Extending practical flow chemistry into the undergraduate curriculum via the use of a portable low-cost 3D printed continuous flow system

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Abstract

Continuous flow chemistry is undergoing rapid growth and adoption within the pharmaceutical industry due to its ability to rapidly translate chemical discoveries from medicinal chemistry laboratories into process laboratories. Its growing significance means that it is imperative that flow chemistry is taught and experienced by both undergraduate and postgraduate synthetic chemists. However, whilst flow chemistry has been incorporated by industry, there remains a distinct lack of practical training and knowledge at both undergraduate and postgraduate levels. A key challenge associated with its implementation is the high cost (>\$25,000) of the system's themselves, which is far beyond the financial reach of most universities and research groups, meaning that this key technology remains open to only a few groups and that its associated training remains a theoretical rather than a practical subject. In order to increase access to flow chemistry, we sought to design and develop a small-footprint, low-cost and portable continuous flow system that could be used to teach flow chemistry, but that could also be used by research groups looking to transition to continuous flow chemistry. A key element of its utility focusses on its 3D printed nature, as low-cost reactors could be readily incorporated and modified to suit differing needs and educational requirements. In this paper, we demonstrate the system's flexibility using reactors and mixing chips designed and 3D printed by an undergraduate project student (N.T.) and show how the flexibility of the system allows the investigation of differing flow paths on the same continuous flow system in parallel.

Keywords 3D Printing · Additive Manufacturing · Flow Chemistry · Reactionware · Fluidics

Introduction

Despite the fact that there are a rapidly increasing number of publications concerning continuous flow chemistry and that

Highlights

- We demonstrate the small-footprint nature of our continuous flow system that is suitable for undergraduate education.
- We demonstrate that it can be used with a variety of 3D printed mixing chips to illustrate mixing and the associated methodology.
- We show how the flexibility of the system allows for parallel reaction optimisation via residence time or reactor design on the same small-footprint continuous flow system.

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the adoption of continuous flow chemistry by industry has been encouraged by both the Federal Drug Agency (FDA) and the Chinese government [1] it is surprising that the subject receives little or no attention within the training of synthetic chemists at an undergraduate level [2, 3]. This deficit often continues into research groups, with postgraduate students also not receiving exposure to continuous flow synthesis at both PhD and postgraduate levels. This growing imbalance between the skills and training that undergraduates and postgraduates receive, versus the continuous flow chemistry requirements of those of the pharmaceutical industry needs urgent rectification if universities and research groups are to equip the next generation of chemists with the skills and required experience for the pharmaceutical industry. Additionally, if flow chemistry is to reach a stage where adoption is not limited only to “early adopters” and becomes concentrated in a few research groups with the financial resources to incorporate it into their research, then the early introduction of flow chemistry in undergraduate practical courses is of paramount importance. Unfortunately, the high costs of

commercial equipment needed for flow chemistry makes this difficult for many universities due to a large capital expenditure requirement. Even if universities have the financial resources to purchase systems, these are often limited to one or two as the high costs (>\$25,000 per system) means that it is fanciful to imagine a case where a university is able to provide access for one system per student pair.

As such, in those Universities incorporating flow chemistry into the curriculum, current “best practice” for undergraduate flow chemistry education focuses on the use of syringe pumps, due to the fact that these are straightforward to use and can be easily distributed along with inexpensive pieces of tubing and connectors [4]. However, costs can easily mount up if teaching to a large class (> 50) at the same time. In addition, there is a practical challenge of using syringe pumps, as they are relatively large and take up a large space in a fume cupboard or laboratory bench, meaning that only larger groupings of students can use these, rather than the more ideal use of a system by a pair of students. A growing alternative to the use of expensive syringe pumps focuses on a “DIY” approach to the construction of flow equipment via the 3D printing of syringe pumps controlled via microcontrollers, but this often leads to widespread differences in practice between universities and research groups and a plethora of systems [5].

As a result of these challenges, along with the growing 3D printing research in our group in both batch and flow, we set out to develop an adaptable, portable, modular, small footprint, low-cost 3D printed continuous flow system that could incorporate a number of flow paths as per user requirements that could be used by undergraduates in practical classes and also by research groups which was described recently [6–9] (Fig. 1).

The system itself was designed to be a pressure driven one where the normal geared syringe pumps or HPLC based pumps were replaced with a compressed gas source of fluidic flow, where the rate could be readily predicted and calculated based on the pressure, solvent viscosity, ambient temperature and dimensions of a variable restrictor capillary placed at the end of the flow path, according to the Hagen-Poiseuille equation [6]. Due to the high resistance through the capillary, the temperature of the reaction and the architecture of the flow path through mesoscale reactors can be readily altered without affecting the flow rate.

In this research, we describe how we sought to try to understand the potential of the system and how it could be used to flexibly teach undergraduate students continuous flow chemistry to illustrate the concept of flow and to allow for reaction analysis from the flow reactor. The student was a masters of Pharmacy project student (N.T.), which made it more challenging as the level of exposure to synthetic chemistry is lower in Pharmacy than in chemistry as a discipline.

As such, rather than burden the student with theoretical explanations behind the setup of the flow equipment, it was decided that they would be involved in the assembly of the modules to help understand how the equipment works and to visualise the flow path. The student would also be able to get an appreciation of the key components required for flow chemistry, namely: a method for pumping fluid, a mixing device, a reaction stage and a back-pressure regulator [10]. In order to save time, the 3D printed parts were prepared in advance. However, the student would gain experience by later designing and 3D printing reactors and mixing devices. Due to the short time available for the project (4 months), we needed to be able to put together the equipment required and disassemble it in a short amount of time. The four modules were stacked on to a magnetic stirrer hotplate which meant that minimal additional space was required when compared to batch reactions (Fig. 2). An additional pedagogical benefit to the student of putting together flow equipment themselves is the ability to visualise the flow path and understand important concepts such as laminar flow, dispersion and residence time as well as the benefits of fine heat control and space integration of multi-step syntheses [11].

Results and discussion

Preliminary mixing experiments

In order to introduce the student to the concept of continuous flow synthesis and its focus on the efficient and timely mixing of reagents, we decided to design a series of experiments that focussed on the mixing of two alcohols (*p*-cresol and 2-chlorophenol) via separate injection at injection loop A and injection loop B of our system at a low flow rate (0.17 mL/

Fig. 1 **a** The structure of our low-cost continuous flow system designed to fit existing stirrer hotplates; **b** The Assembled System; **c** The modular nature means that it is portable and easily fits within a storage briefcase

Fig. 2 Modules of the 3D printed flow system and the final assembled system

min). In this manner the student could easily explore the mixing ability of the reactor chip and retention times via addition or subtraction of one or more circular disk reactors (CDRs). Analysis via HPLC would also provide them with ready access to data whilst increasing the safety for the student as analysis focussed on differences in mixing rates rather than reactions (Fig. 3).

During initial experiments, we observed that the mixing of the two isopropanol solutions of *p*-cresol and 2-chlorophenol (differing viscosities) were travelling through the system at subtly different flow rates as calculated by HPLC (Fig. 4a). In order to demonstrate that this result was due to the viscosity and not the part of an interaction of one of the alcohols with the 3D printed reactors, we carried out a pre-mixing experiment, where the alcohols were injected into the same loop in a 1:1 manner, clearly demonstrating the effect of separate viscosities on the system (Fig. 4b).

Whilst isopropanol is a relatively viscous solvent used in continuous flow organic chemistry, the difference between two different solutions was evidently large enough to result in different flow rates. As a result of the fact that the narrow capillary flow resistor at the end of the flow path dictated the flow rate of the solution, the difference in flow rates of the two solutions at this position was thought to be responsible for the difference in flow rates and strongly suggested that the two solutions had not mixed sufficiently before this point. This was also clearly visible in a qualitative experiment where two coloured solutions were injected via loops A and B (Fig. 5). The opaque nature of the polypropylene (PP) mixing chip

Fig. 3 The setup of the continuous flow system used for experiments

meant that the reduced mixing was clearly visible and could also be observed in the PP CDRs.

As shown in Fig. 5, laminar flow predominated in the designed poor mixing mesoscale mixing chip of this system. This meant that the poor mixing likely led to viscosity-stratified [12, 13] flow which could be responsible for the difference in the observed flow rates of a simple T-mixer. This could clearly have the potential to affect reaction stoichiometry and was therefore an important issue to address in the students' research. In order to determine whether this was an issue with the pressure driven nature of our system or was a more widespread problem within continuous flow chemistry equipment, we carried out the same mixing experiments on commercial systems and in syringe pumps. One system (A) was available in house, and another was one was carried out independently by chemists based in industry (B). In order to avoid commercial sensitivity, the names and systems are not disclosed in this report, but it is indicative of the problems of mixing in flow chemistry at low flow rates in general and raises important questions of reaction stoichiometry when stoichiometric mixing is assumed (Fig. 6).

In all cases, the two different alcohols showed poor mixing and non-ideal ratios. Experiments were repeated following calibration of the flow systems, but with analogous results (supplementary information), clearly illustrating that it is a mixing rather than a pump issue. Swapping of the two injectants to explore pump effects also demonstrated that it was not a failure or fault in one of the pumps. The mixing issue that we observed is likely to be greater in our pressure-driven system, however in a system using HPLC pumps at the low flow rates carried out in this experiment, we attributed the difference in the flow rates and mixing to pulsation from misaligned pump strokes. This raises an important point in continuous flow chemistry, as inefficient or poor mixing in the ratios of reactants at the point of mixing or in the flow path can lead to impurities or incorrect ratios of reactants. This is also an issue between experiments as the stroke paths of the HPLC based

Fig. 4 **a** HPLC graph of the mixing and concentration profile of *p*-cresol and 2-chlorophenol via separate injection; **b** HPLC graph of the mixing and concentration profile of *p*-cresol and 2-chlorophenol via injection from the same loop

pumps can alter between reaction runs. The issue is less problematic in syringe-based systems, but is also a factor leading to imperfect mixing (Fig. 6c). In addition, flash flow chemistry, an area where flow chemistry excels over traditional methods [14, 15], requires the fast and accurate mixing of two reactants and so any mismatch in viscosities can lead to differing stoichiometries.

Design and analysis of mixing chip efficiency for improved reactant stoichiometry

In addition to understanding the basics of flow chemistry and given the initial mixing observations, the student was given the task of preparing a range of prototype mixing devices using FDM 3D printing to study the effect of mixing and laminar flow that could easily be incorporated into the mixing chip of the injection block of the flow reactor (Fig. 7).

The student was tasked with carrying out a brief survey of the literature to find simple architectures that could be quickly incorporated into a mixing device design and that could also be 3D printed in polypropylene. In order to evaluate different mixing devices, the student used Tinkercad®, an easily

accessible free online drawing package. The student was able to quickly design a variety of mixing devices for evaluation (Fig. 8).

Initially, passive mixing devices were printed using an Ultimaker 3 with polypropylene filament. Devices A and B were used to investigate whether the angle of mixing was important as has been suggested [16]. Devices C and D were designed to investigate the effect of increasing turbulence within the channels of the device by incorporating baffles [17]. Following analysis, the T-shaped mixing point offered a small improvement in the ratio of the two phenols as expected [16]. It could be suggested that negative angled Y-type mixers could have been investigated as these have been shown to affect greater mixing efficiency [18]. The use of mixing device C showed another small improvement in mixing efficiency however the additional baffles and longer flow path of mixing device D resulted in a worse ratio. This was thought to be due to the increased likelihood of bubble formation and non-wetting of the channel surface [19] as well as unoptimized spacing of the baffles. It is also worth noting the increased dispersion in this device (Fig. 9).

Fig. 5 **a** Illustration of poor mixing in a specially designed mixing chip to show poor mixing; **b** PFA tubing connecting the mixing chip with the CDRs; **c** the output into the CDRs, highlighting that despite passing through tubing, the two colours are still not mixed

Fig. 6 **a** Commercial system 1 (internal) same protocol followed; **b** Commercial system 2 (external) same protocol followed; **c** Syringe pump – same protocol followed

Design and development of an active mixing chip

Given the relatively low improvements in mixing efficiency, the student designed and prepared an active mixing device which consisted of a chamber where a magnetic stir bar could be placed within the flow path. This was inspired by the relatively unknown miniature continuous flow reactor which was used for ultrafast nitration reactions [20, 21]; more recent examples have shown utility in flow chemistry [22–24]. The mixing device would then be able to be used with a standard laboratory stirrer hotplate. Initially the mixing chamber was designed for a small Teflon coated cylindrical magnetic stir bar (10×3 mm). In a subsequently design the height of the mixing chamber was modified to fit a cross-shape magnetic stir bar (10×5 mm) (Fig. 10).

Fig. 7 Location of the mixing chip used for flow mixing experiments

In order to incorporate the stirrer bead within the 3D printed housing, the magnetic stir bar was placed into the chamber during the 3D print whilst paused and then printing continued to provide a sealed contiguous device. The curvature of the top of the mixing chamber was designed so that the print head would deposit filament in overlapping concentric circles to ensure the device was fully sealed (Fig. 11). In order to 3D print the desired mixing chip, a layer height of 0.15 mm, infill of 100% and a flow rate of 110% was used.

When the two stirrer devices were placed on the stirrer hotplate and the rotation of the stirrer was set at 500 rpm, we were pleased to observe efficient mixing in both cases with the cylindrical stirrer and the crosshead stirrer. Whilst the smaller cylindrical stirrer improved mixing, it had a tendency to “catch” at higher speeds, whilst the larger one possessed improved speed stability leading to the perfect mixing of both alcohols as seen below (Fig. 12b). Increases in speed or reduction led to lower levels of mixing of the two reactants, with 500 rpm representing the optimum speed (Supplementary Information).

The efficient mixing could also be observed qualitatively as seen via the injection and mixing of two different coloured solutions (Fig. 13), standing in stark contrast to that of the chip designed to have poor mixing (Fig. 4).

Fig. 8 **a** Y-mixer chip; **b** T-mixer chip; **c** Simple baffle mixer chip; **d** Increased baffle chip

Fig. 9 **a** HPLC results showing Y-mixer chip mixing efficiency; **b** HPLC results showing T-mixer chip mixing efficiency; **c** HPLC results showing Simple baffle mixer chip mixing efficiency; **d** HPLC results showing Increased baffle chip mixing efficiency

Fig. 10 **a** CAD design from the top face of the active mixer with a cylindrical stirrer bead; **b** CAD design from the side face of the active mixer with a cylindrical stirrer bead; **c** CAD design from the top face of

the active mixer with a crosshead stirrer bead; **d** CAD design from the side face of the active mixer with a crosshead stirrer bead

Fig. 11 **a** 3D Printing paused before addition of stirrer bead showing the central cavity; **b** Crosshead stirrer inserted into the cavity; **c** 3D Printing continued after insertion; **d** Size dimension of the mixer; **e** Size fit of the crosshead stirrer; **f** Fully 3D printed device

Fig. 12 **a** Graph of concentration versus time demonstrating the mixing efficiency of a cylindrical stirrer, mixed at 500 rpm; **b** Graph of concentration versus time demonstrating the mixing efficiency of a crosshead stirrer, mixed at 500 rpm

Fig. 13 Mixing of two different coloured dyes in the crosshead stirrer mixing chip with the speed of rotation of the stirrer hotplate set at 500 rpm

The results of the mixing experiments are summarised in Table 1 and it can clearly be seen that the mixing efficiency of the cross shaped stirrer bar is far greater than that of the passive mixing devices with the lower standard deviation indicative of better mixing efficiency (Table 1).

Development of a single flow system with parallel reaction experimentation

One of the key weaknesses of current continuous flow systems stems from their reliance on a single back pressure regulator. This clearly limits their potential as reactions can only be run in sequence. With an improvement in mixing achieved, we were intrigued by the possibility of modifying the system so that multiple reactions could be run in parallel on the same system as shown below (Fig. 14). As our system regulates the pressure by capillary resistors, we envisaged that it would be possible to

Table 1 Mixing efficiency of mixer chips

Mixing Device	Average Standard Deviation (mM)	Sum of Standard Deviation (mM)
Commercial Tee (PEEK)	2.17	43.4
Y-shape passive (PP)	1.80	34.2
T-shape passive (PP)	1.75	33.2
Short baffle	1.61	27.3
Long baffle	3.45	82.9
Cylindrical stir bar	0.992	16.9
Cross-shape stir bar	0.194	4.08

Fig. 14 Illustration of the flow arrangement for parallel reactions and actual realised experimental setup

run two (or more) reactions in parallel via splitting after the mixing chip and running the two flows through two differing paths from a single input. The addition of the same capillary resistor after each would then enable direct comparison between experiments with no temperature variation as the same stirrer hotplate can be used. Variation in residence time and or

flow path is an obvious possibility with this approach, and also via the use of two hotplates, variation in temperature (Fig. 14).

In order to explore the potential of running multiple reactions at the same time by splitting the output of the active mixing device between 2 identical capillary resistors on the same stirrer hotplate (Fig. 14), we compared the mixing

Fig. 15 **a** Graph of concentration versus time demonstrating the mixing efficiency of the Left-Sided capillary; **b** Graph of concentration versus time demonstrating the mixing efficiency of the Right-Sided capillary

Fig. 16 Combined graphs from Fig. 15 of concentration versus time demonstrating the mixing efficiency of the both the Left- and Right-Sided capillary experiments

profiles after splitting of the two reactor paths via a single CDR (Fig. 15).

As can be seen from the combined graphs, the mixing of the two sides of the flow path were perfectly mixed, demonstrating that reactions could easily be run in parallel with optimal mixing and so would provide ideal information from two reactions (Fig. 16).

Fig. 17 **a** Illustrative picture of the two differing flow paths used in the experiment with a normal CDR and modified narrower flow path CDR on the right; **b** Graph of concentration versus time profile of the normal CDR versus the narrow channel CDR

Fig. 18 **a** Illustrative picture of the two differing flow paths used in the experiment with two CDRs versus a single CDR; **b** Graph of concentration versus time profile of the single CDR versus two CDRs with a longer retention time

The next experiment then looked at the mixing profiles from analysis of two different CDRs. The standard one possessing an internal volume of 2.68 mL and a narrower channelled modified CDR with an internal volume of 4.03 mL. As can be seen from the graph of concentration versus time, the different flow paths lead to differing concentration profiles, clearly illustrating the potential of this approach. The picture of the two paths is illustrative with coloured dyes to highlight the concept used in this experiment (Fig. 17).

Following demonstration of the proof of concept, the student next focussed on a comparison of one versus two CDRs on the reaction profile. This therefore compared a reactor volume of 2.68 mL versus 5.36 mL in the combined system (Fig. 18).

As can be seen, the addition of a second reactor led to an expected slightly more diffuse peak profile of the material that was passed through the two combined CDRs with a greater overall internal volume. Pleasingly, this clearly demonstrates that experiments can easily be run in parallel with differing flow paths and path lengths via addition or subtraction of CDRs.

Conclusions

In this report, we have demonstrated that the teaching of practical flow chemistry to an undergraduate student (N.T.) is clearly possible at low cost as part of a short research project (4 months). Whilst it is obvious that not all projects would lead to such an outcome from such a student, it highlights what is possible with continuous flow at an undergraduate level. In being able to assemble the equipment, the student was able to gain a practical understanding of flow chemistry and applied this to solve a mixing issue due to laminar flow. This clearly raises the prospect of carrying out some practicals detailed herein with undergraduate students due to their simplicity and visual aspect which provides a ready visualisation of flow chemistry with a system that is relatively low in cost due to its 3D printed nature. In addition, the student was also able to develop the concept further via splitting after active mixing to demonstrate that more excitingly, flow chemistry reactions can also be run in parallel from a single reaction input and on a single continuous flow system. This clear reduction in reaction timing and improvement in reaction efficiency, will enable additional multiple parallel experiments to be run not only by undergraduate students, but also on a research-based level. The use of 3D printing to develop both the mixing chips and the CDRs raises the prospect of vastly reduced costs of undergraduate practical chemistry as the reactors used in this study cost less than \$1 to produce.

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