

# Evaluation of an Expired Nontoxic Amlodipine Besylate Drug as a Corrosion Inhibitor for Low-Carbon Steel in Hydrochloric Acid Solutions

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**Abstract** The corrosion inhibition of Amlodipine Besylate drug as a corrosion control of low-carbon steel in 1 M HCl solution was investigated by electrochemical and chemical techniques. The inhibition efficiency (%IE) was found to increase with an increase in drug concentrations but decreases with increasing the temperature. Results showed that this drug acts as a mixed-type inhibitor. It was found that this drug acts via adsorption on the low-carbon steel surface and the adsorption obeys Langmuir adsorption isotherm. Quantum structure–activity relationships have been studied. The surface morphology of low-carbon steel samples was investigated.

**Keywords** Corrosion inhibition · Low-carbon steel · HCl · Amlodipine Besylate drug

## 1 Introduction

Corrosion is a costly and severe materials science problem. The corrosion of low-carbon steel is the most common form of corrosion, especially in acid solution. It has received a considerable attention as a result of its industrial importance, for example in the chemical cleaning and processing, oil well acidizing, and petrochemical industry. Low-carbon steel which is subjected to painting, electroplating, phosphate coating, and cold rolling must have a clean surface free from oxide scale. To remove unwanted scale, the low-carbon steel is immersed in an acid solution, namely in an acid pickling

bath. Hydrochloric acid solutions are by far the most widely used in pickling bath of low-carbon steel. Because of the general aggressiveness of acid solutions, organic inhibitors are commonly used to reduce the corrosion attack on metallic materials. Majority of the well-known inhibitors for the corrosion of steel in acidic medium are organic compounds containing nitrogen, sulfur, oxygen atoms, or N-hetero cyclic compounds with polar groups. A large number of scientific studies have been devoted to the subject of corrosion inhibitors for low-carbon steel in acidic media [1–12]. Most of the commercial inhibitors are toxic in nature; therefore, replacement by environmentally benign inhibitors is necessary. Few nontoxic compounds have been investigated as corrosion inhibitors by some researchers [13, 14]. The use of drugs offers interesting possibilities for corrosion inhibition due to the presence of heteroatoms like nitrogen, sulfur, and oxygen in their structure, and they are of particular interest because of their safe use, high solubility in water, and high molecular size. Most of the drugs are more expensive than organic inhibitors, and therefore expired drugs can be used as corrosion inhibitors. The use of expired drugs can solve two major environmental and economic problems: limitation of environmental pollution with pharmaceutically active compounds and reduction of the disposal costs of expired drugs. It is reported that the active constituent of the drug degrades only infinitesimally. More than 90 % of the drugs maintained stability long time after the expiry dates [15]. Nicolae has tested two expired drugs carbamazepine and paracetamol as corrosion inhibitors on carbon steel corrosion in H<sub>2</sub>SO<sub>4</sub> and CH<sub>3</sub>COOH and obtained 95 and 85 % efficiency, respectively [16]. Some of the azosulfa and antimalarial drugs have been reported as good corrosion inhibitors [17–19]. Also, the use of piperazine [20], septazole [21], and cefixime [22] drugs as corrosion inhibitors has been reported.

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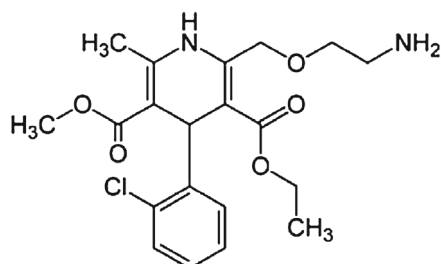
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In the present work, expired Amlodipine Besylate drug has been investigated as a corrosion inhibitor for low-carbon steel in hydrochloric acid using different techniques. Amlodipine Besylate contains N atoms, O atoms,  $-\text{CH}_3$ ,  $-\text{NH}_2$  groups, and  $\pi$ -bond in its structure and has higher molecular size, which are regarded as important factors for good inhibitor performance. Amlodipine Besylate drug is used primarily for lowering blood pressure, to lower the risk of stroke and heart attack, and to prevent chest pains.

## 2 Experimental Methods

### 2.1 Materials and Solutions

Amlodipine Besylate (99.8 % anhydrous) was supplied by Egyptian international pharmaceutical industries company (EIPICO), 10th Ramadan, Egypt. The drug was used without further purification. The test material used was low-carbon steel sample with the following composition (wt %): 0.14 C, 0.6 Mn, 0.05 S, 0.04 P, 0.1 Si, and balance Fe. Test materials were abraded with different emery papers up to 1200 grade, cleaned with acetone, washed with double-distilled water, and properly dried prior to exposure. Analar grade HCl and double-distilled water were used to prepare all solutions.



(*RS*)-3-ethyl 5-methyl 2-[(2-aminoethoxy) methyl]-4-(2-chlorophenyl)-6-methyl-1, 4-dihydropyridine-3, 5-dicarboxylate

Molecular formula  $\text{C}_{20}\text{H}_{25}\text{Cl}\text{N}_2\text{O}_5$ , Molecular weight = 408.9

### 2.2 Weight Loss Tests

Low-carbon steel sheets of  $20 \times 20 \times 2$  mm were abraded with different grades of emery paper and then washed with double distilled water and acetone. After weighing accurately, the specimens were immersed in 100 ml HCl solution with and without addition of different concentrations of the drug. After 3 h, the specimens were taken out, washed, dried, and weighed accurately. The average weight loss of the three parallel low-carbon steel sheets could be

obtained at required temperature. The inhibition efficiency (IE) and the degree of surface coverage ( $\theta$ ) of the investigated drug on the corrosion of low-carbon steel were calculated as follows [23]:

$$\%IE = \theta \times 100 = [1 - (W/W^\circ)] \times 100, \quad (1)$$

where  $W^\circ$  and  $W$  are the values of the average weight losses without and with the addition of the inhibitor, respectively.

### 2.3 Electrochemical Measurements

#### 2.3.1 Potentiodynamic Polarization Measurements

Polarization experiments were carried out in a conventional three-electrode cell with platinum gauze as the auxiliary electrode and a saturated calomel electrode (SCE) coupled to a fine Luggin capillary as the reference electrode. The working electrode was in the form of a square cut from low-carbon steel sheet of equal composition embedded in epoxy resin of polytetrafluoroethylene so that the flat surface area was  $1 \text{ cm}^2$ . Prior to each measurement, the electrode surface was pretreated in the same manner as the weight loss experiments. Before measurements, the electrode was immersed in solution for 30 min until a steady state was reached. The potential was started from  $-600$  to  $+400$  mV versus open circuit potential ( $E_{\text{ocp}}$ ). All experiments were carried out in freshly prepared solutions at  $30^\circ\text{C}$  and were always repeated at least three times to check the reproducibility. Then  $i_{\text{corr}}$  was used for the calculation of inhibition efficiency and surface coverage ( $\theta$ ) as follows:

$$\%IE = \theta \times 100 = (1 - (i_{\text{corr}}/i_{\text{corr}}^\circ)) \times 100, \quad (2)$$

where  $i_{\text{corr}}^\circ$  and  $i_{\text{corr}}$  are the corrosion current densities in the absence and presence of inhibitor, respectively.

#### 2.3.2 Electrochemical Impedance Spectroscopy (EIS) Tests

Impedance measurements were carried out using AC signals of 5 mV peak-to-peak amplitude at the open circuit potential in the frequency range of 100 kHz to 0.1 Hz. All impedance data were fitted to appropriate equivalent circuit.

#### 2.3.3 Electrochemical Frequency Modulation (EFM) Tests

EFM experiments were performed with applying potential perturbation signal with amplitude 10 mV with two sine waves of 2 and 5 Hz. The choice for the frequencies of 2 and 5 Hz was based on three arguments [24, 25]. The larger peaks were used to calculate the corrosion current density ( $i_{\text{corr}}$ ), the Tafel slopes ( $\beta_c$  and  $\beta_a$ ), and the causality factors CF-2 and CF-3 [26]. The  $^\circ$ electrode potential was allowed to

stabilize for 30 min before starting the measurements. All the experiments were conducted at 30 °C. Measurements were performed using Gamry Instrument Potentiostat/Galvanostat/ZRA (PCI4-G750). Gamry applications include DC 105 software for DC corrosion measurements, EIS 300 software for electrochemical impedance spectroscopy measurements, and EFM 140 for electrochemical frequency modulation measurements along with a computer for collecting data. Echem analyst v 6.03 software was used for plotting, graphing, and fitting data.

## 2.4 Quantum Calculations

The molecular structure of the investigated compound was optimized initially with PM3 semi-empirical method so as to speed up the calculation. All the quantum chemical calculations were performed with Material *studio V. 6.0*.

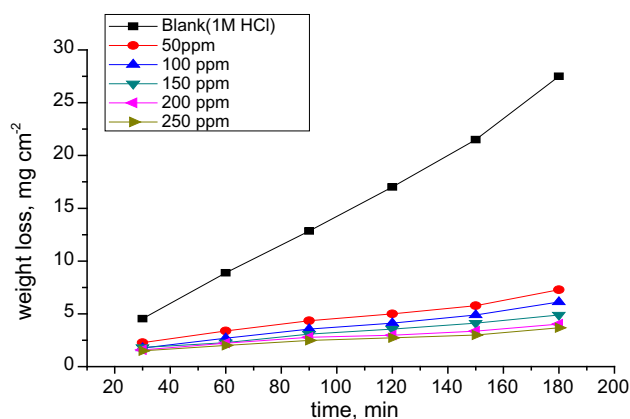
## 2.5 Scanning Electron Microscopy (SEM) Measurements

The electrode surface of low-carbon steel was examined by scanning electron microscope—type JOEL 840, Japan, before and after immersion in 1 M HCl test solution in the absence and presence of the optimum concentrations of the investigated inhibitors at 25 °C, for an immersion time of 1 day. The specimens were washed gently with distilled water, then dried carefully, and examined without any further treatments.

## 3 Results and Discussion

### 3.1 Chemical Method (Weight Loss Tests)

Weight loss of low-carbon steel was determined, at various time intervals, in the absence and presence of different concentrations of Amlodipine Besylate. The obtained weight loss-time curves are represented in Fig. 1. The inhibition efficiency of corrosion was found to be dependent on the inhibitor concentration. The curves obtained in the presence of inhibitor fall significantly below that of free acid. In all cases, the increase in the inhibitor concentration was accompanied by a decrease in weight loss and an increase in the percentage inhibition. These results lead to the conclusion that the compound under investigation is fairly efficient as inhibitors for low-carbon steel dissolution in hydrochloric acid solution. Also, the degree of surface coverage ( $\theta$ ) by the inhibitor would increase by increasing the inhibitor concentration. In order to get a comparative view, the variation of the percentage inhibition (%IE) of the inhibitor with its concentrations was calculated and its values obtained are summarized in Table 1.



**Fig. 1** Weight loss–time curves for the corrosion of low-carbon steel in 1 M HCl in the absence and presence of different concentrations of Amlodipine Besylate at 30 °C

**Table 1** Inhibition efficiency and corrosion rate (C.R) of Amlodipine Besylate for the corrosion of low-carbon steel in 1 M HCl from weight loss measurements at different concentrations and at 30 °C

[Inh] ppm	C.R mg cm <sup>-2</sup> min <sup>-1</sup>	$\theta$	%IE
Blank	0.1420	-	-
50	0.0420	0.706	70.6
100	0.0283	0.758	75.8
150	0.0235	0.791	79.1
200	0.0220	0.825	82.5
250	0.0227	0.840	84.0

### 3.2 Effect of Temperature

The effect of temperature on the corrosion rate of low-carbon steel in 1 M HCl and in the presence of different inhibitor concentrations was studied at two temperatures (30 and 45 °C) using weight loss measurements. As the temperature increases, the rate of corrosion increases and the inhibition efficiency of Amlodipine Besylate decreases as shown in Table 2. The adsorption behavior of Amlodipine Besylate on HCl surface occurs through physical adsorption.

### 3.3 Adsorption Isotherms

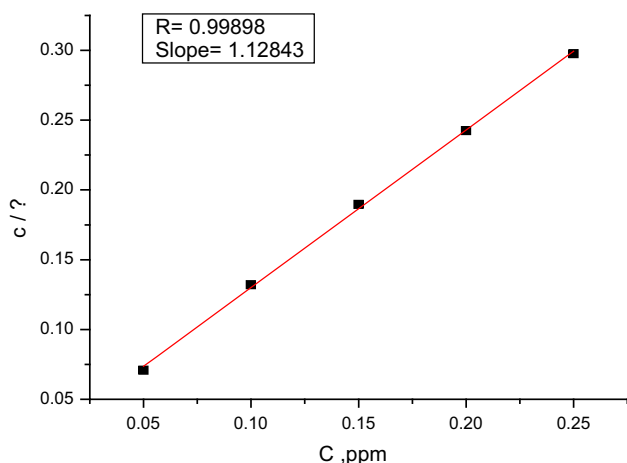
One of the most convenient ways of expressing adsorption quantitatively is by deriving the adsorption isotherm that characterizes the metal/inhibitor/environment system. Various adsorption isotherms were applied to fit  $\theta$  values, but the best fit was found to obey Langmuir adsorption isotherm which is represented in Fig. 2 for Amlodipine Besylate, and Langmuir adsorption isotherm may be expressed as

**Table 2** Data of weight loss measurements for low-carbon steel in 1 M HCl solution in the absence and presence of different concentrations of Amlodipine Besylate at 30 and 45 °C

[Inh] ppm	30 °C		45 °C	
	C.R mg cm <sup>-2</sup> min <sup>-1</sup>	% IE	C.R mg cm <sup>-2</sup> min <sup>-1</sup>	% IE
Blank	0.1420	–	0.46	–
50	0.0420	70.6	0.23	49.9
100	0.0283	75.8	0.21	54.2
150	0.0235	79.1	0.17	62.5
200	0.0220	82.5	0.16	65.8
250	0.0227	84.0	0.14	69.0

$$(C/\theta) = 1/K_{\text{ads}} + C, \quad (3)$$

where  $C$  is the concentration (mol L<sup>-1</sup>) of the inhibitor in the bulk electrolyte,  $\theta$  is the degree of surface coverage ( $\theta = \% \text{ IE}/100$ ), and  $K_{\text{ads}}$  is the adsorption equilibrium constant. A plot of  $C$  versus  $C/\theta$  should give straight line. In order to get a comparative view, the variation of the adsorption equilibrium constant ( $K_{\text{ads}}$ ) of the Amlodipine Besylate with its concentration was calculated. The experimental data give good curve fitting for the applied adsorption isotherm as the correlation coefficients ( $R^2$ ) were more than 0.99. The values obtained are shown in Table 3. These results confirm the assumption that this compound is adsorbed on the metal surface through the protonated (N, O) atoms or via the lone pair of electrons of (N, O) atoms. The extent of inhibition is directly related to the performance of adsorption layer which is a sensitive function of the molecular structure. The equilibrium constant of adsorption  $K_{\text{ads}}$  obtained from the intercept of Langmuir adsorption isotherm is related to the free energy of adsorption  $\Delta G^{\circ}_{\text{ads}}$  as follows:

**Fig. 2** Langmuir adsorption isotherm for Amlodipine Besylate drug**Table 3** Thermodynamic parameters for the adsorption on low-carbon steel surface in 1 M HCl at different temperatures

Temp. °C	$K_{\text{ads}}$ M <sup>-1</sup>	$-\Delta G^{\circ}_{\text{ads}}$ kJ mol <sup>-1</sup>	$Q_{\text{ads}}$ kJ mol <sup>-1</sup>	$R^2$
30	57.971	20.3	–	0.999
45	21.857	18.8	45.4	0.992

$$K_{\text{ads}} = 1/55.5 \exp[-\Delta G^{\circ}_{\text{ads}}/RT], \quad (4)$$

where 55.5 is the molar concentration of water in the solution in M<sup>-1</sup>.

Table 3 clearly shows a good dependence of  $\Delta G^{\circ}_{\text{ads}}$  on T, indicating the good correlation among thermodynamic parameters. The negative value of  $\Delta G^{\circ}_{\text{ads}}$  reflects that the adsorption of the studied compound on low-carbon steel surface from 1 M HCl solution is spontaneous process and stability of the adsorbed layer on the low-carbon steel surface. Generally, the values of  $\Delta G^{\circ}_{\text{ads}}$  around  $-20$  kJ mol<sup>-1</sup> or lower are consistent with the electrostatic interaction between the charged molecules and the charged metal (physical adsorption); those around  $-40$  kJ mol<sup>-1</sup> or higher involve charge sharing or transfer from organic molecules to the metal surface to form a coordinate type of bond (chemisorption) [27]. From the obtained values of  $\Delta G^{\circ}_{\text{ads}}$ , the existence of physical adsorption was observed. The unshared electron pairs in oxygen and nitrogen may interact with d-orbitals of low-carbon steel to provide a protective physical adsorbed film [28]. The values of thermodynamic parameters for the adsorption of tested compound can provide valuable information about the mechanism of corrosion inhibition. An estimate of heat of adsorption was obtained from the trend of surface coverage with temperature as follows [29]:

$$Q_{\text{ads}} = 2.303R \left[ \log \left( \frac{\theta_2}{1 - \theta_2} \right) - \log \left( \frac{\theta_1}{1 - \theta_1} \right) \right] \times \left( \frac{T_1 \times T_2}{T_2 - T_1} \right), \quad (5)$$

where  $\theta_1$  and  $\theta_2$  are the degree of surface coverage at temperature  $T_1$  and  $T_2$ , respectively. The calculated values for both parameters are shown in Table 3.

### 3.4 Kinetic-Thermodynamic Corrosion Parameters

The effect of temperature on corrosion inhibition of low-carbon steel in 1 M HCl solution in the absence and presence of different concentrations of the investigated compound at different temperatures of 30 and 45 °C was studied using weight loss measurements. The corrosion rate was found to increase with increasing temperature both in uninhibited and inhibited solutions. The apparent activation energy ( $E_a^*$ ) for the corrosion process can be calculated from Arrhenius-type equation:

$$\text{Log} \rho_2 / \rho_1 = (E_a^* / 2.303R) \times \left( \frac{1}{T_1} - \frac{1}{T_2} \right), \quad (6)$$

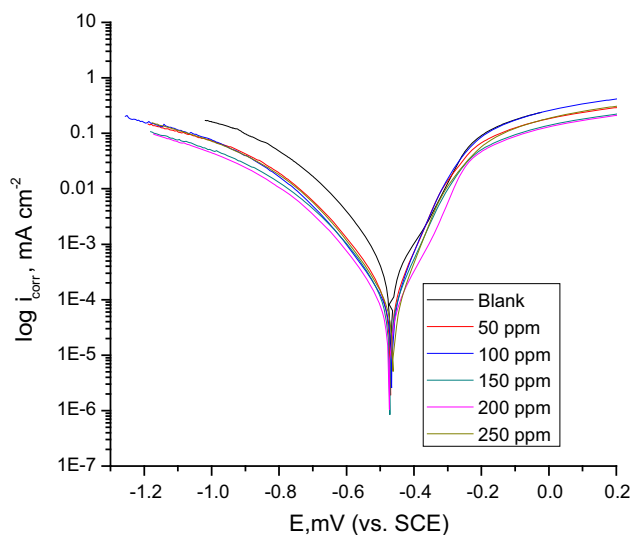
where  $E_a^*$  is the apparent activation corrosion energy,  $R$  is the universal gas constant, and  $\rho_1$  and  $\rho_2$  are the corrosion rates at temperature  $T_1$  and  $T_2$ , respectively

The calculated values of  $E_a^*$  are  $63.5 \text{ kJ mol}^{-1}$  for blank and  $72.2 \text{ kJ mol}^{-1}$  in the presence of the investigated compound. The value of  $E_a^*$  determined in solution containing the investigated compound is higher than that in its absence.

The decrease in %IE values as the temperature is increased and high values of  $E_a^*$  in the presence of the investigated compound can be interpreted as an indication for a physical or columbic type of adsorption [30]. The high  $E_a^*$  value in the inhibited solution can be correlated with the increased thickness of the double layer, which enhances the activation energy of the corrosion process.

### 3.5 Potentiodynamic Polarization Tests

Figures 3 shows typical polarization curves for low-carbon steel in 1 M HCl media. In the presence of Amlodipine Besylate, both the cathodic and anodic current densities were greatly decreased over a wide potential range. Various corrosion parameters such as corrosion potential ( $E_{\text{corr}}$ ), anodic and cathodic Tafel slopes ( $\beta_a$ ,  $\beta_c$ ), corrosion current density ( $i_{\text{corr}}$ ), degree of surface coverage ( $\theta$ ), and inhibition efficiency (%IE) are shown in Table 4. It can be seen from the experimental results that in all cases the addition of Amlodipine



**Fig. 3** Potentiodynamic polarization curves for the dissolution of low-carbon steel in 1 M HCl in the absence and presence of different concentrations of Amlodipine Besylate at 30 °C

Besylate induced a significant decrease in cathodic and anodic currents. The values of  $E_{\text{corr}}$  were affected and slightly changed by the addition of Amlodipine Besylate. This indicates that Amlodipine Besylate acts as a mixed-type inhibitor. The slopes of anodic and cathodic Tafel lines ( $\beta_a$  and  $\beta_c$ ) were slightly changed (Tafel lines are parallel) on increasing the concentration of the tested compound, which indicates that there is no change in the mechanism of inhibition in the presence and absence of Amlodipine Besylate. The order of inhibition efficiency of Amlodipine Besylate at different concentrations as observed by polarization measurements are listed in Table 4. The results are in good agreement with those obtained from weight loss measurements.

### 3.6 Electrochemical Impedance Spectroscopy (EIS) Tests

EIS is well established and is a powerful technique for studying the corrosion. Surface properties, electrode kinetics, and mechanistic information can be obtained from impedance diagrams. Figure 4 shows the Nyquist (a) and Bode (b) plots obtained at open circuit potential. The increase in the size of the capacitive loop with the addition of investigated compound shows that a barrier gradually forms on the low-carbon steel surface (Fig. 4a). Bode plot (Fig. 4b) shows that the total impedance increases with increasing inhibitor concentration ( $\log Z$  vs.  $\log f$ ) except for ( $\log f$  vs. phase). Bode plot also shows the continuous increase in the phase angle shift, obviously correlating with the increase of inhibitor adsorbed on low-carbon steel surface. The Nyquist plot does not yield perfect semicircles as expected from the theory of EIS. The deviation from ideal semicircle was generally attributed to the frequency dispersion [31] as well as to the inhomogeneities of the surface. EIS spectra of the investigated compounds were analyzed using the equivalent circuit (Fig. 5), which represents a single charge transfer reaction and fits well with our experimental results. The constant phase element, CPE, is introduced in the circuit instead of a pure double-layer capacitor to give a more accurate fit [32]. The double-layer capacitance,  $C_{\text{dl}}$ , for a circuit including a CPE parameter ( $Y_0$  and  $n$ ) was calculated using the following equation [33]:

$$C_{\text{dl}} = Y_0(\omega_{\text{max}})^{n-1}, \quad (7)$$

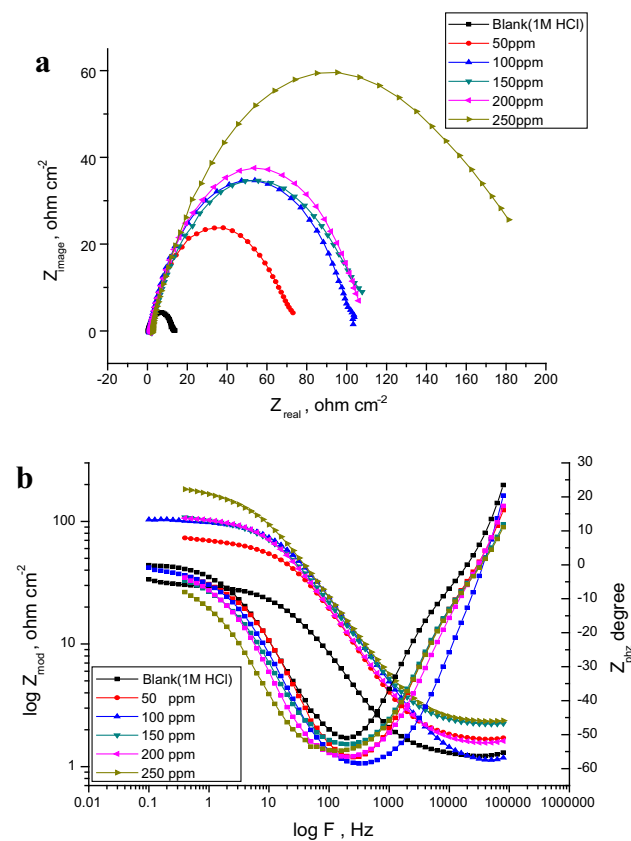
where  $Y_0$  is the magnitude of the CPE,  $\omega_{\text{max}} = 2\pi f_{\text{max}}$ ,  $f_{\text{max}}$  is the frequency at which the imaginary component of the impedance is maximal, and the factor  $n$  is an adjustable parameter that usually lies between 0.50 and 1.0. After analyzing the shape of the Nyquist plots, it is concluded that the curves approximated by single capacitive



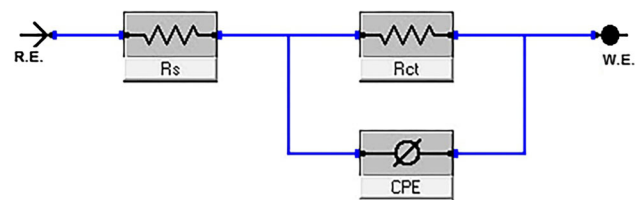
**Table 4** Corrosion potential ( $E_{\text{corr}}$ ), corrosion current density ( $i_{\text{corr}}$ ), Tafel slopes ( $\beta_c$ ,  $\beta_a$ ), corrosion rate (CR), degree of surface coverage ( $\theta$ ), and inhibition efficiency (%IE) of low-carbon steel in 1 M HCl at

[Inh.] ppm	$-E_{\text{corr}}$ mV versus SCE	$i_{\text{corr}} \times 10^{-4}$ $\mu\text{A cm}^{-2}$	$\beta_c$ mV dec $^{-1}$	$\beta_a$ mV dec $^{-1}$	CR mpy	$\theta$	%IE
Blank	469	301.0	117	116	137.40	–	–
50	470	105.0	118	79	47.82	0.651	65.1
100	466	85.9	128	71	39.24	0.715	71.5
150	471	84.5	120	83	38.59	0.719	71.9
200	472	63.1	118	96	28.83	0.790	79.0
250	462	49.7	79	63	22.70	0.835	83.5

30 °C for Amlodipine Besylate in the absence and presence of increasing concentrations of investigated compound at 30 °C

**Fig. 4** **a** Nyquist plots for the corrosion of low-carbon steel in 1 M HCl in the absence and presence of different concentrations of Amlodipine Besylate at 30 °C. **b** Bode plots for the corrosion of low-carbon steel in 1 M HCl in the absence and presence of different concentrations of Amlodipine Besylate at 30 °C

semicircles show that the corrosion process was mainly charge transfer controlled [34, 35]. The general shape of the curves is very similar for all samples (in the presence or absence of inhibitor for different immersion times) indicating no change in the corrosion mechanism [36]. From the impedance data in Table 5, we conclude that the value of  $R_{\text{ct}}$  increases with increasing the concentration of

**Fig. 5** Equivalent circuit model used to fit experimental EIS**Table 5** Electrochemical kinetic parameters obtained by EIS technique for low-carbon steel in 1 M HCl without and with various concentrations of Amlodipine Besylate at 30 °C

[Inh.] ppm	$C_{\text{dl}} \times 10^4$ F cm $^{-2}$	$R_p$ $\Omega$ cm $^2$	$\theta$	%IE
Blank	5.38	16.71	–	–
50	5.00	96.55	0.827	82.7
100	3.59	116.2	0.856	85.6
150	3.72	144.5	0.884	88.4
200	1.75	160.0	0.896	89.6
250	1.67	291.7	0.943	94.3

Amlodipine Besylate and this indicates an increase in %IE<sub>EIS</sub>, which is in concordance with the previous results obtained. In fact, the presence of Amlodipine Besylate enhances the value of  $R_{\text{ct}}$  in acidic solution. The values of double-layer capacitance are also brought down to the maximum extent in the presence of Amlodipine Besylate and the decrease in the values of CPE follows the order similar to that obtained for  $i_{\text{corr}}$  in this study. The decrease in  $\text{CPE}/C_{\text{dl}}$  results from a decrease in local dielectric constant and/or an increase in the thickness of the double layer, suggesting that organic derivatives inhibit the low-carbon steel corrosion by adsorption at metal/acid interface [37]. The inhibition efficiency was calculated from the charge transfer resistance data using the following equation [38]:

$$\%IE_{EIS} = [1 - (R_{ct}^{\circ}/R_{ct})] \times 100, \tag{8}$$

where  $R_{ct}^{\circ}$  and  $R_{ct}$  are the charge transfer resistance values without and with inhibitor, respectively.

### 3.7 Electrochemical Frequency Modulation (EFM) Tests

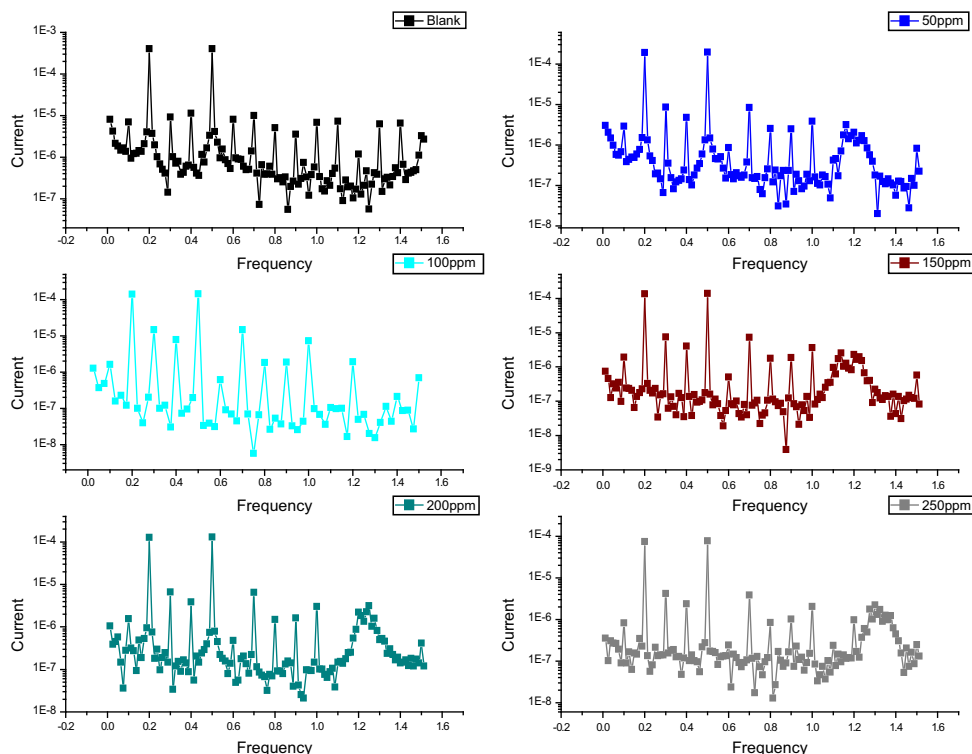
EFM is a nondestructive corrosion measurement technique that can directly and quickly determine the corrosion current values without prior knowledge of Tafel slopes, and with only a small polarizing signal. These advantages of EFM technique make it an ideal candidate for online corrosion monitoring [39]. The great strength of the EFM is the causality factors which serve as an internal check on the validity of EFM measurement. The causality factors CF-2 and CF-3 are calculated from the frequency spectrum of the current responses. Figure 6 shows the EFM intermodulation spectra (current vs frequency) of low-carbon steel in HCl solution containing different concentrations of Amlodipine Besylate. The harmonic and intermodulation peaks are clearly visible and are much larger than the background noise. The larger peaks were used to calculate the corrosion current density ( $i_{corr}$ ), the Tafel slopes ( $\beta_c$  and  $\beta_a$ ), and the causality factors (CF-2 and CF-3). These electrochemical parameters are listed in Table 6. The data presented in Table 6 obviously show that the addition of the tested compound at a given concentration to the acidic

solution decreases the corrosion current density, indicating that this compound inhibits the corrosion of low-carbon steel in 1 M HCl through adsorption. The causality factors obtained under different experimental conditions are approximately equal to the theoretical values (2 and 3) indicating that the measured data are verified and of good quality. The inhibition efficiencies  $\%IE_{EFM}$  increase by increasing the inhibitor concentration and were calculated using Eq. 2.

### 3.8 Surface Examinations

Scanning electron microscope (SEM) and energy-dispersive X-ray (EDX) experiments were carried out in order to verify if the investigated compound is in fact adsorbed on low-carbon steel surface or just peeled off the surface. SEM images were indicative of the changes that accompany both corrosion and protection of the low-carbon steel surface (Fig. 7a–c). Figure 7a shows the free metal, while Fig. 7b shows the damage caused to the surface by hydrochloric acid. Figure 7c shows SEM images of the low-carbon steel surface after treatment with 1 M HCl containing 150 ppm of inhibitor. From these images, it is obvious that the steel surface seems to be almost unaffected by corrosion. This is because of adsorption of inhibitor, forming a thin protective film of the inhibitor on the metal surface. This film is responsible for the highly efficient inhibition by this inhibitor. The corresponding EDX profile

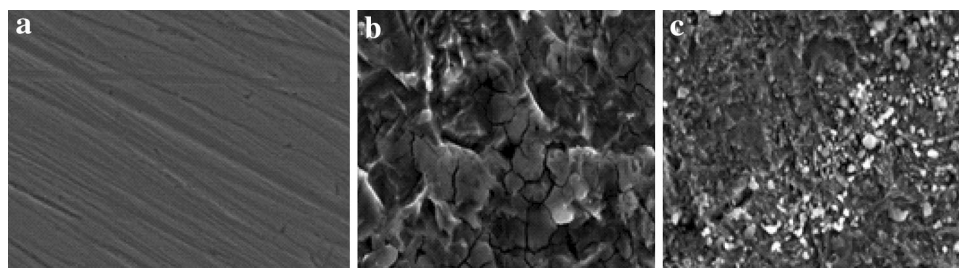
**Fig. 6** EFM spectra for low-carbon steel in 1 M HCl in the absence and presence of different concentrations of Amlodipine Besylate at 30 °C



**Table 6** Electrochemical kinetic parameters obtained by EFM technique for low-carbon steel in 1 M HCl in the absence and presence of different concentrations of Amlodipine Besylate at 30 °C

[Inh] ppm	$i_{\text{corr}}$ ( $\mu\text{A cm}^2$ )	$\beta_a$ (mV dec $^{-1}$ )	$\beta_c$ (mV dec $^{-1}$ )	CF-2	CF-3	CR mpy	$\theta$	%IE
Blank	700.4	104.8	124.0	1.94	2.79	7.37	–	–
50	308.8	91.45	121.0	1.92	2.88	0.23	0.60	60
100	274.4	89.14	204.4	1.97	3.17	1.76	0.61	61
150	210.2	85.76	120.3	1.94	2.77	0.62	0.70	70
200	205.7	89.04	123.3	1.95	3.12	1.26	0.71	71
250	127.9	93.02	133.5	1.94	2.85	0.81	0.82	82

**Fig. 7** SEM micrographs of low-carbon steel surface **a** before immersion in 1 M HCl, **b** after 24 h of immersion in 1 M HCl, and **c** after 24 h of immersion in 1 M HCl + 150 ppm of Amlodipine Besylate



analyses are presented in Fig. 7 for the investigated drug. It is also important to notice the existence of C, N, and O peaks in the EDX spectra of the low-carbon steel surface corresponding to the samples immersed for 1 day in solutions containing 150 ppm of this drug. The formation of a thin inhibitor film is in agreement with the SEM observations (Fig. 8).

The results in Table 7 showed that the % weight of Fe in the presence of the drug is decreased and % weight of C, O, and N atoms increased. This is due to the film formation of the drug on the low-carbon steel surface.

### 3.9 Quantum Calculations

The energy of highest occupied molecular orbital ( $E_{\text{HOMO}}$ ) indicates the ability of the molecule to donate electrons ( $-8.962$  eV) to an appropriate acceptor with empty molecular orbitals, whereas the energy of unoccupied molecular orbital ( $E_{\text{LUMO}}$ ) indicates its ability to accept electrons ( $-0.472$  eV). The lower the value of  $E_{\text{LUMO}}$ , the more the ability of the molecule to accept electrons [40]. The higher the value of  $E_{\text{HOMO}}$  of the inhibitor, the easier is its ability to offer electrons to the unoccupied d-orbital of metal surface and the greater is its inhibition efficiency.

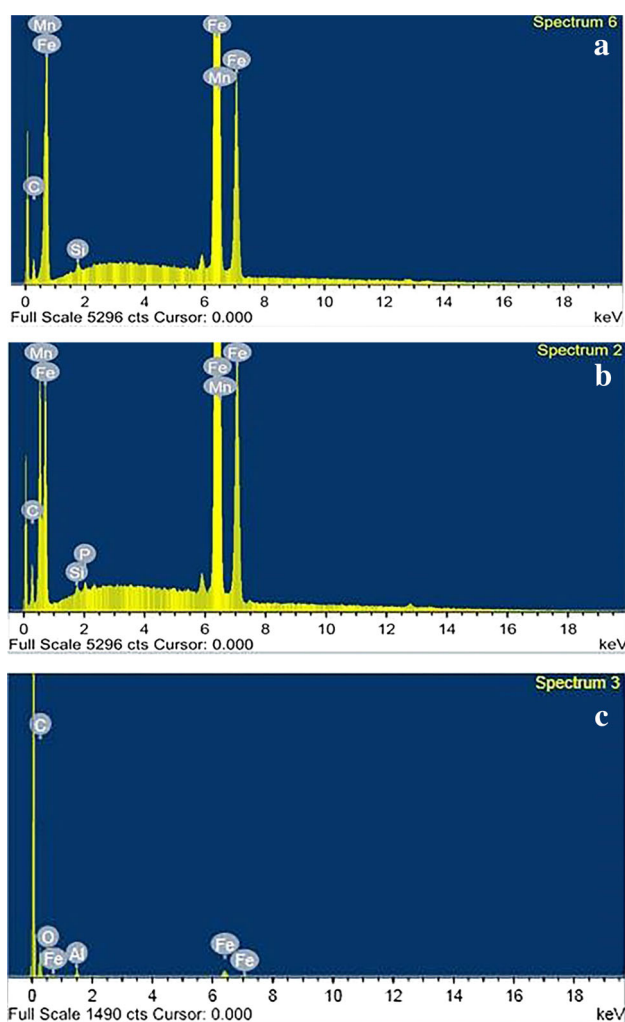
The  $E_{\text{HOMO}} - E_{\text{LUMO}}$  energy gap,  $\Delta E$  approach, ( $8.490$  eV) which is an important stability index, is applied to develop theoretical models for explaining the structure and conformation barriers in many molecular systems. The smaller the value of  $\Delta E$ , the more is the probable inhibition efficiency the compound [41]. Variation in the inhibition

efficiency of the inhibitor depends on the presence of electronegative O and N atoms as a substituent in their molecular structure. The calculated charges of selected atoms are presented in Fig. 9.

### 3.10 Mechanism of Corrosion Inhibition

The inhibition mechanism involves the adsorption of the inhibitor on the metal surface immersed in aqueous HCl solution. Four types of adsorption [42] may take place involving organic molecules at the metal–solution interface: (1) electrostatic attraction between the charged molecules and the charged metal; (2) interaction of unshared electron pairs in the molecule with the metal; (3) interaction of  $\pi$ -electrons with the metal; and (4) combination of all the above. From the observations drawn from the different methods, corrosion inhibition of low-carbon steel in 1 M HCl solutions by the investigated inhibitor as indicated from weight loss, potentiodynamic polarization, and EIS techniques was found to depend on the concentration and the nature of the inhibitor. Amlodipine Besylate contains polar groups such as oxygen and nitrogen. Each atom is a chemisorption center and the inhibition efficiency depends on the electron density around the chemisorption center; the higher the electron density at the chemisorption center, the greater is the inhibition efficiency. This inhibitor has high inhibition efficiency as it has oxygen and N atoms with lone pair of electrons. These electrons interact with the vacant d-orbital of iron present in the low-carbon steel surface and adsorb strongly thereby blocking more number



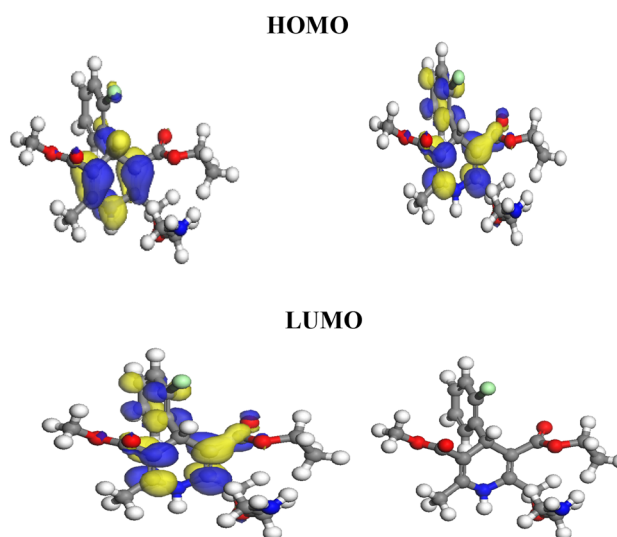


**Fig. 8** EDX spectra of low-carbon steel in 1 M HCl **a** before immersion in 1 M HCl, **b** after 24 h of immersion in 1 M HCl, and **c** after 24 h of immersion in 1 M HCl + 150 ppm of Amlodipine Besylate

**Table 7** Surface composition (wt %) of low-carbon steel after 24 h of immersion in 1 M HCl without and with 150 ppm of the studied drug

Mass %	Fe	C	O	N
Pure	87.72	12.28	–	–
Blank	82.06	17.94	–	–
150 ppm	65.02	23.28	17.8	11.70

of adsorption sites on the low-carbon steel surface. The presence of oxygen and nitrogen caused a resonance effect which facilitates stronger adsorption of inhibitor on low-carbon steel surface. This leads to high IE for Amlodipine Besylate. It has been previously reported in literature that the inhibiting effect depends mainly on inhibitor concentration, molecular structure, size, and structure of the side chain in the organic compounds.



**Fig. 9** Optimized molecular structure of inhibitor and their frontier molecular orbital density distribution (HOMO and LUMO)

## 4 Conclusions

From the overall experimental results, the following conclusions can be deduced:

1. The investigated compound is a good inhibitor and acts as a mixed-type inhibitor for low-carbon steel corrosion in 1 M HCl solution.
2. Reasonably good agreement was observed between the values obtained by the weight loss and electrochemical measurements.
3. The results obtained from all measurements showed that the inhibition efficiency increases with the increase in the inhibitor concentration and decreases with the rise in temperature.
4. Double-layer capacitances decrease with respect to blank solution when the inhibitor is added. This fact confirms the adsorption of this molecule on the low-carbon steel surface.
5. The thermodynamic parameters revealed that the inhibition of corrosion by the investigated compound is due to the formation of a physical adsorbed film on the metal surface.
6. The adsorption of inhibitor on low-carbon steel surface in HCl solution follows Langmuir isotherm for the compound.
7. The values of inhibition efficiency obtained from the different independent quantitative techniques used show the validity of the results.
8. Quantum chemical parameters for this investigated compound were calculated to provide further insight into the mechanism of inhibition of the corrosion process.

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