Research Article

Assessment of natural radioactivity and its radiological hazards in several types of cement used in Senegal



Ousmane Ndour¹ · Coumba Thiandoume¹ · Alassane Traore² · Xavier Cagnat³ · Papa Mbaye Diouf¹ · Maurice Ndeye⁴ · Ababacar Sadikhe Ndao² · Adams Tidjani¹

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Abstract

In this study, the activity concentrations of ²²⁶Ra, ²³²Th and ⁴⁰K in twenty cement samples of four types (CEM, CEM II, CEM III, and CEM IV) collected from building material suppliers in Senegal were measured using a low-background digital gamma-ray spectrometer equipped with broad energy germanium detector. The activity concentrations of ²²⁶Ra, ²³²Th and ⁴⁰K varied from 7.1–150.3 Bq kg⁻¹, 3.7–16.1 Bq kg⁻¹, and 48.7–133.9 Bq kg⁻¹, respectively. Also, possible radiological risks from the usage of these materials were assessed by estimating external and internal index, indoor absorbed gamma dose rate and the corresponding annual effective dose, effective dose rate to different body organs and tissus, and excess lifetime cancer risk. The estimated radiological hazard indices were revised in light of the relevant national and international legislation and guidance. The values of the radiological hazard indices were found to be within relevant all limit values for structural building materials.

Keywords Natural radiouclides · Gamma-ray spectrometry · Activity concentrations · radiological hazards indices · Cement

1 Introduction

Humans are continuously exposed to natural radiation which comes from cosmogenic radionuclides and primordial radionuclides [1]. The cosmogenic radionuclides are continuously produced in the upper part of the atmosphere by the interaction of the cosmic radiation with atoms or molecules. The primordial radionuclides are the uranium series with as parent the ²³⁸U, ²³⁵U series or actinium series, thorium (²³²Th) series, and ⁴⁰K which is a non-series of disintegration. When dealing with naturally occurring radioactive material (NORM), only the primordial radionuclides are of radiological interest. Depending on the geological origin of the raw materials (rocks, soil, and industrial products), the building materials may contain different amounts of natural radionuclides [2, 3]. As cement is most used in building material, it can become a health and environmental problem for the population. According to Mansoor et al., individuals spend 80% of their time at home or office indoor [4]. It is then important to estimate the natural radioactivity in cement.

There are different exposition ways of humans by radionuclides content in cement: internal and external exposure. Internal exposure is due to the inhalation of radon (222 Rn) which emanates from the building material [5]. During the inhalation, radon may decay in the track respiratory conducting to the deposition of its progenies and becomes a permanent source of internal exposure [6]. External exposure is due to the emission of γ -rays by

[○] Ousmane Ndour, ousmanendour9031@gmail.com | ¹Natural and Artificial Radiation Laboratory, Department of Physics, Cheikh Anta Diop University, Dakar, Senegal. ²Institute of Applied Nuclear Technology, Cheikh Anta Diop University, Dakar, Senegal. ³Nuclear Safety and Radiation Protection Institute, Orsay, France. ⁴Carbon-14 Laboratory, Cheikh Anta Diop University, Dakar, Senegal.



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primordial radionuclides (226 Ra, 232 Th, and their daughters and 40 K).

In Senegal, there are three factories of cement, but so far, no data concerning natural radioactivity of cement used are available. To fill this gap, the main objectives of this study are to assess the ²²⁶Ra, ²³²Th, and ⁴⁰K activity concentrations and the radiological hazards in the types of cement used as a building material.

2 Materials and methods

2.1 Sample collection and preparation

Twenty cement samples were collected from building material suppliers and labeled properly. The net weight of the collected samples was 1 kg. The gray samples were manufactured by three different domestic cement factories (CEM I, CEM II, and CEM III). To remove moisture, the collected samples were dried at 105 °C for 24 h and then transferred to 60 mL of cylindrical containers with an internal diameter of 72 mm.

2.2 Gamma-ray spectrometry

The ²²⁶Ra, ²³²Th, and ⁴⁰K activity concentrations were measured using a calibrated broad energy germanium (BEGe) detectors with a relative efficiency of 50% at 1332 keV and an energy resolution of 0.7 keV for 60 keV and 1.8 keV for 1332 keV gamma-rays for ²⁴¹Am and ⁶⁰Co, respectively. The detectors were calibrated to energy and efficiency using a mixed radionuclides standard containing ²⁴¹Am, ²¹⁰Pb, ¹³⁹Ce, ¹³⁷Cs, ¹¹³Sn, ¹⁰⁹Cd, ⁸⁸Y, ⁸⁵Sr, ⁶⁰Co, ⁵⁷Co, and ⁵¹Cr. The sample analysis was conducted by Genie 2000 software program. The samples were measured at least 80,000 s. As in a planar BEGe detector, the sample is placed on the top of the detector, the coincidences summing were corrected using correction factors calculated by the Monte Carlo simulation, using the GESPECOR software package. For self-attenuation correction, a transmission bench was used for the low energies (below 100 keV). The principle of transmission bench consists to detect gamma-rays emitted by a collimated source of ¹³³Ba and ¹⁰⁹Cd passing through a container, then a sample within its container. A schematic diagram of the transmission bench is shown in Fig. 1.

The attenuation coefficient (μ_l) was calculated following the Beer–Lambert equation:

$$N = N_0 e^{-\mu\rho x} \tag{1}$$

where N, N_0 , ρ , and x represent, respectively, the number of photons having passed through the sample within the

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Fig.1 Diagram of transmission bench

geometry, the number of photons detected after crossing the empty geometry, the sample density, and the thickness.

The self-attenuation correction factor (F_{att}) was calculated using the following equation:

$$F_{\rm att} = \frac{1 - e^{-\mu\rho x}}{\mu\rho x} \tag{2}$$

where x, μ , and ρ represent the thickness of the sample, the coefficient of attenuation, and the density, respectively.

As the matrix and the density of the measured samples were different from that of the calibration source, the self-attenuation of the measured samples and the calibration source is therefore different. The relative self-attenuation correction factor $FC_{self}(E)$ is determined by the ratio of the self-attenuation correction factor of the sample to that of the calibration source.

$$FC_{self}(E) = \frac{F_{att.sam}}{F_{att.ref}}$$
(3)

where $F_{\text{att.sam}}$ and $F_{\text{att.ref}}$ are the self-attenuation correction factors of the sample the calibration source, respectively.

The self-attenuation correction factors calculated for ten energies from the transmission source according to their energies were plotted. The interpolated curve obtained was used to calculate the self-attenuation correction factor at other energies. The ²²⁶Ra activity concentration has been estimated using the 186.2 keV gamma-ray. Since the ²³⁵U energy peak at 163 keV has not been identified, the gamma-ray interference between ²²⁶Ra at 186.2 keV with a peak of ²³⁵U at 185.7 keV was resolved taking into account the ratio of ²³⁸U/²³⁵U = 21.7 and the full energy peak of ²³⁴Th at 63.3 keV [7]. The activity concentration of ²³²Th was estimated using the full energy peaks of ²²⁸Ac at 911.2 keV and ²⁰⁸TI at 583.2 keV taking into account the braching ratio. For ⁴⁰ K activity concentration calculation, its peak at 1460.8 keV was used. The following equation was used to calculate the activity concentration of each radionuclide:

$$A(Bqkg^{-1}) = \frac{N_{net}}{P(E_i) \times \varepsilon(E_i) \times t \times m \times F_c}$$
(4)

where N_{net} represents the net counts under the full absorption peak, $P(E_i)$ the emission intensity, $\varepsilon(E_i)$ the detector efficiency at energy E_i , t the counting time, m the sample mass, and F_c the corrective factors taking into account the radioactive decay, the self-attenuation, and the coincidence summing.

2.3 Dose parameters and radiological hazards indices

2.3.1 Absorbed gamma dose rate

At a height of 1 m above the ground, the indoor absorbed gamma dose rate (*D*) due to γ -ray emitted by ²²⁶Ra, ²³²Th, and ⁴⁰ K is evaluated by the following equation [8, 9]:

$$D(nGyh^{-1}) = 0.92A_{Ra-226} + 1.1A_{Th-232} + 0.08A_{K-40}$$
(5)

The conversion coefficients of ²²⁶Ra, ²³²Th, and ⁴⁰K activity concentrations into dose for materials used as building materials are 0.92, 1.1, and 0.08 in nGy h⁻¹/ Bq kg⁻¹, respectively. These conversion coefficients were calculated by the Monte Carlo method using a standard room model of 2.8 m×4 m×5 m in which the wall width is 20 cm and the density 2.35 g.cm⁻³ [10].

2.3.2 Annual effective dose equivalent

The annual effective dose equivalent (AEDE) was calculated by the following equation [10]:

2.3.3 Annual gonadal dose equivalent

Since the gonads are organs of interest, the annual gonadal dose equivalent (AGDE) was calculated using the following equation [11-14]:

$$AGDE(\mu Sv.y^{-1}) = 3.09A_{Ra-226} + 4.18A_{Th-232} + 0.314A_{K-40}$$
(7)

2.3.4 Gamma index and alpha index

The gamma index (I_{γ}) was calculated to find out if the cements had met the safety requirements for building materials by the following equation [2, 8]:

$$I_{\gamma} = \frac{A_{\text{Ra}-226}}{300} + \frac{A_{\text{Th}-232}}{200} + \frac{A_{\text{K}-40}}{3000}$$
(8)

For material used in a bulky amount, the exemption criterion and the upper dose limit are defined. The exemption criterion (0.3 mSv y⁻¹) corresponds to $I_{\gamma} \le 0.5$ and the upper dose limit to $I_{\nu} \le 1$, respectively [8].

The alpha index (I_a) corresponding to the excess alpha radiation due to the ²²²Rn inhalation from cement was calculated using the following equation [15]:

$$I_{\alpha} = \frac{A_{\text{Ra}-226}}{200} \tag{9}$$

The l_a should not exceed the unity since the radon exhalation from cement could cause an indoor radon concentration greater than 200 Bq m⁻³ [8, 16].

2.3.5 Excess lifetime of cancer risk

The excess lifetime cancer risk (ELCR) was evaluated by the following formula [17, 18]:

$$ELCR = AEDE \times RF \times DL$$
(10)

where RF is the fatal cancer risk per Sievert (0.05 Sv^{-1}) and DL the life duration (70 y).

2.3.6 Effective dose rate to different organs and tissues

The effective dose rate to different organs and tissues (D_{org}) was calculated using the following equation [19, 20]:

$$AEDE(\mu Svy^{-1}) = D(nGyh^{-1}) \times 0.7(SvGy^{-1}) \times 0.8 \times 8760hy^{-1} \times 10^{-3}$$
(6)

The conversion coefficient of absorbed dose to an effective dose and the indoor occupancy factor used for the calculation of AEDE were 0.7 Sv Gy^{-1} and 0.8, respectively [10].

$$D_{\rm org}(\mu {\rm Svy}^{-1}) = {\rm AEDE} \times {\rm CF}$$
(11)

Table 1Conversion coefficientCF for different organs ortissues [19]

Organ or tissue	Averages values of CF
Bone marrow	0.69
Whole-body	0.68
Lungs	0.64
Ovaries	0.58
Testes	0.82

where CF is the conversion coefficient for the organ dose from air dose (Table 1).

3 Results and discussions

3.1 ²²⁶Ra, ²³²Th, and ⁴⁰K activity concentrations

Table 2 reports the range and average of ²²⁶Ra, ²³²Th, and ⁴⁰K activity concentrations in the types of cement. The ²²⁶Ra activity concentration in cement samples varied from 7.09 Bq kg⁻¹ to 150.25 Bq kg⁻¹. The ²³²Th and ⁴⁰K activity concentration in cement samples varied from 3.72 Bq kg⁻¹ to 16.09 Bq kg⁻¹ and from 48.67 Bq kg⁻¹ to 133.89 Bq kg⁻¹, respectively.

As shown in Table 2, the highest average value of the ²²⁶Ra and ²³²Th activity concentrations was found in CEM I. The CEM IV (white cement) presented the lowest average value of activity concentration of these two radionuclides. Unlike the ²²⁶Ra and ²³²Th, the highest average activity concentration of ⁴⁰K was found in CEM IV and the lowest average value in CEM I. To make a comparison between the ²²⁶Ra, ²³²Th, and ⁴⁰K average activity concentrations and the worldwide average values in building materials, their respective ratios were calculated. The worldwide average values used for comparison were 50 Bg kg⁻¹, 50 Bg kg⁻¹, and 500 Bg kg⁻¹, respectively for ²²⁶Ra, ²³²Th, and ⁴⁰K [21, 22]. In gray cements, the ratio ranges from 1.84 to 2.72 for ²²⁶Ra. Therefore, the ²²⁶Ra activity concentration in gray cements was then found two times higher than the worldwide average value. In white cement, the ratio was 0.16. Then, the ²²⁶Ra average activity concentration in white cement was lower than the worldwide average value cited above. The ratio ranges from 0.24 to 0.30 for ²³²Th and from 0.12 to 0.16 for ⁴⁰K in the gray cement. In white cement, the ratios were 0.10 for ²³²Th and 0.24 for ⁴⁰K. The ²³²Th and ⁴⁰K average activity concentrations were then below their worldwide average values in all types of cement.

The ²²⁶Ra, ²³²Th, and ⁴⁰K average activity concentrations in the gray and white cements were also compared with results from other countries (Table 3). The ²²⁶Ra average activity concentration in gray cement was lower than that of Albania [23] and China [24]. It was higher compared to other countries. For ²³²Th, its average activity concentration was below the cited results in other countries. Regarding the average activity concentration of ⁴⁰K, this study was only lower than that of Albania [23]. The ²²⁶Ra and ²³²Th average activity concentrations found in white cement in this study had the lowest values. The result of the ⁴⁰K activity concentration in Malaysia was only greater than this study [25].

3.2 Dose parameters and radiological hazard indices

The dose parameters and radiological hazards indices were evaluated and presented in Table 4.

The average values of the indoor absorbed gamma dose ranged from 22.09 ± 2.10 nGy h⁻¹ (CEM IV) to 146.41 ± 6.98 nGy h⁻¹ (CEM I). The indoor absorbed gamma dose rate in air of the types of cement exceeds the population-weighted average of 84 nGy h⁻¹, except for CEM IV [10]. From Table 5, it can be seen that the average value of AEDE varied from 108.42 ± 10.32 µSv y⁻¹ (CEM IV) to 718.72 ± 34.26 µSv y⁻¹ (CEM I). The average value of AEDE of all types of cement is lower than the permissible limit which is 1000 µSv y⁻¹. Among the natural radionuclides, the principal contributor to the indoor AEDE was the ²²⁶Ra with a contribution of 84% in gray cement. The ²²⁶Ra was followed by ²³²Th (11%) and ⁴⁰K (5%). In white cement, the principal contributor was ⁴⁰K (43%), followed by ²²⁶Ra (34%) and ²³²Th (23%).

The average value of AGDE of the types of cement ranged from $81.84 \pm 7.88 \ \mu\text{Sv} \ y^{-1}$ (CEM IV) to

Table 2Range and averagewith their standard deviation(SD) of 226Ra, 232Th, and 40Kactivity concentrations in thetypes of cement

Activity concentrations in Bq kg ⁻¹		Type of cement*					
		CEM I CEM II		CEM III	CEM IV		
²²⁶ Ra	Range	129.99–150.25	75.36–149.96	66.73–105.17	7.09–9.24		
	Average \pm SD	135.95 ± 8.19	109.95 ± 28.42	92.17±16.86	8.07±0.81		
²³² Th	Range	14.02-16.09	10.15-13.27	10.62-15.04	3.72-5.85		
	Average \pm SD	15.09 ± 0.83	12.04±1.16	12.24 ± 1.74	4.68 ± 0.78		
⁴⁰ K	Range	48.67–66.22	50.29 ± 98.80	52.00-95.72	104.70–133.89		
	$Average \pm SD$	59.25 ± 7.26	80.72 ± 18.26	80.07 ± 19.78	118.91 ± 11.88		

*CEM I, CEM II, and CEM III: Portland cement composite; CEM IV: white cement

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Table 3 Comparison of 226 Ra,	Туре	Country	Activity concent	rations in Bq kg ⁻	1	References
concentrations of gray and			²²⁶ Ra	²³² Th	⁴⁰ K	
obtained in other countries	Gray cement	Albania	179.7±48.9	55.0±5.8	17.0±3.3	[23]
		Algeria	41±7	27±3	422±3	[26]
		Cameroon	27±4	15±1	277±117	[27]
		China	118.7±14.2	36.1±17.8	444.5±163.1	[24]
		Egypt	36±4	43±2	82±4	[28]
		Ghana	35.94 ± 0.78	25.44 ± 0.80	233 ± 3.95	[<mark>6</mark>]
		Iraq	24.25 ± 1.45	25.41 ± 1.65	93.17±7.30	[4]
		Laos	41.12±2.44	16.60 ± 2.37	141.48±4.50	[29]
		Morocco	31±5	19±3	238 ± 29	[30]
		Pakistan	25±10	37±9	245 ± 95	[31]
		Turkey	34±4	15±2	220±13	[<mark>9</mark>]
		Senegal	112.69±26.02	13.12 ± 1.88	73.35±18.12	In this study
	White cement	Cote d'Ivoire	18.85±1.68	22.94 ± 1.96	111.10±7.03	[32]
		Egypt	15±3	17±2	10±5	[33]
		Qatar	18.9±0.5	4.9 ± 0.5	62.9±22.6	[34]
		Malaysia	25.3±1.2	23.4±1.2	362.2±6.7	[25]
		Saudi Arabia	28.53 ± 3.75	43.46±2.18	67.38±3.36	[35]
		Senegal	8.07±0.81	4.68 ± 0.78	118.91±11.88	In this study

Table 4 Average with their standard deviation of dose parameters and radiological hazards indices according to the types of cement

		Cement type			
		CEM I	CEM II	CEM III	CEM IV
Dose parameters	D (nGy h ⁻¹)	146.41±6.98	120.85±27.18	104.67±16.42	22.09±2.10
	AEDE (μ Sv y ⁻¹)	718.72±34.26	593.27±133.43	513.80±80.63	108.42 ± 10.32
	AGDE (μ Sv y ⁻¹)	501.75 ± 23.15	415.41 ± 41.04	361.11±24.93	81.84±7.88
Radiological hazards indices	I_{ν}	0.55 ± 0.03	0.45 ± 0.10	0.40 ± 0.06	0.09 ± 0.01
	, I _a	0.68 ± 0.04	0.55 ± 0.14	0.46 ± 0.08	0.040 ± 0.004
	ELCR (10 ⁻³)	2.52 ± 0.12	2.08 ± 0.47	1.80 ± 0.28	0.38±0.04

 Table 5
 Effective dose rate to different organs and tissues according to types of cement

Type of cement	Effective dose rate (mSv y^{-1})				
	Lungs	Ovaries	Bone mar- row	Testes	Whole-body
CEM I	0.46	0.42	0.50	0.59	0.49
CEM II	0.38	0.34	0.41	0.49	0.40
CEM III	0.33	0.30	0.36	0.42	0.35
CEM IV	0.07	0.06	0.08	0.09	0.07

 $501.75 \pm 23.15 \ \mu\text{Sv y}^{-1}$ (CEM I). The average value of AGDE of CEM I, CEM II, and CEM III was higher than the worldwide average value of $300 \ \mu\text{Sv y}^{-1}$ calculated by considering a house containing worldwide average activity concentrations of 226 Ra, 232 Th, and 40 K in soil [10, 36].

Table 4 shows that the average value of the gamma Index (I_{γ}) and the alpha index (I_{a}) varied from 0.09 ± 0.01 (CEM IV) to 0.55 ± 0.03 (CEM I) and from 0.040 ± 0.004 (CEM IV) to 0.68 ± 0.04 (CEM I), respectively. The I_{γ} in all types of cement was in the range of the exemption criterion ($I_{\gamma} < 0.5$) except the CEM I which was slightly greater but below the recommended limit ($I_{\gamma} = 1$) [8]. The I_{a} of the types of cement was lower than the recommended limit value of 1 [8].

The ELCR for each type of cement is presented in Table 4 with an average value ranging from $(0.38 \pm 0.04) \ 10^{-3}$ (CEM IV) to $(2.52 \pm 0.12) \ 10^{-3}$ (CEM I). The excess lifetime cancer risk in all types of cement was higher than the worldwide average value which is $0.29 \ 10^{-3}$ [10]. The values of ELCR equivalent to 1000, 100, 10, and 1 µSv y⁻¹ will increase the risk of developing mortal cancer by 4%, 0.4%, 0.04%, and 0.004%, respectively [37, 38]. Even all ELCR calculated are

higher than the worldwide value, the chances to increase the risks of cancer in life duration remains negligible.

The values of $D_{\rm org}$ evaluated in different types of organs and tissues according to the types of cement shown in Table 5 were less than the set limit. The calculated values of $D_{\rm org}$ showed that the testes were more sensitive to the radiations, and the ovaries were less sensitive.

3.3 Statistical analysis

3.3.1 Descriptive statistics

A descriptive statistics was performed to describe and also to have a better understanding of the statistical characteristic of the activity concentrations of the natural radionuclides (²²⁶Ra, ²³²Th, and ⁴⁰K). As the ²²⁶Ra and ²³²Th activity concentrations in white cement samples are found very low compared to gray cements, then they cause a large deviation of the distribution of the activity concentrations. Therefore, they are not used for the statistical analysis of the data. The results of the statistical anlysis are reported in Table 6.

The skewness, kurtosis, and the *p* value using the Shapiro–Wilks test were calculated to have a comprehensive understanding of the distribution of the data. The skewness characterizes the degree of asymmetry of the data [39]. In the theory of probability for a normal distribution, the skewness is equal to zero [40]. However, the data points are not always perfectly symmetric. The absolute magnitude of the ratio between the skewness and its standard error was calculated. If the ratio is less than two, the probability distribution can be assumed to be normally distributed. The distributions of ²³²Th and

Table 6 Descriptive statistics of $^{\rm 226}{\rm Ra},\,^{\rm 232}{\rm Th},$ and $^{\rm 40}{\rm K}$ activity concentrations in cement samples

	Activity concentration in Bq kg ⁻¹			
	²²⁶ Ra	²³² Th	⁴⁰ K	
Arithmetic mean \pm MSD [*]	112.69±6.72	13.12±0.48	73.35±4.68	
Standard deviation	26.02	1.88	18.12	
Geometric mean	109.67	12.99	71.21	
Min	66.73	10.15	48.67	
25th percentile	96.48	11.74	57.76	
Median	115.23	12.73	66.39	
75th percentile	132.24	14.80	89.78	
Max	150.25	16.09	98.80	
Skewness	-0.24	0.08	0.04	
Kurtosis	-0.90	- 1.19	- 1.68	
Shapiro–Wilks test (p value)	0.65	0.64	0.10	

*MSD Mean Standard Deviation

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⁴⁰K activity concentrations in this study had a weak positive skewness, whereas a weak negative skewness was observed for the distribution of ²²⁶Ra activity concentration. The ratios between the skewness and its standard error of the distributions of ²²⁶Ra ²³²Th and ⁴⁰K activity concentrations were found lower than two.

The kurtosis measures the extent of which data points cluster around the center of the distribution. For a normal distribution, the kurtosis is equal to zero. Negative kurtosis indicates that the data points are less clustered around the center, and the distribution has a thicker tail [41]. Unlike a negative kurtosis, the data points are clustered around the center of the distribution for a positive kurtosis and a thinner tail can be observed [41]. The ratio between the absolute magnitude and the standard error of the kurtosis must be less than two for a normal distribution. These ratios were found less than two for the distributions of 226 Ra, 232 Th, and 40 K activity concentrations.

The Shapiro–Wilks was also used to test the normality of the data. In the Shapiro–Wilks test, if the *p* value is less than or equal to 0.05, the distribution will not be normal. The found results in Table 3 show that the *p* values were greater than 0.05 for the distributions of ²²⁶Ra, ²³²Th, and ⁴⁰K activity concentrations.

The calculated values of the skewness, the kurtosis, and the *p* value found by the Shapiro–Wilks test showed that the 226 Ra, 232 Th, and 40 K activity concentrations can be assumed normally distributed.

3.3.2 Pearson correlation

Pearson correlation analysis was performed to determine the interdependency and the strength of the relation between the natural radionuclides (²²⁶Ra, ²³²Th, and ⁴⁰K) in cement samples. The results of the Pearson correlation analysis are shown in Table 7. Between ²²⁶Ra and ⁴⁰K, a weak negative correlation was observed, whereas a high positive correlation was observed between ²²⁶Ra and ²³²Th. It indicates that ²²⁶Ra and ²³²Th have a common source which in general due to the mineralogical components [42]. A high negative correlation was found between ²³²Th and ⁴⁰K which can be due to the mineral composition in cement that can affect the mobility of radionuclides [42].

Table 7Pearson correlationmatrix for variables

Variables	²²⁶ Ra	²³² Th	⁴⁰ K
²²⁶ Ra	1		
²³² Th	0.60	1	
⁴⁰ K	-0.23	-0.76	1

4 Conclusion

The ²²⁶Ra, ²³²Th, and ⁴⁰K activity concentrations were assessed in different types of cement available in Senegal by gamma-ray spectrometry. All activity concentrations were less than the worldwide values except the ²²⁶Ra in the gray cement. The Raeg was found less than the recommended value. The absorbed dose rate was greater than the worldwide average value of 84 nGy h^{-1} only in the gray cement. The AEDE was less than the recommended limit of 1 mSv y⁻¹. In the CEM I, CEM II, and CEM III, the AGDE was higher compared to the worldwide average of 300 μ Sv y⁻¹. The I_{y} of CEM I was only greater than the exemption criterion, but it was found below the recommended limit. The I_a was slightly greater than the recommended exemption level value in the CEM I and CEM II. However, the alpha index of these two types of cement was below the recommended limit which indicates that the concentration of radon will be less than 200 Bg m⁻³. The calculated ELCR was greater than the worldwide value; however, the chances to increase the risks of cancer in lifetime remain negligible. The absorbed dose rate according to different types of organs or tissues showed that the testes are more radiosensitive and the higher values of different organs or tissues are found in the CEM I. The contribution of the radiological hazard from the cement under this study is not significant. However, the activity concentration of ²²⁶Ra was found greater compared to its worldwide average value, which could serve as an alert to the radiation protection authority.

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Compliance with ethical standards

Conflict of interest On behalf of all authors, the corresponding author states that there is no conflict of interest.

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