

# In Vivo and In Vitro Nitinol Corrosion Properties

Melissa K. Lonn<sup>1</sup> · Justin M. Metcalf<sup>2</sup> · Brian D. Choules<sup>2</sup>

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Abstract Regulatory authorities often require in vitro testing on medical devices prior to approval. Current standardized corrosion testing methods (ASTM F2129) require testing in a non-physiologic, de-oxygenated solution for a pre-exposure time of  $\leq 1$  h; however, no correlations between the prescribed simulated environment and whole blood conditions have been elucidated. This study compared open circuit potential (OCP), breakdown potentials ( $E_b$ ),  $E_b - OCP$ , and cyclic polarization curves tested in vivo (OCP only) and in vitro in whole blood to those tested in phosphate-buffered saline (PBS). Two oxide thicknesses of Nitinol, two solution oxygen contents (deaerated and aerated solutions), and two pre-exposure durations (acute and chronic) were investigated. The in vitro OCP in whole blood was not significantly different than the in vivo OCP, suggesting that whole blood in vitro can be used to determine baseline corrosion behavior of medical implants. E<sub>b</sub> - OCP tested per ASTM F2129 was comparable to acute whole blood and was conservative compared to chronic whole blood for both oxide thicknesses. However, OCP, E<sub>b</sub>, and cyclic polarization curves were not always comparable to whole blood. Testing in aerated PBS achieved  $E_b$ ,  $E_b - OCP$ , and cyclic polarization curves that were comparable to or more

<sup>2</sup> MED Institute, Inc., West Lafayette, IN, USA

conservative than whole blood testing, regardless of preexposure duration and oxide thickness.

**Keywords** NiTi < materials  $\cdot$  Shape memory stents  $\cdot$ Corrosion  $\cdot$  In vivo  $\cdot$  Open circuit potential  $\cdot$  Breakdown potential

# Introduction

In vitro testing is essential for gaining insight into the performance of medical devices. Ideally, in vitro tests closely represent the clinical performance of the device. However, a poorly designed test may cause many hours of unnecessary design iterations, testing, and regulatory activities in an effort to interpret results which do not adequately mimic clinical performance.

It is imperative to fully understand how in vitro results correlate to in vivo results. Designing in vitro tests to mimic chronic physiologic conditions is necessary, and often the tests need to be run in a short amount of time. However, interpretation of short-term results to predict chronic conditions can be difficult. ASTM F2129 is a well accepted in vitro corrosion test for metallic implants that describes a 1–2 h test in a deaerated solution to assess chronic corrosion resistance [1]; however, defining a clinically relevant acceptance criterion has proven difficult and controversial [2]. A clinically relevant acceptance criterion for Nitinol (NiTi) is especially important, since there are multitudes of ways to prepare the surface, which can dramatically affect the ASTM F2129 results.

To develop a clinically relevant acceptance criterion, the open circuit potential (OCP or the rest potential) of the sample in vivo must be understood. Several in vivo studies have been performed on NiTi [3, 4]; however, the reported

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Melissa K. Lonn mlonn@medinst.com

<sup>&</sup>lt;sup>1</sup> Cook Research Incorporated, 1 Geddes Way, West Lafayette, IN 47906, USA

range of NiTi rest potentials was quite large  $(-330 \text{ mV}_{\text{SCE}})$  to  $+10 \text{ mV}_{\text{SCE}}$ ), and the results were not directly compared to in vitro results.

It has been previously recommended to set an acceptance criterion without consideration of the test sample OCP [5, 6]. Specifically, it has been recommend that  $E_b < 300 \text{ mV}$  is unacceptable,  $E_b$  between 300 and 600 mV is marginal, and  $E_b > 600 \text{ mV}$  is acceptable. It is important to note that these recommendations were made with consideration of only a few metallic alloys (316 stainless steel, cobalt chromium, titanium, and Nitinol). The application of an absolute acceptance criterion for breakdown potential is problematic, since the OCP is different for various metals and metallic surface finishes, and varies with implant duration. Therefore, due to the wide variety of OCPs, an absolute acceptance criterion related to breakdown alone might not be appropriate for the medical device industry.

An alternative to using absolute  $E_b$  as the acceptance criterion is to evaluate the corrosion resistance using the difference between breakdown and the open circuit potential  $(E_{b} - OCP)$ , which has been recommended previously [7–9]. This difference provides more information about the device's corrosion behavior and how much the device OCP is able to deviate without inducing localized corrosion (i.e., pitting and breakdown). The argument against  $E_b - E_r$  (where ASTM F2129 defines  $E_r$ , rest potential, as the OCP following <1 h deaerated pre-exposure) has been that E<sub>r</sub> is measured in a non-physiologic solution that is not representative of in vivo OCP. In vivo OCP values are not well known, and can vary based on immersion solution, oxygen content, immersion time, and surface finish. Several studies have been performed to understand how oxygen content and immersion time affect OCP,  $E_{\rm b}$ , and  $E_{\rm b}$  – OCP [7, 8]; however, no direct correlation with in vivo results has been reported.

Therefore, the aim of this study was to compare the corrosion results of two different NiTi oxide thicknesses tested in vivo (measuring short-term OCP only) and in vitro in whole blood to the results in phosphate-buffered saline (PBS). Additionally, this study investigated the effect of oxygen content of the test solution and pre-exposure time on OCP,  $E_b$ , and  $E_b - OCP$ .

# **Materials and Methods**

Testing was conducted on two NiTi oxide thicknesses used for medical devices: black oxide (BO), and electropolished and passivated (EP). These surface finishes were chosen to encompass the range of oxide thicknesses typically used for NiTi medical devices. NiTi #1 (Fort Wayne Metals, Fort Wayne, IN) with a black oxide finish was acquired in the straight annealed condition, with a diameter of 0.026''. NiTi #1 is better than or equal to the chemical composition defined by ASTM F2063. The BO oxide thickness was measured to be 670 Å using Auger electron spectroscopy (Fig. 1a). For the EP processing, BO NiTi samples from the same lot were electropolished and passivated. To illustrate changes in breakdown potential due to testing environment and pre-exposure time, a suboptimal electropolish exhibiting occasional breakdown was chosen for EP so that breakdown would occur in a portion of samples prior to E<sub>v</sub>. The resulting oxide thickness was measured to be 34 Å (Fig. 1b). All samples were rinsed with distilled water (ASTM Type 1) and alcohol, and then dried prior to sending to Evans Analytical Group (EAG) for Auger testing and analysis.

Electrochemical corrosion testing was performed with Gamry Reference 600 potentiostats. All potentials were measured in reference to saturated calomel electrodes (SCE). Gamry DC105 software was used to perform the test.

BO and EP NiTi wires were tested in 4 different environments: (1) in vivo arterial blood, (2) in vitro venous whole blood, (3) in vitro aerated PBS, and (4) in vitro deaerated PBS.

#### In Vivo Studies

For the in vivo studies, an ovine model was used. Anesthesia was induced, and heparin was administered between 100-200 IU/kg. Testing was approved under facility approved IACUC. Exposed wire (2.1 cm<sup>2</sup>) was placed within the animal, while the remainder of the wire was masked off with a non-conductive resin (Miccrostop). The wire was inserted through an 18 French sheath placed within the aorta via femoral access. Bilateral femoral arteries were accessed, allowing two wires to be tested simultaneously. An elongated SCE was also placed within the 18 French sheath, parallel to the test specimen. The tip of the elongated SCE was placed near the wire, outside the sheath. Placement was verified via fluoroscopy. The potential difference between the elongated SCE and the inhouse standard SCE was verified to be within  $\pm 3 \text{ mV}$ . Bilateral BO and EP wires were tested, and the access location was alternated with each new sample to eliminate the potential variable effects of test location and animal. The potential after 1 h was recorded as the OCP. Arterial blood chemistries including pH, partial pressure of oxygen (pO<sub>2</sub>), saturation of oxygen (sO<sub>2</sub>), hemoglobin (Hb), ionic calcium concentration (iCa), chlorine concentration (Cl), sodium concentration (Na), and potassium concentration (K) were measured before and after each open circuit scan using an Abaxis i-Stat blood analyzer (cartridges CHEM8+ and CG4+).



Fig. 1 Auger analysis of BO (a) and EP (b) oxide thicknesses resulting in thicknesses of 670 Å and 34 Å, respectively

#### In Vitro Studies

Samples were placed within a 1 L jacketed electrochemical corrosion cell containing whole blood, deaerated PBS, or aerated PBS. Samples were electrically connected to stainless steel mandrels using a silver solder epoxy. Miccrostop was applied to the sample/mandrel interface and the cut ends of the sample. The exposed surface area of the wire samples was 1.6 cm<sup>2</sup>. Heparinized bovine whole blood (LAMPIRE Biological Laboratories, Inc., Pipersville, PA) with 1X penicillin/streptomycin was used to prevent bacterial growth. Ionic concentrations were measured from each blood lot. Oxygen concentration, oxygen saturation, and pH were measured before and after each test and daily blood exchanges. PBS [1] was either deaerated (bubbled with nitrogen) or aerated (bubbled with compressed laboratory air) and buffered to a pH of  $7.4 \pm 0.2$ . Test solutions were maintained at 37 °C  $\pm$ 1 °C. Open circuits (or pre-exposures) were measured for either 1 h (acute) or 200 h (chronic), which were monitored discretely for a minimum of 1 h each day until the end of the test. NiTi OCP has been reported to reach steady state after 200 h [7, 8]; therefore, this was chosen to represent a chronic state. Table 1 shows the sample sizes for each OCP test group.

For all in vitro studies, a cyclic polarization scan was conducted following the open circuit (pre-exposure) delay. Cyclic polarization testing followed ASTM F2129, except for the experimental changes to the aeration and open circuit duration. The forward and reverse scan rates were 1 mV/s. The cyclic polarization scan was started at the OCP, and the  $E_v$  (vertex potential) was 1200 mV. Pitting of the samples was confirmed using light microscopy of up to  $\times 25$  magnification.

Pre-exposure solution, pre-exposure time, and scan solution were investigated; specifically, samples were assigned to eight different cyclic polarization experimental groups (Table 2). Group 1 (acute) samples and Group 2 (chronic) samples were tested in heparinized bovine whole blood. The natural oxygen content in the whole blood was desired, eliminating the need to bubble the solution. Group 3 (acute) samples and Group 4 (chronic) samples were tested in aerated PBS. Additionally, Group 5 (acute) and Group 6 (chronic) samples were used to investigate the effect of pre-exposure in aerated PBS prior to testing in deaerated PBS, in which case the solution was deaerated for 30 min with nitrogen prior to the scan. Finally, Group 7 (acute—the control group tested fully to ASTM F2129) and Group 8 (chronic) samples were tested in deaerated PBS.

## **Data Analysis**

Experimental groups were compared using the GLM procedure in SAS (Statistical Analysis Software, version 9.3) with a least-square mean statement utilizing Tukey test ( $\alpha = 0.05$ ). For groups with censored data (i.e., lack of breakdown prior to reversing the scan), a Kaplan–Meier survival curve (lifetest procedure in SAS) was used to compare groups.

# Results

### Acute and Chronic Open Circuit Potential (OCP)

OCP following 1 h pre-exposure (acute) in solution for all test environments is presented in Fig. 2. The OCP for acute in vitro whole blood was not significantly different from

Table 1Open circuitexperimental groups

Surface finish	Solution	Number of samples tested		
		1 h open circuit	200 h open circuit	
BO NiTi	In vivo whole blood	8	N/A	
	In vitro whole blood	12	4	
	In vitro aerated PBS	32	16	
	In vitro deaerated PBS	16	8	
EP NiTi	In vivo whole blood	8	N/A	
	In vitro whole blood	12	4	
	In vitro aerated PBS	40	16	
	In vitro deaerated PBS	28	16	

Table 2 Cyclic polarization experimental groups

Cyclic polarization experimental group	Open circuit (OC)		Polarization scan solution	Sample size	
	Solution	Duration (h)		BO NiTi	EP NiTi
1	In vitro whole blood	1	In vitro whole blood	8	8
2		200		4	4
3	In vitro aerated PBS	1	In vitro aerated PBS	8	11
4		200		8	7
5	In vitro aerated PBS	1	In vitro deaerated PBS	8	11
6		200		8	8
7 (control)	In vitro deaerated PBS	1	In vitro deaerated PBS	8	11
8		200		7	7

the OCP for in vivo whole blood for both oxide thicknesses (p = 0.0636 for BO, 0.9964 for EP). For the acute BO groups, in vitro aerated and deaerated PBS were significantly different from the whole blood groups (p < 0.0001). For the acute EP groups, only the aerated PBS group was significantly different from the whole blood groups (p < 0.0001). Oxygen content influenced mean OCP for all samples at 1 h (Fig. 3), though the effect was greater on samples with thicker oxides. Therefore, depending on the

oxide thickness, testing in conditions performed per ASTM F2129 (deaerated PBS for 1 h) might result in OCPs which are not representative of in vivo OCPs.

OCPs after 200 h (chronic) compared to 1 h (acute) OCPs are shown in Fig. 2. All potentials increased with longer pre-exposure times, and all groups, except EP in deaerated PBS, trended toward a similar potential (11–58 mV). Therefore, even after 200 h, deaerated OCPs were not representative of in vivo potentials for all oxide



Fig. 2 Acute and chronic open circuit potentials



Fig. 3 Open circuit potential versus oxygen partial pressure



Fig. 4 Percent increase in oxide thickness versus pre-exposure duration of EP NiTi wires

thicknesses, whereas chronic-aerated OCPs were similar to chronic whole blood OCPs for both oxide thicknesses (p = 0.9976 and p = 0.7397).

Auger was performed on EP NiTi samples following 1 and 200 h in PBS to compare to the untested samples (Figs. 4 and 5). All samples increased in oxide thickness following testing, with the largest increase occurring in aerated PBS following 200 h. This is consistent with results reported previously, indicating that oxide changes over time and increases corrosion resistance [10, 11].

### **Breakdown Potentials** (E<sub>b</sub>)

The results for  $E_b$  of all groups investigated are presented in Fig. 6 using Kaplan–Meier survival curves to account for censored data (i.e., the  $E_v$  was reached prior to breakdown). Representative cyclic polarization curves are presented in Fig. 7.

For both oxide thicknesses,  $E_b$  improved with longer pre-exposure time. The acute BO samples exposed exclusively to aerated solutions (pre-exposure and scan) were



Fig. 5 Auger analysis of EP oxide thicknesses following pre-exposure: acute aerated (a); acute deaerated (b); chronic aerated (c); chronic deaerated (d)



Fig. 6 Kaplan-Meier curves for E<sub>b</sub>: acute BO (a); acute EP (b); chronic BO (c); chronic EP (d)

most similar to whole blood (p = 0.7774) (Figs. 6a and 7a). The  $E_{\rm b}$  of chronic BO samples exposed exclusively to deaerated solutions (pre-exposure and scan) and the samples exposed exclusively to aerated solutions were most similar to the whole blood  $E_{\rm b}$  (p = 0.9850 and p = 0.1439, respectively) (Fig. 6c). Most importantly, the  $E_{\rm b}$  occurring after chronic immersion in whole blood was significantly different than the control as tested per ASTM F2129 (1 h deaerated pre-exposure with deaerated scan), p < 0.0001. For both acute and chronic EP experimental groups, no significant difference in E<sub>b</sub> was observed for the different testing conditions (p = 0.2297 and p = 0.6482, respectively). However, acute EP samples exposed exclusively to aerated solutions had the most conservative (i.e., resulting in the lowest  $E_{\rm b}$ ) breakdown survival curve (Fig. 6b). Overall, fewer EP samples broke down after chronic preexposure compared to acute pre-exposure (Fig. 6b and d).

It is also interesting to note that acute BO samples preexposed to aerated solutions followed by a deaerated scan were not significantly different than the samples exposed exclusively to deaerated solutions (p = 0.9957, Figs. 6a and 7a), whereas chronic BO samples pre-exposed to aerated solutions followed by a deaerated scan were similar to the samples exposed exclusively to aerated solutions (p = 0.7786, Figs. 6c and 7c).

#### Difference Between $E_b$ and OCP ( $E_b - OCP$ )

For both oxide thicknesses,  $E_b - OCP$  increased with preexposure duration, Fig. 8. For Groups 5 and 6, OCPs were taken after the aerated pre-exposure, prior to deaerating with nitrogen to start the cyclic polarization scan.

The BO samples exposed exclusively to aerated solutions were more conservative (i.e., resulting in a lower  $E_b - OCP$ ) than whole blood for both acute and chronic time points (Fig. 8a and c). The  $E_b - OCP$  results for BO samples exposed only to deaerated solutions were most similar to whole blood for both acute and chronic durations (Fig. 8a and c). However, acute cyclic polarization scans for deaerated PBS and whole blood were noticeably



Fig. 7 Representative cyclic polarization curves: acute BO (a); acute EP (b); chronic BO (c); chronic EP (d)

different (Fig. 7a). Thus, in vivo conditions are not fully represented with a 1 h deaerated pre-exposure with deaerated scan, depending on oxide thickness.

For both acute and chronic EP experimental groups, no significant difference between the potential difference survival curves was observed for the different testing conditions (p = 0.0580 and p = 0.6482, respectively). The most conservative condition for acute EP E<sub>b</sub> – OCP was the aerated pre-exposure with an aerated scan.

A summary of results is presented in Table 3.

# Discussion

The cyclic polarization testing standard for metallic devices (ASTM F2129) has been well received by regulatory agencies as an acceptable test for corrosion resistance for implant devices [1]. However, determination of an acceptance criterion has been a topic of much debate. The standard states that the method is intentionally severe and meant for comparison purposes only; however, an absolute acceptance criterion for  $E_b$  has been proposed [5, 6]. The standard defines a pre-exposure time  $\leq 1$  h; however, oxide thicknesses have been found to change over time [10, 11], which can potentially change the corrosion resistance. Therefore, care must be taken when determining clinically relevant acceptance criteria. Additionally, the standard dictates that testing be conducted in a non-physiological de-oxygenated solution, with the aim of producing a lower  $E_b$ . However, blood and other body fluids are not anoxic (typical arterial and venous oxygen partial pressure ranges are 80–100 and 40–50 mmHg, respectively) [12]. Finally, the corrosion standard for galvanic testing of medical implants, ASTM F3044, states that testing should be performed in an aerated solution and that the coupled potential be compared to  $E_b$  as found in ASTM F2129; thus, further confounding testing practices when comparing aerated galvanic results to deaerated breakdown results [13].

Therefore, this study investigated the effect of oxygen content and pre-exposure time on OCP,  $E_b$ , and  $E_b - OCP$  for two different NiTi oxide thicknesses (BO and EP). Both EP and BO samples were investigated since medical devices with EP and BO oxide thicknesses are currently available in the market. By analyzing two extremes in oxide thicknesses, a better understanding of how test conditions affect corrosion results for a broad range of NiTi medical devices can be achieved. Samples were tested in vivo (acute OCP only) and in vitro in whole blood to



Fig. 8 Kaplan–Meier curves for  $E_b$  – OCP: acute BO (a); acute EP (b); chronic BO (c); chronic EP (d)

generate baseline physiologic results to compare against simulated fluid (aerated and deaerated PBS) results.

This study showed that both oxygen content and preexposure time had a significant effect on the corrosion behavior of NiTi, regardless of oxide thickness. Performing testing in vivo allows full understanding of the physiologic corrosion behavior. In this study, in vitro and in vivo whole blood resulted in similar OCP. Although not investigated in this study, it is expected that in vitro E<sub>b</sub> and cyclic polarization curves in whole blood would be similar to that occurring in vivo. However, testing in whole blood alone is undesirable, due to the number of samples needed to establish reliability and the increased cost of testing. This study determined that 1 h data in whole blood were more conservative (i.e., lower  $E_b - OCP$ ) than chronic data for both BO and EP. Therefore, a reasonable compromise might be to test a small sample size in whole blood for 1 h to gain an understanding of the representative physiologic corrosion behavior of the implant and compare those

results to larger scale testing performed in a simulated solution.

Previous investigators have shown that  $E_b - OCP$  remained constant or increased with time, suggesting that 1 h pre-exposure time was conservative [8]. This is in agreement with the results obtained in this study. OCP,  $E_b$ , and  $E_b - OCP$  improved with time for both oxide thicknesses and aerations.

For deaerated PBS testing conditions,  $E_b - OCP$  was comparable to whole blood for both oxide thicknesses and pre-exposure times. However, the actual values of OCP,  $E_b$ , and the cyclic polarization curves were not always similar to those obtained in whole blood. In fact, the chronic EP OCP for deaerated PBS remained ~200 mV more active than whole blood, and the acute BO  $E_b$  for deaerated PBS was found to be ~250 mV more negative than whole blood. Additionally, the cyclic polarization curves for acute deaerated pre-exposure were very different than the curves tested in whole blood, depending on the oxide thickness. The

#### Table 3 Summary of results

Result	Figure
Open circuit potentials (OCP)	
In vitro whole blood OCP was not significantly different than in vivo OCP for both oxide thicknesses $(p = 0.0636 \text{ and } p = 0.9964)$	Figure 2
Control (ASTM F2129) OCP was significantly different than in vivo OCP, depending on oxide thickness $(p < 0.0001 \text{ for BO})$	Figure 2
All OCPs increased over time	Figure 2
Chronic deaerated PBS samples were significantly different than chronic whole blood, depending on the oxide thickness ( $p < 0.0001$ for EP)	Figure 2
Chronic-aerated PBS samples were not significantly different than chronic whole blood regardless of the oxide thickness ( $p = 0.9976$ and $p = 0.7397$ )	Figure 2
Breakdown potentials $(E_b)$	
All E <sub>b</sub> improved over pre-exposure time	Figure 6
$E_b$ tested per ASTM F2129 were significantly different than $E_b$ chronically submerged in whole blood depending on oxide thickness ( $p < 0.0001$ for BO)	Figures 6 and 7
Aerated $E_b \leq$ whole blood $E_b$ for both oxide thicknesses and pre-exposure times, and had similar cyclic polarization curves	Figures 6 and 7
Difference in $E_b - OCP$	
All $E_b - OCP$ values improved over pre-exposure time	Figure 8
Acute pre-exposure to aerated PBS prior to testing in deaerated PBS resulted in negative $E_b - OCP$ values with no pitting observed during open circuit	Figures 8 and 9
Deaerated PBS and whole blood were comparable and the least conservative (i.e., the highest difference between $E_b$ and OCP) test conditions regardless of pre-exposure time and oxide thickness. However acute cyclic polarization curves in deaerated PBS and whole blood were different, depending on oxide thickness	Figures 7 and 8
Aerated PBS was more conservative (i.e., the lower difference between $E_b$ and OCP) than or comparable to whole blood regardless of pre-exposure time and oxide thickness	Figure 8

acute deaerated BO samples exhibited a passivation potential where no such behavior was observed in whole blood. Therefore, testing in a deaerated environment may not fully capture the physiologic corrosion behavior of the sample in a physiologically relevant environment.

Aerated pre-exposure prior to performing the cyclic polarization scan in a deaerated environment has been recommended previously and resulted in an increased OCP and a more conservative  $E_b - OCP$  than testing with a deaerated pre-exposure [7]. Similarly, an increase in OCP and a conservative  $E_b - OCP$  with aerated pre-exposure followed by a deaerated scan were observed in this study. However, acute aerated pre-exposure was not sufficient to prevent the OCP from immediately becoming more active during the deaeration of the solution with nitrogen (Fig. 9a), resulting in a polarization scan starting at a more negative potential than the recorded aerated OCP. This resulted in an extremely conservative  $E_{b}$  – OCP value, in which some values were negative (though corrosion was not observed during the open circuit). Therefore, testing in a deaerated environment following 1 h of aerated pre-exposure produces potentially misleading results. It was found that 200 h of pre-exposure in an aerated solution was sufficient to reach a steady state such that the OCP was not influenced when nitrogen was introduced (Fig. 9b).

Furthermore, chronic-aerated pre-exposure followed by a deaerated scan achieved a representative OCP and a conservative  $E_b$ , resulting in a conservative  $E_b - OCP$  compared to whole blood (~390 mV difference for BO). Therefore, a chronic pre-exposure in an aerated environment prior to a deaerated scan is a conservative testing option; however, it is essential that the OCP reaches a steady state.

Samples were also evaluated in an aerated environment following an aerated pre-exposure. For both oxide thicknesses, acute-aerated OCPs were most comparable to chronic physiologic OCP values. For both time points and oxide thicknesses, aerated cyclic polarization curves and E<sub>b</sub> were similar to whole blood. Additionally, aerated  $E_{b}$  – OCP was less than or equal to whole blood for both time points and oxide thicknesses. Overall, corrosion properties (OCP, Eb, and  $E_b - OCP$ ) increased with time, indicating that acute aerated testing is conservative compared to chronic pre-exposure durations. However, increasing the pre-exposure duration might be a useful option for determining actual chronic corrosion properties. Additionally, testing in an aerated environment allows for a direct comparison to galvanic testing per ASTM F3044 [13]. Regardless of pre-exposure duration, testing in an aerated environment following an aerated pre-exposure is a viable and conservative option for



Fig. 9 BO pre-exposure: 1 h aerated followed by 30 min deaeration with nitrogen (a), 200 h aerated followed by 30 min deaeration with nitrogen (b)

determining the physiologic corrosion behavior of NiTi implants used for medical devices.

# Conclusions

Whole blood can be used to perform in vitro testing to determine baseline corrosion behavior of medical implants and aid in acceptance criterion development.  $E_{\rm b} - OCP$ tested according to the conditions defined in ASTM F2129 was comparable to acute whole blood and is conservative compared to chronic whole blood for both oxide thicknesses of NiTi. However, testing per the conditions in ASTM F2129 resulted in OCP, E<sub>b</sub>, and cyclic polarization curves that were not always comparable to whole blood depending on oxide thickness. A standardized corrosion assessment method should not be dependent on metallic surface finish. Pre-exposing and conducting the polarization scan in aerated PBS achieved  $E_b$ ,  $E_b - OCP$ , and cyclic polarization curves that were comparable to or more conservative than whole blood testing, regardless of preexposure duration and oxide thickness. Testing in aerated PBS also allows direct comparison to coupled galvanic potentials measured using the methods in ASTM F3044. Thus, testing in aerated PBS provides a more conservative and complete assessment of corrosion resistance of metallic medical implants.

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