponding results. A total of 36 samples were prepared for the present study.

**Table 2** Sample details for uniaxial compression strength (UCS) tests of limestone

Sample no.	Dimensions (D in mm/L in mm)	Pre-treatment	UCS (MPa)
LC 1	55.1/118.30	None	158.67
LCF 1	55.1/121.60	Heating at 100 °C for 4 h	150.21
LCF 2	55.0/110.91	Heating at 200 °C for 4 h	141.33
LCF 3	55.1/116.16	Heating at 400 °C for 4 h	129.39
LCF 4	55.3/111.63	Heating at 600 °C for 4 h	50.44
LCFL 1	55.0/112.81	Heating at 600 °C for 4 h + LIN quenching for 15 min	81.63
LCFL 2	55.1/112.82	Heating at 600 °C for 4 h + LIN quenching for 30 min	79.16
LCFL 3	55.1/112.50	Heating at 600 °C for 4 h + LIN quenching for 45 min	66.88
LCFL 4	55.1/114.96	Heating at 600 °C for 4 h + LIN quenching for 60 min	47.18
LC 2	55.1/108.37	None	152.40
LCF 5	55.1/111.46	Heating at 100 °C for 4 h	153.16
LCF 6	55.0/112.58	Heating at 200 °C for 4 h	129.96
LCF 7	55.2/114.89	Heating at 400 °C for 4 h	102.22
LCF 8	55.0/110.71	Heating at 600 °C for 4 h	66.31
LCFL 5	55.0/115.32	Heating at 600 °C for 4 h + LIN quenching for 15 min	60.88
LCFL 6	55.2/116.25	Heating at 600 °C for 4 h + LIN quenching for 30 min	58.63
LCFL 7	55.1/111.11	Heating at 600 °C for 4 h + LIN quenching for 45 min	55.28
LCFL 8	55.0/110.93	Heating at 600 °C for 4 h + LIN quenching for 60 min	46.39

Two samples for each pre-treatment method have been tested and the average values were tabulated.

## 2.2 Thermal treatment

The different types of pre-treatments are as follows:

- (i) *Heat treatment using furnace* The samples undergone furnace treatment at the temperature of 100 °C, 200 °C, 400 °C, 600 °C for 4 h. After the treatment, the samples were allowed to cool in normal room temperature before testing. The samples under furnace treatment are shown in Fig. 2. However, before pre-treatment, initial properties of limestone were measured in order to establish a good comparison in normal room temperature (25 °C).
- (ii) *Heat treatment and sudden cryogenic quenching* Initially, the samples were treated in furnace at 600 °C temperature for 4 h and suddenly quenched in LIN for different time durations like 15 min, 30 min, 45 min and 60 min. The samples under cryogenic quenching are shown in Fig. 3.

## 2.3 Instruments and test methods

### 2.3.1 Determination of compressive strength

In this paper, the mechanical test of rocks involves determination of UCS. An INSTRON make, SATEC series KN

**Table 3** Sample details for Brazilian tensile strength (BTS) tests of limestone

Sample no.	Dimensions (D in mm/L in mm)	Pre-treatment	BTS (MPa)
LT 1	55.1/27.00	None	12.43
LTF 1	55.1/27.20	Heating at 100 °C for 4 h	12.66
LTF 2	55.1/27.30	Heating at 200 °C for 4 h	9.15
LTF 3	55.0/28.10	Heating at 400 °C for 4 h	7.50
LTF 4	55.0/27.30	Heating at 600 °C for 4 h	1.20
LTFL 1	55.3/28.33	Heating at 600 °C for 4 h + LIN quenching for 15 min	1.69
LTFL 2	55.0/27.12	Heating at 600 °C for 4 h + LIN quenching for 30 min	1.54
LTFL 3	55.0/27.39	Heating at 600 °C for 4 h + LIN quenching for 45 min	2.01
LTFL 4	55.0/27.00	Heating at 600 °C for 4 h + LIN quenching for 60 min	1.12
LT 2	55.1/27.10	None	11.08
LTF 5	55.1/27.20	Heating at 100 °C for 4 h	11.90
LTF 6	55.2/27.00	Heating at 200 °C for 4 h	10.11
LTF 7	55.1/27.33	Heating at 400 °C for 4 h	6.57
LTF 8	55.1/27.17	Heating at 600 °C for 4 h	2.58
LTFL 5	55.3/27.00	Heating at 600 °C for 4 h + LIN quenching for 15 min	2.01
LTFL 6	55.0/27.00	Heating at 600 °C for 4 h + LIN quenching for 30 min	1.82
LTFL 7	55.1/27.32	Heating at 600 °C for 4 h + LIN quenching for 45 min	1.29
LTFL 8	55.0/27.11	Heating at 600 °C for 4 h + LIN quenching for 60 min	1.23

**Fig. 2** Samples under furnace pre-treatment at 600 °C temperature

model, universal testing machine (UTM) was used in this study, as shown in Fig. 4. As explained earlier, all the experiments were performed at normal room temperature. UCS is the compressive stress at which the sample fails was calculated by using the following formula.

$$UCS = \frac{P_{max}}{\pi D^2/4}$$

where  $P_{max}$  = load at failure, D = diameter of the sample.

### 2.3.2 Determination of Brazilian tensile strength

Brazilian test is proposed for the measurement of indirect tensile strength of a rock specimen. BTS of the sample is calculated by dividing the maximum load carried by the sample during the test, by the contact area of the sample. The BTS is calculated as described below:

$$BTS = \frac{2P'_{max}}{\pi DL}$$

where  $P'_{max}$  = load at failure during the test, D = diameter of the sample, L = axial length of the sample.

### 2.3.3 Ultrasonic pulse velocity (UPV) test

Cylindrical limestone core samples with diameter around 55–55.3 mm, length of 110.2–121.6 mm and velocity measuring equipment (as shown in Fig. 5) were used in this study based on the ISRM (2007) recommendations. The present UPV unit has two transducers including one transmitter and one receiver with a frequency of 150 kHz.



**Fig. 3** Samples under cryogenic treatment using LIN



**Fig. 4** UTM machine

### 3 Results and discussions

#### 3.1 Mechanical properties

The UCS and BTS results of limestone with high temperature treatment and cryogenic quenching were presented in Figs. 6, 7, 8 and 9. Decreasing trend in both the strengths was observed for all the cases. The amount of decrease, however, varies with the samples as well

as with the duration of pre-treatment. Figures 6 and 7 illustrate the UCS and BTS of limestone samples under varying pre-treatment conditions. Significant drop in UCS was observed in case of heat treatment at 600 °C. The treated samples (heating at 600 °C for 4 h) show reduction in UCS by 62% (Fig. 6) and BTS by 84% (Fig. 7) compared to untreated samples. The rise in strength after 100 °C temperature is probably due to the effect of structural reorientation of the molecules without developing any significant thermal crack. The structural reorientation can be found in metals during cryogenic treatment of cutting tools [25] which helps in increasing the strength of the tools. However, in rocks, corroboration with more investigation is needed. Figures 8 and 9 demonstrate the UCS and BTS of limestone samples under varying pre-treatment conditions followed by LIN quenching. Significant drop in UCS was observed in case of heat treatment at 600 °C and sudden LIN quenching for 60 min. The treated samples (combined process of heating at 600 °C for 4 h and LIN quenching for 60 min) depict reduction in UCS by 70% (Fig. 8) and BTS by 89% (Fig. 9) compared to untreated samples.

#### 3.2 Effect of pre-treatment on the physical properties

This paper explains the influence of high temperature treatment i.e., 600 °C for 4 h and sudden LIN quenching on the physical properties of limestone. A significant decrease has been monitored in the UPV test of the pre-treated sample. Before pre-treatment, the properties of limestone were measured in order to provide a good comparison in normal room temperature (25 °C). The sample lengths and the corresponding UPV test results are tabulated in Tables 4 and 5. Two samples were tested in each case and the average results were noted down. Figures 10 and 11

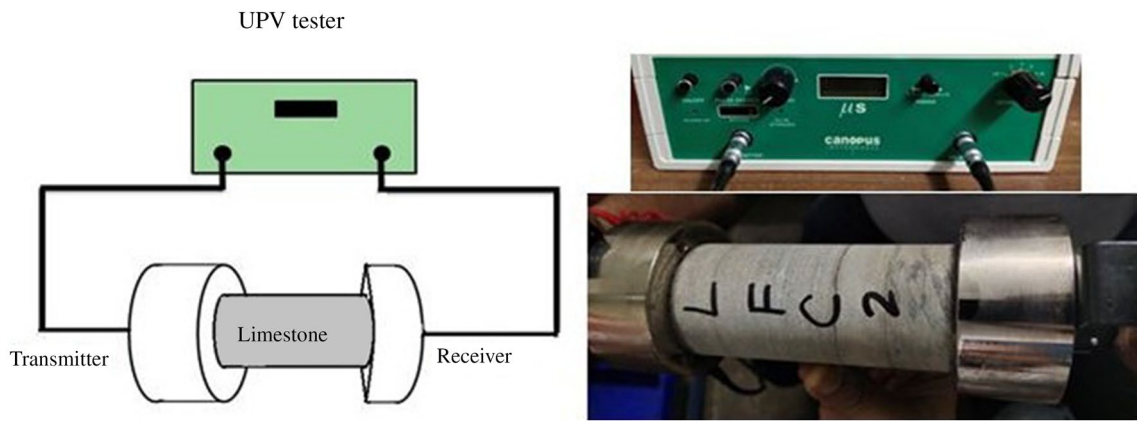


Fig. 5 Ultrasonic pulse velocity (UPV) testing apparatus

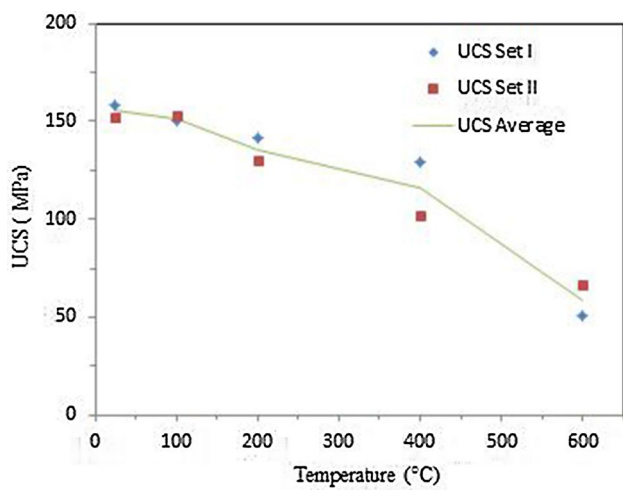


Fig. 6 UCS of limestone with varying duration of individual pre-treatment

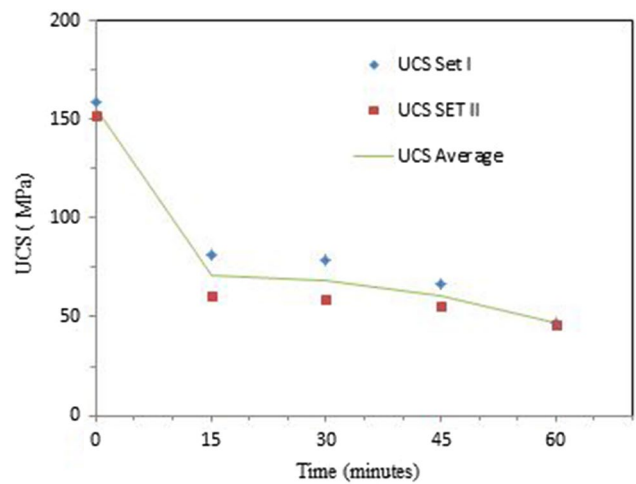


Fig. 8 UCS of limestone with combined process of pre-treatment at 600 °C for 4 h followed by varying duration of LIN quenching

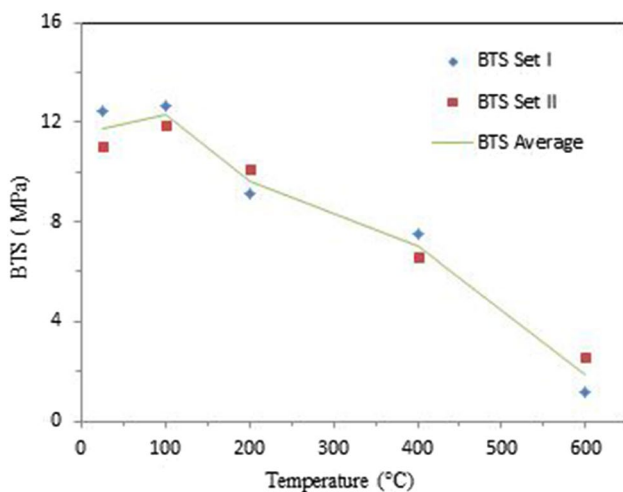


Fig. 7 BTS of limestone with varying duration of individual pre-treatment

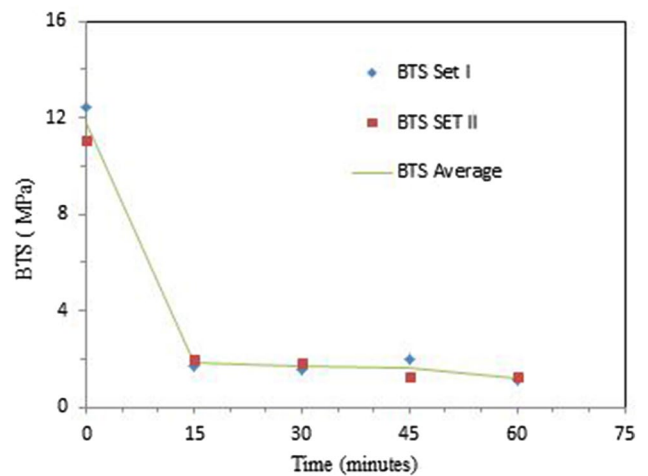


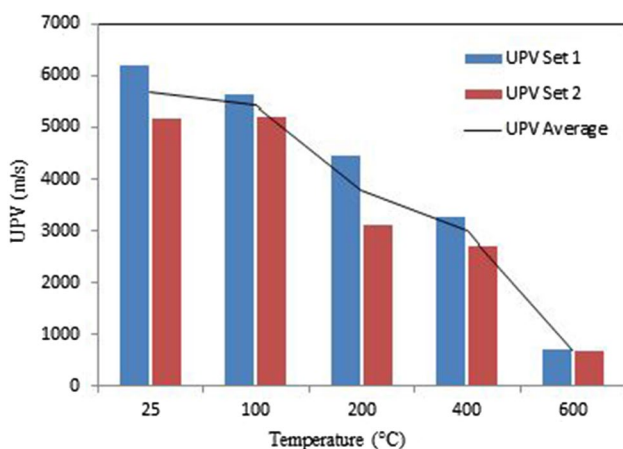
Fig. 9 BTS of limestone with combined process of pre-treatment at 600 °C for 4 h followed by varying duration of LIN quenching

**Table 4** Comparison of ultrasonic pulse velocity (UPV) test results between high temperature pre-treated limestone and untreated limestone samples

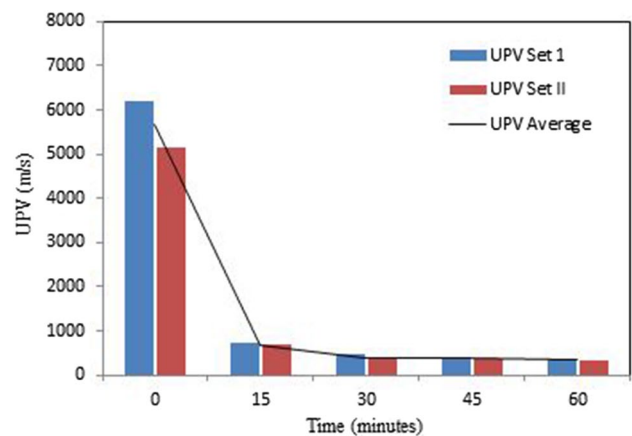
Sample no.	Distance (m)	Time (s)	UPV (m/s)
LC 1	0.1183	0.0000191	6193.717
LCF 1	0.1216	0.0000216	5629.630
LCF 2	0.1109	0.0000249	4453.815
LCF 3	0.1161	0.0000355	3270.423
LCF 4	0.1116	0.0001577	707.673
LC 2	0.1083	0.0000210	5157.143
LCF 5	0.1114	0.0000214	5205.607
LCF 6	0.1125	0.0000361	3116.343
LCF 7	0.1148	0.0000425	2701.176
LCF 8	0.1107	0.0001609	688.005

**Table 5** Comparison of ultrasonic pulse velocity (UPV) test results between combined process of pre-treated limestone at 600 °C for 4 h followed by LIN quenching and untreated limestone samples

Sample no.	Distance (m)	Time (s)	UPV (m/s)
LC 1	0.1183	0.0000191	6193.717
LCFL 1	0.1128	0.0001569	718.929
LCFL 2	0.1128	0.0002299	490.648
LCFL 3	0.1125	0.0002714	414.517
LCFL 4	0.1149	0.0003117	368.623
LC 2	0.1083	0.0000210	5157.143
LCFL 5	0.1153	0.0001712	673.481
LCFL 6	0.1162	0.0002971	391.114
LCFL 7	0.1111	0.0002990	371.571
LCFL 8	0.1109	0.0003290	337.082



**Fig. 10** UPV of limestone with varying duration of individual pre-treatment

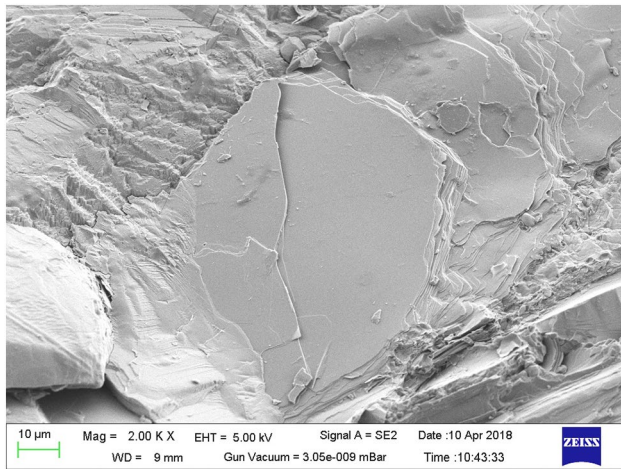


**Fig. 11** UPV of limestone with combined process of pre-treatment at 600 °C for 4 h followed by varying duration of LIN quenching

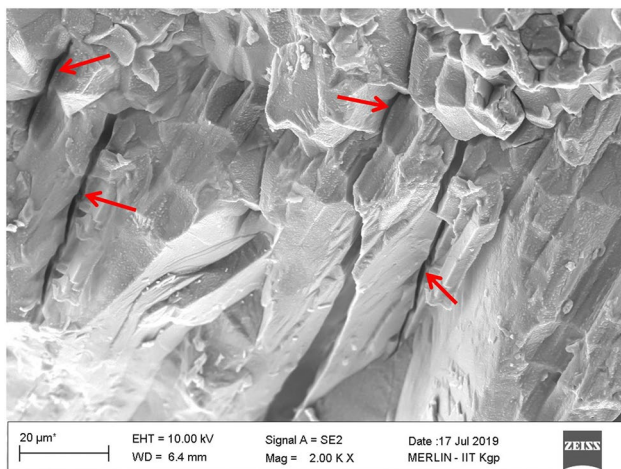
explain the UPV results of two samples at two different working conditions. As shown in tables, untreated sample has UPV values of 6193.7 m/s and 5157.1 m/s, which was classified as very high velocity [26]. However, the samples after pre-treatment at 600 °C for 4 h has UPV values of 707.7 m/s and 688 m/s, which was considered as very low velocity. Similarly, LIN quenching treatment is more effective than the single treatment of high temperature. So, the samples undergone pre-treatment at 600 °C for 4 h followed by sudden LIN quenching of 60 min displays UPV values as 368.62 m/s and 337.18 m/s, which was still considered to be a very low velocity. These results indicated that granular cementation is damaged and cracks have generated on the rocks may be the reason behind this findings. In addition, several micro-fissures can also be generated in its inter-grain due to the thermal stress during high temperature treatment and LIN quenching. The significant decrease in UPV values with gradual increase in temperature and duration of LIN quenching has been studied and depicted in Figs. 10 and 11. As like all the experiments, two samples were tested in each case and the average results were noted down for further interpretation.

### 3.3 Effect of pre-treatment on the morphological characterizations

For understanding the mineral grain structure of rock through microscope, SEM was used in this study. It is one of the significant techniques to understand the micro-structure of rocks. The mineral grain distribution and the micro-fissures in the rocks have been seen with proper magnifications. Accordingly, SEM was utilized to quantify the surface micro-topographies of rock slices before and after pre-treatment. The outcomes are subjectively

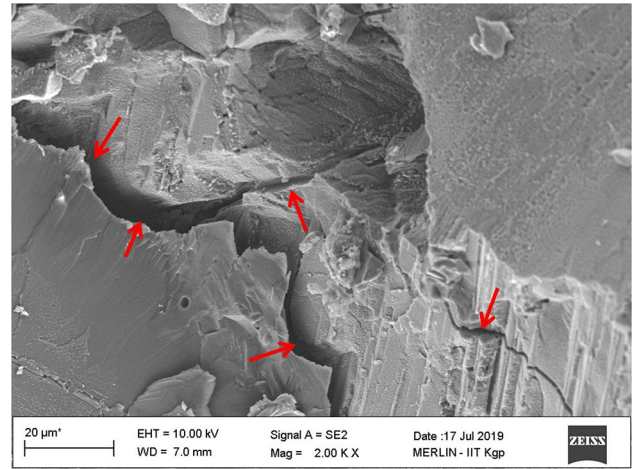


**Fig. 12** SEM image of untreated limestone sample



**Fig. 13** SEM image of limestone sample with individual pre-treatment at 600 °C for 4 h

investigated to derive the effect of heat treatment on the pore structure of rocks. SEM analyses of the pre-treated and untreated samples were done by utilizing ZEISS scanning electron microscope. Figures 12, 13 and 14 depict the SEM images of limestone samples before pre-treatment, after pre-treatment at 600 °C for 4 h and thirdly, pre-treatment at 600 °C for 4 h followed by LIN quenching for 60 min respectively. The analysis has been performed at a magnification of 2 K times to understand mineral grain distribution of limestone. The arrangements of mineral grains in the limestone are very compact and it has good inter-grain cementation. However, the untreated granite sample (Fig. 12) does not show any fracture. Figures 13 and 14 depict that the inter-grain cementation is damaged and the cracks have appeared. Several micro-fissures have been found in its inter-grain, which shows the thermal



**Fig. 14** SEM image of limestone sample with combined process of pre-treatment at 600 °C for 4 h followed by LIN quenching for 60 min

stress created during LIN cooling, whereas high temperature treatment breaks the granular cementation and new cracks are generated.

## 4 Conclusions

The effect of rock pre-treatment including high temperature treatment and combined process of pre-treatment followed by LIN quenching were carried out for studying the physical and mechanical properties of limestone samples. Following salient points were observed from the experimental results.

- For limestone, 62% reduction in UCS was observed in 600 °C high temperature pre-treatment for 4 h and 70% reduction was observed in combined process (heating at 600 °C for 4 h followed by LIN quenching for 60 min). Slight increases in strength properties are observed at 200 °C. This increment in compressive strength possibly ascribed to the beginning of phase changes of the minerals which thus gave a temporary plastic reaction when externally loaded, prompting slight increment in strength at 200 °C.
- In terms of BTS of limestone, 84% reduction in UCS was observed in 600 °C high temperature pre-treatment for 4 h and 89% reduction was observed in combined process (heating at 600 °C for 4 h followed by LIN quenching for 60 min). The combined process is more effective than individual pre-treatment process.
- The UPV results showed the same decreasing trend with the increasing temperature, whereas the velocity decreased to 697.85 m/s in the case of 600 °C pre-



treatment for 4 h and 352.9 m/s in the combined process, which was considered as very low velocity. The UPV results mainly influenced due to the thermal stress induced due to sudden temperature changes and LIN quenching. The obtained UPV results are in line and support the UCS and BTS results of limestone in all the conditions.

After the phase change, as a result of thermal expansion of the different minerals, more micro-cracks have been developed in the rock which mainly affected the physico-mechanical behavior of the same. Advantage of pre-treatment on rocks is highly dependent on the mineral composition of those particular samples. To extend this area of research, the more detailed investigations on pre-treatment methods along with other issues such as cost, complexity and feasibility etc. are considered to be very much essential.

### Compliance with ethical standards

**Conflict of interest** On behalf of all authors, the corresponding author states that there is no conflict of interest.

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