### **ORIGINAL PAPER**



# Multi-Objective Metaheuristic Algorithm for Optimal Distributed Generator Placement and Profit Analysis

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#### Abstract

The drastic growth in power demand and the high capital investment for infrastructure developments, power system utilities are forced to concentrate on improving the reliability and efficiency by integrating Distributed Generators(DG) to the existing grid. The integration of DG to grid faces many challenges. This paper presents the implementation of an algorithm based on multiobjective function for optimal placement of Distributed Generator(DG), which is one among the major challenges in DG integration. Optimal placement and sizing of Distributed Generator (DG), is done with the objective of loss minimization and maximization of loading capability without affecting voltage stability of the system. Flower Pollination Algorithm (FPA), which is a metaheuristic algorithm is used to solve this problem, since this algorithm is based on updating tuning parameters to obtain the most effective solution. The major expenditure in DG integration, as installation costs, operational cost and maintenance cost are taken into consideration and a cost based analysis is also carried out in this work to check the feasibility of optimum placement and sizing in a DG interconnected system. The benefits due to DG placement at optimum location with suitable size are the loss reduction and cost reduction. The performance of the proposed algorithm is tested on standard IEEE 33 bus and IEEE 69 bus systems. The effectiveness of the proposed algorithm is also tested on a 301 bus distribution system of Kerala State Electricity Board (KSEB). The test results are compared with other metaheuristic methods like Discrete Artificial Bee Colony algorithm (DABC) and Particle Swam Optimization (PSO) algorithm.

Keywords Distributed Generation · Optimal Placement · Flower Pollination Algorithm · Loadability Index

# Introduction

In an attempt to improve the infrastructure to meet the ever increasing demand of power and operate power system economically, there is a need to implement Distributed Generators (DGs) in the existing system. The power utilization and power production are done at the distribution side in DG interconnected power system. As DGs are supplying power from renewable energy resources, to get the maximum benefits from

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G. R. Bindu bgr100@gmail.com DG installation optimal handling of these resources are essential. The optimal DG placement problem is done by many researchers with the objective of loss minimization, voltage profile improvement and to maintain the stability. Higher losses cause breaking of thermal limits and voltage limits in the conductor material. In distribution system more emphasis is given to improve the maximum loadability limit rather than thermal limit.

One among the challenges in DG placement is the determination of suitable location and size of DG. Most of literature discusses this problem with loss minimization techniques [1, 2]. Another DG sitting and sizing method using Genetic Algorithm is discussed in [3]. Voltage stability improvement by placing DG is proposed in [4] and voltage stability and thermal limits to improve the loadability of the system is discussed in [5]. The loadability maximization method using continuation power flow is detailed in [6] and the maximum saving approach due to capacitor placement in [7]. The optimum DG placement algorithm proposed with maximization of system loadability is also considered in [8].

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The discussed techniques of minimization of loss and improving voltage stability can be solved with many techniques such as analytical method like Linear Programming (LP) and heuristic methods like Genetic Algorithm (GA), Simulated Annealing (SA) and Particle Swam Optimization (PSA). Metaheuristic approaches based on analytical method are faster and easy to implement but its drawback is the difficulty in solving non-convex problems. The difficulties in previous algorithms and the nonconvexity are solved in this method [9]. But the disadvantage is that the problem concentrates only on loss minimization.

Optimal DG placement Problem solved in [10, 11] discuss the problem as a single objective one by Flower Pollination Algorithm. The proposed method discussed in this paper views the problem as a multi-objective [12, 23] one to minimize the losses with DG interconnection along with system loadability maximization. To attain this Flower Pollination Algorithm (FPA), which is based on the pollination process in the flowers is used [21]. It is proved that this algorithm is better in convergence compared to genetic algorithm and particle swarm optimization since it updates tuning parameters to obtain the most effective solution.

Most of the research in the area of DG interconnection to an existing grid mainly concentrates on the minimization of losses [22]. However the related profit maximization is not addressed. This paper also discusses a cost based analysis on DG interconnected systems. The analysis is done by considering generation, operating, investment and maintenance costs including the inflation rate and interest rate for a period of 10 years [13]. After the placement of DG, the energy purchase from utility can be reduced, and benefits due to loss minimization can be taken in to account.

The organization of the paper is as follows: In section II, the effect of DG on improving voltage stability and loadability is explained by the formulation of the problem as a multiobjective one which minimizes the losses. In section III, the implementation of the proposed method of DG placement algorithms with test results and discussions explained. Section IV details the cost analysis and incurred profits in test systems. Section V concludes the works.

### Formulation of Problem

### **Objective Function**

The proposed method aims at placing DG at suitable location with suitable size with the objective of loss minimization and loading capability maximization. Hence the problem is framed as a multiobjective optimisation problem and fitness as in (1). Minimize.

 $f(P_{loss}, \lambda_{\max}) = a(P_{loss}) + b(\lambda_{\max})$ (1)

where,  $P_{loss}$  is real power loss,  $\lambda_{max}$  is maximum loadability limit a, b are multiplication factors [0,1], where (a + b) = 1.

The loadability  $(\lambda)$  is the ability of the system to handle maximum load connected, without breaking the system operation [15]. Here the voltage at each bus is the operating constraint and line current limits are system constraints.

Real power loss is given by (2)

$$P_{loss} = \sum_{i=1}^{NB} I_i^2 R_i \tag{2}$$

Reactive power loss is given by (3) as

$$Q_{loss} = \sum_{i=1}^{NB} I_i^2 X_i \tag{3}$$

where, I <sub>i</sub> is current through the i<sup>th</sup> transmission line, R <sub>i</sub> is resistance in the i<sup>th</sup> transmission line, X <sub>i</sub> is reactance of the i<sup>th</sup> transmission line and NB is total number of branches.

Substituting for current in eqs. (2) and (3) the total real power loss and reactive power loss in the feeders of the given system are given by the (4) and (5).

Real power loss is given by

$$P_{loss} = \sum_{i=0}^{NB} \frac{P_{i,j}^2 + Q_{i,j}^2}{|V_i^2|} R_{i,j}$$
(4)

Reactive power loss is given by

$$Q_{loss} = \sum_{i=0}^{NB} \frac{P_{i,j}^2 + Q_{i,j}^2}{|V_i^2|} X_{i,j}$$
(5)

The objective function is formulated by considering the total losses in the system by connecting DG at optimum locations.

 $P_{loss}$  in (1) becomes  $P_{DGloss}$  in (6) when DG is integrated into the existing system.

The actual loss [9] in the DG interconnected system is calculated as (6)

$$P_{DGLoss} = \sum_{i=0}^{n-1} \frac{\left(P_{i,j} - P_{DG,j}\right)^2 + \left(Q_{i,j} - Q_{DG,j}\right)^2}{|V_i|^2} R_{i,j}$$
(6)

where,  $P_{DG,j}$ ,  $Q_{DGj}$  are the capacity of the DG unit or active and reactive power injections at bus j.

### Constraints

The inequality constraints are given by voltage constraint, line current limits and size of DG given by (7), (8) and (9).

Voltage constraint is that the voltage in each bus should be maintained within limits

$$V_{i\min} \le V_i \le V_{i\max} \tag{7}$$

Size of the DG should also be maintained within the given limits

$$S_{DG\min} \le S_{DG} \le S_{DG\max} \tag{8}$$

Current limits must be less than the maximum fault current rating of switch gear.

$$I^{i}_{\min} \leq I^{i}_{Limit} \leq I^{i}_{\max} \tag{9}$$

where I limit is i<sup>th</sup> branch current limit.

Position of DG should be such that  $DG_{pos} \neq 1, 1$  is the slack bus.

The other constraints for the calculation of fitness function are the variations in load to maximize the loadability [8], as in Fig. 1. The actual power load and reactive power load are increased in steps of 1% and new values are calculated as in (10) and (11)

$$P_{load} = P_0 \times \lambda \tag{10}$$

$$Q_{load} = Q_0 \times \lambda \tag{11}$$

where,  $P_0$  and  $Q_0$  are the initial actual power load and reactive power load respectively and loading factor is  $\lambda$ .

The kilo Volt Ampere Margin to Maximum Loadability (KMML) [15] is calculated in (12)

$$KMML = S_{Load}(\lambda_{\max} - 1) \tag{12}$$

where,  $S_{Load}$  is base MVA load and is given by (13)

$$S_{Load} = \sqrt{\sum_{i=2}^{NB} P_i^2 + \sum_{i=2}^{NB} Q_i^2}$$
(13)



Fig. 1 Variation of voltage with loading Factor [15]



Fig. 2 33-Bus distribution test system

### Identification of Maximum Loadability

The lambda max is the factor of load which can be added to the power system without violating the voltage limit. It is identified using the Maximum Loadability Index (MLI) [8]. Following are the steps involved,

- Step 1: Read the bus data, line data, and accuracy for power flow.
- Step 2: Set the lambda values for 1 to 10 in steps of 0.01 factor. Calculate the new real power load and reactive power load as in (14) and (15).

$$P_L = P_{Lold} + P_{Lold} \times \lambda \tag{14}$$

$$Q_L = Q_{Lold} + Q_L old \times \lambda \tag{15}$$

Here and  $Q_L$  are the new real and reactive loads applied,  $P_{Lold}$  and  $Q_{Lold}$  are the old real and reactive loads in the power system.

Step 3: Perform the power flow using new load data. Identify minimum voltage, power loss and Maximum Loadability Index (MLI) value (calculated as per equation in [16]), which must be greater than 1 if the bus system is not weak.



Fig. 3 IEEE 69 Bus distribution test system

Test System 33	Bus Radial Syste	3m		69 Bu	is Radial Syste	in the second seco		301	Bus Radial Sys	tem
CC Br	ase Case 1 ase1) c	FPA as single objective [10]	Multiobjective method (with	e FPA Base DG) (case]	Case F l) o	<sup>7</sup> PA as single M bjective [10] IT	Aultiobjective FF nethod (with DG	PA Bas	e Case sel)	FPA (with DG)
Active power	210.9	89.30	49.49	22	4.95 7	1.9	50.79		33.687	23.63
loss (kW) Reactive power	143.01	61.10	36.024	10	2.15 3	96	29.77		1.4268	1.0014
loss (k VAK) Lambda max	3.4	I	4.49		3.21 –		4.6		4.35	5.81
KMML 10		1	15,249	10,29	- 7.87	-	6,775	23,5	517	33,766
NBBV	- 21	I	0		- 6		0	1	148	0
Test System	33 Bus Dis	stribution System			69 Bus Distr	ribution System			301 Bus Distri	bution System
Case 2 (with DG)	DG Placem	lent			DG Placeme	ant			DG Placement	
Method	DABC [1]	FPA as single	e objective[10]	Proposed method (Multiobjective) FPA	DABC [1]	FPA as single objectiv	ve [10] Propo (Mult FPA	osed Method tiobjective)	FPA	
DG Location (Bus Number	r) 32,14	30,13		30,14	61	17,61	61,12	0	127,195	
DG Size (kVA)	2072, 1637	7.1 1240.1817.1		1778.78,943.98	3635.00	1844,513.2	2831	.78,1077.23	99.41,700.16	
Active Power Loss(kVA)	113.15	89.30		49.49	104.86	71.9	50.75	•	23.63	
Reactive Power Loss(KVA	.R) 90.63	61.10		36.024	46.02	36.0	29.77	7	1.0014	

- Step 4: Increment the value and go to step 2 if the (MLI) is greater than 1 and convergence is achieved from power flow.
- Step 5: Else save the values of power loss, voltages and  $\lambda$  as  $\lambda_{\max}$  value. Evaluate Number of Buses Violating the Voltage constraint (NBVV) [16].
- Step 6: Plot the graph between Lamda max values and minimum voltage calculated in step 3.
- Step 7: Display the final results.

### Size of Distribution Generator

In the proposed method the DG is supplying actual power and reactive power to the connected bus. The range of DG sizes considered between 0.1 MVA to 5 MVA and two DGs are placed as in [8] for comparative study. The power factor assumed is 0.95 for all the systems. Real power and reactive power given by (16) and (17),

$$P_{DG} = S_{DG} \times \cos\varphi \tag{16}$$

$$Q_{DG} = \sqrt{S_{DG}^2 - P_{DG}^2}$$
(17)

where,  $P_{DG}$  is actual power of DG,  $Q_{DG}$  is reactive power of DG and  $S_{DG}$  rating of DG.

### **Flower Pollination Algorithm**

**Fig. 4** Voltage in pu at each bus (33 bus distribution system)

The Flower Pollination Algorithm (FPA) is formulated by Xin-She Yang in 2013. [14]. The different steps of algorithm given below.

- Step 1: Initialize the population number (n), total iteration, search probability and dimensions. (Here 4 dimensions in the format of [DG location-1 DG size-1 DG location-2 DG size-2] which has 4 columns of population. Here population size is taken as 40. So, the number of flowers considered here is 40 and the total of [40X4] is the population considered, total iteration is 100 and switch probability is 0.8.
- Step 2: Evaluate the fitness function (1) and find the initial global best flower  $(g_*)$ .
- Step 3: While the maximum iteration is not reached perform the global pollination operation using  $X_i^{t+1} = X_i^t + L(g_*-X_i^t)$  if the probability value is less than any random value between [0, 1]. Here 'i' is the population number and 't' is iteration number. X is the 4dimension population matrix and L is the levy's distribution.
- Step 4: If the random value is greater than the probability value then perform the local pollination using  $X_i^{t+1}$

 $= X_i^t + \in \left(X_j^t - X_k^t\right) \text{ here } X_j \text{ and } X_k \text{ are the pollens}$ of different flowers of the same type. is the uniform distribution between [0, 1].

- Step 5: Calculate the new fitness values from (1) using new pollens from the step 3 or step 4.
- Step 6: if the new fitness is less than the old then modify them in the population
- Step 7: find the global best g\*
- Step 8: iteration count incremented and go to step 3.
- Step 9: If maximum iterations reached, display the results.







# **Implementation of FPA in Test Systems**

## **Test systems**

(69-Radial bus system)

The proposed algorithm is applied on 3 phase system of 12.66 kV standard IEEE 33 bus a distribution system and IEEE 69 bus distribution systems [15]. The type of DG chosen is a Type 2 system, injecting actual power and reactive power. The systems are assumed to be operating at a constant power factor of 0.95. Figure 2. shows the line diagram of a 33bus radial distribution test system consisting of 33 buses and 39 line segments with a base load of 4369.35kVA. 69 bus system shown in Fig.3. has 76 line segments. The base case load is

4659.67kVA for this system and the results for both the systems are tabulated in Table 1 and Table 2.

# Real system (KSEB)

The future demands of power system will be met mainly by integrating DGs. Since the major source of power in the state of Kerala is hydroelectric power plants and are also dependent on climatic conditions. As an initiative by Ministry of New and Renewable Energy Sources(MNRES), Kerala State Electricity Board (KSEB) has also started to promote consumers to install roof top solar panels and wind turbines. Hence a typical sample 301





bus radial distribution feeder is considered for the validation of the proposed method. The system consists of 11 kV feeders with base MVA of 100, with 301 buses and 302 lines. The base case load is 700.6kVA. The results are tabulated in Table 1 and Table 2.

### **Results and Discussion**

The algorithm is applied to different systems and the results without DG and with DG are shown in Table 1. There are significant improvement in loss reduction and maximum loadability with the integration of DGs. The results of the multiobjective FPA is compared with Discrete Artificial Bee Colony optimization (DABC) technique [8], Modified Flower Pollination Algorithm(MFPA) [10] and are tabulated in Table 2.

The result indicates that the proposed method utilizing FPA performs better. For sizing and placement of DG for 33-bus system, 2 DGs with rating of 5 MW are connected to the system. The real power losses reduce from 113.15 kW [DABC], 89.30 kW[MFPA] to 49.49 kW. Similarly reactive power also gets reduced from 90.63kVAR[DABC], 61.10Kvar [MFPA] to 36.024 kVAR with proposed method.



**Fig. 8** Voltage in pu at each bus (301-Radial bus system)

Fig. 9 Lambda max versus minimum voltage in pu (301-Radial bus system)



In case of 69-bus system two DGs are connected to the system with 5 MW capacity. The generation from each DG are 2831.78 kW and 1077.23 kW. The real power losses reduced from 104.86 kW [DABC], 71.9 kW [MFPA] to 50.79 kW and reactive power reduced from 46.02kVAR[DABC], 36.0 kVAR[MFPA] to 29.77 kVAR. The DGs are placed at bus 61 and 12 there is considerable reduction in losses as shown in Table 2. The added advantage of the loss reduction in proposed method is that extra loads can be connected in the system, thus attaining the objective of load maximization.

Thus the optimal placement and sizing by considering losses and maximization of loadability limit is obtained in the proposed method.

Along with DG placement the voltage profile of the system is ploted for all the buses. The variation of minimum voltage with lambda maximum values are obtained for the minimum voltage bus. It is seen that the voltage profile got improved with the interconnection of distributed generators. Figure 4. and Fig.6 shows the voltage profile graphs. The KMML value for 33 bus and 66 bus systems are drastically incressed in FPA compared to base case due the loss reduction.

The number of buses exceeding or Violating Voltage limits(NBVV) are 21 for 33 bus and 9 for 69 bus systems with no DG. The lodability margin improvement is shown in Fig.5 and Fig.7. Thus it is proved that the kilo Voltampere Margin to Maximum Loadability (KMML) also improved with interconnection of DGs in the distribution systems.

The results on real system data also proves that the losses in the system reduce due to the interconnection of DGs. The voltage profile is better and is shown in Fig.8 and Lodability plot is shown in Fig.9. The proposed method performs well in loss minimization, optimal DG selection and loadability margin.

Test System Method	33 Bus Radial system			69Bus Radial system			301 Bus Radial system
	DABC [8]	PSO [13]	FPA	DABC [1]	PSO [20]	FPA	FPA
Installation cost in INR(lacs)	927.275	375	680.69	908.75	375	977.25	199.85
Operating cost in INR(lacs)	6169.5	2490	4528.9	6046.2	2490	6502	1329.7
Maintenance cost in INR(lacs)	1565.2	634	1149	1533.9.	634	1649.5	337.42
Benefits of reduced loss in INR(lacs)	325.52	435	537	399.67	652	579.54	33.45
Benefit of DG in INR (lacs)	12,339	4990	9057	12,092	4990	13,004	2659.4
Total profit in INR(lacs)	4002.6	1937.94	3236.5	4003.3	2137.19	4454.8	825.89

 Table 3
 Cost Analysis of Proposed Method [17–19]

### **Cost analysis**

### Major expenditure in DG installation

The cost of installation, cost of operation and maintenance cost are the major expenditure involved while adding DGs in an existing system [13]. The mathematical modelling done by (18) to (21).

### Installation cost of DG (IC)

The installation cost includes the expenditure for site investigation, construction, equipment monitoring and cost of DG as in (17)

$$IC = \left(DG_{size}^{1} + DG_{size}^{2}\right) \times DG_{cost}^{IC}$$

$$(18)$$

where,  $DG_{size}^{1}$ ,  $DG_{size}^{2}$  are optimal selected DG sizes in MW and  $DG_{cost}^{IC}$  is DG investment cost in INR.

### Operating cost of DG (OC)

$$OC = \left( DG_{size}^{1} + DG_{size}^{2} \right) \times DG_{cost}^{oc} \times OT \times \beta$$
(19)

where, $DG_{cost}^{OC}$  is DG operating cost in INR and OT is total time of operation in hours

$$\beta = \sum \left(\frac{1 + IF}{1 + IR}\right)^t \tag{20}$$

where,  $\beta$  is present worth factor, IF is inflation rate, IR is interest rate and 't' is the duration in years as 1 to 10.

#### Maintenance cost (MC)

This cost comes as yearly cost including the mechanical and electrical cost of renovation and given in (21)

$$MC = \left(DG_{size}^{1} + DG_{size}^{2}\right) \times DG_{cost}^{IC} \times IC \times \beta \times MC_{ratio} + 10,000$$
(21)

where MC  $_{ratio}$  is ratio of the maintenance cost to investment cost and is taken as 20% of DG investment cost per year.

### **Benefit analysis**

With DG installation the power taken from the grid is lesser and more power is injected to the grid. The additional benefit due to reduction in loss is given in (22).

Benefit due to loss minimization  $(B_L)$ 

$$B_L = \left(P^b_{loss} - P^{DG}_{loss}\right) * EP_G * OT * \beta$$
(22)

where,  $EP_G$  is the price of power purchased from grid,  $P_{lossb}$  is base case real power loss in kW and  $P_{loss}^{DG}$  is real power loss with DG placement in kW.

Benefits due to not using grid power

$$B_g = \left( DG_{size}^1 - DG_{size}^2 \right) \times EP_G \times OT \times \beta \tag{23}$$

$$Profit = (B_L + B_g) - (IC + OC + MC)$$
(24)

(23) gives the profit which is the difference between the total cost and benefit.

Profit based feasibility of DG placement for long term planning with cost analysis is carried out. Analysis is done for 10 years period and the total operating hours of the DGs are calculated as 7884 h. DG units used are assumed as non operating for a period of 10% of the total operating period. The rate of interest is 12.5% and inflation rate is 9% for this case. The total purchase cost of the power from grid is taken as 5/kWh INR [13]. The cost data are given as

Cost of installation with DG, ICi =  $25 \times 10^6$  /MW, Operational cost, with DG, OCi =  $2.5 \times 10^3$ /MWh Maintenance cost with DG, MC<sub>DG</sub> = (10,000 + 20% of DG installation cost)/year Rate of Interest IR = 12.5% Rate of Inflation rate, IF = 9% Planning period, *n* = 10 years.

Table 3 shows the results of cost analysis of proposed DG placement method compared to [8, 13]. Though the cost incured in the proposed method seems to be high compared to PSO, this increase can be attributed to the fact that in the proposed method two DGs are used while the PSO method uses one DG. This reflects in the installation cost, operating cost and mainteance cost naturally. In comparison with DABC method which also uses two DGs the proposed method clearly shows an improvement in the overall profit. In 69- bus system the total profit for the proposed method is higher than the DABC method and PSO method. It indicates that as the number of nodes increases, FPA method seems to be the most suitable one. The test results on 301-bus distribution system profit is calculated as 825.89lacks INR for an operating period of 10 years.

# Conclusion

The DG systems there optimal placement and sizing form a major area of research. This paper presents an optimal DG placement method for loss minimization along with maximization of system loadability using Flower Pollination Algorithm. The application of this algorithm proved that there is a major reduction in power loss in the proposed systems. The loadability margin also improved with the integration of DGs in the existing system. The benefit of this method is that the existing infrastructure can be utilized by increasing the loadability rather than providing extra lines in the system, thereby improving the efficiency and reliability of the system. Further cost analysis with DG placement at optimum locations and with suitable size proves that the method is beneficial. The advantage is that the voltage stability limits are also maintained with no buses violating the constrained limits which show better power quality of system.

The comparison results show the superiority of the algorithm with existing metaheuristic algorithms. The validation of the algorithm in the real system proves that this method can be effectively applied in real DG interconnected distribution systems. For long term planning with DG, feasibility based on cost analysis gives better profit.

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