



# Failure mode analysis on compression of lattice structures with internal cooling channels produced by laser powder bed fusion

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**Abstract** Conformal cooling coils have been developed during the last decades through the use of additive manufacturing (AM) technologies. The main goal of this study was to analyze how the presence of an internal channel that could act as a conformal cooling coil could affect compressive strength and quasi-elastic gradient of AlSi10Mg lattice structures produced by laser powder bed fusion (LPBF). Three different configurations of samples were tested in compression at 25 °C and 200 °C. The reference structures were body centered cubic (BBC) in the core of the samples with vertical struts along Z (BCCZ) lattices in the outer perimeter, labelled as NC samples. The main novelty consisted in inserting a straight elliptical channel and a 45° elliptical channel inside the BCCZ lattice structures, labelled as SC and 45C samples respectively. All the samples were then tested in as-built (AB) condition, and after two post process heat treatments, commonly used for AlSi10Mg LPBF industrial components, a stress relieving (SR) and a T6 treatment. NC lattice structures AB exhibited an overall fragile fracture and therefore the SC and 45C configuration samples were tested only after thermal treatments. The test at 25 °C showed that all types

of samples were characterized by negligible variations in their quasi-elastic gradients and yield strength. On the contrary, the general trend of stress-strain curves was influenced by the presence of the channel and its position. The test at 200 °C showed that NC, SC and 45C samples after SR and T6 treatments exhibited a metal-foam like deformation.

**Keywords** Laser powder bed fusion (LPBF) · Conformal cooling channel · Lattice structures · Failure mode analysis · Mechanical properties at 200 °C

## 1 Introduction

Additive manufacturing (AM) has revolutionized many industrial sectors including the mold industry. In fact, in the last few years some studies showed the possibility of creating molds with conformal cooling coils, i.e., channels that optimized thermal distribution and sped up cooling and production times, through additive technologies [1, 2]. In addition, thanks to AM processes, lattice structures were easily included into the mold bulk in order to minimize the mass of the component maintaining constant structural characteristics and enhancing heat dissipation [3]. Generally, research activities on AM molds are focused on the mold design, that is optimized through numerical simulation to improve heat exchange [4, 5] or to evaluate the structural characteristics of lattice samples [6, 7].

Besides the mold industry, the use of lattice structures in light alloys produced by AM has also been adopted in other industrial sectors, such as automotive or aerospace due to the lightweight and the obvious related benefits, encouraging the development and characterization of different types of lattices, such as faces centered cubic (FCC), body

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centered cubic (BCC), their variants with reinforcement rods along the Z axis (FCCZ or BCCZ), gyroid and diamond lattices [8, 9]. In particular, in the last years an increasing number of papers presented the mechanical responses of various types of AM trabecular structures, from static [10–15] to dynamic [16–18] points of view. Most of these studies [8, 10, 11, 15] were focused on the evaluation of load-bearing capacity of the different lattice types. Other investigations evaluated the effects of the number and dimension of cells and of the struts [10, 12] and of the volume fraction [13, 14] on the mechanical performances of lattice structures. Furthermore, other studies confirmed that the fracture process depended on lattice type and number of layers [8, 19], volume fraction and lattice parameters [20–23] and thermal treatment applied [24, 25]. The type of fracture is a key aspect to assess in the tested samples [10, 11, 14] due to the fact that stable fracture modes prevent catastrophic component failure.

Through the choice of design parameters for the construction of the lattice structures [21] and the correct evaluation of their volume fraction [20, 22], it is possible to modulate their static mechanical characteristics. By varying the relative density of the samples, results similar to the model proposed by Gibson-Ashby for foams were obtained for aluminum lattice structures [20, 22].

In addition, a recent study focused on AlSi10Mg BCCZ structures by laser powder bed fusion (LPBF)—the ISO/ASTM 52900 standard name of the process also known in literature as selective laser melting (SLM) or direct metal laser sintering (DMLS)—revealed that the number of layers and cells affected Young's modulus, compressive strength and fracture mode [19]. It was demonstrated that as the number of layers increased both the initial compressive strength and the quasi-elastic gradient decreased. In addition, whereas in BCCZ mono-layer samples' fracture was caused by Z axis strut buckling and subsequent collapse of the diagonal struts, in samples with more than 5 layers the load-bearing capacities of cells decreased by the unconstrained boundary conditions of nodes. In another study, Ferro et al. [23] observed that in BCCZ samples with more than 5 layers the damaging process was based on the shear band fracture with localized fracture zones and no evidence of a homogeneous plastic deformation through the samples.

On the other hand, the fracture conditions of AlSi10Mg lattice structures can be modified also through suitable post

process heat treatments [24, 25]. It is well known that AM products are often treated with annealing to reduce residual stresses due to repeated heating and cooling and high thermal gradients [26, 27]. In other studies, solutioning, quenching and artificial aging heat treatments (T6) were carried out on LPBF aluminum parts to study the effects on mechanical properties, despite the loss of the very fine microstructure, typical of the as-built (AB) state. It has been demonstrated that AB parts have superior mechanical strength compared to thermally treated ones, with a lower ductility [27, 28]. As known, this behavior can be explained considering the strengthening given by the interactions of dislocations and residual stresses [29].

However, putting together the extensive research which has been carried out on trabecular structures produced by AM for the mold industry and for lightweight structural applications, to the authors knowledge there is not a study to evaluate the effects of introducing in the lattice design a channel for a conformal cooling coil on the lattice structure mechanical behavior. Therefore, the main goal of this study was to analyze how the presence of internal channels could affect compressive strength and quasi-elastic gradient of AlSi10Mg lattice structures produced by LPBF. Starting from the work carried out by Ferro et al. [23], the fracture behavior was assessed for lattice samples with and without a cooling coil inside the structure at room temperature and at 200 °C. This temperature is considered of great interest in designing lightweight structures in aluminum alloy by LPBF able to work also as heat-exchanging systems. The samples with channels were produced in two different configurations in order to evaluate the effect of the relative internal position and in order to have two simple “bricks” which can be used as starting elements to design more complex structures. Samples were tested in AB condition and after two post process thermal treatments, a stress relieving (SR) and a T6.

## 2 Materials and methods

AlSi10Mg spherical powder used in this work was produced by gas atomization (EOS GmbH), with a mean size of 24  $\mu\text{m}$ . The chemical composition is reported in Table 1, as specified in the supplier datasheet [30].

On the basis of a previous study [23], the lattice structures considered have BCC type cell in the sample core and BCC with struts along Z axis (BCCZ) in the perimetric

**Table 1** AlSi10Mg powder chemical composition (mass fraction, %)

Al	Si	Fe	Cu	Mn	Mg	Ni	Zn	Pb	Sn	Ti
Balance	9.0–11.0	0.55	0.05	0.45	0.2–0.04	0.05	0.10	0.05	0.05	0.15

outer cells of the specimens. The whole outer dimensions for the samples are 21.0 mm length, 21.0 mm width and 41.4 mm height. The relative density, i.e., the ratio of the density of the actual structure to that of the bulk specimen, was set uniform for all specimens and equal to 0.4. On the basis of results described by Ferro et al. [23] in order to maximize sample quasi-elastic gradient and yield strength, BCCZ structures with cells size of 4 mm and struts diameter of 1.2 mm were exploited. The studied structure consists of 10 planes of elementary cells reinforced by 2 continuous outer surfaces at the basement and at the top of the specimen. Three configurations of specimens were designed and labelled as follows (see Fig. 1).

- (i) NC: with no channel, studied as a reference;
- (ii) SC: with straight channel, in which the channel is placed parallel to one of the smaller sides of the specimens;
- (iii) 45C: with 45° channel, in which the channel is placed at 45° respect to one of the smaller sides of the specimens.

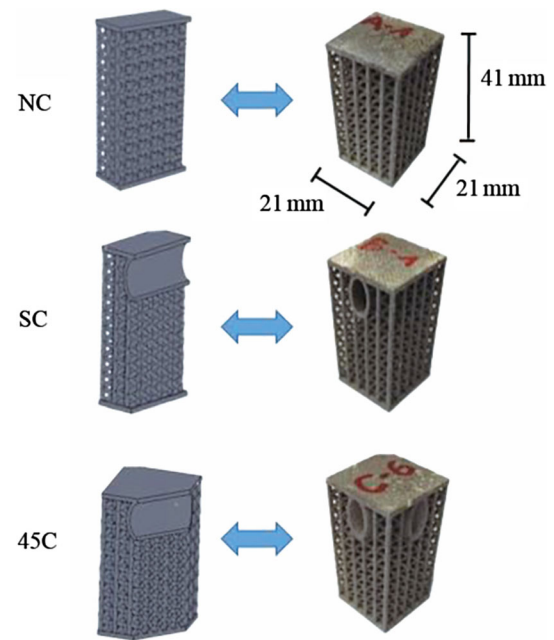
The SC and 45C samples could be considered as starting elements to build a more complex lightweight structure with a lattice network and a cooling coil inside it.

The design of the elliptical channel in SC and 45C specimens was optimized from a mechanical and hydraulic point of view. Firstly, it could be manufactured by LPBF without support structures inside being self-sustaining; secondly, good mechanical responses could be obtained for compressive stresses along the major axis of the ellipse and then the external pressure drop could be minimized [31].

The AlSi10Mg lattice specimens were produced using an EOSINT M270 machine Dual Mode (EOS GmbH). The machine is equipped with a Yb fiber laser system of 200 W and a nominal spot diameter of 100  $\mu\text{m}$ . In this work, the building platform was kept at 100 °C, and the main process parameters employed were a laser power of 195 W, a scanning speed of 800 mm/s and a hatch distance of 0.17 mm, to ensure high density of the struts, as demonstrated in previous studies [23, 32]. The specimens were built with supports at the square base to avoid distortions during growth. After the LPBF process, all specimens were detached by manual operations and polished to guarantee planar and parallel surfaces.

With respect to the specimen nominal dimensions, the produced ones are characterized by slightly different values, as appreciable from average (Mean) and standard deviation (Std. Dev.) data reported in Table 2. However, as confirmed by mass measurements, the relative density of each sample configuration is equal to the nominal 0.4.

Mechanical tests were carried out to define the static behavior of three specimens for each configuration. The obtained results of tests were processed to determine the



**Fig. 1** Comparison between CAD project for the three configuration considered and AlSi10Mg samples produced by LPBF, from top to bottom: NC, SC and 45C samples

mean curves representative of the mechanical behavior. In order to compare the effect of post process heat treatments, specimens were analyzed AB, after an SR treatment consisting of 2 h at 300 °C [32], and after a T6 treatment. The T6 consisted of a solution treatment of 5 h at 530 °C, followed by water quenching, and then an artificial aging for 12 h at 160 °C [33].

The specimens were subjected to uniaxial compression tests according to ISO 13314: 2011 in Ref. [36] and considered as metallic foams. The tests were performed using a Zwick-Roell electro-mechanical testing machine with a 100 kN load cell. The trabecular nature of the samples did not allow to use conventional methods for deformation acquisition (strain-gages or extensometers), so the deformations were acquired through the displacement of the crosspiece and the test was carried out in position control. To avoid slipping effects of the specimen during data

**Table 2** Average geometrical feature values with their standard deviation values measured for lattice structures analyzed

Specimen		Length/mm	Width/mm	Height/mm	Weight/g
NC	Mean	21.22	21.23	41.34	19.87
	Std. Dev.	0.05	0.04	0.04	0.51
SC	Mean	21.19	21.21	41.30	20.09
	Std. Dev.	0.05	0.05	0.05	0.47
45C	Mean	21.15	21.17	41.29	19.92
	Std. Dev.	0.01	0.04	0.04	0.39

acquisition, a 1 kN preload was applied. The tests were carried out at 1 mm/min. The tests were carried out both at room temperature (25 °C) and 200 °C. To perform high temperature tests, the machine was equipped with a thermal chamber that allowed to evaluate the mechanical behavior in a range of temperatures up to 250 °C. The following data were obtained.

- (i) Quasi-elastic gradient, i.e., the slope of the curve in the elastic phase;
- (ii) Yield strength, or the stress at which a specific amount of plastic deformation was produced, usually taken as 0.2% of the unstressed length.

In order to better understand the fracture mechanism of the NC samples, thermography was chosen as visual analysis in AB condition. By monitoring heat and its dissipation during the test, information on the fracture mode could be evaluated. An Optris camera model PI 400 was used to acquire thermal images. To improve their emissivity, tested samples were black-painted. The fracture surfaces were then observed with an optical stereo microscope (OM) Leica EZ4W. This type of analysis is not useful on thermal treated samples due to the collapsing of the lattice structure at the end of the compression tests. To evaluate the fracture mode of AB samples, vision research high speed camera model Miro C110 was used to acquire data.

### 3 Results and discussion

In order to assess the performance of AlSi10Mg BCCZ lattice samples as reference, NC samples were tested at 25 °C. Quasi-elastic gradient and yield strength of tested samples are summarized in Table 3. A quasi-elastic gradient very close to the AB condition was maintained with both the post process thermal treatments, considering a standard deviation less than 10%, assuring a similar structural behavior. In Refs. [27, 28, 33, 35], it has been demonstrated that AB parts produced by SLM have superior mechanical strengths compared to thermally treated ones, but with more limited ductility.

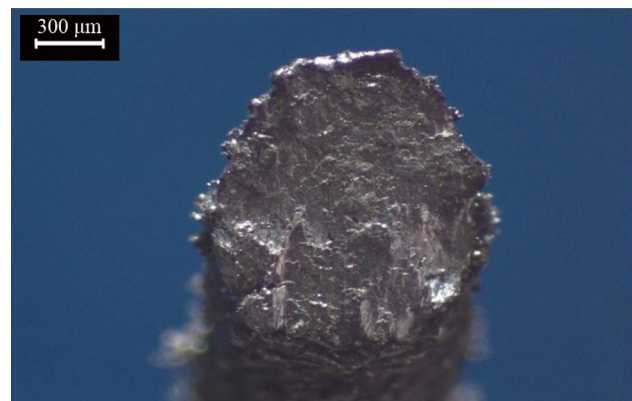
**Table 3** Static compressive properties of AlSi10Mg NC samples AB, SR, T6 tested at 25 °C

Thermal treatment	Quasi-elastic gradient / GPa	Yield strength / MPa
AB	2.2 ± 0.2	39.8 ± 3.6
SR	2.2 ± 0.1	29.8 ± 2.1
T6	2.1 ± 0.1	30.1 ± 1.6

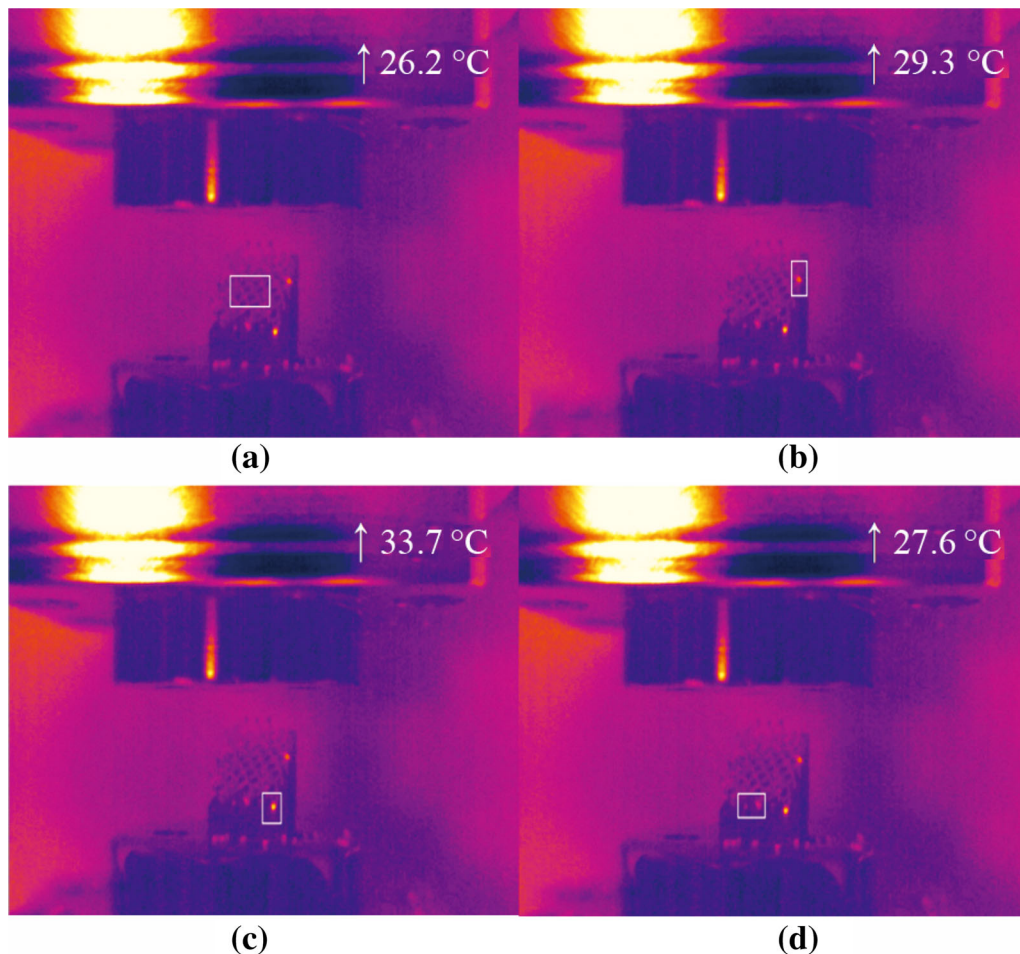
In the case of NC specimens AB, a rupture at the end of the elastic phase was observed. Therefore their fracture surfaces were analyzed identifying areas in which a brittle fracture occurred and areas in which struts underwent plastic deformations. In particular, some of the struts of the outer sample's border presented only evident signs of plastic work, with slipping bands on the whole surface, as shown in Fig. 2.

Indeed, in these zones of the samples, struts were characterized by ductile fracture surfaces, as already reported in Ref. [14]. On the contrary, all the fracture surfaces of struts inside the sample presented a uniform breakage of a fragile type. Moreover, the orientation of the border struts after the sample break allowed to understand that they underwent a flexural load since they faced towards the inside of the specimen. Furthermore, the areas subjected to plastic work were identified by thermography. It is possible to note that, at the end of a compression test, the average temperature of the specimen volume inside the white rectangle in Fig. 3a is 26.2 °C. Despite this, there are some external areas where the local temperature is much higher, with zones in which temperature rises up to 33.7 °C (see Fig. 3b–d).

This localized temperature increase can be due to the plastic work carried out by the strut during the breaking phase. Indeed, due to micro-plasticity activation and dislocations motion, the intrinsic material dissipation may be expressed by a corresponding thermal emission. Therefore, in the fracture zones of the internal struts no heat development was measured and no plastic work was observed [37]. On the basis of the overall fragile fracture, as shown in the video of supplementary info called Online Resource 1, AB lattice structures were then considered not technologically useful, and therefore the SC and 45C configuration samples were tested only after thermal treatments. In fact, it is well known that SR and T6 AlSi10Mg samples by LPBF exhibit ductile behavior, even if a lower yield



**Fig. 2** Slipping bands on the fracture surface of external struts of AlSi10Mg NC sample AB tested at 25 °C



**Fig. 3** Thermal images of the in-situ fracture of NC specimen in AB condition **a** internal zone, **b**, **c** and **d** external zones

strength and a higher elongation at break are obtained after SR, with a similar microstructure at optical microscope with respect to the AB condition [33–35]. While after T6, the yield strength increases and ductility reduces to values near AB condition, but with a coarser microstructure [33, 35].

Considering NC samples after SR and T6, the stress-strain graphs of Fig. 4 present the following trend: at the beginning of the plastic phase, there is a peak of tension ( $\sigma_{\max}$ ) followed by a quick stress decrease ( $\sigma_{\min}$ ), determining a drop of stresses ( $\Delta\sigma$ ). Moreover, the curves of Fig. 4 are characterized by a different evolution of falling stress corresponding to the sliding of the structure, observed in these samples along struts at  $45^\circ$  with respect to Z-axis (as illustrated in Supplementary Fig. 4 for a NC sample after SR, as an example). It is known from literature that shear stresses in a material have their maximum value on planes at  $45^\circ$  to the tensile axis [38]. The deformation began along the slipping planes more favorable and less energetic, probably due to the presence of defects or micro-porosity. Then deformation propagated along a direction

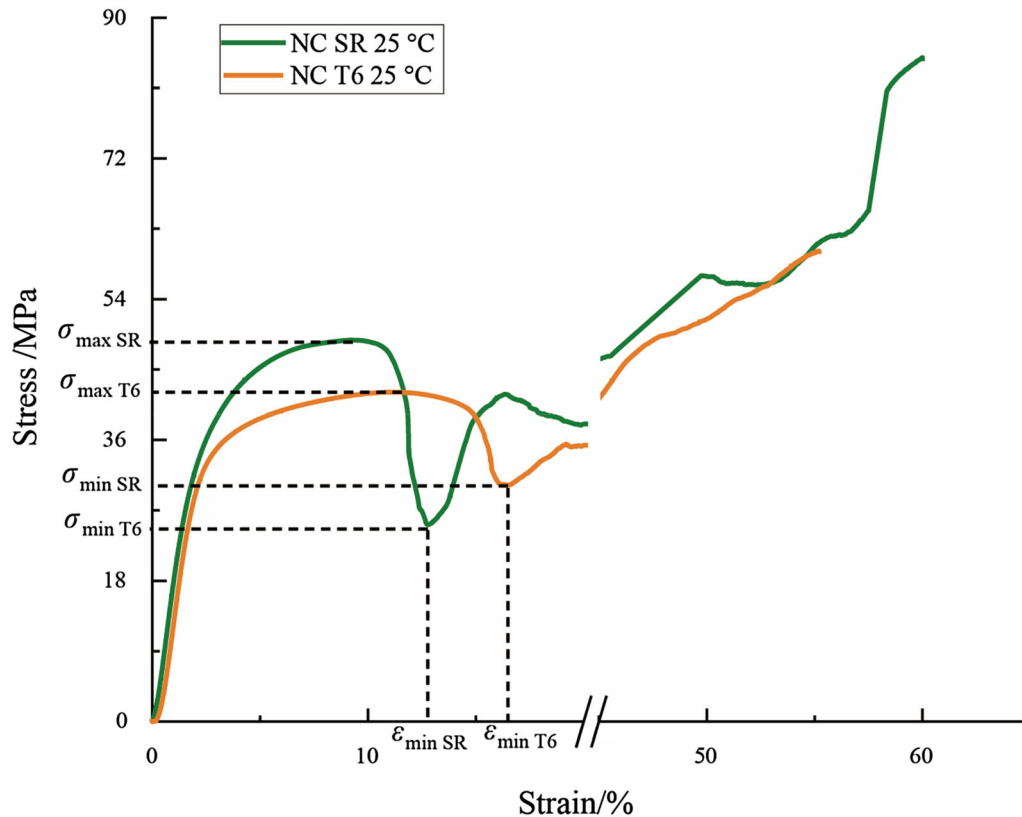
perpendicular to these planes, allowing the structure to collapse, as already observed in Ref. [21].

As shown in Fig. 4, the SR samples have higher  $\sigma_{\max}$  than the T6 ones. The improved mechanical strength of SR samples, however, is compensated by an earlier slipping behavior of structure. In fact, SR specimens slipped at 12.7% of strain ( $\varepsilon_{\min,SR}$ ) while T6 ones at 16.5% ( $\varepsilon_{\min,T6}$ ) with a greater  $\Delta\sigma$  for the SR structures with respect to the T6 ones, with values of  $-48\%$  and  $-28\%$ , respectively.

Once assessed the influence of the thermal treatments on the NC structures mechanical behavior, the focus moved on the effect of the channel presence in the lattice structure during compressive test at room temperature.

All types of samples were characterized by negligible variations in their quasi-elastic gradients and yield strength, as can be observed from the data summarized in Table 4, ensuring similar structural responses by configurations with or without channel.

On the other hand, the general trend of stress-strain curves is influenced by the presence and the type of channel, as can be seen in Fig. 5. It compares the stress-



**Fig. 4** Compressive stress-strain behavior obtained as mean curve for NC samples after SR and T6 tested at 25 °C

**Table 4** Compressive properties of SC and 45C samples after SR and T6 tested at 25 °C in comparison with NC ones

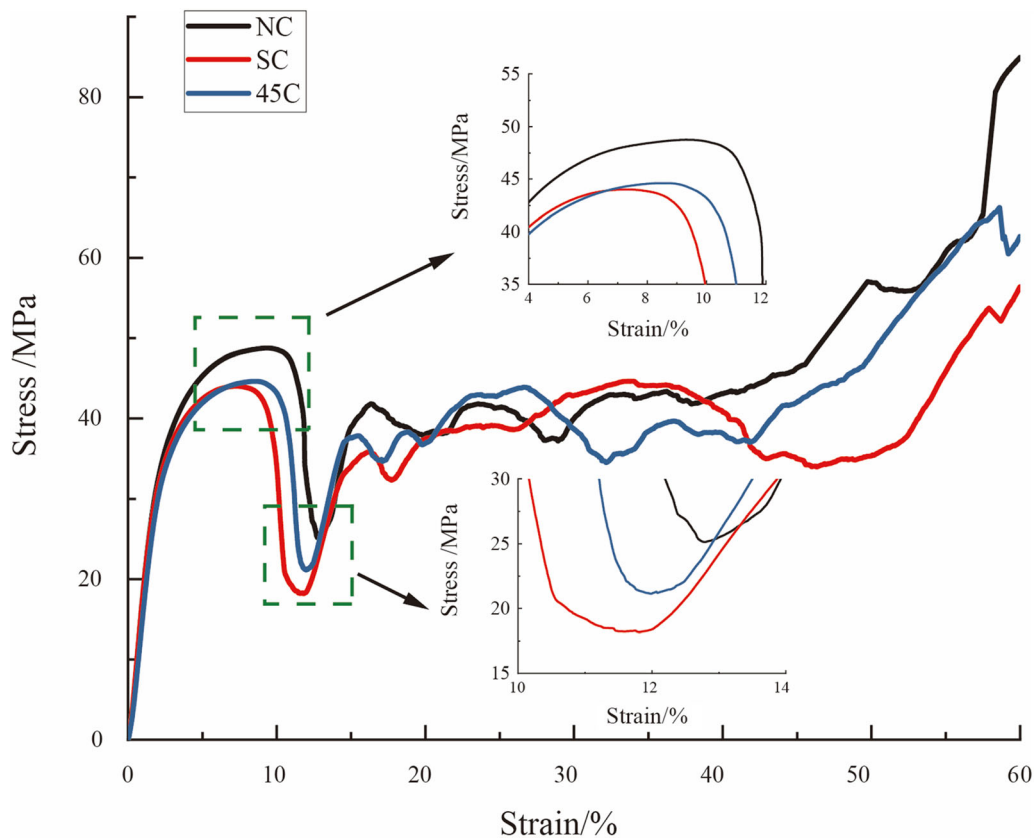
	Quasi-elastic gradient /GPa		Yield strength /MPa	
	SR	T6	SR	T6
NC	2.1 ± 0.1	2.1 ± 0.1	29.8 ± 2.1	30.1 ± 1.6
SC	2.1 ± 0.2	2.0 ± 0.1	29.8 ± 2.1	25.6 ± 2.9
45C	2.0 ± 0.2	1.9 ± 0.1	30.1 ± 1.8	27.5 ± 2.3

strain mean curves recorded at 25 °C for the NC, SC and 45C samples all after SR. The same trends were observed for the whole samples after T6.

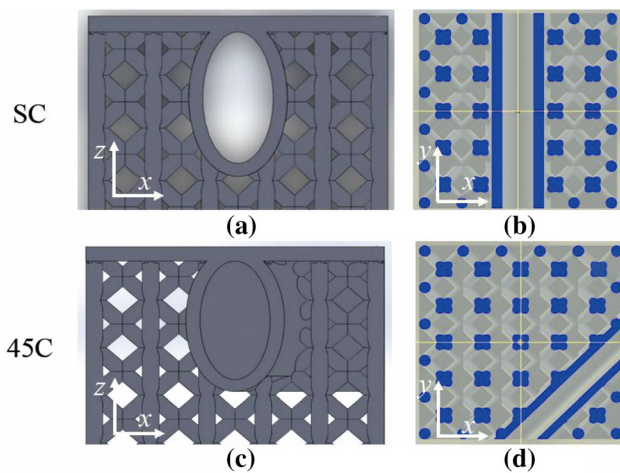
As can be seen in the insets of Fig. 5, the NC samples presented higher  $\sigma_{\max}$  and  $\sigma_{\min}$  than the SC and 45C samples; moreover, the  $\Delta\sigma$  is recorded at a greater percentage of deformation being  $\varepsilon_{\min,NC} > \varepsilon_{\min,45C} > \varepsilon_{\min,SC}$ . There are also important differences between SC and 45C specimens: in fact, the latter have higher  $\sigma_{\max}$  and  $\sigma_{\min}$  than the former. The percentage deformation at which these events occur,  $\varepsilon$  at  $\sigma_{\max}$  and  $\varepsilon$  at  $\sigma_{\min}$ , are also greater for the 45C samples than for the SC ones. It can be assumed that there is an influence in the elasto-plastic characteristics of the artifacts due to the presence and type of channels.

The slight higher mean value of strength of the 45C samples compared to the SC samples can be attributed to the number of elementary cells of the lattice. In SC and 45C structures a channel with an oval section with a major axis of 8 mm is present. In particular, in SC samples the channel is long as one side of the samples, whereas in 45C samples the channel length is equal to half the length of the diagonal of the specimen itself which, being a square base, will be equal to  $\sqrt{2}$  length. Considering that the elementary cells measure 4 mm and that the side of the sample is approximately 20 mm, 5 elementary cells for SC and 3.5 for 45C are eliminated considering as reference the section of the channel mid plane. In this way, considering the length of the major axis, the channel substituted a total of 10 cells for SC and 7 cells for 45C, as displayed in the views of Fig. 6.

As can be seen in Figs. 1–3 of supplementary info, at room temperature, the failure modes of NC, SC and 45C samples after SR and T6 are dominated by a mix of brittle-ductile fractures. The Z-struts failed in buckling mode firstly, then BCC struts dominate fracture mechanisms through a 45° collapse after reaching the maximum load bearable (red lines in Figs. 1–3 of the supplementary info). These phenomena were discussed also by Ferro et al. [23]. They found that the effect of cell struts in fracture modes



**Fig. 5** Compressive stress-strain behavior obtained as mean curve for NC, SC and 45C samples after SR tested at 25 °C



**Fig. 6** CAD drawings of SC **a, b** and 45C **c, d** samples with frontal view **a–c** and top section of the channel mid-plane **b, d**, respectively

was negligible if cells were localized in other planes distant from the one of the rupture. Only at the end of the compression test, they all tend to collapse.

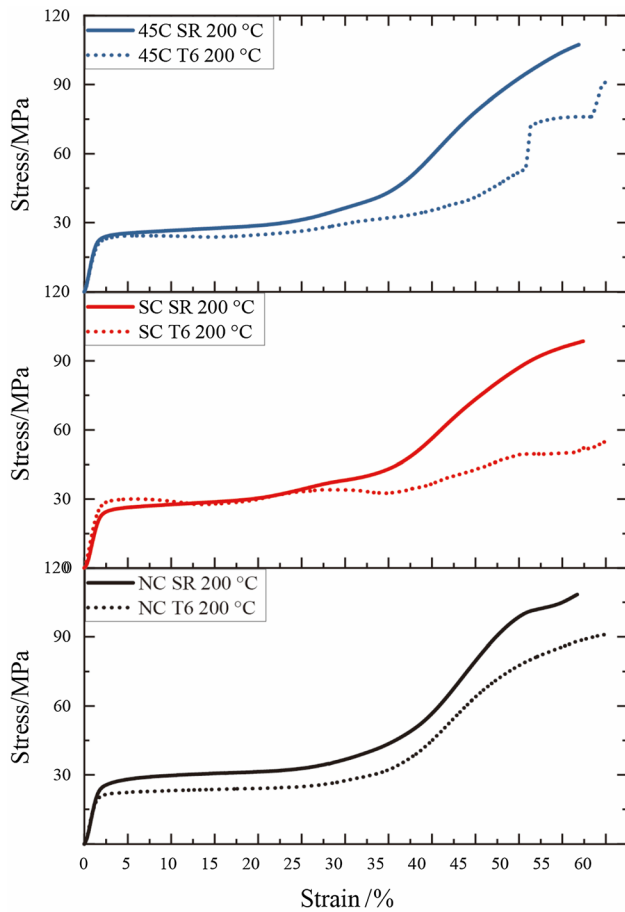
Considering the compression test at 200 °C, there is not an appreciable variation in the quasi-elastic gradient between different types of samples, as reported in Table 5.

**Table 5** Static compressive properties of NC, SC and 45C samples after SR and T6 tested at 200 °C

	Quasi-elastic gradient /GPa		Yield strength /MPa	
	SR	T6	SR	T6
NC	1.8 ± 0.2	1.8 ± 0.0	23.4 ± 3.6	19.2 ± 0.4
SC	1.6 ± 0.2	1.9 ± 0.1	22.2 ± 1.1	23.0 ± 3.3
45C	1.8 ± 0.2	1.7 ± 0.1	21.6 ± 1.1	20.4 ± 1.3

While it is possible to note a net decrease in yield strength up to 30% less respect to room temperature values.

This occurs consistently for NC, SC and 45C treated with both SR and T6. The curves recorded for all types of the AlSi10Mg BCCZ samples present constant trends, as illustrated in Fig. 7. At this temperature, samples behave as metal foams. As observable in Fig. 7, the stress-strain graphs can be divided into 3 sections: in the first part there is a perfectly elastic behavior. Then a plateau zone follows, up to 40% of the deformation, and finally stresses increase as a consequence of the sample densification. The possibility of densifying and achieving a foam-like behavior can be ascribed to the increase in temperature.

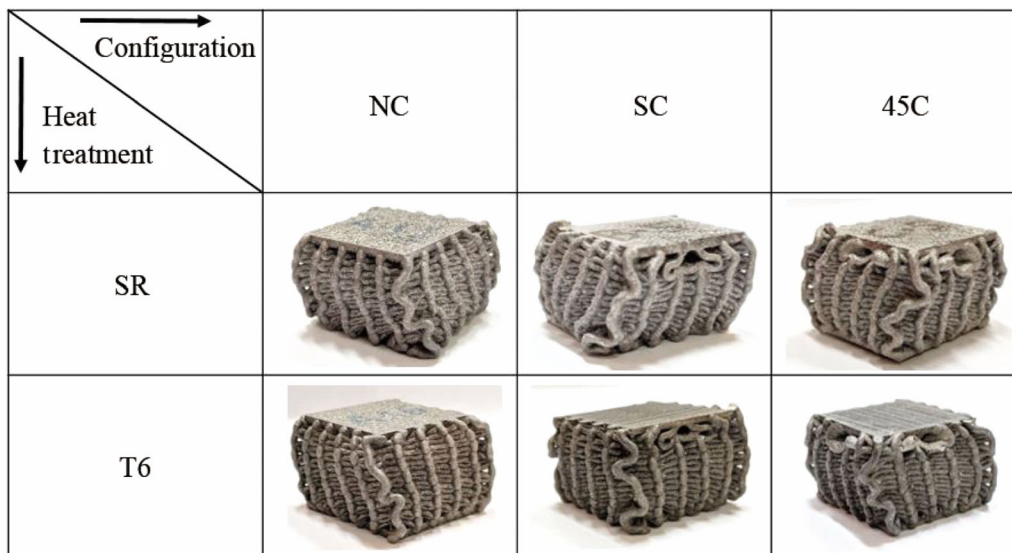


**Fig. 7** Compressive stress-strain behavior obtained as mean curve for NC, SC and 45C samples after SR and T6 tested at 200 °C

It is known that at 200 °C AlSi10Mg samples exhibit a lower strength and a higher elongation at break in tensile test, making the mechanical behavior of this alloy similar to the one of a ductile pure metal at room temperature [39]. Therefore the failure mode of all configurations is dominated by a ductile fracture, reaching the same level of densification as visible in Fig. 8. The struts along Z axis avoid euler buckling mode failure while BCC cells inside the sample fold in predictable way thanks to the high elongation at rupture. This kind of plastic collapse could be described by the mean curves of Fig. 7, similarly to aluminum metal open-cell foams [40].

At 200 °C, SR samples have a metal-foam like deformation in each type of lattice (NC, SC or 45C); moreover the curves are extremely repeatable in every configuration. T6 samples have a plateau stress lower or equal to those of the SR specimens with non-constant deformations, as illustrated in Fig. 7. This can be attributed also to a lower level of densification at the end of the test of the lattice samples in T6 condition with respect to SR.

Considering that T6 treatment needs higher furnace temperatures and longer process times, being more expensive and time-consuming than the SR one, the SR condition results in the best choice for possible applications of aluminum lattice structures with conformal coils as part of lightweight heat exchangers.



**Fig. 8** Evaluation of densification level for each configuration and condition tested at 200 °C



## 4 Conclusions

In this study three different configurations of AlSi10Mg lattice structures by LPBF were tested in compression at 25 °C and 200 °C. The reference structures were BCCZ lattices, BCC in the core of the samples with vertical struts along Z in the outer perimeter [23], labelled as NC samples. The main novelty consisted in inserting a straight elliptical channel and a 45° elliptical channel inside the BCCZ lattice structures, labelled as SC and 45C samples, respectively. In fact, the use of cooling channels inside lattice structures is of great potential interest for many industrial sectors, such as mold industry, aerospace and automotive. Therefore, all the samples were tested after LPBF process, in AB condition, and after two post process heat treatments, commonly used for AlSi10Mg LPBF industrial components: an SR and a T6 treatment.

The main findings observed regarding the fracture behavior under compressive tests of these above mentioned samples are summarized as follows.

- (i) NC lattice structures AB exhibited an overall fragile fracture; they were considered as a condition not useful for the fabrication of complex parts, and therefore the SC and 45C configuration samples were tested only after thermal treatments.
- (ii) The test at room temperature showed that all types of samples were characterized by negligible variations in their quasi-elastic gradients and yield strength ensuring similar structural responses by configurations with or without channel.
- (iii) On the contrary, the general trend of stress-strain curves is influenced by the presence of the channel and its position. The slightly greater resistance of the 45C samples compared to the SC samples can be attributed to the number of elementary cells substituted by the presence of the channel: 10 cells for SC and 7 cells for 45C.
- (iv) The test at 200 °C showed that NC, SC and 45C samples after SR and T6 treatments exhibited a metal-foam like deformation. SR samples can sustain a higher stress than T6 specimens. This can be attributed to a higher level of densification with a constant deformation at the end of the test of the lattice samples in SR condition with respect to T6.
- (v) Considering that T6 treatment needs higher furnace temperatures and longer process times, being more expensive and time-consuming than the SR one, the SR condition results in the best choice for possible applications of aluminum lattice structures with conformal coils as part of lightweight heat exchangers.

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