



# 3D nonlinear photolithography of tin oxide ceramics via femtosecond laser

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**ABSTRACT** As a wide band gap semiconductor material, tin oxide (SnO<sub>2</sub>) has been widely used in gas sensing, optoelectronics and catalysis. The complex micro and nanoscale three-dimensional (3D) geometric structures endow the conventional SnO<sub>2</sub> ceramics with novel properties and functionalities. Nevertheless, ceramics cannot be cast or machined easily due to their high mechanical toughness and resistance. The additive manufacturing opens a great opportunity for flexibly geometrical shaping, while the arbitrary shaping of SnO<sub>2</sub> ceramics at micro and nanoscale is always a challenge. Herein, preceramic monomers which can be polymerized under ultrafast laser irradiation, were utilized to form complex and arbitrary 3D preceramic polymer structures. After calcination treatment, these green-body structures could be converted into pure high-dense SnO<sub>2</sub> ceramics with uniform shrinkage, and the feature size was down to submicron. Transmission electron microscopy (TEM) analysis displays that the printed SnO<sub>2</sub> ceramic nanostructures can be nanocrystallized with grain sizes of 2.5 ± 0.4 nm. This work provides the possibility of manufacturing 3D SnO<sub>2</sub> ceramic nanostructures arbitrarily with sub-100 nm resolution, thus making it promising for the applications of SnO<sub>2</sub> in different fields.

**Keywords:** tin oxide ceramics, nonlinear photolithography, femtosecond laser

## INTRODUCTION

Metal oxides have been intensively employed in sensors, optoelectronics and catalysis devices for their excellent electronic and chemical properties [1–3]. Structuring metal oxides down to micro and nanoscale enables the exotic properties. For example, the conductivity and the

performance of gas sensors can be tailored *via* three-dimensional (3D) stacking metal oxide nanowires [3], and crumpling metal oxides nanosheets [4], respectively. And the photocatalytic performance can be highly enhanced *via* dehiscent mesoporous titanium oxide (TiO<sub>2</sub>) microspheres [5]. As typical 1D or 2D nanomaterials, nanowires and thin films are known to possess exceptional properties. However, their size-dependent properties would disappear when they are scaled up. Their overall performances could also be weakened by the interfaces when they are clustered in a composite in particular [6]. In order to overcome the dilemma, highly ordered 3D nanostructured materials are indispensable. Combining 3D-ordered nanostructures with multi-physical interaction, unnatural properties have been designed for various applications [7–10]. Compared with metals and polymers, constructing metal oxides into complex nanostructures arbitrarily is more difficult due to their extremely high melting point [11–13]. In addition, the conventional 3D printing technologies based on powder-based layer-by-layer processes would cause unavoidable limited resolution and residual porosity, thus leading to a decrease in strength [14–18]. Therefore, the technology that can prepare arbitrary 3D metal oxide nanostructures with high resolution and high density is highly desired.

Recently, two-photon polymerization induced by nonlinear absorption *via* femtosecond pulses has been proved to be a high-resolution 3D printing technique [19]. Various 3D geometrical nanostructures fabricated through this technique have been demonstrated [20–22]. By using photosensitive TiO<sub>2</sub> resist, the complex 3D nanostructures were patterned by femtosecond laser direct

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writing, which provided a novel way to structure 3D ceramic materials [23]. Followed by calcination, 3D-architected zinc oxide ceramics were fabricated by femtosecond laser direct writing [24]. Furthermore, by controlling the shrinkage, sub-100 nm of structural feature size was achieved while keeping the 3D geometry [25,26].

As a semiconductor material with a band gap of 3.6 eV, SnO<sub>2</sub> has been widely used in sensors, electrodes and catalysis [27–29]. In this work, a high-resolution approach to manufacture arbitrary 3D nanostructured SnO<sub>2</sub> ceramics was proposed. A simple tin-containing photoresist for two-photon lithography (TPL) was prepared. By adjusting the tin content of the photoresist, the two-photon polymerization threshold could be tailored. The exposure dose was changed by tuning the laser scanning velocity and the effective intensity. Various feature sizes of SnO<sub>2</sub> preceramic structures from 400 nm to 2.3 μm were fabricated under loose focusing condition with a numerical aperture (NA) of 0.26. After demonstrating this technique, an oil immersion objective lens with an NA of 1.3 was used to fabricate complex 3D microstructures. The preceramic structures were calcined with well controlled shrinkage whereby the feature sizes ranging from sub-100 nm to 400 nm were achieved. The calcination process was optimized through simultaneous thermal analysis (STA). The calcined structures were characterized by X-ray diffraction (XRD) and Fourier transform infrared (FTIR). High-resolution transmission electron microscopy (HRTEM) analysis reveals that the calcined SnO<sub>2</sub> was fully dense and nanocrystallized, with an average grain size around 2.5 ± 0.4 nm. These findings demonstrated a promising way to fabricate complex and arbitrary 3D nanostructured SnO<sub>2</sub> ceramics.

## EXPERIMENTAL SECTION

### Preparation of tin-containing photoresist

In Fig. 1a, stannic chloride hydrated (SnCl<sub>4</sub>·5H<sub>2</sub>O) was dissolved in poly(ethylene glycol) diacrylate (PEGDA) with 1 wt% 2,2-dimethoxy-2-phenylacetophenone (DMPA). A total of 200 μL deionized water was added to help SnCl<sub>4</sub>·5H<sub>2</sub>O and DMPA to dissolve in PEGDA better. The mixture was magnetically stirred at 60°C for 4 h.

### Ultrafast laser 3D nonlinear photolithography and calcination

Tin-containing photoresist was drop-casted on the silicon chip and covered with a glass slide. The glass slide was separated from the silicon chip with kapton tapes. A

homebuilt TPL system was used for two-photon polymerization (Fig. 1b). A femtosecond laser (Pharos-10 W, light conversion) with a center wavelength of 515 nm and pulse duration around 260 fs was installed, and a three-axis positioning stage with galvometer scanning system (ES112166, Aerotech Inc., USA) was integrated. An attenuator (2-EWP-R-0515-M, Altechna) was placed in the optical path to adjust the effective laser intensity. A 10× objective lens (NA = 0.26) (M Plan Apo NIR, Mitutoyo Corporation) was applied to investigate the two-photon polymerization process *via* fabricating 3D microbridges (a nanorod suspended between two piers), and a 100× oil immersion objective lens (NA = 1.3) was used to fabricate the complex 3D nanostructures. To measure the laser power, a photodiode power meter was used (S120VC, Thorlabs). After the polymerization, samples were first developed in acetone for 5 min, and then immersed in ethanol for 5 min, followed by drying at 60°C for 5 min. After development, the samples were calcined in a muffle furnace at ambient pressure in air. The entire process is schematized in Fig. 1c.

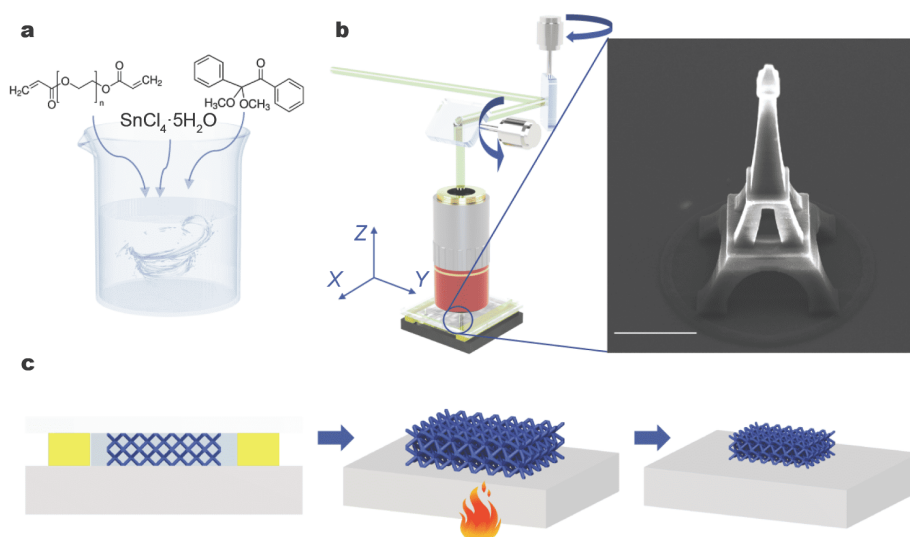
### Characterization

To investigate the composition, thermal property and phase during sintering, the samples were prepared with an ultraviolet (UV) curing lamp for 30 min. The FTIR spectra were measured at room temperature with wave number of 4000–400 cm<sup>-1</sup> (VERTEX80V, Bruker). Thermogravimetric (TG) analysis, derivative thermogravimetric (DTG) analysis and differential scanning calorimetry (DSC) were carried out with a simultaneous thermal analyzer (STA449F3, Netzsch). The XRD patterns were measured with a powder XRD (PANalytical-Empyrean) using a Cu Kα radiation. Scanning electron microscopy (SEM) (ProX, Phenom) and TEM (Titan Cubed Themis G2 300, Thermo Fisher) were used to investigate the morphology and the crystalline structure of the microstructure fabricated by TPL after calcination.

## RESULTS AND DISCUSSION

### Photolithography process

The polymerization reactions only occur at the region where the exposure dose reaches the critical value, which is the polymerization threshold. Otherwise, the polymerization reactions would not be initiated and propagated [30]. By varying the scanning velocity and laser effective intensity, the exposure dose for polymerization can be tuned. Different sizes of suspended preceramic 3D microbridge nanostructures were fabricated *via* tuning



**Figure 1** Schematic diagram of 3D nanostructuring approach of SnO<sub>2</sub> ceramics. (a) Preparation process of the tin-containing photoresist. (b) Preparation process of 3D structures with oil immersion objective lens. The inset is the SEM image of a tower made *via* the tin-containing photoresist. Scale bar: 20 μm. (c) The developing and sintering process of the 3D structures.

the polymerization threshold and exposure dose. The intensity distribution of a Gaussian laser beam in TPL can be described as

$$I^2 = I_0^2 \exp(-4r^2/r_0^2), \quad (1)$$

where  $I_0$  is the laser effective intensity at the center of the focal spot,  $r$  and  $r_0 = 0.61\lambda/\text{NA}$  ( $\lambda$  is the laser wavelength) are the radial coordinate and the diffraction-limited spot radii, respectively. Compared with the linear absorption in single photon polymerization, the absorption is proportional to the square of light intensity in TPL, leading to the smaller polymerized region as shown in Fig. 2a (the green and blue curves). By reducing the  $I_0$  (the blue, brown, and red curves), the feature size of polymerized voxel can be controlled (Fig. 2a). By tuning the concentration of SnCl<sub>4</sub>·5H<sub>2</sub>O, the polymerization threshold and the density of photoresist (Fig. 2b) can be tailored, which introduces an additional freedom to control the fabrication resolution before and after calcination.

Theoretically, the linewidth of the resolution of TPL is affected by the polymerization threshold, laser exposure dose and other laser parameters, which can be described as [31,32]

$$d = r_0 \left[ \ln \left( \frac{\sigma_2 N_0^2 n \tau_L}{C} \right) \right]^{1/2}, \quad (2)$$

where  $\sigma_2$  refers to the effective two-photon absorption cross section,  $n$  stands for the number of pulses which equals to  $2r_0 f/\nu$  ( $f$  is the pulse repetition rate,  $\nu$  means the

scanning velocity), and  $\tau_L$  is the pulse duration and  $C$  is an integration constant.  $N_0$  is the photon flux intensity which equals to  $2P/(\pi r_0^2 \tau_L f \hbar \omega_L)$ , where  $P$  indicates the laser effective intensity. By substituting the specific expression of  $n$  and  $N_0$  in Equation (2), the estimated linewidth can be obtained:

$$d = r_0 \left[ \ln \left( \frac{4\sigma_2 P^2}{C \pi^2 r_0^3 \tau_L f \hbar^2 \omega_L^2 \nu} \right) \right]^{1/2}. \quad (3)$$

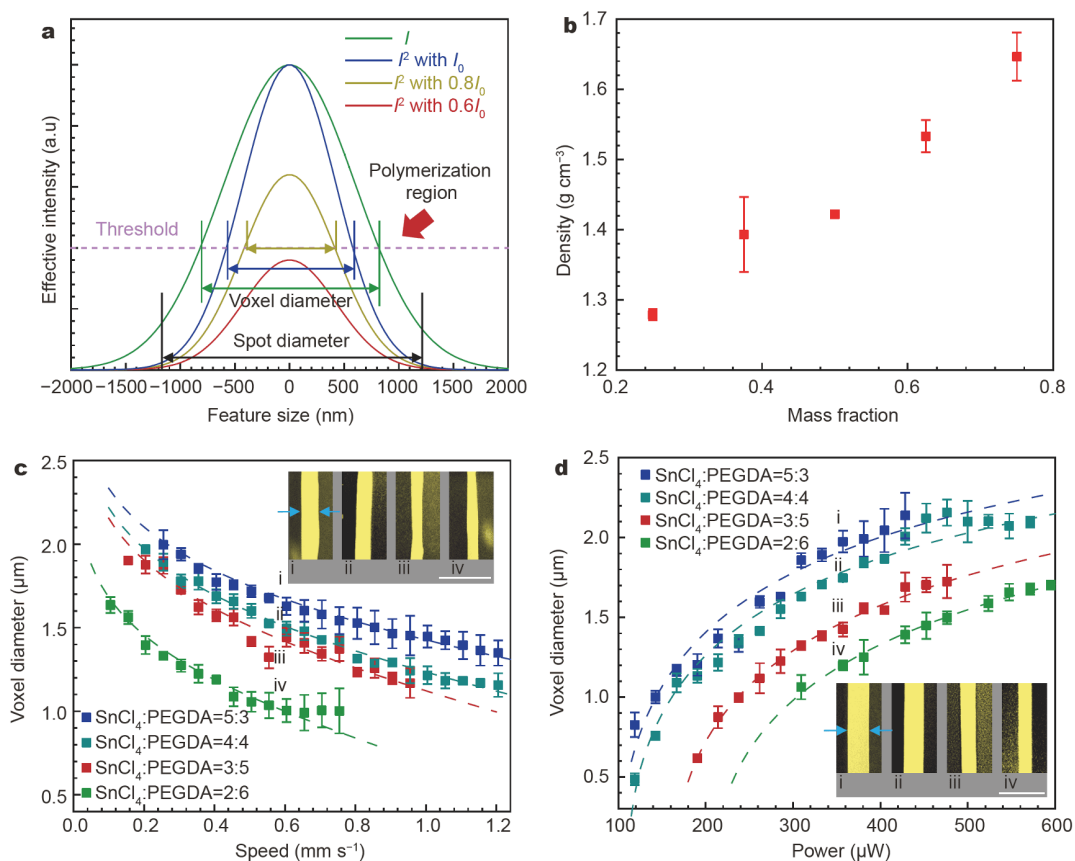
The relationship between  $d$  and  $P$  can be further simplified as Equation (4):

$$d = A [\ln(BP^2)]^{1/2}, \quad (4)$$

and the relationship between  $d$  and  $\nu$  can be further simplified as Equation (5):

$$d = A' \left[ \ln \left( \frac{D}{\nu} \right) \right]^{1/2}. \quad (5)$$

By tuning the laser power and the velocity, the diameters of the fabricated structures in different tin-containing photoresists were measured. The experimental data were fitted according to Equations (4) and (5). The corresponding fitting curves are illustrated in Fig. 2c, d with the dash lines. The values of parameters  $A$  and  $A'$  are close to 1.208 μm, which are the theoretical value of the diffraction-limited spot radius with the laser wavelength of 515 nm and NA of 0.26, as shown in Fig. 2a. By reducing the content of SnCl<sub>4</sub>·5H<sub>2</sub>O in the photoresist, the values of unknown parameters  $B$  and  $D$  decrease ac-



**Figure 2** (a) Achievement of sub-diffraction-limit resolution. The feature size is controlled by adjusting the laser intensity  $I_0$ . (b) The relationship of the photoresist density and the mass fraction of  $\text{SnCl}_4 \cdot 5\text{H}_2\text{O}$ . (c, d) The sizes of the fabricated structures with different scanning velocities and effective intensities. The insets are SEM images of the nanorods marked in yellow. Scale bars are 5  $\mu\text{m}$ .

**Table 1** The  $A$ ,  $B$ ,  $A'$ ,  $D$  values of different tin contents processed with different laser powers and scanning velocities<sup>a</sup>

	$\text{SnCl}_4:\text{PEGDA}$			
	5:3	4:4	3:5	2:6
$A$	1.21028	1.17372	1.18875	1.18538
$B$	$9.65231 \times 10^{-5}$	$7.93994 \times 10^{-5}$	$3.61204 \times 10^{-5}$	$2.20081 \times 10^{-5}$
$A'$	1.21726	1.21378	1.21223	1.01048
$D$	3.94847	2.81311	2.35697	1.59638

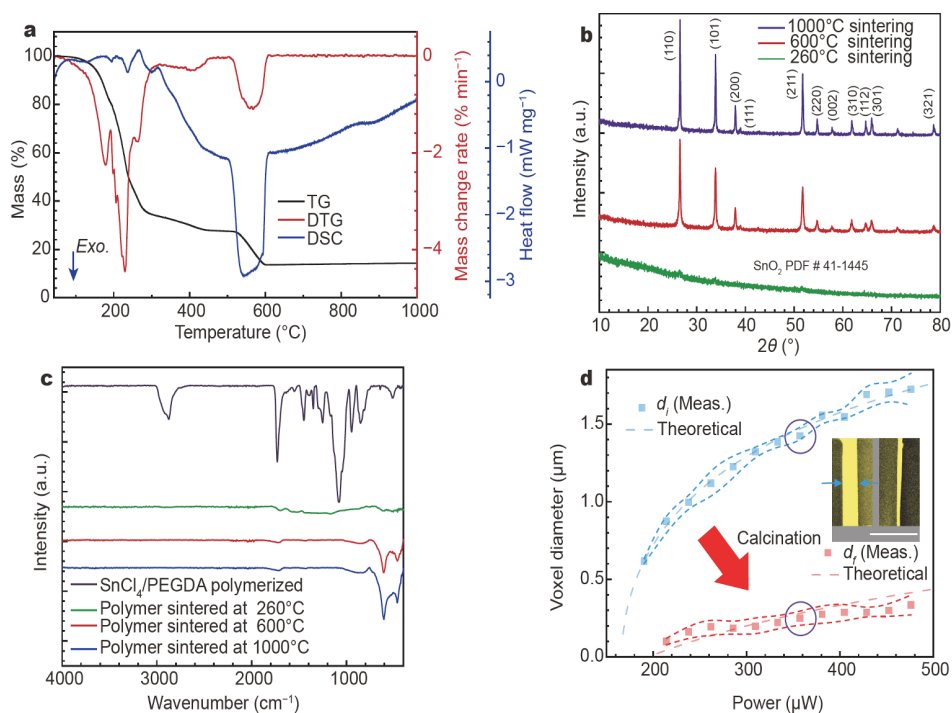
a)  $A$  and  $A'$ : fitted values of  $r_0$  in Equations (4) and (5);  $B$  and  $D$ : constants related to  $\sigma_2$ .

cordingly. This phenomenon can be explained by decreasing  $\sigma_2$  because the relative concentration of DMPA to PEGDA is reduced. In general, the accuracy of the structure can be controlled by adjusting the laser power, scanning velocity and the concentration of  $\text{SnCl}_4 \cdot 5\text{H}_2\text{O}$ .

### Sintering process

The STA results of tin-containing polymer are shown in Fig. 3a. The sample rapidly loses about 54% of its mass

from 140 to 260°C with no significant thermal effect, and there is no obvious peak in the XRD pattern (Fig. 3b). This process is caused by the slow evaporation of the solution moisture and the carbonization of the organic matter. At the same time, the intensity of characteristic peaks of the polymer in FTIR spectra decreases above 260°C (Fig. 3c), indicating the polymer decomposition and carbonization occur. Between 500 and 600°C, there is another stage of rapid mass reduction in the TG curve,



**Figure 3** (a) STA results containing TG, DTG and DSC. (b, c) XRD and FTIR characterizations of UV-cured samples. The SnCl<sub>4</sub>·5H<sub>2</sub>O content of the above samples is 50 wt%. (d) The experimental results and theoretical values before and after sintering. The insets are the SEM images before (left) and after (right) calcination. Scale bar: 5 μm.

and a large amount of heat release in this stage as well, which is an obvious combustion process, suggesting that the sample starts to combust from 500°C until the end of 600°C, losing about 14% of its mass. Combining the STA, XRD and FTIR results, the calcination procedure was determined consisting a heat ramp of 5°C min<sup>-1</sup> from ambient temperature to 140°C, 260 to 500°C, and a heat ramp of 0.5°C min<sup>-1</sup> from 140 to 260°C, 500 to 600°C, respectively. It is expected to maintain the structures as a result of slowing down the reaction rate including evaporation and combustion. When the temperature reaches 600°C, a dwell time of 3 h is set for better crystallization.

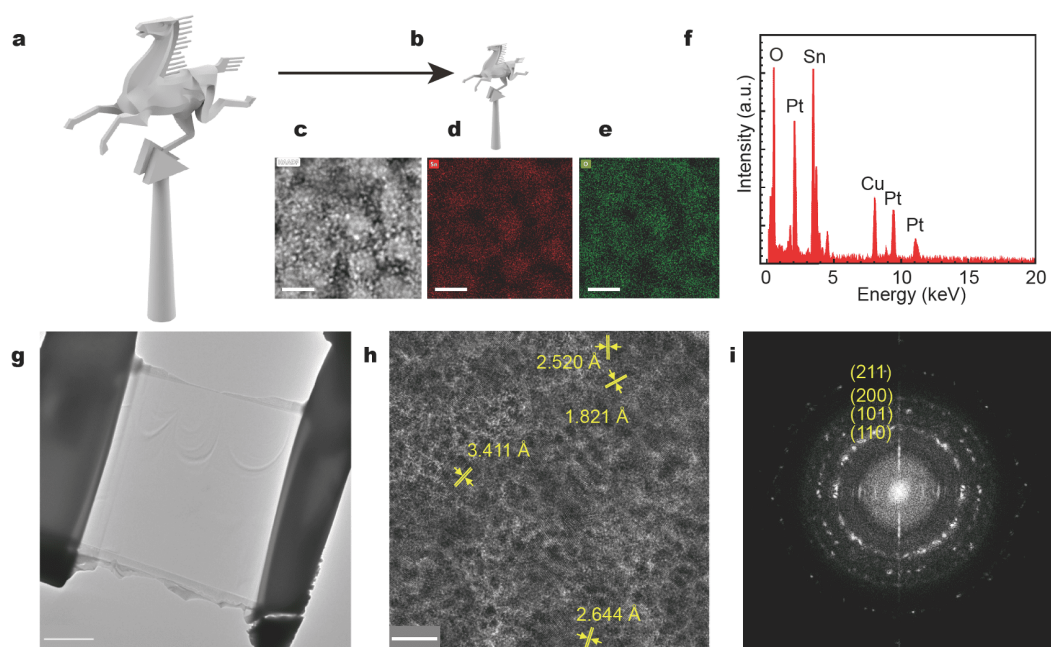
The XRD patterns suggest a single phase of tetragonal SnO<sub>2</sub>. The XRD result shows that under the calcination condition of 600°C, the organic components almost disappear, and the crystallized SnO<sub>2</sub> nanoparticles can be formed successfully. The characteristic peaks of FTIR spectra at about 549 and 600 cm<sup>-1</sup> are ascribed to the metal–oxygen bonding (Sn–O) modes (Fig. 3c). With the increase of temperature, the characteristic peak intensities in the XRD patterns and FTIR spectra of the sample increase, revealing that the crystallinity of SnO<sub>2</sub> increases. As shown in Fig. 3d, before and after sintering, the actual measurement results are in accordance with the theo-

retical value using Equation (4) fitting, and the ratio of shrinkage is about 80.6%–88.7%. The remaining data are presented in Figs S1 and S2. With different mass ratios of SnCl<sub>4</sub>·5H<sub>2</sub>O, the feature shrinkage of the structures is illustrated in Fig. S3. The concept of a pegasus-like sculpture before and after calcination is demonstrated in Fig. 4a, b. SEM images of other 3D microstructures before and after calcination are displayed in Fig. S4. It should be noted that there is some deformation at the bottom of the structures, because the bottom section is firmly adhered to the silicon substrate and calcinated under the constraint conditions, while the top section keeps nearly isotropically uniform shrinking.

#### Microstructure and chemical composition of the SnO<sub>2</sub> ceramic structures

After focused ion beam (FIB) cutting, the calcinated sample was prepared, and a thin slice is displayed in Fig. 4g. The high-angle annular dark field (HAADF) reveals that the calcined SnO<sub>2</sub> is nearly fully dense and nanocrystallized, with an average crystalline grain size of 2.5 ± 0.4 nm. And the elemental distribution is proved by the energy dispersive spectrometer (EDS), giving information that the O and Sn atoms are uniformly dis-





**Figure 4** The illustration of a pegasus-like sculpture (a) before and (b) after the calcination treatment. (c) Scanning TEM image of a calcinated structure and the EDS mapping of (d) tin and (e) oxygen. (f) EDS spectrum. (g) TEM sample created with FIB and micromanipulator. (h) HRTEM image of a calcinated structure. (i) The analysis of interplanar distances using FFT. Scale bars are 20 nm for (c–e), 2  $\mu\text{m}$  for (g), and 10 nm for (h).

tributed throughout the structure (Fig. 4c–f). The Pt and Cu elements come from the Pt sputtered during FIB cutting and the copper coils in the TEM, respectively. By combining the HRTEM image with the fast Fourier transform (FFT) image (Fig. 4h, i), it can be confirmed that the four distinct lattice spacings of 1.821, 2.520, 2.644, and 3.411  $\text{\AA}$  correspond to the interplanar distances of tetragonal  $\text{SnO}_2$  (211), (200), (101), and (110) planes, respectively. Nanocrystallized  $\text{SnO}_2$  ceramic nanostructures are formed *via* this technique.

## CONCLUSIONS

An approach with high resolution to manufacture 3D  $\text{SnO}_2$  ceramic nanostructures was developed. Through this process,  $\text{SnO}_2$  could be fabricated into arbitrary nanostructures without complex chemical synthesis. By tuning the concentration of  $\text{SnCl}_4 \cdot 5\text{H}_2\text{O}$ , the polymerization threshold can be adjusted, and the feature size of the fabricated structures can be controlled by varying the laser exposure conditions. Through the control of the pyrolysis process, a uniform shrinkage of the structure can be achieved. This work provides the possibility of manufacturing 3D  $\text{SnO}_2$  ceramic structures with sub-micrometer resolution. Considering the excellent property of  $\text{SnO}_2$ , it opens a new door for catalysis and electrochemical performance engineering *via* geometrical

structure tuning, thus offering a new freedom for material property design.

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**Author contributions** Cheng Y and Mai L were in charge of this scientific research project; Wang X and Gan Z finalized the manuscript; Chai N and Liu Y conducted most of the experiments and data analyses together as well as wrote the manuscript; Zhang Q and Huang F contributed to the photoresist preparation and analysis; Zeng Z and Wei P performed the HRTEM analysis and helped discuss and revise the manuscript; Yue Y and Zhao J performed the pyrolysis experiments and contributed to revising the manuscript. The manuscript was written through contributions of all authors. All authors have given approval to the final version of the manuscript.

**Conflict of interest** The authors declare that they have no conflict of interest.

**Supplementary information** Supporting data are available in the online version of the paper.



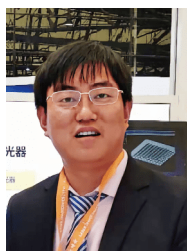
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## 氧化锡陶瓷的飞秒激光3D非线性光刻

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**摘要** 氧化锡是一种宽带隙半导体材料, 广泛用于气体传感、光电和催化等领域. 微米级至纳米级的复杂三维几何结构使传统的氧化锡陶瓷具有新的特性和功能. 由于具有高的机械韧性和强度, 陶瓷不易铸造或加工. 增材制造为陶瓷材料灵活的几何造型带来了巨大的机会, 但是极高的熔化温度使其在普通的3D打印方法上更加困难, 而在微米或纳米尺度任意成形氧化锡陶瓷始终是一个挑战. 本文中, 我们利用在超快激光辐照下聚合的陶瓷前驱体, 形成复杂且任意的3D陶瓷聚合物结构, 通过煅烧处理后转变为具有均匀收缩率的高密度纯氧化锡陶瓷, 特征尺寸可降至亚微米. 透射电子显微镜(TEM)分析显示, 氧化锡陶瓷纳米晶体的晶粒尺寸为 $2.5 \pm 0.4$  nm. 这项工作为制造精度高达亚百纳米的任意3D氧化锡陶瓷纳米结构提供了可能性, 从而使其在不同领域更具应用前景.