ORIGINAL PAPER



Montmorillonite-anchored magnetite nanocomposite for recovery of ammonium from stormwater and its reuse in adsorption of Sc³⁺

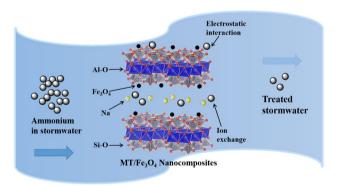
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Abstract

The treatment of stormwater to remove and recover nutrients has received increasing interest. The objective of this study was to develop a novel adsorbent that is easy to handle, has good adsorption capacity, and is economical to use. A novel nanocomposite of montmorillonite (MT)-anchored magnetite (Fe₃O₄) was synthesised by co-precipitation as an adsorbent for ammonium. The MT/Fe₃O₄ nanocomposite had pore sizes (3–13 nm) in the range of narrow mesopores. The dispersion of the anchored Fe₃O₄ was confirmed by transmission electron microscopy, scanning electron microscopy, and X-ray photoelectron spectroscopy (XPS). The nanocomposite exhibited higher affinity towards ammonium than the original MT. The Langmuir isotherm model was found to be the most suitable model to explain the ammonium adsorption behaviour of the nanocomposite. The maximum adsorption capacity for ammonium was 10.48 mg/g. The adsorption mechanism was a combination of ion exchange and electrostatic interaction. In an authentic stormwater sample, the synthesised adsorbent removed 64.2% of ammonium and reduced the amount of heavy metal contaminants including Mn, Ni, Cu and Zn. Furthermore, the ammonium loading on MT/Fe₃O₄ during adsorption functionalised the adsorbent surface. Additionally, the spent nanocomposite showed potential for rare earth elements (REEs) adsorption as a secondary application, especially for the selective adsorption of Sc³⁺. The versatile application of montmorillonite-anchored magnetite nanocomposite makes it a promising adsorbent for water treatment.

Graphic abstract



Keywords Stormwater · Montmorillonite · Magnetite · Nanocomposite · Ammonium recovery · REE recovery

Extended author information available on the last page of the article

Introduction

Urban living is replacing rural land use, increasing the size of impervious areas, reducing the availability of arable land, reducing infiltration and leading to increased surface runoff during storm events. Stormwater mobilises pollutant



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loads (e.g. suspended solids, nutrients, metals, and oxygen-demanding matter) and transports them to receiving water bodies such as rivers, lakes and ponds [1-3]. Nutrients (ammonium and phosphate salts) accumulating in the aquatic environment result in eutrophication and algal blooms, causing the death of aquatic life and degradation of water quality [4]. Ammonium is conventionally removed by biologic processes through nitrification and denitrification. Then, it is finally converted to N_2 but with the presence of by-products such as nitrate [5–7]. Moreover, the ammonium content in stormwater varies throughout the year depending on the season and amount of precipitation; this has a negative impact on the biologic treatment. An abiotic process such as adsorption can recover ammonium with low energy consumption as well as deal with the fluctuations in ammonium concentration since adsorbents work efficiently with high concentrations of pollutants as well as trace amounts of contaminants [8–10]. Adsorption is also simple to execute and has low energy requirements [11]. For practical applications, adsorbents should be of low cost with high efficiency and easy recoverability.

Clay minerals are inexpensive, non-toxic natural materials which are widely used in the ceramic, paper, rubber, plastics, cosmetics and medicine industries. Among them is montmorillonite (MT), a one-dimensional crystal of aluminosilicate layers with interlayers of alkali metal and earth cations—typically Na⁺, Ca²⁺, and Mg²⁺. It is a potential adsorbent owing to its large surface area, stable chemical properties and high cation exchange capacity [12, 13]. It was reported as an adsorbent with or without modification for the removal of copper (Cu²⁺) [14] and ammonium [15]. The net negative charge on the structure of MT can attract and capture cations, making it a natural candidate for ammonium adsorption.

Recently, many efforts have been made for synthesis of adsorbent material by the incorporation of magnetic nanoparticles. As one of the popular inorganic nanoparticles [16] for wastewater treatment, magnetite (Fe₃O₄) possesses a high adsorption capacity and a fast adsorption rate. Furthermore, its magnetic feature allows for easy recovery after use [17, 18]. It was recently investigated as an adsorbent for the removal of cadmium (Cd²⁺) [19]. Additionally, an ammonium-pillared MT/Fe₃O₄ nanocomposite was synthesised for caesium (Cs⁺) removal from water and soil [20]. Moreover, the semiconductor properties of magnetite provide possible photocatalytic reactions—such as the degradation of organic pollutants—as an extra merit [21–24].

To the best of our knowledge, the use of the nanocomposite form of MT and Fe_3O_4 as adsorbents for ammonium recovery has not been reported. In this study, MT/ Fe_3O_4 nanocomposites were synthesised using the co-precipitation method which consumes little power and is environmentally friendly [25] as a low-cost, non-toxic, easy-to-handle

adsorbent for ammonium recovery in stormwater treatment. The characterisation of adsorbents—adsorption performance under various dosages, contact time, initial pH of ammonium solutions, initial concentration of ammonium solutions, kinetics, isotherm models, and stormwater treatment—has been studied thoroughly. Likewise, the ammonium-loaded nanocomposite was applied as an adsorbent for rare earth elements (REEs) recovery, especially for the selective adsorption of Sc³⁺.

Materials and experimental methods

Materials

The montmorillonite (MT, K10 powder) was purchased from Sigma Aldrich. The chemicals used, including iron(II) chloride tetrahydrate (FeCl₂·4H₂O), iron(III) chloride hexahydrate (FeCl₃·6H₂O), ammonium chloride (NH₄Cl), sodium hydroxide (NaOH) and hydrochloric acid (HCl), were obtained from Sigma Aldrich and used without further purification.

Synthesis of MT/Fe₃O₄ nanocomposites

The method for the synthesis of Fe_3O_4 and MT/Fe_3O_4 nanocomposite was adapted from previous studies with minor modifications [20]. First, 1.8 g of $FeCl_2\cdot 4H_2O$ was dissolved in 150 mL of deionised water. Then, MT was added to the solution in an ultrasonic bath for 10 min, and the mixture was stirred and heated in an oil bath for 20 min. Next, 2.7 g of $FeCl_3\cdot 6H_2O$ was dissolved in the mixture and stirred for 30 min under N_2 flux at 80 °C, then 50 mL of NaOH (1.6 mol/L) solution was pumped into the mixture solution at a constant rate (0.5 or 2 mL/min) and stirred under N_2 atmosphere for times varying from 2 to 4 h. After the reaction, the suspension was centrifuged and washed thoroughly in ethanol and water. Finally, the solid product was dried in a hot air oven (Termaks) for 24 h at 60 °C.

Characterisation of adsorbent

MT/Fe $_3O_4$ nanocomposites synthesised in different conditions were thoroughly characterised using different techniques. The phase identification was done by X-ray Diffraction (XRD) in a PANalytical X-ray diffractometer using Co K α irradiation at $\lambda = 1.79$ Å with 2θ ranging from 5° to 80° at 40 kV and 40 mA. The magnetic features of the synthesised adsorbents were characterised using a vibrating sample magnetometer (VSM, Princeton Measurements Micromag Model 3900); the field applied ranged from -1.2 T to 1.2 T. Transmission electron microscopy (TEM) was conducted using a Hitachi HT-7700 at 100 kV. Its morphological and



elemental characteristics were evaluated through scanning electron microscopy (SEM) and energy-dispersive X-ray spectroscopy (EDS) in a Hitachi S-4800 microscope at 20 kV. Surface functional groups were identified by Fourier transform infrared spectroscopy (FTIR) using the Bruker Vertex 70 model in a spectra range of 4000–400 cm⁻¹. X-ray photoelectron spectroscopy (XPS) was done using a Thermo Fisher Scientific ESCALAB 250Xi (Thermo Fisher Scientific, UK), with an X-ray source of monochromatic Al Kα (1486.6 eV). The specific surface area and pore size distribution were determined by the N₂ Adsorption-desorption Isotherm (Tristar® II Plus). Samples were degassed at 60 °C under N2 overnight and analysed using liquid nitrogen (77 K). The surface charge was investigated through a Surface Zeta Potential (ζ) study using a Malvern Zeta sizer Nano ZEN350 model; a 2 mg sample was dispersed in 10 mL of deionised water, and the pH was adjusted to 1-10 by HCl and NaOH.

Batch adsorption experiments for ammonium removal

The stock solution of ammonium was prepared by dissolving NH₄Cl in deionised water as 1,000 mg/L. The working solutions with desired concentrations were diluted from the stock solution. All the adsorption experiments were conducted using 15 mL tubes by mixing 10 mL of working solutions with known amounts of adsorbent. The tubes were shaken in an orbital shaker (IKA KS 4000 ic control) at a speed of 300 rpm for a given time at 25 °C or 35 °C. After shaking, the mixture was filtered using a 0.45 µm cellulose acetate syringe filter and analysed through Ion Chromatography (IC, Shimadzu; Shodex IC YS-50 column, column oven temperature 40 °C, 4 mM methanesulphonic acid eluent, pump flow 1 mL/min) for the concentrations of ammonium. The iron leaching from the adsorbents under different initial pH was analysed by inductively coupled plasma-optical emission spectrometry (ICP-OES, Thermo iCAP 6300 series) to determine the concentrations of iron in the treated solution after adsorption. The effects of adsorbent dosage, contact time, initial concentration and initial pH of working solutions were studied. The initial pH of working solutions was investigated in a range of 2 to 12 and adjusted by adding HCl (1 M and 0.1 M) and NaOH (1 M and 0.1 M). Adsorption experiments were also performed using real stormwater to investigate the efficiency of MT/Fe₃O₄ nanocomposites.

The amount of ammonium adsorbed was calculated from the mass balance, assuming constant liquid phase density:

$$q_{\rm e} = \frac{V^{\rm L}}{m_{\rm ads}} \left(C_0 - C_{\rm e} \right) \tag{1}$$

where q_e (mg/g) is the adsorbed amount, V^L (L) is the volume of liquid phase, $m_{\rm ads}$ (g) is the mass of adsorbent, and C_0 and C_e (mg/L) are the ammonium concentrations initially and at equilibrium, respectively. The removal efficiency RE was calculated by the following equation:

$$RE = \frac{C_0 - C_e}{C_0} \times 100\%$$
 (2)

Results and discussion

Preliminary adsorption experiments

Several batches of nanocomposite adsorbents were prepared by varying the amount of MT, the reaction time, and the flow rate of NaOH addition as listed in Table 1. The table also shows the preliminary characterisation of the surface area using the BET method.

Preliminary adsorption tests were conducted to determine the adsorbent batch with the highest uptake of NH₄⁺. The initial NH₄⁺ concentration was 50 mg/L, and the solid-toliquid phase ratio was kept low (1:500 g/L) to avoid adsorbing all of ammonium which would yield only small differences in uptake between the adsorbent batches. Both the original MT and the prepared Fe₃O₄ showed limited removal efficiency of NH₄⁺ at 4.90% and 2.52%, respectively, while the synthesised adsorbents were able to remove NH₄⁺ with various efficiencies ranging from 16.58% to 37.20%.

The performance of the synthesised adsorbents with respect to NH₄⁺ adsorption increased with retention time and the amount of MT used during synthesis. A possible reason for this is that the longer retention time ensures

Table 1 Adsorbent batches synthesised

MT/Fe ₃ O ₄ ID	MT (g)	Time (h)	NaOH (mL/ min)	$S_{\rm BET}$ (m ² /g)*	RE (%)**
Fe ₃ O ₄	_	_	_	37.66	4.90
MT	_	_	_	245.99	2.52
517	1.0	2	0.5	92.86	16.58
522	2.0	2	0.5	129.65	17.61
529	3.0	2	0.5	122.70	25.29
528	3.0	4	0.5	128.68	28.70
603	4.0	4	0.5	88.22	30.34
604	4.0	4	2	100.17	37.20
605	5.0	4	0.5	98.16	32.33
610	5.0	4	2	123.32	24.73

^{*} Specific surface area (BET)

^{**}Solid-to-liquid phase ratio 1:500, initial NH₄⁺ concentration 50 mg/L



better dispersion of Fe_3O_4 on the surface of the MT. The higher flow rates of NaOH pumped to the reaction lead to higher specific surface area (S_{BET}), but the NH_4^+ uptake ability changes depending on the amount of MT. The obvious improvement of the NH_4^+ uptake ability of MT after the modification indicates that the addition of iron creates and stimulates new active sites. However, excessive Fe_3O_4 may cover partial active sites resulting in lower removal efficiency of NH_4^+ . As shown in Table 1, MT/Fe_3O_4604 has the highest adsorption towards NH_4^+ . Therefore, further studies were conducted with sample MT/Fe_3O_4604 and reaction conditions were optimised for the enhancement of ammonium removal efficiency. The spent (ammonium loaded) adsorbent was then named MT/Fe_3O_4604N .

Characterisation of MT/Fe₃O₄ nanocomposites

Structure and magnetic properties

The crystal structures of MT, Fe₃O₄, and MT/Fe₃O₄ were investigated via XRD; the diffraction patterns (converted from Co K α to Cu K α) are shown in Fig. 1a. The seven strong peaks at 18.3°, 30.1°, 35.5°, 43.1°, 53.5°, 57.0°, and 62.7° corresponded to the cubic inverse spinel structure of Fe₃O₄, which was synthesised through co-precipitation of Fe^{2+} and Fe^{3+} [19, 26–28]. The diffraction peaks at 8.8°, 17.8° , 19.8° , 35.1° , and 45.5° corresponded to MT (montmorillonite K10), which were well matched with the reported spectra [29–31]. Quartz is present in MT, evidenced by the pattern at 20.8° , 26.6° , 50.1° , and 60.0° [32]. The spectra of MT/Fe₃O₄604 and MT/Fe₃O₄604N were almost the same as MT, suggesting that neither the modification by Fe₃O₄ nor the adsorption of NH₄⁺ changed the crystal structure of MT. All the other MT/Fe₃O₄ nanocomposites expressed identical patterns, as shown in Fig. S1 in the Supplementary Document. The peak of Fe₃O₄ at 35.5°, presented beside the MT 35.1° (110) peak in the spectra of MT/Fe₃O₄604 and MT/Fe₃O₄604N, indicated that the (110) plane of MT/ Fe₃O₄ became more disordered than that of MT due to the loading of Fe₃O₄.

The magnetic properties of the prepared MT/Fe $_3$ O $_4$ products were evaluated by VSM, as shown in Figs. 1b and S2. All of the products exhibited superparamagnetic properties with extremely narrow hysteresis loops [33, 34]. Moreover, sample MT/Fe $_3$ O $_4$ 517 (Fig. S2) had a relatively high saturation magnetisation, which is favourable for magnetic separation. The Fe $_3$ O $_4$ aggregated to larger sizes due to the relatively high amount of it, resulting in low removal efficiency of MT/Fe $_3$ O $_4$ 517. It was not selected as the sample to be further studied since the more important property is the high adsorption capacity. Although the magnetic moments of the products are relatively low, their magnetic feature can accelerate separation in the after-adsorption processes.

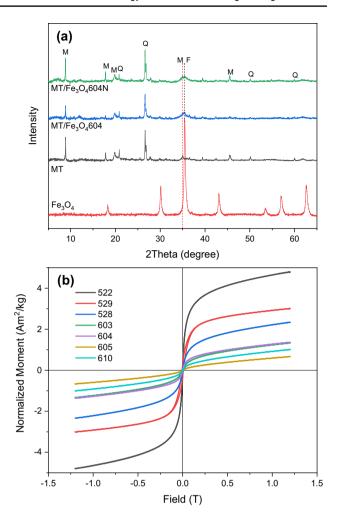


Fig. 1 a XRD patterns (M: montmorillonite, Q: quartz, F: Fe_3O_4), **b** hysteresis loops of the synthesised adsorbents. See Fig. S2 for data on sample 517

Morphology and composition analysis

The TEM images showed the sheet-like nature and small number of rod-like structures of MT (Fig. 2a) as well as the Fe_3O_4 nanoparticles and aggregates (Fig. 2b). The sizes of the Fe_3O_4 nanoparticles were around 15–25 nm, as shown in Fig. 2b. Similarly sized Fe_3O_4 nanoparticles were observed in the MT/ Fe_3O_4 nanocomposites, as shown in Fig. 2c. The Fe_3O_4 nanoparticles were either dispersed on the surface and around the rod-like structures or intercalated between the layers of MT (Fig. 2c). This observation is confirmed by a SEM image of MT/ Fe_3O_4 604, as shown in Fig. 3c.

The morphologies of the representative samples were characterised by SEM, as shown in Fig. 3a-d. MT (Fig. 3a) had a shape of flakes and a layered, relatively smooth surface, while the Fe₃O₄ was in the shape of granules and seen on the surface of modified MT (Fig. 3c); this is direct evidence of the successful synthesis of MT/Fe₃O₄



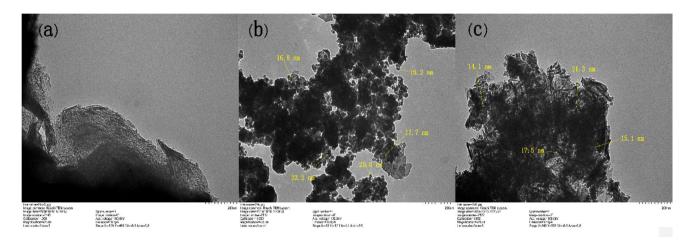


Fig. 2 TEM images of a MT, b Fe₃O₄, c MT/Fe₃O₄604

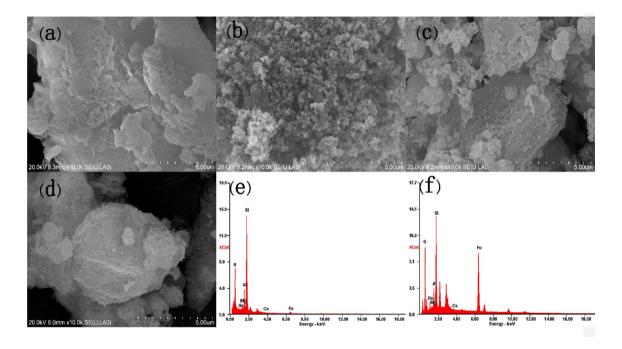


Fig. 3 SEM images of a MT, b Fe_3O_4 , c MT/ Fe_3O_4604 , d MT/ Fe_3O_4604 N, EDS plots of e MT, f MT/ Fe_3O_4604

nanocomposite [35]. The fine Fe₃O₄ particles adhere to the surface of MT as shown in Fig. 3c. The existence of Fe was confirmed by the EDS results (Fig. 3e-f), as the Fe content increased markedly in MT/Fe₃O₄604 compared to MT. After the adsorption process, the structure of MT/Fe₃O₄604N (Fig. 3d) was not significantly changed in compare with MT/Fe₃O₄604 (Fig. 3c), except for that the surface of MT/ Fe₃O₄604N (Fig. 3d) was less covered by Fe₃O₄ particles which was corresponded by the iron leaching phenomenon (Fig. 6a).

The surface composition was analysed by XPS, as shown in Fig. 4a-b. Peaks at 724.9 eV and 711.4 eV—as two typical spectra of Fe 2p_{1/2} and Fe 2p_{3/2}, respectively—confirmed the existence of Fe_3O_4 in the as-synthesised adsorbents [36, 37]. The Mg 1s peak was present in the spectrum of MT, but barely showed after modification, indicating that Fe took the place of Mg. As expected, N 1s appeared in the spectrum of MT/Fe₃O₄604N after adsorption, as evidence of the existence of NH₄⁺ on the surface of the MT/Fe₃O₄ nanocomposite. The characteristic peak of Si 2p verified the composition of MT [20]. The binding energy of Si 2p increased by 1.2 eV from MT to MT/Fe₃O₄604, indicating a strong interaction between Si and Fe atoms. The lowered intensity of Si 2p in MT/Fe₃O₄ nanocomposite compared with MT suggests that partial Si sites were covered by Fe₃O₄. The Na 1s was not observed in MT but appeared clearly in the MT/Fe₃O₄



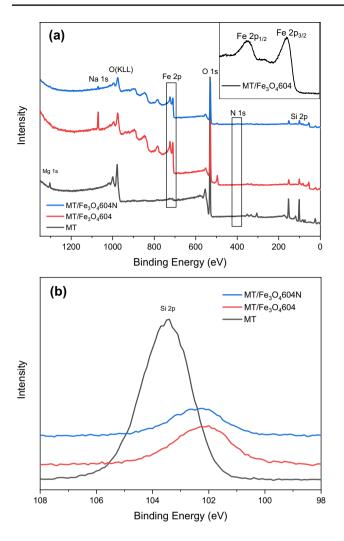


Fig. 4 XPS spectra of adsorbent materials a survey, b Si 2p

nanocomposite (Fig. S3), coming from the NaOH used in the modification. During the adsorption process, Na was released to the aqueous solution, so there was a low-intensity peak of Na 1s in the used adsorbent (MT/Fe₃O₄604N).

The infrared spectra of MT, Fe₃O₄ and the adsorbent before and after the adsorption of NH₄⁺ are shown in Fig. 5a. The band at 544 cm⁻¹ in the spectra of Fe₃O₄ corresponds to the characteristic band of magnetite, which is attributed to the mixture of Fe²⁺ and Fe³⁺ in the sample [38, 39]. The characteristic strong bands at 1,031 and 449 cm⁻¹ of MT are assigned to the stretching of Si–O. The Si–O bands are present in the spectra of modified samples at around 1000 cm⁻¹. The bands showed at around 3600 and 1630 cm⁻¹ are related to the stretching and bending of hydroxyl groups, respectively [40, 41]. The shifting of Si–O and hydroxyl groups from MT to MT/Fe₃O₄604 indicated that the loaded Fe₃O₄ encountered these groups on the surface of MT. One new band appeared in the spectra of the after-adsorption sample at 1,443 cm⁻¹ due to the deformation of NH₄⁺, indicating

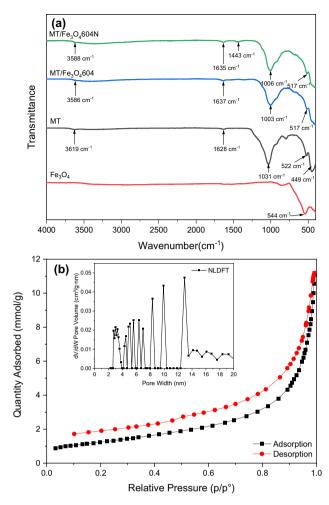


Fig. 5 a FTIR spectra of Fe_3O_4 , MT, MT/ Fe_3O_4604 , and MT/ Fe_3O_4604N , b N_2 adsorption–desorption isotherm and NLDFT pore size distribution of MT/ Fe_3O_4604

that chemisorption of NH₄⁺ happened during the contact [15]. The bands at around 520 cm⁻¹ are attributed to the vibrations of the Si–O–Al structure [20].

Specific surface area and pore size analysis

According to IUPAC classification, the N₂ adsorption—desorption isotherm of MT/Fe₃O₄604 (Fig. 5b) is a Type IV physisorption isotherm and Type H3 hysteresis loop, given by non-rigid aggregates of plate-like particles; in this case, it is montmorillonite, with slit-shaped pores. The Kelvin equation-based Barrett—Joyner—Halenda (BJH) method would underestimate the pore size for narrow mesopores, so the non-local-density functional theory (NLDFT)-based method was applied to obtain a more reliable assessment of pore size distribution [42]. As shown in Fig. 5b, the pore sizes of MT/Fe₃O₄604 are distributed in the range of narrow mesopores, which are in the range of 3–13 nm. The particle size of MT/Fe₃O₄604 was analysed by Zeta sizer, found to



be 609.4 nm in diameter. The physical dimensions of the pores suggest a good molecular sieving effect, which indicate that the nanocomposite can be used as a filling material to be dispersed into polymer matrices of membranes for a better separation performance in water treatment [43, 44].

The S_{BET} was calculated by the Brunauer–Emmett–Teller (BET) method and listed in Table 1. The raw MT has the highest S_{BET} of 245.99 m²/g, while all the MT/Fe₃O₄ nanocomposites have lower S_{BET} . There is no clear trend of surface area among the prepared adsorbent samples based on the MT amount for the reaction, but the flow rate of NaOH affected the S_{BET} in a such a way that the higher flow rate (2 mL/min) led to a higher S_{BET} than that of the lower flow rate (0.5 mL/min) when the MT amount and retention time were the same.

This is possibly due to the behaviour of Fe_3O_4 aggregates on the MT surface; more Fe_3O_4 was formed inside the pores of MT at a lower rate. The results also suggested that the adsorptive property need not always be positively correlated to the specific surface area. It is noteworthy that the best adsorption capacity was obtained with MT/Fe $_3O_4604$ even though the highest S_{BET} was attained with MT/Fe $_3O_4522$. The main difference is higher MT/Fe ratio and longer reaction time in the synthesis of MT/Fe $_3O_4604$.

Adsorption mechanism and kinetics

Adsorption mechanism

A series of adsorption equilibrium studies were performed with initial NH_4^+ concentrations of 10 to 80 mg/L at 25 and 35 °C. These are typical ambient temperatures in many geographic regions. Higher temperatures were not studied because the high energy requirement for stormwater heating was not economic. The concentrations of NH_4^+ in

stormwater vary throughout seasons. Therefore, concentrations ranging up to 80 mg/L were appropriate.

 $\mathrm{NH_4}^+$ uptake increased with increasing initial concentration of $\mathrm{NH_4}^+$ (Fig. 6b), meaning that some of the available active sites remain unoccupied at lower $\mathrm{NH_4}^+$ concentrations. Similar results were observed in other studies on the adsorption of $\mathrm{NH_4}^+$ by clay and $\mathrm{Fe_3O_4}$ materials [45, 46]. Additionally, higher equilibrium loading was achieved at 35 °C than at 25 °C, which suggests that the adsorption process is endothermic.

The pH of the $\mathrm{NH_4}^+$ solution influences the adsorption process. Therefore, the adsorption of ammonium ions by MT/Fe₃O₄604 was also investigated in different pH ranges. 50 mg/L $\mathrm{NH_4}^+$ solution was adjusted to an initial pH of 2, 4, 6, 7, 8, 10, and 12, respectively, and contacted with MT/Fe₃O₄604 through shaking at 300 rpm for 60 min at 25 °C. As shown in Fig. 6a, the abundant H⁺ ions inhibited the adsorption of $\mathrm{NH_4}^+$ in highly acidic conditions (pH 2) through competitive adsorption [47] while the adsorption amounts of $\mathrm{NH_4}^+$ under other pH conditions are affected to some extent. This may have been because the added adsorbents affected the pH of the solutions, resulting in a reduction in the effect of the initial pH of the $\mathrm{NH_4}^+$ solutions on the adsorption behaviour.

A possible issue with the nanocomposite adsorbent is dissolution of iron. A high solid-to-liquid phase ratio of 1:4 was used to observe this phenomenon even if leaching was low. As observed in Fig. 6a, iron leaching was significant at pH 2 (51.3 mg/L) but negligible at pH ranging from 4 to 10 (<0.85 mg/L). Leaching of iron increased again under alkaline conditions (pH 12, 1.43 mg/L). Therefore, we conclude that the nanocomposite adsorbents are stable at the pH range of their most likely applications.

The cations in the MT framework contributed to the removal of NH₄⁺ by MT/Fe₃O₄ nanocomposite through ion

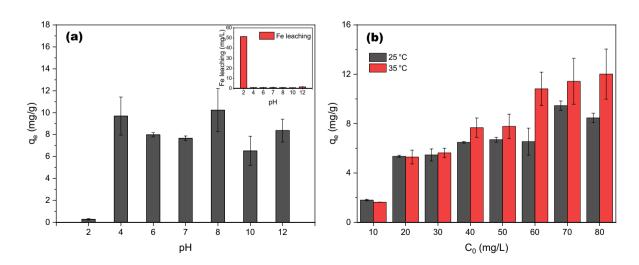


Fig. 6 Influence of pH and temperature on adsorption of ammonium at initial concentrations of 10 to 80 mg/L at 25 °C and 35 °C



exchange [48, 49]. It was indicated in the results of XPS and stormwater test that $\mathrm{Na^+}$ took the role of ion exchange during the contact of MT/Fe₃O₄604 and the $\mathrm{NH_4}^+$ -containing solution. Meanwhile, co-existing cations such as $\mathrm{K^+}$, $\mathrm{Mg^{2^+}}$, and $\mathrm{Ca^{2^+}}$ worked as competitive cations during the removal of $\mathrm{NH_4}^+$.

As shown in Fig. 7a, we further investigated the zeta potential (ζ) of MT, Fe₃O₄, and MT/Fe₃O₄604, dispersing it in deionised water at different pH values. The surface charge features of MT were in accordance with the literature [15]. The loading of Fe₃O₄ particles changed the zeta potential variation of MT. The isoelectric point (pH point of zero charge, pH_{pzc}) of MT/Fe₃O₄604 was 5.01, close to that of Fe₃O₄, which was 4.80. The similarity of MT/Fe₃O₄604 and Fe₃O₄ revealed the successful coating of Fe₃O₄ on the surface of MT [50]. At pH>pH_{pzc}, MT/Fe₃O₄604 was negatively charged, which is favourable for electrostatic interaction with cationic NH₄⁺ [51].

Based on the analysis above, the mechanism (Scheme 1) of the uptake of $\mathrm{NH_4}^+$ by the MT/Fe₃O₄ nanocomposite may be pictured as the following reactions, which contribute to ion exchange and electrostatic interaction, respectively. The sodium ions (Na⁺) existing in the interlayers of MT/Fe₃O₄ nanocomposite exchange with $\mathrm{NH_4}^+$ during the adsorption procedure, as shown in Eq. (3). The MT/Fe₃O₄ nanocomposite exhibits a negative charge at a pH that is higher than 5. Thus, $\mathrm{NH_4}^+$ can be captured through electrostatic interaction, Eq. (4).

$$Na - MT/Fe3O4 + NH4Cl \Rightarrow NH4 - MT/Fe3O4 + NaCl$$
(3)

$$MT/Fe3O4- + NH4+ \rightleftharpoons NH4+ \bullet MT/Fe3O4-$$
 (4)

Adsorption isotherms

The adsorption isotherms were studied by correlating them with Langmuir, Freundlich, and Fowler–Guggenheim isotherm models [52–55]. The Langmuir isotherm [56] is written as

$$q_e = \frac{q_{\rm m} K_{\rm L} C_e}{1 + K_{\rm L} C_e} \tag{5}$$

where $C_{\rm e}$ (mg/L) is the concentration of NH₄⁺ in equilibrium, $q_{\rm e}$ (mg/g) and $q_{\rm m}$ (mg/g) are the amount of NH₄⁺ adsorbed in equilibrium and the maximum uptake, respectively, and $K_{\rm L}$ (L/mg) is the Langmuir constant.

The equation for Freundlich isotherm [57] is

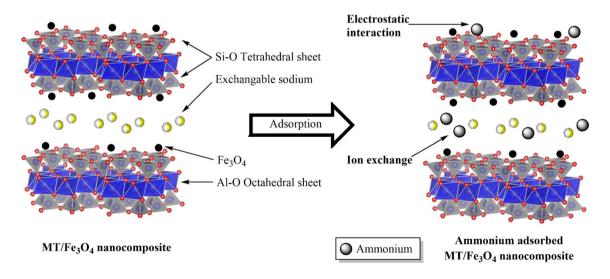
$$q_e = K_f C_e^{\frac{1}{n}} \tag{6}$$

where *n* represents the heterogeneity factor related to the distribution of interaction energies of adsorption sites, and $K_f (\text{mg/g}\cdot(\text{L/mg})^{1/n})$ is the Freundlich constant.

The Fowler–Guggenheim isotherm (Eq. 7) assumes an energetically homogeneous adsorbent surface like the Langmuir isotherm but includes an additional parameter to describe interactions between adsorbed species. Such interactions can be positive or negative (i.e. lead to increased or decreased surface concentration on the adsorbent). While the model is not explicit, solving Eq. (7) for the equilibrium loading $q_{\rm e}$ is straightforward with standard numerical methods.

$$K_{\rm FG}C_{\rm e} = \frac{q_{\rm e}}{q_{\rm m} - q_{\rm e}} \exp\left(-\chi \frac{q_{\rm e}}{q_{\rm m}}\right) \tag{7}$$

In Eq. (7), K_{FG} and q_{m} have the same meaning as the corresponding parameters in the Langmuir isotherm. χ describes the lateral interactions between adsorbed molecules.



Scheme 1 Mechanism of ammonium adsorption on MT/Fe $_3$ O $_4$ nanocomposite



To avoid artefacts arising from linearising the isotherm models and data, the parameters of the isotherm models were fitted with the nonlinear least squares method. The best-fit values are listed in Table 2, and plots for adsorption at 25 °C are shown in Fig. 7b. The Langmuir isotherm model was best model to explain the NH₄⁺ adsorption at 25 °C, indicating monolayer adsorption to a finite number of adsorption sites. The Freundlich model predicts unreasonably high ammonia uptake at low concentrations. The Fowler-Guggenheim model, which includes interaction between adsorbed molecules, gives a somewhat higher R^2 than the Langmuir isotherm. However, it fails to predict the increase of loading beyond 8 mg/g in the high concentration range. The lateral interaction parameter, $\gamma = 2.43$, is quite large, suggesting a strong attractive interaction between adsorbed species. Considering that ammonium is charged, it is unlikely that this is the case. We therefore concluded that the improved fit is only due to the additional degree of freedom and that the model is overparameterised.

The maximum Langmuir adsorption capacity was found to be 10.48 mg/g for MT/Fe₃O₄604 towards NH₄⁺. This capacity is comparable to or better than reported for other clay-based materials (Table 3). For example, a capacity of 12.5 mg/g for NH₄⁺ on montmorillonite-biochar composites has been reported [58]. On the other hand, capacities of 1.54 mg/g and 1.38 mg/g have been reported for montmorillonite nano-clay and natural vermiculite, respectively [59]. Significantly higher capacity (40.4 mg/g) has been reported for NH₄⁺ uptake in montmorillonite, but the liquid phase concentration was tenfold that in this study [15]. At conditions comparable to this study, however, the uptake in montmorillonite was slightly lower than here (q_e =7 mg/g at C_e =60 mg/L) [15].

Adsorption kinetics

The adsorption kinetics were studied in a batch adsorber using 2.5 g/L adsorbent dosage and initial $\mathrm{NH_4}^+$ concentrations of 30 mg/L, 50 mg/L, and 80 mg/L. As shown in Fig. 8, the $\mathrm{NH_4}^+$ uptake reaches a high level within 5 min for

Table 2 Parameters of the isotherm models and goodness of fit to equilibrium data

Isotherm	Parameters			R^2
Langmuir	q _m (mg/g) 10.48	K _L (L/mg) 0.075		0.8841
Freundlich	n 2.46	$K_{\rm f} (\text{mg/g} \cdot (\text{L/mg})^{1/n})$ 1.73		0.8731
Fowler-Guggen- heim	$q_{\rm m}$ (mg/g)	$K_{\rm FG}$ (L/g)	χ	0.8935
	8.24	0.037	2.43	

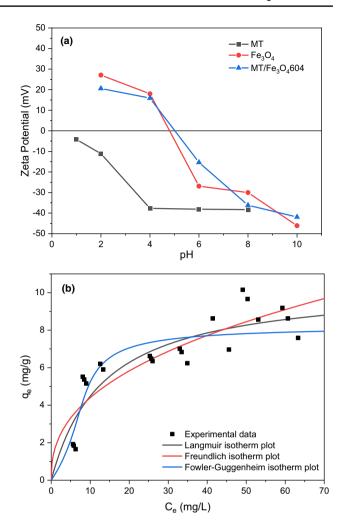


Fig. 7 a Zeta potential plots, b isotherm models

30 mg/L, and within 3 min for 50 and 80 mg/L. The batch method is not well suited for such fast adsorption; the data are not accurate enough for discrimination between kinetic models. Nevertheless, the intra-particle diffusion model that assumes Fickian diffusion in a homogeneous medium with constant boundary conditions was applied to check if

Table 3 Comparison of adsorption capacities of similar adsorbents for NH_4^+

Adsorbent	Adsorption capacity (mg/g)	References	
MT/Fe ₃ O ₄ nanocomposite	10.48	Current study	
MT nano-clay	1.54	[59]	
Natural vermiculite	1.38	[59]	
MT biochar composite	12.52	[58]	
Natural MT	40.4	[15]	



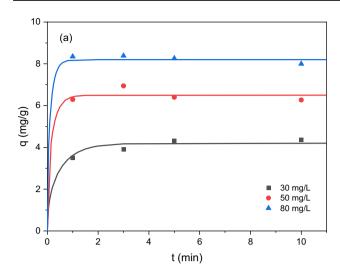


Fig. 8 Ammonium adsorption kinetics. Lines are calculated with Fickian intra-particle diffusion model (Eq. 8)

intra-particle diffusion resistance could explain the results. The loading as a function of time was calculated from Eq. (8)

$$q = q_{eq} \left(1 - \frac{6}{\pi^2} \sum_{j=1}^{\infty} \frac{1}{j^2} \exp\left(-j^2 \pi^2 D' t \right) \right)$$
 (8)

where q and $q_{\rm eq}$ (mg/g) are the amount adsorbed at time t and at equilibrium, and D' (1/s) is the mass transfer parameter that includes the diffusion coefficient and the (unknown) Sauter mean diameter of the particles. The infinite series was truncated at j=30, which is more than sufficient as the series converges rapidly (e.g. below 1e-17 with j=15 at t=0.1 min). As observed in Fig. 8, this model fits reasonably well to the data, suggesting that the intra-particle diffusion is the sole rate-limiting step [60, 61]. The mass transfer parameter D' was found to increase with increasing initial concentration (and thus loading). Values of 0.15 1/s, 0.40 1/s and 0.60 1/s were obtained with initial concentrations 30 mg/L, 50 mg/L and 80 mg/L, respectively. Since ammonium adsorption is strongly nonlinear, this suggests that diffusion may take place also in the adsorbed phase.

Ammonium removal from authentic stormwater

Application of the adsorbent to remove ammonium from an authentic stormwater was studied at laboratory scale. The operating conditions and suitable adsorbent dosing were first determined in preliminary tests.

The adsorbent dosage was varied from 1 to 5 g/L, studied using 50 mg/L NH₄⁺ solution, shaking at 300 rpm for 120 min at 25 °C. The removal efficiency of NH₄⁺ increased with increasing dosage due to the increased

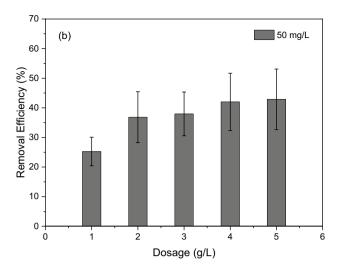


Fig. 9 Effect of adsorbent dosage on ammonium removal efficiency

active sites for NH₄⁺ adsorption which increased the uptake amount. As shown in Fig. 9, the removal efficiency was improved by more than 10 percentage points from 1 to 3 g/L, but less than 5 percentage points from 3 to 5 g/L. This is typical for Langmuir-type adsorption and originates from the decrease in the equilibrium concentration when the adsorbent dosage increases. Considering the cost and removal efficiency, 2.5 g/L was selected as the optimal dosage for a single-contact adsorption process; this was used in the subsequent adsorption studies.

The adsorption efficiency of MT/Fe₃O₄604 was investigated for real stormwater collected from the landfill factory Metsäsairila Oy in Mikkeli, Finland, on August 19, 2019. The sample was filtered and used as a working solution directly for adsorption at conditions of 2.5 g/L dosage, shaking at 300 rpm for 1 h at 25 °C. The contents of the stormwater were examined by ICP-OES for Na, Mg, Al, K, Ca, Cr, Mn, Fe, Co, Ni, Cu, and Zn; all these elements were detected except Cr and Co, which were under the detection limit.

 $\mathrm{NH_4}^+$ removal efficiency reached 64.2% as shown in Fig. 10. Simultaneously, the concentrations of Mg, K, and Ca in the stormwater were reduced significantly. Heavy metals, including Mn, Ni, Cu, and Zn, were diminished to zero or nearly zero. Na as well as a small amount of Al were released by the adsorbent, which confirms the role of ion exchange mechanism. As previously discussed, Fe leaching was low since the pH of stormwater was 6.54. Overall, the new adsorbent recovered $\mathrm{NH_4}^+$ well in the presence of other metallic ions during treatment of stormwater. The additional benefit of eliminating heavy metals such as Mn, Ni, Cu, and Zn to extremely low concentrations (in current case \leq 0.1 mg/L, which is lower than the detection limit of ICP-OES) is notable.



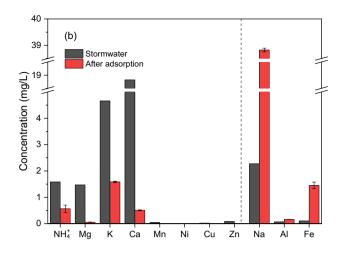


Fig. 10 Removal of ammonium and other cations from authentic stormwater using adsorbent MT/Fe₃O₄604 (solid-to-liquid phase ratio 1:400)

Potential of reusing NH₄⁺ loaded adsorbents in REE recovery

To improve the economics of adsorptive ammonium removal from stormwater, we studied the reuse of the spent (ammonium loaded) adsorbent in a secondary application. Utilising the ammonium ion-loaded adsorbents for selective recovery of valuable elements avoids the generation of chemical waste from the regeneration of adsorbents. To this end, the adsorbents were first loaded with 50 mg/L NH₄⁺ solution; then, the uptake of REEs from aqueous solution was studied. The REEs used for the study include scandium (Sc), yttrium (Y), and all the lanthanides except promethium (Pm). The adsorption study was conducted at conditions of 2.5 g/L dosage, 20 mg/L working solution, shaking at 300 rpm for 1 h at 25 °C.

As observed in Fig. 11, the used MT/Fe₃O₄ nanocomposite achieved almost 100% removal efficiency for all 16 REE ions in the single-REE containing solutions. In the mixture of all REEs, the adsorbent showed selective affinity towards Sc^{3+} . The results indicate that the spent (ammonium loaded) MT/Fe₃O₄ nanocomposite possesses the potential for REE recovery as a secondary application, especially for selective adsorption of Sc3+ among other REEs. However, regeneration of the adsorbent to recover REEs was not studied.

Conclusions

In this study, the nanocomposite of montmorilloniteanchored magnetite was synthesised and studied for the removal of ammonium in stormwater. FTIR, XRD and XPS confirmed the successful loading of Fe₃O₄ onto MT. The Fe₃O₄ enhanced the adsorption of NH₄⁺ and provided

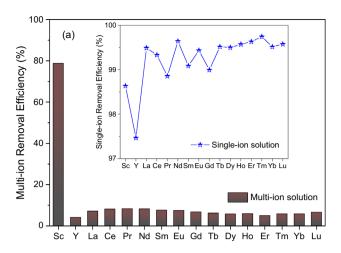


Fig. 11 Removal efficiency of spent (ammonium loaded) MT/ Fe₃O₄604 for recovery of REEs from aqueous solution

magnetic features to MT, which accelerated the separation of the adsorbent from water. It was observed that the adsorption was influenced by dosage, contact time, initial concentration, and pH. The adsorption behaviour of NH₄⁺ was well expressed by pseudo-second-order kinetics and the Temkin isotherm model. Both ion exchange and electrostatic interaction contributed to its affinity for NH_4^+ . The adsorbent MT/Fe₃O₄604 was able to treat real stormwater, reducing the NH₄⁺ as well as heavy metal contents. Moreover, the ammonium-loaded nanocomposite possesses the potential for REE recovery as a secondary application, especially for the selective adsorption of Sc³⁺ among other REEs. Further study regarding the desorption of Sc³⁺ could be conducted to affirm and maximize the recovery potential. This study suggests that MT/Fe₃O₄ nanocomposites are potential adsorbents for stormwater treatment regarding NH₄⁺ recovery. Furthermore, the nanocomposites could be utilised as functional material in a membrane or in polymer beads that are better suitable for large scale water treatment operations than powders [62, 63].

Appendix A. Supplementary data

Supplementary data associated with this article can be found in the online version.

Supplementary Information The online version contains supplementary material available at https://doi.org/10.1007/s41204-021-00151-y.

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Declarations

Conflict of interest On behalf of all authors, the corresponding author states that there is no conflict of interest.

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