REVIEW ARTICLE



Expansive Soil Characterisation: an Appraisal

Sridharan Asuri¹ · Prakash Keshavamurthy²

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Abstract Expansive soils, which are considered as problematic soils, have worldwide distribution and hence, their proper identification and characterisation becomes an absolute necessity in the perspective of the present day geotechnical engineering practice. This paper intends to discuss relative merits of various methods available to a field geotechnical engineer to achieve this important goal.

Keywords Characterisation · Clay mineralogy · Expansive soils · Free swell tests · Testing methods

Introduction

Any soil whose volume changes are moisture sensitive is normally considered as an expansive soil. Expansive soils are regarded as problematic soils as they affect the stability of structures founded on them. Hence, it becomes very essential for a practicing geotechnical engineer to appropriately identify and characterise such soils. This in turn will help in material, time, financial and human resource managements, which are the essential components of any project management.

The expansive soils are characterised by the presence of expanding lattice type of clay minerals belonging to

 Prakash Keshavamurthy kprakash60@yahoo.com
 Sridharan Asuri sridharanasuri@yahoo.com

¹ FNAE, Indian National Academy of Engineering, New Delhi, India

² Department of Civil Engineering, Sri Jayachamarajendra College of Engineering, Mysuru 570 006, India smectite group, montmorillonite being an important member of that group. These clay minerals are characterised by

- Very weak van der Waals' forces in between the adjacent unit cells of the mineral.
- Appreciable isomorphous substitution during the clay mineral formation, leading to very high negative surface charges.
- Very high cation exchange capacity (i.e., 80–150 meq/ 100 g)
- Large specific surface (i.e., 400–900 m²/g).

It has been well established that these minerals respond quite differently to any external physico-chemical environment when compared with the response of non-expanding lattice type of clay minerals like kaolinite, which may also be present in any natural soil.

Characterisation of Expansive Soils

Various criteria adopted to recognise the presence of expanding lattice type clay minerals in a natural soil can be broadly classified into two categories namely, mineralogical identification and inferential testing methods.

Mineralogical Identification Methods

The techniques belonging to this category of methods are:

- X-ray diffraction analysis.
- Differential thermal analysis.
- Dye adsorption.
- Chemical analysis.
- Scanning electron microscopy.



Chen (1988) opined that these techniques should be used in combination for better and reliable results. However, these techniques have restricted usage and are confined to research laboratories only in view of their requirement of sophisticated and specialised instrumentation, which are costly and also expert interpretation of the resulting data.

Inferential Testing Methods

These methods try to link some of the index properties of fine-grained soils with the soil clay mineralogical composition and hence, to estimate their swell potential. They can be classified as indirect methods and direct methods.

Indirect Methods

These methods make use of soil index properties such as liquid limit, shrinkage limit, percent clay size composition of soils and also some of the indices such as plasticity index, shrinkage index and the like to estimate the swell potential of soils.

- 1. Liquid limit related properties:
 - *Liquid limit:* This upper bound plasticity limit is determined in the laboratory by the conventional Casagrande method or by the fall cone method. Liquid limit of a soil is regarded as the water holding capacity of the soil, which in turn has been taken as a measure of soil swell potential. Many classification schemes are available in the geotechnical engineering literature to recognise the degree of soil swell potential based on the liquid limit of fine-grained soils (Table 1).
 - *Plasticity Index:* It is the difference between the liquid limit and plastic limit of fine-grained soils. Higher the plasticity index, more plastic the soil is and higher will be the soil swell potential. Different schemes available to recognise the soil expansivity based on the plasticity index of the soils are given in Table 2.

The indirect methods of characterising the soil swell potential suffer from the following limitations:

Table 1 Expansive soil classification based on liquid limit

Swell potential	Liquid limit (%)		
	Chen (1965)	Snethan et al. (1977)	IS: 1498 (1970)
Low	<30	<50	20-35
Medium/marginal	30-40	50-60	35-50
High	40-60	>60	50-70
Very high	>60	_	70–90



Table 2 Expansive soil classification based on plasticity index

Swell potential	Plasticity index (%)			
	Holtz and Gibbs (1956)	Chen (1988)	IS: 1498 (1970)	
Low	<18	0–15	<12	
Medium	15–28	10-35	12–23	
High	25-41	20-55	23-32	
Very high	>35	>35	>32	

 Table 3
 Expansive soil classification based on shrinkage limit (Holtz and Gibbs 1956)

Swell potential	Shrinkage limit (%)
Low	>15
Medium	10–16
High	7–12
Very high	<11

 Table 4 Expansive soil classification based on shrinkage limit (Altmeyer 1956)

Volume change	Shrinkage limit (%)
Non-critical	>12
Marginal	10–12
Critical	<10

- The liquid limit tests are empirical and strength based (Sridharan and Prakash 1998a).
- There is no unique mechanism controlling the liquid limits of soils containing expanding lattice type clay minerals and the soils containing non-expanding lattice type clay minerals (Sridharan et al. 1986, 1988).
- The mechanisms controlling the liquid limit of fine-grained soils and the mechanisms governing the test procedures (i.e., Casagrande method and fall cone method) may not match (Sridharan and Prakash 2000a).
- Dependency of plasticity index on liquid limit.
- 2. Shrinkage limit related properties:
 - *Shrinkage limit:* It represents the lower bound water content for any volume reduction of a soil mass and hence, regarded as a measure of volume stability of the in situ soil. Tables 3 and 4 present the schemes available to recognise the swell potential of fine-grained soils based on shrinkage limit.
 - Shrinkage Index: It is defined by the Bureau of Indian Standards (IS: 2809 1972) as the difference between plastic limit and shrinkage limit. The

 Table 5
 Expansive soil classification based on shrinkage index (IS 1498)

Degree of expansivity/swell potential	Shrinkage index (%)	
Low	<15	
Medium	15-30	
High	30-60	
Very high	>60	

 Table 6 Expansive soil classification based on particle size composition

Degree of expansivity/swell potential	Percent clay size fraction (Chen 1965)	Colloid content (Holtz and Gibbs 1956)
Low	<30	<15
Medium	30-60	13–23
High	60–95	20-31
Very high	>95	>28

classification of swell potential of fine-grained soils based on their shrinkage index is given in Table 5.

It has been noted by many researchers that the shrinkage limit and the shrinkage index are not good predictors of the swell potential of fine-grained soils. This is because that the shrinkage limit is not a plasticity characteristic of finegrained soils and that the mechanism controlling the shrinkage limit is quite different from the mechanism controlling the soil swelling. While the soil swelling is controlled by the presence of expanding lattice type of clay minerals, the shrinkage limit is a result of packing phenomenon and is primarily controlled by the relative particle size distribution of fine-grained soils (Sridharan and Prakash 1998b).

- 3. Particle size composition related properties:
 - Many researchers have proposed criteria based on percentage clay size fraction (i.e., <0.002 mm size) or colloid content (i.e., content of particles of size less than 0.001 mm) to predict the swell potential of fine-grained soils, as per the scheme given in Table 6.
 - Activity: Activity of a soil is normally calculated as the ratio of plasticity index of the soil to its percentage clay size fraction. The soils can be classified based on their activity according to the guidelines given in Table 7.

The classification criteria based on particle size related properties have very strong limitations:

• The swelling of the soil is due to the amount of expanding lattice type clay minerals present in the soil

Table 7 Expansive soil classification based on the activity

Activity (A_c)	Nature of the soil	Probable degree of swell potential
<0.75	Inactive	Low
0.75–1.25	Normal	Medium
>1.25	Active	High

Table 8 Expansive soil classification based on oedometer swell tests

Swell potential	% Expansion in oedometer (Holtz and Gibbs 1956)	% Expansion in oedometer (Seed et al. 1962)
Low	<10	0–1.5
Medium	10–20	1.5–5
High	20-30	5–25
Very high	>30	>25

rather than the percentage of clay size fraction present in the soil.

 The percent clay size fraction or colloid content of a soil is determined by the sedimentation analysis (Ex: hydrometer analysis), which is based on many unrealistic assumptions.

Direct Methods

The methods coming under this category measure the swell potential of a soil directly.

 Oedometer Tests: According to Winterkorn and Fang (1986), the most useful and reliable assessment of swell potential of a soil could be obtained from the conventional oedometer swell tests.

According to USBR (Holtz and Gibbs 1956), the criterion for the classification of degree of soil expansivity is the total volume change of a soil from air dry to a saturated condition under a surcharge of 7 kPa in an oedometer (Table 8).

According to Seed et al. (1962), the criterion for the classification of degree of soil expansivity is the percent expansion exhibited by the soil compacted at maximum dry density and OMC under a surcharge of 7 kPa (Table 8).

The major limitations of oedometer tests are that they are tedious to perform and are time consuming.

- 2. Free swell tests:
 - Free Swell Value (FSV) Test: This test was first proposed by Holtz and Gibbs (1956). This test consists of pouring slowly 10 cm³ of oven dried soil passing 425 μm sieve into a 100 cm³ measuring jar filled with distilled water and noting the





Fig. 1 Relationship between free swell value and volume change (air dry to saturated condition under a load of 7 kPa) (Holtz and Gibbs 1956)

equilibrium volume of the sediment formed. The free swell value is then calculated as the increase in the volume of the soil expressed as a percentage of the initial volume.

Holtz and Gibbs (1956) had not advised any specific values of free swell to classify the soils. However, they suggested a pictorial relationship between FSV and the volume change of undisturbed soil specimens placed in the laboratory consolidometer from air dry to saturated condition under a load of about 7 kPa (i.e. 1 psi) (Fig. 1). The other limitation of this method is that the mass of the soil contained in 10 cm³ dry volume is a variable. Measurement of 10 cm³ volume of dry soil is purely based on personnel judgement, and it does not account for the variation in density of the soil, which is dependent on the height of pouring of the soil into the jar.

• *Differential Free Swell Test:* In this method, which is a standard method of practice specified by the Bureau of Indian Standards (IS: 2720 1977), the initial dry mass of the soil to be taken for the free swell test is 10 g, thus overcoming the limitation of the free swell volume test. In this method, the free swell index is defined by the Eq. (1).

$$FSI(\%) = \left[\frac{V_d - V_k}{V_k}\right] 100 \tag{1}$$

where, V_d and V_k are the equilibrium sediment volumes of 10 g oven dried soil samples passing 425 μ m sieve placed in 100 ml graduated measuring jars containing distilled water and kerosene respectively, after an equilibration period of a minimum of 24 h. The swell potential of the soil based on FSI is classified as per the guidelines given in Table 9.



Table 9Expansive soil classi-
fication based on FSI (IS 1498
1970)

Swell potential	FSI (%)
Low	<50
Medium	50-100
High	100-200
Very high	>200

 Table 10
 Expansive soil classification based on FSR (Sridharan and Prakash 2000b)

Free swell ratio	Clay type	Swell potential	Dominant clay mineral type
≤1.0	Non-swelling	Negligible	Kaolinitic
1.0–1.5	Mixture of swelling and non-swelling	Low	Mixture of kaolinitic and montmorillonitic
1.5-2.0	Swelling	Moderate	Montmorillonitic
2.0-4.0	Swelling	High	Montmorillonitic
>4.0	Swelling	Very high	Montmorillonitic

The major limitation of the differential free swell method is that it gives negative free swell indices for kaolinite rich soils (Sridharan et al. 1985).

• *Free swell ratio* (*FSR*) *method:* Free swell ratio is defined as the ratio of the equilibrium sediment volume of 10 g oven dried soil sample passing 425 μ m sieve placed in 100 ml graduated measuring jar containing distilled water to that in kerosene, after an equilibration period of a minimum of 24 h. The guidelines to classify degree of expansivity of a soil based on its FSR are indicated in Table 10. Table 10 also gives the probable dominant clay mineral composition of the soil.

The merits of the free swell ratio method of characterising the expansive soils are listed below:

- The test procedure is very simple and user friendly.
- It does not require any sophisticated instrumentation and interpretation.
- The type of principal clay mineral(s) composing the soil can be predicted quite accurately.
- The test results have been validated with oedometer swell tests (Sridharan and Prakash 2000b).
- The predicted dominant clay mineral type composing the soil from the FSR method and the actual dominant clay mineral(s) composing the soil have been shown to have an excellent one-to-one match (Prakash and Sridharan 2004).

Conclusions

Various methods of characterising expansive soils can be broadly grouped into two categories namely, mineralogical identification methods and inferential testing methods. This paper has discussed these two groups of methods and their sub groups critically and brought out the merits and limitations of various methods discussed. Free swell ratio method has been shown to be a simple and user friendly method that can be adopted in the field for characterising the expansive soils and for the identification of their mineralogical composition (Table 10).

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