



A tough, resilient, and fluorinated solid-electrolyte interphase stabilizing lithium metal in carbonate electrolytes

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ABSTRACT The unstable interface between lithium metal anodes and carbonate-based electrolytes is a key challenge limiting the cycling lifespan of high-energy lithium metal batteries. Here, a resilient artificial solid electrolyte interphase (RASEI) was designed by regulating poly(hexafluorobutyl acrylate) (PHFBA) matrix with the benzene-containing bisphenol A ethoxylate dimethacrylate (BAED) crosslinker to address this issue. The rigid BAED molecule can finely tune the flexible PHFBA matrix, enabling superior resilience from 600% elongation to 90% compression with a high Young's modulus of over 2 MPa. RASEI with these characteristics can accommodate large volume changes of lithium metal and ensure the intimate contact between the lithium metal and the RASEI during battery operation. Consequently, it facilitated homogeneous lithium deposition while mitigating parasitic side reactions. Thanks to the tough and resilient nature of the fluorinated RASEI, the long-term cycling of Li||Li symmetric cells can be achieved for over 500 h at 1 mA cm⁻² and 1 mAh cm⁻². The following post-mortem of cycled Li metal reveals that Li dendrite growth is effectively inhibited. Furthermore, the NCM811 pouch cell with a high cathode loading of 20 mg cm⁻² exhibits a capacity retention of over 85% after 200 cycles at 1 C.

Keywords: lithium metal anode, carbonate electrolytes, resilient ASEI, high cathode loading

INTRODUCTION

Lithium metal anode, with a high theoretical specific capacity (3860 mAh g⁻¹) and the lowest redox potential (−3.04 V vs. the standard hydrogen electrode), has been considered as the “holy grail” of higher energy density batteries [1,2]. In addition, carbonate electrolytes demonstrate anodic stability at high potentials, which makes them promising candidates for matching with high-voltage cathodes, such as LiNi_xMn_yCo_{1-x-y}O₂ and LiCoO₂, to achieve higher energy density [3,4]. However, studies have delineated that conventional carbonate electrolytes may not be apt for lithium metal batteries, as they readily undergo reactions with lithium metal anodes, engendering unstable solid-electrolyte interphases (SEIs) [5–7]. Unstable SEIs lead to uncontrolled lithium dendrite growth and limited Coulombic efficiency during repeated plating/stripping processes, which remain key

challenges limiting their practical application [8–10].

Up to now, plenty of strategies have been proposed to solve the issue of lithium dendrites, such as electrolyte modification [11–13], separator modification [14–16], and artificial solid electrolyte interfaces (ASEIs) [17–20]. Among these strategies, ASEIs have been extensively explored to enhance the stability of lithium metal anodes. ASEIs can be categorized into inorganic and polymeric interphases [21–23]. Inorganic ASEIs such as LiF [24,25], LiPON [26], Al₂O₃ [27], and others [28–31] exhibit high mechanical strength or excellent ionic conductivity, which can effectively prevent the growth of dendrites. However, their brittle nature makes them prone to fracturing and delamination during lithium stripping/plating, especially under bending and stretching. Loss of contact with the lithium anode leads to uncontrolled dendrite growth and rapid capacity fading. Meanwhile, conventional polymeric ASEIs with narrow elasticity limit typically undergo plastic deformation, which cannot sustain conformal interfacial contact with lithium metal anodes. In contrast, high elastic artificial solid electrolyte interfaces using rubbery polymer matrices exhibit superior flexibility and fracture resistance under large deformation [32–36]. The elastic ASEIs accommodate huge volume changes of lithium metal, ensuring sustained intimate contact with the lithium substrate. Resilient ASEIs (RASEIs) have great potential for lithium metal protection, but there are still few relevant reports.

RASEIs necessitate not only favorable mechanical properties but also specific characteristics including the resistance to electrolyte degradation and facilitation of ion transport at interfaces. A common approach to obtain elastic materials is by introducing an appropriate quantity of multifunctional cross-linking agent into the monomer and achieving cross-linking. By carefully designing the monomers, cross-linking agents, and reaction conditions, it becomes possible to precisely control the physical and chemical properties of the final polymer to better meet diverse application requirements. Extensive investigations have established that fluorinated acrylates exhibit superior electrochemical and thermal stability compared with their non-fluorinated counterparts, thus making them as promising monomers [37–39]. Moreover, the incorporation of fluorine induces the formation of interfacial LiF, which effectively reinforces the integrity of the electrode–electrolyte interface and contributes to extending the battery's lifespan [40,41]. Among various fluorinated acrylates, hexafluorobutyl acrylate offers the advantages of

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being readily available and cost-effective. Furthermore, the inclusion of benzene rings in the cross-linking agent significantly enhances the strength, stiffness, and corrosion resistance of the polymer network.

In this study, we propose a RASEI coating layer on lithium metal (RASEI@Li) to improve the interfacial stability of lithium metal anodes against carbonate-based electrolytes. The RASEI was synthesized by cross-linking hexafluorobutyl acrylate (HFBA) by the bisphenol A ethoxylate dimethacrylate (BAED) *via* an instant photocuring process. The inclusion of a benzene-containing crosslinker regulated the mechanical properties of poly(hexafluorobutyl acrylate) (PHFBA). Remarkably, the RASEI with only 2% BAED content exhibits exceptional resilience, capable of withstanding elongations of up to 600% and compressions of up to 90%, while maintaining a high Young's modulus exceeding 2 MPa. On the one hand, the elasticity of the RASEI coating allows it to stretch and deform alongside the expansion and contraction of lithium metal, thereby minimizing the cracking and delamination. On the other hand, the RASEI coating effectively hinders the dendrite formation by mechanically obstructing the lithium penetration. Thus, the elastic coating with a unique combination of strength, flexibility, and stability, makes it a highly suitable protective layer for high-performance lithium metal anodes.

As a result, the Li||Li symmetric cells incorporating the RASEI@Li demonstrate remarkable cycling stability with a duration exceeding 500 h, under 1 mA cm^{-2} , 1 mAh cm^{-2} in carbonate-based electrolyte. Additionally, the cell with a high-nickel NCM811 cathode ($\sim 20 \text{ mg cm}^{-2}$) exhibits an exceptional capacity retention rate of 90% after 190 cycles. Furthermore, a practical pouch cell, coupled with the commercially available high-nickel cathodes and RASEI@Li anode, displays an impressive capacity retention of over 85% over 200 cycles under 1 C discharge conditions.

RESULTS AND DISCUSSION

As shown in Fig. 1a, the RASEI was prepared by cross-linking HFBA and BAED *via* an instant photocuring process, called P(HFBA-BAED). Notably, HFBA is chosen as the primary monomer due to its F-containing functional group, which aids in achieving a more stable electrode-electrolyte interface. In addition, BAED molecules contain benzene rings that significantly enhance the rigidity of the polymer. The precursor solution was coated on the surface of lithium metal using a simple tape-casting technique, and then cured under ultraviolet light to obtain RASEI@Li.

The utilization of UV curing enables the instant reaction, improving production efficiency. The homogeneous precursor solution can be entirely cured by exposing it to a UV lamp for 1 min (Fig. 1b). To verify the cross-linking reactions, Fourier transform infrared (FTIR) spectroscopy was conducted. In the FTIR spectra (Fig. 1c), a clear adsorption peak can be detected at $\sim 1637 \text{ cm}^{-1}$ corresponding to the vibration of C=C of the FBA monomer and BAED, while this group cannot be observed in the P(HFBA-BAED). The disappearance of the C=C peak verifies the success of this polymerization reaction. From the X-ray photoelectron spectroscopy (XPS) results (Fig. 1d), a pronounced fluorine (F) signal is observed on RASEI@Li, indicating the presence of the characteristic F element stemming from the P(HFBA-BAED) coating. The emergence of this distinct F signature peak provides the evidence that the P(HFBA-BAED)

layer was successfully fabricated onto the lithium metal substrate. Top-view scanning electron microscopy (SEM) image of RASEI@Li is shown in Fig. 1e, where the surface of RASEI@Li is smoother with coating compared with bare Li which has many scratches and pits (Fig. S1). Furthermore, energy-dispersive spectroscopy (EDS) analysis confirmed the uniform distribution of the F element on the lithium metal surface with the elastic coating, providing additional support for the uniformity of the coating (Fig. 1f). Even without adding lithium salts, the fluorine element was still evenly distributed (Fig. S2). Cross-sectional SEM image (Fig. 1g) shows that the elastic coating adhered to the lithium metal with a thickness of $< 3 \mu\text{m}$. In addition, top-view atomic force microscopy (AFM) image provides more detailed evidence for the evenness of lithium metal with elastic coating. As exhibited in Fig. 1h, the surface of RASEI@Li is very smooth with a height variation of about 7.9 nm. Moreover, the possibility of large-scale manufacturing was demonstrated by processing larger areas of lithium ribbons used for the pouch cell assembly. (Fig. 1i).

A coating possessing high mechanical stiffness and good elastic strength can effectively inhibit dendrite growth and adapt to large volume changes of lithium metal to maintain structural integrity [32]. The elastic coating is cross-linked by flexible HFBA and rigid BAED, whereby the mechanical properties of the elastic coating depend on the proportion of the BAED incorporated into the polymer structure. The difference in the physical properties of the elastic coating was characterized by uniaxial tensile and compression testing.

As depicted in Fig. 2a and 2b, the elastic coating with P(HFBA-2%BAED) demonstrates the ability to withstand 90% compression without undergoing the destruction and subsequently recovered its original shape after unloading. However, cross-linked polymers with 5% or 10% BAED are broken and fail to restore their original shape after the compression (Fig. S3). The uniaxial tensile stress-strain curves of the elastic coating with varying BAED contents (Fig. 2c) reveal that as the BAED content increases, their tensile strength gradually increases while causing a gradual decrease in elongation. The rigid planar structure of the benzene ring can improve the rigidity of the polymer chain, enhance the inter-chain interaction force and improve the material strength. The P(HFBA-0%BAED) without the addition of BAED has a linear molecular structure, exhibiting the good molecular chain segment mobility and outstanding tensile properties, and can stretch up to 16 times itself (Fig. S4). The Young's modulus of the P(HFBA-2%BAED) (2.1 MPa) is approximately 52.5 times higher than that of P(HFBA-0%BAED) (0.04 MPa). It is obvious that adding an appropriate amount of BAED can significantly increase the Young's modulus of the P(HFBA-BAED), and it also has an elongation exceeding 600% without fracture (Fig. 2d). However, upon further addition of BAED, the Young's modulus of P(HFBA-5%BAED) (2.74 MPa) is only 1.3 times as high as that of P(HFBA-2%BAED), and the maximum elongation rate decreased to less than 300%. These results indicate that the BAED content does not always positively correlate with the tensile properties of P(HFBA-BAED). Excessive BAED can damage some of its mechanical performance. To sum up, P(HFBA-2%BAED) exhibits significantly superior mechanical behavior, and therefore represents a promising candidate for the elastic coating.

To assess the chemical stability between the elastic coating and

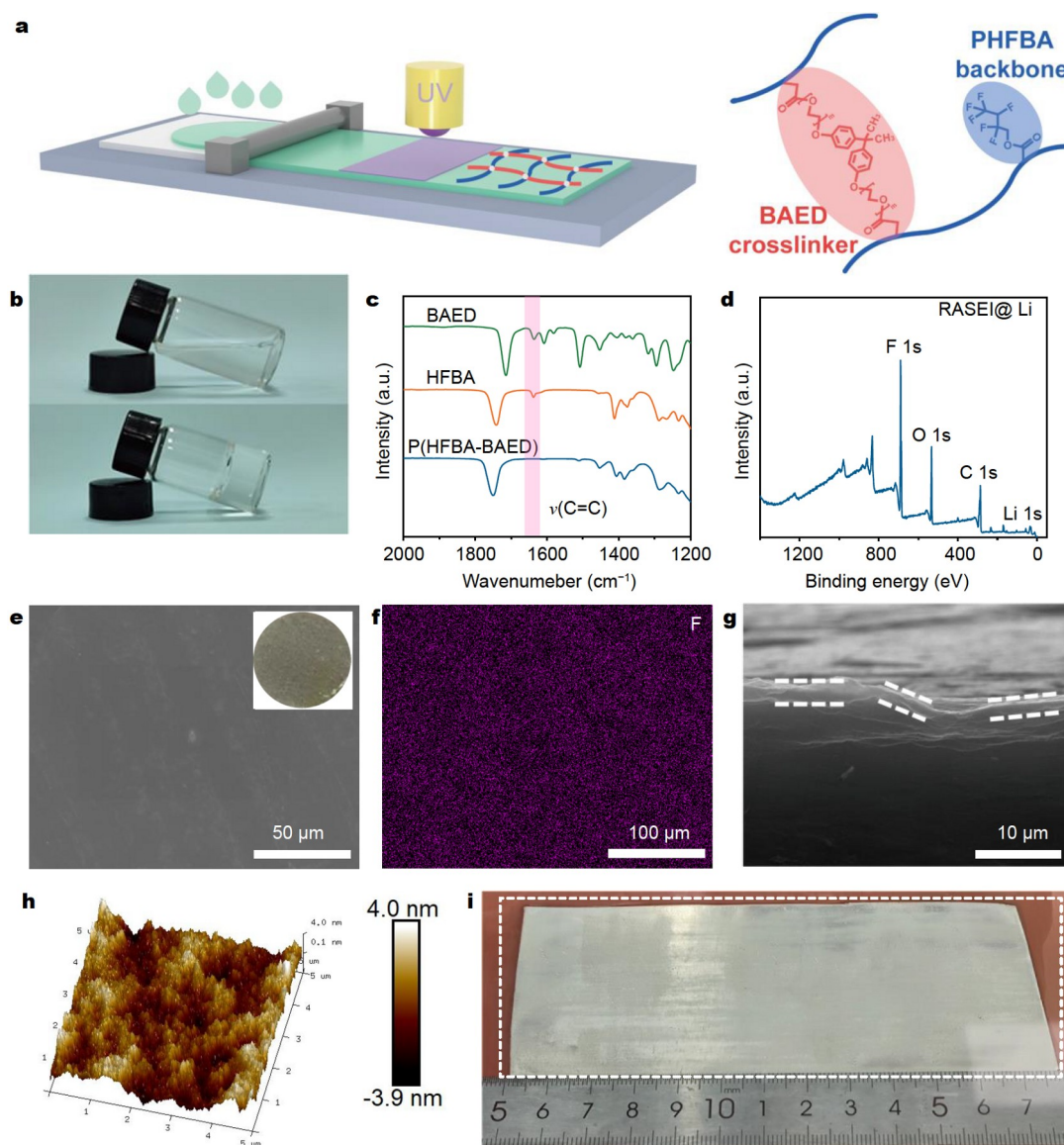


Figure 1 (a) Schematic illustration of the fabrication process of RASEI@Li. (b) Photographs of the P(HFBA-BAED) polymerization process after 1 min of UV curing. (c) FTIR spectra of BAED, HFBA and P(HFBA-BAED). (d) XPS pattern of RASEI@Li. (e) Top-view SEM image of RASEI@Li. The inset in (e) is the photograph of RASEI@Li. (f) EDS elemental mapping image of F for RASEI@Li. (g) Cross-sectional SEM image of RASEI@Li. (h) AFM image of RASEI@Li. (i) Photograph of lithium ribbon with RASEI.

electrolyte, the P(HFBA-BAED) was immersed in a carbonate-based electrolyte, and remained the structural integrity after 30 days (Fig. 2g). The optical photo before P(HFBA-BAED) immersion is shown in Fig. S5. In addition, elastic coating of P(HFBA-BAED) has extremely low electronic conductivity of $1.66 \times 10^{-7} \text{ S cm}^{-1}$ (Fig. S6) and good ionic conductivity of $2.52 \times 10^{-6} \text{ S cm}^{-1}$ (Fig. S7), which gives the SEI its critical passivating functionality to stabilize the highly reducing anode surface.

To evaluate the effectiveness of RASEI in enhancing the interfacial stability of the lithium metal anode, the cycling performance of the symmetric cells in a carbonate-based electrolyte was investigated. Li||Li symmetric cells employing RASEI@Li anodes with different BAED content of elastic coating were assembled to determine the optimal electrochemical performance configuration. As shown in Fig. 3a, the symmetric cell with an elastic coating of P(HFBA-2%BAED) exhibits excellent

cycle stability over 500 h under a high areal capacity of 1 mAh cm^{-2} at a current density of 1 mA cm^{-2} . By contrast, the symmetric cells with bare Li only exhibit significantly reduced cycling life (320 h). Meanwhile, the symmetric cells with the coating of P(HFBA-0%BAED) perform poor cycle stability, and the reason may be that P(HFBA-0%BAED) is too soft and lacks elasticity. In addition, the cycle performance of the symmetric cells with P(HFBA-5/10%BAED) is inferior to those with P(HFBA-2%BAED) (Fig. S8). These findings demonstrate that a coating with a balance of rigidity and flexibility is the most suitable, and P(HFBA-2%BAED) is the optimal formulation thus far. Unless otherwise specified, all ensuing mentions of RASEI will refer to P(HFBA-2%BAED).

The electrochemical impedance spectroscopy (EIS) test result shows that the impedance of Li||Li symmetric cells with RASEI@Li-2% exhibits only a slight increase when compared with bare Li (Fig. S9), suggesting that the coating does not

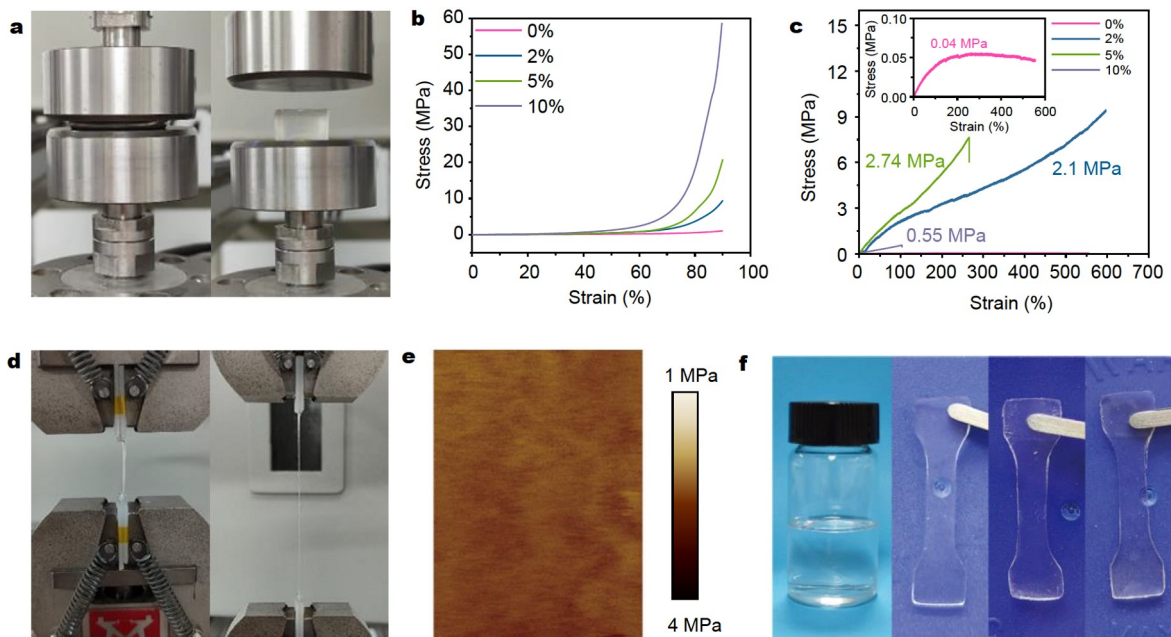


Figure 2 (a) Photographs of P(HFBA-2%BAED) compressed by 90%. (b) Compressive stress–strain curves for P(HFBA-*x*%BAED). (c) The uniaxial stress–strain curves for P(HFBA-*x*%BAED). (d) Uniaxial tensile behavior of P(HFBA-2%BAED). (e) Young's modulus mapping of P(HFBA-2%BAED). (f) Optical images of P(HFBA-BAED) soaked in carbonate-based electrolyte for 10, 20 and 30 days.

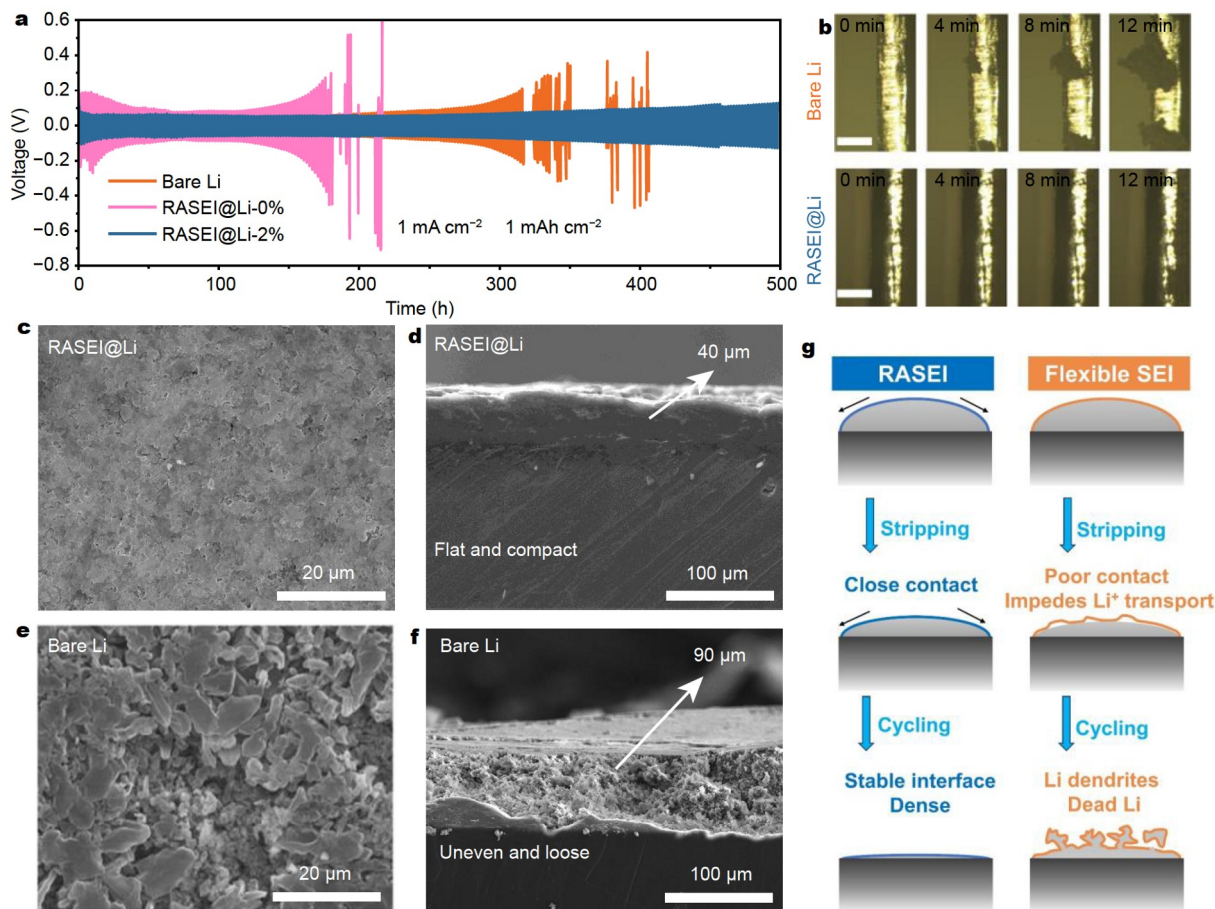


Figure 3 (a) Voltage profiles of bare Li and RASEI@Li-0%/2% anodes in symmetric cell. (b) *In-situ* optical images of Li deposition on bare Li and RASEI@Li in the symmetric cell at different minutes (scale bar, 100 μm). Top surface and cross-sectional SEM images of RASEI@Li (c, d) and bare Li (e, f) after 50 cycles at 1 mAh cm^{-2} and 1 mA cm^{-2} . (g) Li stripping/plating behavior for lithium of RASEI and conventional flexible SEI.

impede the ion transport at the interface. The Li||Li symmetric cells with RASEI@Li also achieved 1300 h stable cycling under conditions of 0.5 mA cm^{-2} of area current density and 1 mAh cm^{-2} of areal capacity, with the overpotential not exceeding 60 mV (Fig. S10). However, for the cells paired with bare Li, the overpotential exceeded 100 mV after 900 h. Moreover, the Li||Li symmetric cells with RASEI@Li also exhibits enhanced cycle performance at an area capacity of up to 4 mAh cm^{-2} compared with the cells with bare Li (Fig. S11). To evaluate the improved stability of the lithium metal interface achieved by RASEI, *in-situ* optical microscopy was used to monitor the Li^+ deposition process. Fig. 3b shows the real-time optical images of the *in-situ* Li deposition on the RASEI@Li and bare Li substrates, recorded at various time intervals (0, 4, 8, and 12 min) at a current density of 2 mA cm^{-2} . The deposition of Li on the surface of bare Li showed non-uniform distribution, accompanied by obvious lithium dendrites, while no visible dendrites were observed in the experiments conducted using RASEI@Li. Due to the excellent mechanical properties of the elastic layer, the growth of Li dendrites on the RASEI@Li surface was effectively suppressed.

To gain further insight into the Li electrodeposition and electrochemical dissolution in bare Li and RASEI@Li, the surface and cross-sectional SEM images of the Li anodes after cycling were acquired. The SEM images revealed that the RASEI@Li surface exhibited a flat and compact morphology (Fig. 3c). Meanwhile, the cross-sectional image confirmed uniform Li deposition (Fig. 3d). By contrast, the surface of cycled bare Li was uneven and cracked, with a loose and porous morphology, indicating serious dendrite growth (Fig. 3e, f). The plating morphology of Li metal on bare Cu and RASEI@Cu electrodes was captured by SEM. As seen in Fig. S12, the Li deposition on RASEI@Cu was compact and continuous after plating with a capacity of 3 mAh cm^{-2} . Quite different from the dense Li layer on the RASEI@Cu electrode, a porous and loose Li deposition occurred on bare Cu at the same current density. As depicted in Fig. S13, the exchange current density of RASEI@Li was twice higher than that of bare Li, which confirmed that RASEI has the potential to enhance Li^+ mobility and rate capability in lithium metal batteries.

To show the advantage of elastic coating, schematics illustrating the structure evolutions of conventional flexible-SEI@Li and RASEI@Li are displayed in Fig. 3g. Due to the good elasticity of ASEI, tight contact between the coating and lithium metal is maintained during lithium plating and stripping. This effectively minimized the side reaction between electrolyte and lithium metal during cycling, enabling uniform Li deposition and suppressing dendrite growth. Conversely, a coating without elasticity will lead to the formation of gaps between the coating and lithium metal during lithium stripping, hindering Li transport and promoting dendrite growth.

In order to demonstrate the potential of the RASEI@Li in lithium metal batteries, the electrochemical performance of Li/NCM811 and Li/LFP cells was investigated. Fig. 4a illustrates the cycling performance of Li/NCM811 cells using bare Li and RASEI@Li at 0.5 C. The cells with RASEI@Li exhibit greatly improved cycling performance (over $\sim 80\%$ capacity retention after 300 cycles), and more stable charge and discharge voltage profile (Fig. S14) than that of cells with bare Li. Moreover, Li/LFP cells with bare Li experience rapid capacity fading, with less than 80% capacity retention after only 220 cycles (Fig. S15a).

By contrast, the cells with RASEI@Li demonstrate significantly improved cycling performance, with a capacity retention of $\sim 85\%$ even after 400 cycles. This enhancement is further validated by the galvanostatic charge and discharge curves presented in Fig. S15b and c, which clearly illustrate the substantial capacity fading observed in the bare-Li/LFP cells, whereas the RASEI@Li/LFP cells exhibit minimal capacity changes during cycles. To verify the feasibility of RASEI@Li in practical applications, cells with the NCM811 cathode with a loading capacity of $\sim 20 \text{ mg cm}^{-2}$ were assembled for tests. As shown in Fig. 4b, the cells with RASEI@Li delivered a capacity retention of 90% after 190 cycles with a small voltage hysteresis (Fig. S16), while the cells based on bare Li quickly short-circuited after 45 cycles (Fig. 4c). In order to investigate the failure mechanism of the Li/NCM811 cell with bare Li, the disassembly and SEM characterization of the failed cells were conducted after 45 cycles. Fig. S17 demonstrates that the surface of the bare Li electrode exhibits a dendritic structure, which eventually results in the penetration through the separator, ultimately leading to battery failure [42].

Additionally, the surface chemistries of cycled lithium metal anodes were studied *via* X-ray photoelectron spectroscopy (XPS) analysis to further illustrate the advantage of RASEI@Li. In the C 1s spectrum of RASEI@Li after the first cycle (Fig. 4d), the new peak located at $\sim 293.8 \text{ eV}$ corresponds to $-\text{CF}_3$, which is attributed to elastic coating. In addition, it has a stronger C-C (285.1 eV) peak intensity than bare Li, which probably originates from the HFBA in the protective layer. The above results indicate that the coating was still on the surface of lithium metal after the first cycle. There is a clear peak of CO_2-3 (290.2 eV) in the C 1s spectrum of bare Li, which primarily arises from the decomposition product of solvents through the side reactions. However, the presence of the peak of CO_2-3 is absent on the surface of RASEI@Li, indicating that the RASEI can effectively impede the penetration of the electrolyte and reduce the decomposition of the solvents. To investigate the durability of the coating after extended cycling, Li metal anodes cycled 20 times were also examined. As shown in Fig. 4e, although the peak of CO_2-3 also appears in the C 1s spectrum of RASEI@Li (20%), the peak intensity is much weaker than that of bare Li (25.5%). In the F 1s spectrum of RASEI@Li (Fig. 4f), the prominent CF_3 peak can be observed, as well as corresponding peaks in the C spectrum, indicating that the presence of elastic coating on the lithium metal surface after long-term cycling. Besides, the peak intensity of LiF (684.85 eV) for RASEI@Li is much higher than that of bare Li, which is attributed to the decomposition of HFBA.

Furthermore, a practical pouch cell using commercial high-nickel cathodes and RASEI@Li anodes exhibited an impressive capacity retention of over 85% after 200 cycles under 1/3 C charge and 1C discharge conditions (Fig. 5a, b). Though the pouch cell with bare Li showed a similar capacity at the initial cycles, it experienced a rapid decline after 120 cycles. Compared with other elastic ASEIs, lithium metal batteries equipped with RASEI@Li have excellent cycle performance (Table S1).

To investigate the occurrence of parasitic reactions, particularly gas generation, between the lithium anode and electrolyte, the ultrasonic transmission mapping (UTM) technique was employed [43,44]. The transmitted ultrasonic signal will have an obvious decrease when the ultrasonic wave encounters the gas, which manifests blue color on the distribution map. As shown in

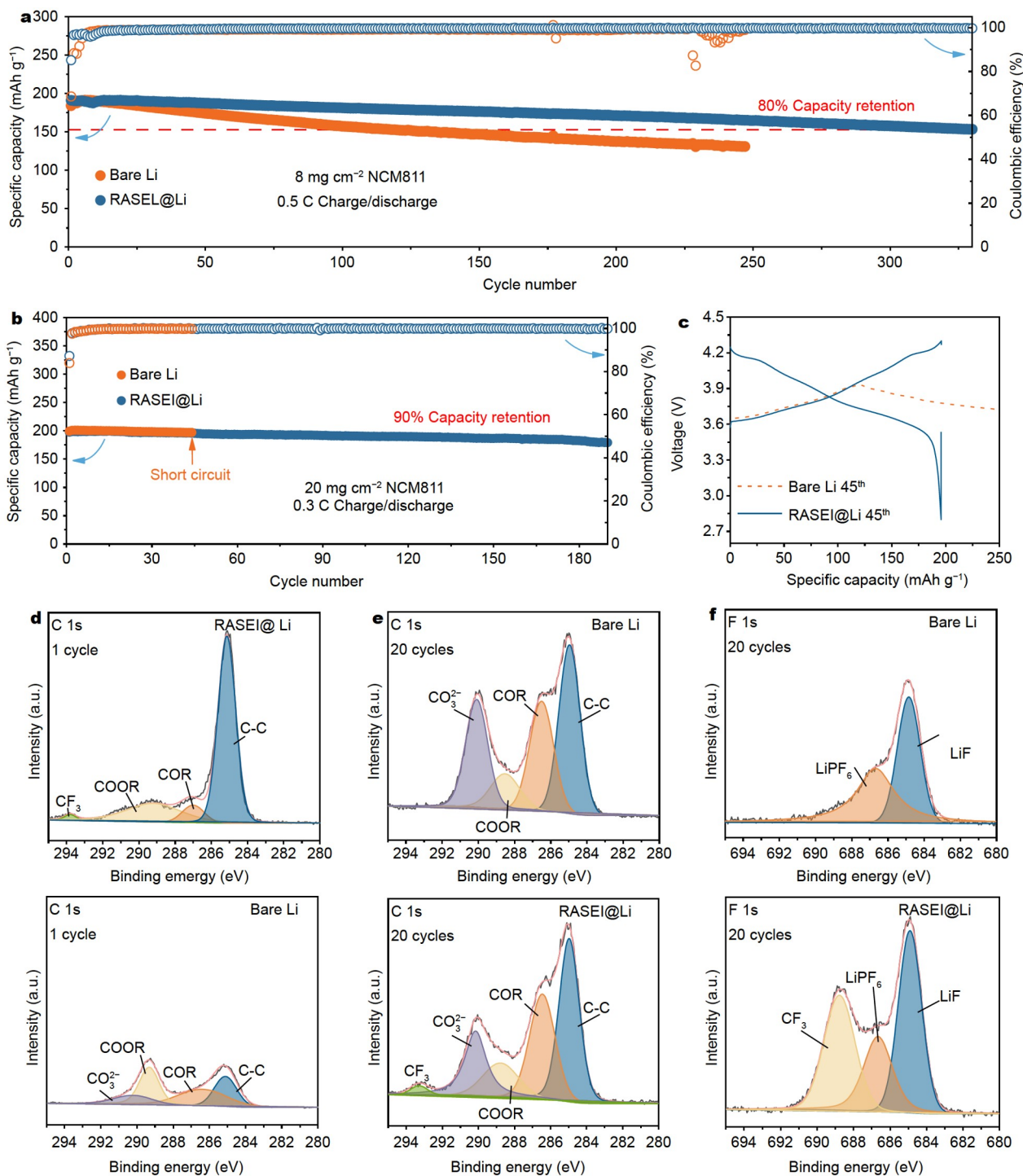


Figure 4 (a) Cycling stability of RASEI@Li/NCM811 and bare Li/NCM811 cells at 0.5 C. (b) Cycling stability of RASEI@Li/NCM811 and bare Li/NCM811 cells at 0.3 C. (c) Voltage profiles of RASEI@Li/NCM811 and bare Li/NCM811 cells at the 45th cycle. (d) C 1s XPS spectra of RASEI@Li and bare Li anodes after 1 cycle. (e) C 1s and (f) F 1s XPS spectra of RASEI@Li and bare Li anodes after 20 cycles.

Fig. 5c, there was no obvious color change in the distribution map, indicating that the pouch with RASEI@Li produced almost no gas in the initial ten cycles. Even after 30 cycles, there were no observable blue signals. By contrast, the map of the pouch cell with bare Li was predominantly covered in blue color after 30 cycles (Fig. 5d), which indicates the occurrence of strong parasitic reactions accompanied by large amounts of gas production.

These ultrasound results provide the evidence that the RASEI coating can effectively mitigate side reactions between the electrolyte and Li anode to achieve impressive cycle stability.

CONCLUSIONS

In summary, a resilient artificial solid-state electrolyte interphase (RASEI) coating was developed to enhance the interfacial sta-

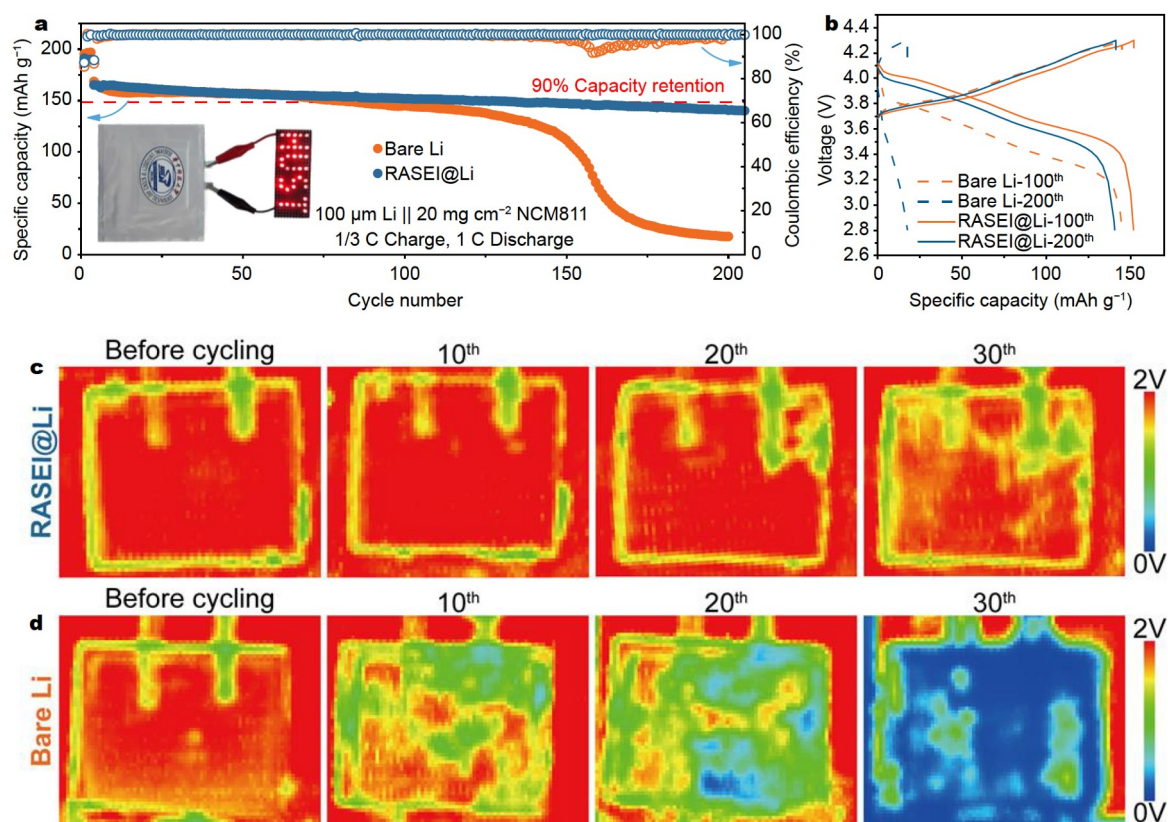


Figure 5 (a) Cycle performances and (b) voltage profiles of RASEI@Li/NCM811 and bare Li/NCM811 cells under 1/3 C charge and 1 C discharge. Ultrasonic transmission mappings of (c) RASEI@Li/NCM811 and (d) bare Li/NCM811 pouch cells.

bility of lithium metal anodes. The mechanical properties of RASEI enable it to withstand the significant volume expansion of lithium metal and maintain conformal interfacial contact during Li plating and stripping processes, thereby ensuring a stable interfacial connection. By acting as a barrier, RASEI effectively hinders the direct contact between the electrolyte and lithium metal anode, leading to a reduction in undesirable side reactions and suppressed growth of lithium dendrites. Moreover, the highly efficient UV curing process offers great potential for large-scale production of RASEI. Through the implementation of RASEI, the Li||Li symmetric cell with the RASEI@Li cycles over 500 h at 1 mA cm⁻² and 1 mAh cm⁻² in the carbonate-based electrolyte. Additionally, a practical NCM811/Li pouch cell exhibits a capacity retention of over 85% after 200 cycles under 1/3 C charge and 1 C discharge conditions. Our work highlights the potential value of elastic ASEIs in lithium metal anode protection.

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Conflict of interest The authors declare no conflict of interest.

Supplementary information Experimental details and supporting data are available in the online version of the paper.



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坚韧、弹性的氟化固体电解质界面稳定碳酸酯电解质中的锂金属

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摘要 锂金属负极和碳酸酯类电解液之间不稳定的界面是限制高比能锂金属电池循环寿命的关键挑战. 本文使用含苯环的双酚A乙氧基化物二甲基丙烯酸酯(BAED)交联剂调节聚(丙烯酸六氟丁酯)(PHFBA), 设计了一种弹性人造固体电解质中间相(RASEI)来解决这个问题. 刚性BAED分子可以对柔性PHBA基体进行调控, 实现从600%伸长率到90%压缩率的卓越回弹性, 并具有超过2 MPa的高杨氏模量. RASEI可以适应锂金属较大的体积变化, 并确保电池运行过程中锂金属与RASEI之间的紧密接触, 促进均匀的锂沉积并减少副反应. 因此, 经过RASEI修饰的Li||Li对称电池可以在 1 mA cm^{-2} 和 1 mAh cm^{-2} 下实现超过500小时的长期循环. 对循环后锂金属进行测试分析表明锂枝晶的生长得到了有效的抑制. 此外, 搭配 20 mg cm^{-2} 高阴极负载的NCM811软包电池在1 C下, 经过200次循环后容量保持率超过85%.