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Petrophysical characterization for Thebes and Mutulla reservoirs in Rabeh East Field, Gulf of Suez Basin, via well logging interpretation

Mohammad Abdelfattah Sarhan¹

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Abstract

The current work assesses the sandstones of the Mutulla Formation as well as the limestone of the Thebes Formation for being promising new oil reservoirs in Rabeh East field at the southern portion of the Gulf of Suez Basin. This assessment has been achieved through petrophysical evaluation of wireline logs for three wells (RE-8, RE-22 and RE-25). The visual analysis of well logs data revealed that RE-25 Well is the only well demonstrating positive criteria in five zones for being potential oil reservoirs. The favourable zone within Thebes Formation locates between depths 5084 ft and 5100 ft (Zone A). However, the other positive zones in Mutulla Formation occur between depths: 5403.5–5413.5 ft (Zone B), 5425.5–5436 ft (Zone C), 5488–5498 ft (Zone D) and 5558.5–5563.5 ft (Zone E). The quantitative evaluation shows that the Zone A of Thebes Formation is the best oil-bearing zone in RE-25 Well in terms of reservoir quality since it exhibits lowest shale volume (0.07), minimum water saturation (0.23) and lowest bulk volume of water (0.03). These limestone beds include type of secondary porosity beside the existing primary porosity. On the other hand, the sandstones of Mutulla Formation in RE-25 contain four reservoir zones (B, C, D and E) with the total net pay thickness of 35.5 ft. Moreover, the obtained results revealed that it is expected for zones B, C and D to produce oil without water but Zone E will produce oil with water.

Keywords Petrophysical characterization · Rabeh East field · Thebes Formation · Mutulla Formation · Gulf of Suez Basin

Introduction

The Gulf of Suez Basin (GSB) province is the oldest and the most productive oil region in Egypt. It represents an intercontinental rift extending for about 325 km northward from Hurghada city in the south (El Nady et al. 2016). Despite the fact that its rifting process began in the Miocene epoch, both post-rift and pre-rift periods contain prospective source rocks and reservoirs (Shahin and Shehab 1984; EGPC, 1996; Atta et al. 2002).

The GSB encompasses more than 80 fields producing oil from Precambrian to Tertiary reservoirs. Due to the large amounts of exploration data as well as the existence of wellexposed syn-rift strata, numerous geological studies covering the evolution of the GSB rifting have been carried out (e.g. Winn et al. 2001; Alsharhan 2003; El Nady et al. 2015; Radwan, et al. 2020; Moustafa and Khalil 2020; Radwan and Sen 2021; Radwan 2021a,b; Radwan et al. 2021a,b,c).

The rifting fault blocks are the main hydrocarbon traps within the GSB oil fields (Sultan 2002; Chowdhary and Taha 1987). The Miocene clastics hold nearly 60% of oil reserves in the GSB, and the residual is frequently existing in the Pre-Cenomanian Nubia sandstones (Peijs et al. 2012).

Rabeh East field is located between longitudes: $33^{\circ} 39'$ 16.8" E, $33^{\circ} 47' 56.1"$ E and latitudes: $27^{\circ} 9' 36.3"$ N, 27° 17' 0.7" N at the southern portion of the GSB (Fig. 1). The sandstones of Nubia and Nukhul formations as well as the carbonates of Rudies Formation exhibit the essential targets for oil production at Rabeh East oil field (Sarhan and Basal 2019; Sarhan 2020, 2021).

Consequently, the present work aims to perform geophysical assessment using well log data for the limestone of Thebes Formation and the sandstones of Mutulla Formation in order to add new promising targets to the well-known oil reservoirs in Rabeh East field.



Mohammad Abdelfattah Sarhan msarhan@du.edu.eg

¹ Geology Department, Damietta University, New Damietta City 34517, Egypt



Fig. 1 a Regional map shows the location of Rabeh East Field at the southern GSB. b Study area with well locations

Geological setting

The rifting of the GSB started through the Early Miocene age because of the divergence between the African plate and the Arabian plate, which led to forming a series of extensional faults trending NW–SE to NNW–SSE (Bosworth et al. 2005; Patton et al. 1994). These fault arrays moved to the north-west and affected the Late Miocene sequence beneath the Nile Delta area (Sarhan et al. 2014).

The structural and depositional setting of the GSB is complex due to the superimposing of the rifting-related faults with the pre-rift structures (Abul Karamat and Meshref 2002). The faulted blocks of the GSB are bounded principally by NW extensional faults, which are linked to each other by WNW-, NNE- and NE-oriented faults (Abd-Allah et al. 2014).

The lithostratigraphy of the GSB including Rabeh East Field starts with the clastics of Nubia Formation, which are overlain by the Matulla, Duwi and Sudr formations. These units are topped by Esna Shale Formation (Palaeocene) and then the Thebes Formation (Eocene). The Miocene stratigraphy comprises: Nukhul, Rudeis, Kareem, Belayim, South Gharib and Zeit formations, respectively, from base to top (Fig. 2).

Based on the available wells in Rabeh East Field, the Eocene Thebes Formation is mainly composed of limestones (Fig. 3), whereas the Matulla Formation consists principally of sandstones and shale interbeds (Fig. 4).

The limestone of Thebes Formation was deposited during the Tethyan major transgression over the north-east of



Africa in the Eocene times. This limestone characterises a potential source rock with TOC equal to 3.2% of type I/ II kerogens; however, the generated hydrocarbon has low API gravity, high sulphur content and high HI and low OI values (Alsharhan 2003). The fractured limestones of the Thebes Formation provide around 1.1% of oil production in the GSB with 13% average porosity, and net pay thickness varies between 15 and 17 m. Numerous fields, such as Sudr, Asal, Kareem, Ras Matarma, Bakr, West Bakr, Ali, Issaran, Shoab and Rahmi, produce oil from the entire carbonates of Thebes Formation (Alsharhan 2003).

The Matulla Formation is separated between the overlain Brown limestone Formation and the underlain Wata Formation by two unconformity surfaces. The entire clastics of the Matulla Formation were deposited throughout the Coniacian–Santonian time span. A diverse planktonic foraminiferal content including *Dicarinella concavata* and *D. asymetrica* zones revealing the Coniacian–Santonian age characterizes the Matulla Formation (Alsharhan 2003).

The Matulla Formation represents a complete third-order depositional sequence that embraces the Coniacian–Santonian interval and is subdivided into LST, TST and HST system tracts. This sequence was deposited through a reduction in the accommodation space towards the inner shelf water depth, resulting in the sedimentation of the lowest part of Matulla Formation as lowstand system tracts (LSTs). This step was followed by a transgressive stage within a relatively deeper marine setting (outer shelf conditions), resulting in the deposition of the middle part of the Matulla Formation as transgressive system tracts (TSTs). The deposition of the uppermost parts of the Matulla Formation as highstand



Fig. 2 Stratigraphic column at West Hurghada region comprising Rabeh East field (after Abd El Hafez et al. 2016). Note the stratigraphic position for the examined formations in the present study, which outlined by dotted red polygons

system tracts (HSTs) was due to a significant decline in the holding accommodation space at the final basin filling stage (Elhossainy et al. 2021).

Data and methods

The available geophysical data in this paper comprise the conventional wireline logs from three examined wells drilled in Rabeh East oil field. These wells are: Rabeh East-8 (RE-8), Rabeh East-22 (RE-22) and Rabeh East-25 (RE-25) as presented in Fig. 1b. The mud logs for the three wells are also accessible.

The current work appraises the mud logs with the electric well logs data for the Thebes and Mutulla formations in the

three studied wells at Rabeh East field. The three wells' mud logs were initially evaluated qualitatively to identify the prospective hydrocarbon yielding zones within the Thebes and Mutulla formations. After that, the wireline logs for the three wells were analysed using Techlog software to determine the most essential petrophysical parameters for the zones of interest. These parameters contain shale volume (VShale), total porosity (Φ T), effective porosity (Φ E), water saturation (Sw) and bulk volume of water (BVW).

Shale volume

The amount of shale (Vsh) in the studied intervals has been determined using the following equation:





Fig. 3 Mud log displays the Thebes Formation in RE-25 Well. Note the green rectangle outlines the most promising zone within the Thebes Formation (Zone A) between depths 5084 and 5100 ft

$$\mathbf{Vsh}_{(\mathbf{N}-\mathbf{D})} = \left(\mathbf{\Phi}_{\mathbf{N}} - \mathbf{\Phi}_{\mathbf{D}}\right) / \left(\mathbf{\Phi}_{\mathbf{N}(\mathbf{shale})} - \mathbf{\Phi}_{\mathbf{D}(\mathbf{shale})}\right)$$
(1)

where Vsh $_{(N-D)}$ is the calculated shale volume from neutron and density logs; Φ_N is the neutron porosity; Φ_D is the density porosity; Φ_N (shale) is the neutron porosity of shale; Φ_D (shale) is the density porosity of shale.

Total porosity

Following Asquith and Gibson (1982), total porosity (ϕ_T) was determined from neutron–density logs using the following formula:

$$\Phi_{\rm T} = \left(\Phi_{\rm N} + \Phi_{\rm D}\right)/2 \tag{2}$$

where Φ_T is the total porosity; Φ_N is the neutron porosity; Φ_D is the density porosity.

Effective porosity

The effective porosity (ϕ_e) has been measured by the following equation of (Asquith and Gibson 1982):

$$\phi_{\mathbf{e}} = \phi_{\mathbf{T}*} (\mathbf{1} - \mathbf{V} \mathbf{s} \mathbf{h}) \tag{3}$$

where ϕ_e is the effective porosity; ϕ_T is the total porosity; V_{sh} is the shale volume.



Water saturation

The water saturation (S_w) for the examined zones has been calculated by the Indonesia model (Poupon and Leveaux 1971) from the following equation:

$$S_{w} = \left\{ \left[\left(\frac{V_{sh}^{2-Vsh}}{R_{sh}} \right)^{1/2} + \left(\frac{\phi_{e}^{m}}{R_{w}} \right)^{1/2} \right]^{2} R_{t} \right\}^{-1/n}$$
(4)

where S_w is the water saturation; V_{sh} is the shale volume; ϕ_e is the effective porosity; \mathbf{R}_{sh} is the shale resistivity; \mathbf{R}_t is the deep resistivity; \mathbf{R}_w is the connate water resistivity (set equal to 0.025 Ω m²/m according to Ganoub El-Wadi Petroleum Company); **m** is the cementation exponent (set equal to 2); **n** is the saturation exponent (set equal to 2); **a** is the tortuosity factor (set equal to 1).

Bulk volume of water

The bulk volume of water (**BVW**) has been estimated by applying the following equation of Buckles (1965):

$$\mathbf{BVW} = \boldsymbol{\phi}_{\mathbf{e}*} \mathbf{S}_{\mathbf{w}} \tag{5}$$



Fig. 4 Mud log shows the Mutulla Formation in RE-25 Well. Note the green rectangles outline the most promising oil-bearing zones between depths: 5403.5 to 5413.5 th (Zone B), 5425.5 to 5436 ft (Zone C), 5488 to 5498 ft (Zone D) and 5558.5 to 5563.5 ft (Zone E)

where **BVW** is the bulk volume of water; ϕ_e is the effective porosity; S_w is the water saturation.

Results

The qualitative examination for Thebes and Mutulla formations in the studied wells (RE-8, RE-22 and RE-25) exposed that RE-25 Well is the only well exhibiting optimistic criteria in five zones for being potential oil reservoirs. The first zone (A) locates between depths 5084 and 5100 ft in the limestone of Thebes Formation (Fig. 5). However, the sandstones of Mutulla Formation have four promising oil-bearing zones (B, C, D and E). These intervals situate between depths: 5403.5–5413.5 ft (Zone B), 5425.5–5436 ft (Zone C), 5488–5498 ft (Zone D) and 5558.5–5563.5 ft (Zone E) as shown in Figs. 6, 7 and 8.

The favourable signals for the recommended five zones comprise the existence of oil shows as well as the high values of the ditch gas analysis opposite to the five examined intervals (Figs. 3 and 4). Also, these intervals display high deep resistivity, which confirm the occurrence of the nonconducive oil in addition to the relatively low gamma-ray approving the little shale content (Figs. 5–8). The sandstones of the examined zones in Mutulla Formation have been defined in the mud log as: colourless, white, greyish white, yellowish white, fine-grained graded to siltstones, occasionally medium-grained, sub-rounded to sub-angular, moderately sorted with calcareous cement, glauconitic and pyritic, brown spotty-patchy oil stain with pale-yellow to yellow fluorescence, moderate fast yellowish white streamcut (Fig. 4).

Consequently, the wireline log suites for the motivating zones (A, B, C, D and E) have been quantifiable appraised. This assessment encompasses the calculations of the vital petrophysical parameters obligatory for judging the potentiality for hydrocarbon reservoirs. These calculations include: shale volume, total porosity, effective porosity, water saturation and bulk volume of water. The results of these parameters for zone A within Thebes Formation in Rabeh East-25





Fig. 5 Petrophysical data with interpretation for the Thebes Formation in RE-25 Well representing the favourable characteristics for oil production in Zone A



Fig. 6 Petrophysical data with interpretation for the Mutulla Formation in RE-25 Well displaying the positive characteristics for Zones B and C for being oil-bearing intervals

Well are displayed in Table 1, while the calculations for zones B, C, D and E in have been shown in Mutulla Formation, as given in Table 2.

The neutron-density cross-plot (Schlumberger 1972) for the studied zones shows clearly higher porosity values for zones B, C, D and E within Mutulla Formation (between 20 and 30%) rather than Zone A in Thebes Formation (only between 10 and 20%) as shown in Fig. 9. The calculated amount of shale in the inspected zones as demonstrated in Tables 1 and 2 reveals that the maximum shale volume (27%) was documented in Zone D and the minimum value (7.0%) was noted in Zone A. However, the estimated total porosity shows that the lowest average value (16%) was noted in Zone A and the highest total porosity (28%) was recorded in Zone E as given in Tables 1 and 2. The measured effective porosity reaches the highest value





Fig. 7 Petrophysical data with interpretation for the Mutulla Formation in RE-25 Well displaying the optimistic characteristics for oil production in Zone D



Fig. 8 Petrophysical data with interpretation for the Mutulla Formation in RE-25 Well displaying the bright characteristics of Zone E for being oil-bearing interval

(23%) that was recorded in Zone C, whereas the lowest value (14%) was noted in Zone A.

It is worth mentioning that the total and effective porosities for the entire limestone of Zone A have been also calculated using sonic log in order to examine the existence of secondary type of porosity (e.g. fractures, vugs, etc.). This is because the sonic measures only the primary porosity; however, the neutron-density porosity estimates both primary and secondary porosities. The results show that the calculated sonic total porosity (PHIT_S) is 11% and sonic effective porosity (PHIE_S) is 9%. Whereas the neutron-density total porosity (PHIT_ND) is 16%, the neutron-density effective porosity (PHIE_ND) is 14% (Table 1). This notable variance between sonic and neutron-density porosities reflects the existence of a specific type of secondary porosity within Zone A, which increase



oth Ca.	lliper De () cor C3	nsity (rec- r n (G/)	Gamma ay (API)	Sonic (US/F)	Photo- electric (B/E)	Neutron porosity	Density (G/C3)	Micro- spherical resistivity (\Omegam2/m)	Shallow resistivity (Ωm2/m)	Deep resistivity (Ωm2/m)	VSH_ ND	PHIT_ ND	PHIT_S	PHIE_ ND	PHIE_S	SW_ INDO
4 8.2	5 -0	.01 6	51.65	73.21	3.98	0.12	2.48	7.00	14.14	14.37	0.08	0.13	0.13	0.10	0.11	0.38
4.5 8.3	2 -0	2 10.0	58.63	77.82	4.45	0.13	2.44	4.15	13.73	13.98	0.04	0.15	0.17	0.14	0.15	0.30
5 8.3	2 0.0	0 6	51.65	74.84	4.63	0.13	2.45	3.68	16.05	16.18	0.05	0.15	0.14	0.13	0.13	0.29
5.5 8.3	0 0.0	5 0	59.48	75.87	4.61	0.14	2.47	4.78	24.61	24.47	0.11	0.14	0.15	0.11	0.12	0.28
6 8.2	3 0.0	Ō	58.10	74.60	4.63	0.15	2.47	6.62	20.16	19.72	0.16	0.15	0.14	0.10	0.09	0.32
6.5 8.2	1 0.0		51.84	73.88	4.67	0.17	2.44	8.47	24.06	23.56	0.17	0.16	0.14	0.11	0.08	0.26
7 8.2	1 -0	5 10.0	53.52	79.44	4.74	0.18	2.39	8.85	26.84	26.68	0.10	0.18	0.18	0.15	0.15	0.19
37.5 8.1	8 – (0.01 4	40.63	77.06	4.84	0.18	2.35	9.23	23.65	23.82	0.00	0.20	0.16	0.20	0.16	0.16
8 8.1)- 6	0.01 4	41.04	75.70	4.91	0.18	2.33	6.33	17.30	17.24	0.00	0.21	0.15	0.21	0.15	0.18
8.5 8.1)- 6	0.01 3	39.59	74.87	4.91	0.18	2.35	5.74	19.30	19.24	0.01	0.20	0.15	0.20	0.14	0.18
9 8.1	8 – (0.01 4	44.13	70.99	4.87	0.19	2.39	6.24	22.68	22.78	0.16	0.19	0.12	0.14	0.06	0.21
9.5 8.1	8 0.0	0	44.55	68.99	4.86	0.17	2.42	7.53	23.48	23.65	0.11	0.17	0.10	0.14	0.07	0.22
0 8.1	8 0.0	0	43.68	68.51	4.89	0.16	2.42	6.60	26.70	26.91	0.08	0.17	0.10	0.14	0.07	0.21
0.5 8.2	1 0.0	0	40.22	70.57	4.90	0.17	2.40	6.36	30.56	31.00	0.09	0.18	0.11	0.15	0.08	0.18
1 8.1	6 0.0	0	39.37	72.98	4.88	0.19	2.38	5.73	28.56	29.43	0.11	0.19	0.13	0.16	0.09	0.18
1.5 8.1	8 0.0	0 4	40.45	74.87	4.87	0.20	2.36	3.92	23.51	24.73	0.12	0.20	0.15	0.17	0.10	0.18
2 8.1	8 0.0	0 V	43.48	75.74	4.84	0.19	2.35	3.76	32.38	35.76	0.03	0.20	0.15	0.19	0.14	0.13
12.5 8.2	1 -0	۰.01 م	43.85	77.14	4.82	0.19	2.34	3.54	22.77	25.38	0.00	0.21	0.16	0.21	0.16	0.15
3 8.2	1 -0	۰.01 A	42.12	76.37	4.80	0.19	2.33	2.70	20.34	22.55	0.00	0.21	0.16	0.21	0.16	0.16
3.5 8.2	1 -0	0.01 3	38.01	75.22	4.79	0.19	2.35	2.52	32.41	36.47	0.02	0.20	0.15	0.20	0.14	0.13
94 8.2	1 -(0.01 3	35.90	74.40	4.74	0.18	2.37	3.06	29.00	32.31	0.06	0.19	0.14	0.17	0.12	0.16
94.5 8.2	2 –(0.01 3	33.09	73.00	4.74	0.17	2.39	6.70	22.60	24.92	0.06	0.18	0.13	0.16	0.11	0.19
95 8.2	3 –(0.01 3	37.63	69.97	4.75	0.17	2.40	6.27	19.85	21.69	0.08	0.17	0.11	0.15	0.08	0.22
)5.5 8.2	3 –(0.01 3	38.94	66.85	4.78	0.15	2.43	6.76	24.29	26.35	0.05	0.16	0.09	0.14	0.07	0.21
96 8.2	5 0.0	0	38.07	65.29	4.81	0.12	2.47	8.24	32.37	34.88	0.05	0.13	0.07	0.12	0.06	0.22
96.5 8.3	5 0.0	0	32.45	61.16	4.84	0.11	2.50	13.87	30.17	32.67	0.09	0.12	0.04	0.09	0.01	0.28
97 8.2	3 0.0	0	28.12	59.33	4.88	0.11	2.51	12.45	32.71	35.51	0.08	0.11	0.03	0.09	0.00	0.28
7.5 8.2	1 0.0	0	26.18	60.35	4.82	0.10	2.52	12.06	35.24	38.86	0.10	0.11	0.04	0.08	0.00	0.30
9.2	5 0.0	0	27.91	59.54	4.80	0.09	2.52	14.39	32.41	35.72	0.07	0.10	0.03	0.08	0.01	0.31
98.5 8.2	5 0.0	0	27.91	60.46	4.87	0.09	2.51	16.90	30.66	33.36	0.05	0.11	0.04	0.09	0.02	0.29
99 8.2	1 -0	0.01 3	32.25	61.75	4.98	0.10	2.49	11.02	27.28	29.52	0.03	0.12	0.05	0.11	0.04	0.26
9.5 8.2	6 0.0	0	30.87	60.91	4.99	0.10	2.51	9.21	32.90	35.82	0.05	0.11	0.04	0.09	0.02	0.28
0 8.2	8 0.0	2	29.35	59.80	4.94	0.09	2.56	8.38	34.08	37.11	0.12	0.09	0.03	0.05	0.00	0.42
trage 8.2	300	0	11 35	70.25	01 1	210	ç				1000					

	Denth	Zone	Calliner	Density	Gamma	Sonic	Photo-	Neutron	Density	Micro-	Shallow	Deen	HSV	pHIT	PHIF	MS	RVW
403.5Zone B 81.6 -0.01 83.07 96.96 2.68 0.23 227 5404.5 81.8 -0.01 77.45 99.20 2.60 0.23 2274 5404.5 81.18 -0.01 77.47 97.68 2.55 0.24 2225 5405.5 81.16 0.00 72.47 97.68 2.55 0.24 2235 5405.5 81.16 0.00 73.55 95.51 2.260 0.23 2236 5405.5 81.81 0.00 73.55 96.53 2.50 0.24 2235 5405.5 81.81 -0.01 73.55 96.53 2.50 0.24 2236 5405.5 82.11 -0.01 73.36 93.77 2.60 0.27 2347 5407.5 82.11 -0.01 73.36 95.56 2.56 0.27 2.367 5408.5 82.21 -0.01 73.36 95.35 2.50 0.27 2.367 5408.5 82.21 -0.01 73.36 95.35 2.56 0.27 2.37 5408.5 82.21 -0.01 73.37 96.13 2.56 0.27 2.37 5408.5 82.11 0.01 73.36 95.35 2.56 0.27 2.37 5408.5 82.11 0.001 73.37 96.13 2.56 0.25 2.34 5411.5 82.11 0.001 81.37 96.13 2.56 0.256 2.57 <	(tf)	name	(II)	correc- tion (G/ C3)	ray (API)	(US/F)	electric (B/E)	porosity	(G/C3)	spherical resistivity (Ωm2/m)	resistivity (Ωm2/m)	resistivity (Ωm2/m)	QN	DN	DN	OQNI	
54048.18 -001 77.45 99.20 2.60 0.23 2.27 5404.58.18 -001 73.98 99.51 2.56 0.26 2.23 5405.58.17 0.00 73.47 97.68 2.57 0.24 2.28 5405.58.16 0.00 73.55 95.51 2.56 0.24 2.28 54068.18 0.00 73.55 95.51 2.60 0.24 2.28 54068.18 0.00 73.55 95.56 2.60 0.24 2.28 54078.18 0.00 73.55 96.33 2.50 0.24 2.28 54088.21 -0.01 73.36 95.56 2.60 0.25 2.31 54088.21 -0.01 73.57 96.33 2.50 0.27 2.36 54088.21 -0.01 73.36 95.56 2.57 0.27 2.36 54088.21 -0.01 73.57 96.33 2.56 0.27 2.36 54098.21 -0.01 73.37 96.13 2.56 0.27 2.36 54108.23 -0.01 73.57 96.33 96.13 2.56 0.27 2.36 54118.16 -0.01 73.57 96.33 96.13 2.56 0.27 2.36 54128.23 -0.01 73.57 96.13 2.56 0.27 2.36 54138.16 -0.01 73.31 96.13 2.56 </td <td>5403.5</td> <td>Zone B</td> <td>8.16</td> <td>-0.01</td> <td>83.07</td> <td>96.96</td> <td>2.68</td> <td>0.23</td> <td>2.31</td> <td>1.35</td> <td>3.23</td> <td>3.15</td> <td>0.11</td> <td>0.23</td> <td>0.20</td> <td>0.43</td> <td>0.09</td>	5403.5	Zone B	8.16	-0.01	83.07	96.96	2.68	0.23	2.31	1.35	3.23	3.15	0.11	0.23	0.20	0.43	0.09
5404.58.1.8 -0.01 73.9899.512.560.252.245405.58.1.70.0072.4797.682.550.242.255405.58.1.70.0073.5595.942.580.242.285405.58.1.80.0073.5595.942.580.242.285406.58.210.0073.5595.632.590.242.285406.58.210.0073.5595.632.590.252.235406.58.21-0.0173.5595.632.590.252.3654098.21-0.0173.5595.632.560.272.345409.58.20-0.0173.5793.262.570.272.345409.58.21-0.0173.5794.292.560.272.345409.58.21-0.0173.5794.292.570.272.3454118.18-0.0173.5794.292.570.272.345413.58.160.0094.3394.482.560.242.355413.58.160.0088.9192.762.870.242.355413.58.21-0.0178.3394.482.840.252.315413.58.21-0.0178.3394.482.840.252.315413.58.21-0.0178.3394.482.840.252.315425.52000	5404		8.18	-0.01	77.45	99.20	2.60	0.23	2.27	1.12	4.04	4.06	0.00	0.25	0.25	0.32	0.08
405 8.17 0.00 7.47 97.68 2.57 0.24 2.25 5405.5 8.16 0.00 74.20 96.78 2.57 0.24 2.28 5405.5 8.16 0.00 73.55 95.94 2.58 0.24 2.28 5405.5 8.18 0.00 73.55 95.94 2.58 0.24 2.28 5405 8.11 -0.01 72.55 95.56 2.50 0.25 2.23 5407 8.21 -0.01 77.55 95.56 2.57 0.27 2.31 5408.5 8.21 -0.01 77.55 95.56 2.57 0.27 2.37 5408.5 8.21 -0.01 77.55 94.26 2.56 0.27 2.37 5408.5 8.21 -0.01 77.35 94.29 2.56 0.27 2.37 5408.5 8.21 -0.01 77.35 94.29 2.50 0.29 2.37 5411.5 8.16 0.00 92.60 2.56 0.27 2.37 5413.5 8.16 0.00 92.50 2.57 0.27 2.34 5413.5 8.16 0.00 92.60 2.56 0.24 2.37 5413.5 8.16 0.00 86.33 94.43 2.84 0.25 2.34 5413.5 8.16 0.00 86.33 94.36 2.57 0.24 2.36 5413.5 2000 8.21 0.00 86.33 94.36	5404.5		8.18	-0.01	73.98	99.51	2.56	0.25	2.24	1.06	4.64	4.75	0.02	0.27	0.26	0.28	0.07
3405.5 8.16 0.00 74.20 96.78 2.57 0.24 2.28 5405.5 8.18 0.00 73.55 95.94 2.58 0.24 2.28 5407.5 8.18 0.00 73.55 95.63 2.59 0.24 2.28 5407.5 8.18 0.00 73.55 95.63 2.59 0.24 2.28 5407.5 8.18 -0.01 72.25 95.63 2.59 0.24 2.28 5407.5 8.21 -0.01 77.39 97.75 2.50 0.27 2.34 5408.5 8.21 -0.01 77.39 97.35 95.63 2.57 0.27 2.34 5409.5 8.21 -0.01 77.39 97.35 96.13 2.51 0.27 2.34 5410.5 8.21 -0.01 77.37 96.49 2.56 0.27 2.34 5411.5 8.16 -0.01 77.37 96.49 2.56 0.27 2.34 5411.5 8.16 -0.01 77.37 96.49 2.56 0.27 2.34 5411.5 8.16 -0.01 77.37 96.49 2.56 0.27 2.34 5411.5 8.16 -0.01 77.37 96.49 2.57 0.24 2.37 5411.5 8.16 -0.01 77.31 97.36 2.264 0.25 2.34 5413.5 8.20 0.00 8.33 94.48 2.46 0.24 2.26	5405		8.17	0.00	72.47	97.68	2.55	0.24	2.25	1.09	4.85	4.97	0.01	0.26	0.26	0.28	0.07
54068.210.00 73.55 95.942.580.242.2854078.180.00 73.55 96.632.590.252.2354078.18-0.01 72.25 96.632.590.252.2354078.18-0.01 72.55 95.632.590.252.3154088.21-0.01 73.36 93.362.560.272.3454098.21-0.01 73.39 92.560.272.3454098.30-0.01 73.77 96.132.510.292.3754108.31-0.01 73.77 96.132.510.292.3754118.18-0.01 73.77 96.492.560.272.34541158.16-0.01 73.77 96.492.500.292.3754128.16-0.01 73.77 96.492.500.292.3754138.16-0.01 73.77 96.492.560.242.3654138.16-0.01 73.77 96.492.570.262.3754138.16-0.01 78.33 94.482.840.242.3654138.16-0.01 78.33 94.482.840.252.3454138.16-0.01 78.33 94.482.840.252.3454138.21-0.01 78.33 94.482.840.252.3554138.21-0.01<	5405.5		8.16	0.00	74.20	96.78	2.57	0.24	2.27	1.16	4.82	4.87	0.01	0.25	0.25	0.29	0.07
5406.5 8.18 0.00 73.55 96.29 2.58 0.24 2.28 5407.5 8.18 -0.01 72.25 96.63 2.59 0.25 2.231 5407.5 8.21 -0.01 72.26 95.56 2.60 0.25 2.231 5408.5 8.21 -0.01 73.39 93.77 2.60 0.25 2.31 5408.5 8.21 -0.01 73.36 92.56 2.57 0.27 2.34 5409.5 8.23 -0.01 73.37 94.26 2.57 0.27 2.34 5409.5 8.23 -0.01 73.37 94.26 2.56 0.27 2.34 5401.5 8.21 -0.01 73.37 96.13 2.51 0.27 2.34 5411.5 8.16 -0.01 73.37 96.13 2.51 0.27 2.34 5411.5 8.16 -0.01 73.37 96.13 2.51 0.27 2.34 5411.5 8.16 -0.01 73.37 96.13 2.51 0.27 2.34 5411.5 8.16 -0.01 73.37 96.13 2.51 0.27 2.34 5411.5 8.24 0.00 92.60 92.60 2.23 0.25 2.24 5411.5 8.24 0.00 92.60 92.60 2.24 0.25 2.24 5412.5 8.24 0.00 92.60 92.60 2.25 2.24 5425.5 2.27 8.2	5406		8.21	0.00	73.55	95.94	2.58	0.24	2.28	1.15	4.47	4.49	0.04	0.25	0.23	0.32	0.07
5407 8.18 -0.01 72.25 96.63 2.59 0.25 2.21 5407.5 8.21 -0.02 $71.3.68$ 95.56 2.60 0.25 2.28 5408.5 8.21 -0.01 $71.3.98$ 93.77 2.60 0.29 2.31 5408.5 8.21 -0.01 73.36 92.56 2.57 0.27 2.36 5409.5 8.23 -0.01 73.77 94.29 2.556 0.27 2.34 5409.5 8.21 -0.01 73.77 94.29 2.55 0.27 2.34 5410.5 8.21 -0.01 73.77 96.49 2.56 0.27 2.34 5411.5 8.16 -0.01 73.77 96.49 2.57 0.27 2.34 5411.5 8.16 -0.01 80.69 92.60 2.64 0.25 2.34 5411.5 8.16 -0.01 80.61 91.70 2.79 0.25 2.34 5411.5 8.16 0.00 92.60 92.60 2.25 0.25 2.34 5411.5 8.16 0.00 88.91 91.70 2.79 0.25 2.34 5411.5 8.16 0.00 92.60 92.60 2.64 0.25 2.34 5411.5 8.16 0.00 86.33 94.36 2.87 0.24 2.36 5413.5 8.16 0.00 86.33 94.36 2.84 0.25 2.34 5425.5 2.0	5406.5		8.18	0.00	73.55	96.29	2.58	0.24	2.28	1.13	4.53	4.51	0.06	0.25	0.23	0.32	0.07
5407.5 8.21 -0.02 72.68 95.56 2.60 0.25 2.28 5408 8.21 -0.01 73.98 93.77 2.60 0.29 2.31 5408 8.22 -0.01 73.39 93.77 2.60 0.27 2.36 5409 8.28 -0.01 78.31 93.26 2.57 0.27 2.34 5409 8.28 -0.01 73.77 94.29 2.56 0.27 2.34 5410 8.21 -0.01 73.77 96.49 2.50 0.29 2.23 5411 8.18 -0.01 73.77 96.49 2.50 0.29 2.23 5411 8.18 -0.01 73.77 96.49 2.50 0.26 2.23 5411 8.16 -0.01 91.07 91.70 2.79 0.24 2.36 5413 8.16 -0.01 73.77 96.49 2.56 0.27 2.34 5413.5 8.20 -0.01 78.83 94.36 2.87 0.24 2.36 5413.5 8.20 -0.01 78.83 95.22 2.64 0.25 2.34 5413.5 8.20 -0.01 78.83 95.22 2.46 0.27 2.36 5413.5 8.20 -0.01 78.83 95.22 2.64 0.25 2.34 5426.5 8.21 -0.01 76.99 103.00 2.56 0.27 2.26 5426.5 8.21 $-0.$	5407		8.18	-0.01	72.25	96.63	2.59	0.25	2.27	1.10	4.39	4.36	0.10	0.25	0.22	0.33	0.07
54088.21 -0.01 73.98 93.77 2.600.292.315408.58.22 -0.01 79.39 92.56 2.570.272.3654098.28 -0.01 78.31 93.26 2.560.272.345409.58.30 -0.01 73.55 94.29 2.560.272.345410.58.21 -0.01 73.57 96.13 2.510.292.285411.58.18 -0.01 73.77 96.49 2.500.292.345411.58.18 -0.01 73.77 96.49 2.500.292.375411.58.16 -0.01 73.77 96.49 2.500.292.345411.58.16 -0.01 91.0791.0791.702.790.252.345413.58.16 -0.01 78.3194.362.870.252.345413.58.21 -0.01 78.8394.482.890.252.345413.58.21 -0.01 78.8394.362.500.252.345413.58.21 -0.01 78.8394.360.252.342.365413.58.21 -0.01 78.8394.360.252.342.355413.58.21 -0.01 78.3394.480.252.342.355413.58.21 -0.01 76.39103.062.532.342.355425.520neC8.21 -0.01 74.39104.54 <td>5407.5</td> <td></td> <td>8.21</td> <td>-0.02</td> <td>72.68</td> <td>95.56</td> <td>2.60</td> <td>0.25</td> <td>2.28</td> <td>1.15</td> <td>4.31</td> <td>4.25</td> <td>0.10</td> <td>0.25</td> <td>0.22</td> <td>0.33</td> <td>0.07</td>	5407.5		8.21	-0.02	72.68	95.56	2.60	0.25	2.28	1.15	4.31	4.25	0.10	0.25	0.22	0.33	0.07
5408.5 8.22 -0.01 79.39 92.56 2.57 0.27 2.36 5409 8.28 -0.01 73.55 94.29 2.56 0.27 2.34 5410 8.21 -0.01 73.77 96.49 2.56 0.27 2.34 5410.5 8.21 -0.01 73.77 96.49 2.50 0.27 2.34 5411.5 8.18 -0.01 73.77 96.49 2.50 0.26 2.27 5411.5 8.18 -0.01 91.07 91.70 2.79 0.26 2.27 5411.5 8.16 -0.01 91.07 91.70 2.79 0.26 2.27 5411.5 8.16 -0.01 91.07 91.70 2.79 0.26 2.34 5412.5 8.23 0.00 92.60 92.66 2.88 0.25 2.34 5413.5 8.16 0.00 94.33 94.48 2.84 0.25 2.34 5413.5 8.20 0.00 86.33 94.48 2.84 0.25 2.34 5413.5 8.20 0.00 86.33 94.48 2.84 0.25 2.34 5413.5 8.20 0.00 86.33 94.48 2.84 0.25 2.34 5413.5 8.20 0.00 86.33 94.48 2.84 0.25 2.34 5425.5 $200c$ 8.23 0.00 8.24 0.25 2.34 5425.5 $200c$ 8.24	5408		8.21	-0.01	73.98	93.77	2.60	0.29	2.31	1.27	3.94	3.89	0.34	0.26	0.16	0.42	0.07
5409 8.28 -0.01 78.31 93.26 2.56 0.27 2.34 5409.5 8.30 -0.01 73.55 94.29 2.50 0.27 2.34 5410.5 8.21 -0.01 73.77 96.49 2.50 0.29 2.28 5410.5 8.21 -0.01 73.77 96.49 2.50 0.27 2.34 5411.5 8.18 -0.01 91.07 91.70 2.79 0.26 2.27 5411.5 8.16 -0.01 91.07 91.70 2.79 0.26 2.34 5412.5 8.23 0.00 92.60 92.76 2.88 0.25 2.34 5413.5 8.24 0.00 94.33 94.36 2.87 0.24 2.37 5413.5 8.21 0.00 86.33 94.48 2.84 0.25 2.34 5413.5 8.20 0.00 88.91 92.76 2.86 0.24 2.37 5413.5 8.21 0.00 86.33 94.48 2.84 0.25 2.34 5413.5 8.20 0.00 86.33 94.48 2.84 0.25 2.34 5413.5 8.20 0.00 86.33 94.48 2.84 0.25 2.34 5425.5 $200c$ 8.23 -0.01 83.77 90.94 2.74 0.25 5426.5 8.21 -0.01 79.36 2.44 0.25 2.20 5426.5 8.21 -0.01	5408.5		8.22	-0.01	79.39	92.56	2.57	0.27	2.36	1.40	3.97	3.86	0.38	0.24	0.12	0.52	0.06
5409.5 8.30 -0.01 73.55 94.29 2.52 0.27 2.34 5410.5 8.21 -0.01 73.77 96.49 2.50 0.29 2.28 5411.5 8.18 -0.01 73.77 96.49 2.50 0.29 2.29 5411.5 8.18 -0.01 80.69 92.60 2.63 0.26 2.24 5411.5 8.16 -0.01 80.69 92.60 2.63 0.26 2.37 5412.5 8.16 -0.01 80.69 92.60 2.63 0.26 2.37 5413.5 8.24 0.00 94.33 94.48 2.87 0.24 2.37 5413.5 8.20 0.00 86.33 94.48 2.84 0.25 2.34 5413.5 8.20 0.00 86.33 94.48 2.84 0.25 2.34 5413.5 8.20 0.00 86.33 94.36 2.87 0.24 2.37 5413.5 8.20 0.00 86.33 94.48 2.84 0.25 2.34 5425.5 2.000 8.32 -0.01 78.83 95.22 2.64 0.25 2.34 5425.5 2.000 8.32 -0.01 78.93 95.22 2.64 0.25 2.31 5425.5 2.000 8.32 -0.01 74.39 104.54 2.47 0.26 2.26 5426.5 8.21 -0.01 77.32 2.84 0.25 2.24 <td>5409</td> <td></td> <td>8.28</td> <td>-0.01</td> <td>78.31</td> <td>93.26</td> <td>2.56</td> <td>0.27</td> <td>2.37</td> <td>1.61</td> <td>4.75</td> <td>4.63</td> <td>0.41</td> <td>0.23</td> <td>0.11</td> <td>0.50</td> <td>0.06</td>	5409		8.28	-0.01	78.31	93.26	2.56	0.27	2.37	1.61	4.75	4.63	0.41	0.23	0.11	0.50	0.06
5410 8.21 -0.01 69.23 96.13 2.51 0.29 2.23 5410.5 8.21 -0.01 73.77 96.49 2.50 0.29 2.27 5411.5 8.18 -0.01 80.69 92.60 2.63 0.26 2.29 5411.5 8.16 -0.01 91.07 91.70 21.70 2.79 0.25 2.34 5411.5 8.23 0.00 92.60 92.76 2.87 0.26 2.37 5412.5 8.24 0.00 94.33 94.48 2.84 0.25 2.34 5413.5 8.26 0.00 86.33 94.48 2.84 0.25 2.36 5413.5 8.20 0.00 86.33 94.48 2.84 0.25 2.36 5413.5 8.20 0.00 88.91 92.72 2.86 0.24 2.36 5413.5 8.20 -0.01 78.83 95.22 2.64 0.25 2.34 5413.5 $200eC$ 8.32 -0.01 78.83 95.22 2.64 0.25 2.34 5425.5 $ZoneC$ 8.21 -0.01 78.93 95.22 2.64 0.25 2.34 5426.5 $ZoneC$ 8.21 -0.01 78.93 95.22 2.64 0.26 2.24 5426.5 $ZoneC$ 8.21 -0.01 74.39 104.54 2.44 0.25 2.24 5427.5 8.21 -0.01 79.18 107.29 <t< td=""><td>5409.5</td><td></td><td>8.30</td><td>-0.01</td><td>73.55</td><td>94.29</td><td>2.52</td><td>0.27</td><td>2.34</td><td>1.58</td><td>4.91</td><td>4.83</td><td>0.32</td><td>0.24</td><td>0.15</td><td>0.41</td><td>0.06</td></t<>	5409.5		8.30	-0.01	73.55	94.29	2.52	0.27	2.34	1.58	4.91	4.83	0.32	0.24	0.15	0.41	0.06
5410.5 8.21 -0.01 73.77 96.49 2.50 0.29 2.27 5411.5 8.18 -0.01 80.69 92.60 2.63 0.26 2.34 5411.5 8.16 -0.01 91.07 91.70 2.79 0.25 2.34 5412.5 8.23 0.00 92.60 92.76 2.88 0.23 2.37 5413.5 8.24 0.00 94.33 94.36 2.84 0.24 2.36 5413.5 8.25 0.00 86.33 94.48 2.84 0.25 2.36 5413.5 8.20 -0.01 78.83 94.36 2.84 0.25 2.36 5413.5 8.20 -0.01 78.83 94.36 2.84 0.25 2.36 5413.5 8.20 -0.01 78.83 94.36 2.84 0.25 2.36 5413.5 $2oneC$ 8.32 -0.01 78.83 94.36 2.76 0.26 2.32 5425.5 $ZoneC$ 8.21 -0.01 78.83 95.22 2.64 0.25 2.31 5426.5 8.21 -0.01 78.93 95.22 2.64 0.26 2.32 5427.5 8.21 -0.01 79.93 104.54 2.45 0.27 2.26 5428.5 8.21 -0.01 79.18 102.23 2.44 0.26 2.26 5428.5 8.21 -0.01 79.18 107.29 2.76 2.26 5	5410		8.21	-0.01	69.23	96.13	2.51	0.29	2.28	1.39	5.24	5.21	0.29	0.27	0.18	0.33	0.06
5411 8.18 -0.01 80.69 92.60 2.63 0.26 2.29 5411.5 8.16 -0.01 91.07 91.70 279 0.25 2.34 5412 8.23 0.00 92.60 92.76 2.88 0.23 2.37 5412.5 8.23 0.00 94.33 94.36 2.87 0.24 2.38 5413.5 8.26 0.00 86.33 94.48 2.84 0.25 2.36 5413.5 8.25 0.00 88.91 92.72 2.86 0.24 2.37 5413.5 8.20 -0.01 78.83 94.48 2.84 0.25 2.36 5413.5 8.20 -0.01 78.83 94.48 2.84 0.25 2.36 5413.5 8.20 -0.01 78.83 95.22 2.64 0.25 2.36 5413.5 $2oneC$ 8.32 -0.01 78.83 95.22 2.64 0.25 2.31 5426 8.21 -0.01 78.83 95.22 2.64 0.25 2.31 5426.5 8.21 -0.01 74.39 104.54 2.46 0.27 2.29 5426.5 8.21 -0.01 79.36 103.00 2.55 0.27 2.26 5427.5 8.21 -0.01 79.18 107.29 2.44 0.26 2.26 5428.5 8.21 -0.01 77.32 98.98 2.44 0.26 2.26 5428.5 8.21 -0.01 <td>5410.5</td> <td></td> <td>8.21</td> <td>-0.01</td> <td>73.77</td> <td>96.49</td> <td>2.50</td> <td>0.29</td> <td>2.27</td> <td>1.17</td> <td>4.86</td> <td>4.79</td> <td>0.26</td> <td>0.28</td> <td>0.20</td> <td>0.33</td> <td>0.07</td>	5410.5		8.21	-0.01	73.77	96.49	2.50	0.29	2.27	1.17	4.86	4.79	0.26	0.28	0.20	0.33	0.07
5411.5 8.16 -0.01 91.07 91.70 2.79 0.25 2.34 5412 8.23 0.00 92.60 92.76 2.88 0.23 2.37 5412.5 8.23 0.00 94.33 94.36 2.87 0.24 2.38 5413.5 8.16 0.00 86.33 94.48 2.84 0.25 2.36 5413.5 8.16 0.00 86.33 94.48 2.84 0.25 2.36 5413.5 8.25 0.00 86.33 94.48 2.84 0.25 2.36 5413.5 8.20 -0.01 78.83 95.22 2.64 0.25 2.36 5413.5 8.20 -0.01 78.83 95.22 2.64 0.25 2.31 5425.5 $2.00cC$ 8.32 -0.01 76.99 103.00 2.55 0.27 2.24 5426.5 8.21 -0.01 76.99 103.00 2.55 0.27 2.24 5426.5 8.21 -0.01 76.99 103.00 2.55 0.27 2.29 5427.5 8.21 -0.01 77.32 99.04 2.70 0.26 2.26 5428.5 8.21 -0.01 79.18 101.29 2.44 0.26 2.26 5428.5 8.23 -0.01 77.32 98.98 2.45 0.26 2.26 5428.5 8.18 -0.01 77.32 98.98 2.45 0.26 2.26 5428	5411		8.18	-0.01	80.69	92.60	2.63	0.26	2.29	1.13	4.30	4.20	0.18	0.25	0.20	0.36	0.07
5412 8.23 0.00 92.60 92.76 2.88 0.23 2.37 5412.5 8.24 0.00 94.33 94.36 2.87 0.24 2.38 5413 8.16 0.00 86.33 94.48 2.84 0.25 2.36 5413.5 8.26 0.00 88.91 92.72 2.86 0.24 2.37 5413.5 8.20 -0.01 78.83 95.22 2.64 0.25 2.31 5426 8.20 -0.01 78.83 95.22 2.64 0.25 2.31 5426 8.21 -0.01 78.93 95.22 2.64 0.25 2.31 5426.5 8.21 -0.01 78.93 95.22 2.64 0.27 2.29 5426.5 8.21 -0.01 76.99 103.00 2.55 0.27 2.20 5426.5 8.21 -0.01 74.39 104.54 2.46 0.27 2.29 5426.5 8.21 -0.01 79.18 102.23 2.44 0.27 2.29 5428.5 8.21 -0.01 79.18 102.23 2.44 0.26 2.26 5428.6 8.18 -0.01 79.18 102.23 2.44 0.26 2.26 5429.5 8.21 -0.01 79.18 102.23 2.44 0.26 2.26 5429.5 8.21 -0.01 77.32 98.98 2.45 0.27 2.26 5429.5 8.21 </td <td>5411.5</td> <td></td> <td>8.16</td> <td>-0.01</td> <td>91.07</td> <td>91.70</td> <td>2.79</td> <td>0.25</td> <td>2.34</td> <td>1.31</td> <td>4.70</td> <td>4.58</td> <td>0.22</td> <td>0.23</td> <td>0.17</td> <td>0.40</td> <td>0.07</td>	5411.5		8.16	-0.01	91.07	91.70	2.79	0.25	2.34	1.31	4.70	4.58	0.22	0.23	0.17	0.40	0.07
5412.5 8.24 0.00 94.33 94.36 2.87 0.24 2.38 5413.5 8.16 0.00 86.33 94.48 2.84 0.25 2.36 5413.5 8.25 0.00 88.91 92.72 2.86 0.24 2.37 5413.5 8.20 -0.01 78.83 95.22 2.64 0.25 2.31 5425.5 $2.0ne C$ 8.32 -0.01 78.83 95.22 2.64 0.25 2.31 5426 8.21 -0.01 76.99 103.00 2.55 0.27 2.24 5426 8.21 -0.01 74.39 104.54 2.45 0.27 2.20 5426 8.21 -0.01 79.18 102.23 2.44 0.27 2.20 5427.5 8.21 -0.01 79.18 102.23 2.44 0.27 2.20 5428 8.18 -0.01 79.18 102.23 2.44 0.26 2.26 5429 8.18 -0.01 77.32 98.98 2.45 0.26 2.26 5429 8.18 -0.01 77.32 98.98 2.45 0.26 2.26 5429 8.18 -0.01 77.32 98.98 2.45 0.26 2.26 5429 8.18 -0.01 77.32 98.98 2.46 0.26 2.26 5429 8.21 -0.01 80.34 98.13 2.50 0.26 2.26 5430 8	5412		8.23	0.00	92.60	92.76	2.88	0.23	2.37	1.62	4.00	3.89	0.25	0.22	0.14	0.50	0.07
5413 8.16 0.00 86.33 94.48 2.84 0.25 2.36 5413.5 8.25 0.00 88.91 92.72 2.86 0.24 2.37 Average 8.20 -0.01 78.83 95.22 2.64 0.25 2.31 Average 8.20 -0.01 78.83 95.22 2.64 0.25 2.31 5425.5 8.21 -0.01 78.33 95.22 2.64 0.26 2.32 5426 8.21 -0.01 76.99 103.00 2.55 0.27 2.24 5427 8.21 -0.01 74.39 104.54 2.45 0.27 2.20 5427 8.21 -0.01 79.18 102.23 2.44 0.27 2.20 5427.5 8.21 -0.01 79.18 102.23 2.44 0.26 2.26 5428.5 8.23 -0.01 79.18 101.29 2.44 0.26 2.26 5429.5 8.18 -0.01 77.32 98.98 2.45 0.26 2.26 5429.5 8.21 -0.01 77.32 98.98 2.45 0.26 2.26 5429.5 8.21 -0.01 77.32 98.98 2.45 0.26 2.26 5429.5 8.21 -0.01 80.34 98.13 2.50 0.26 2.26 5430.5 8.21 -0.01 81.12 98.30 2.55 0.277 2.26 5430.5 8.21 </td <td>5412.5</td> <td></td> <td>8.24</td> <td>0.00</td> <td>94.33</td> <td>94.36</td> <td>2.87</td> <td>0.24</td> <td>2.38</td> <td>1.75</td> <td>3.19</td> <td>3.15</td> <td>0.31</td> <td>0.22</td> <td>0.13</td> <td>0.58</td> <td>0.07</td>	5412.5		8.24	0.00	94.33	94.36	2.87	0.24	2.38	1.75	3.19	3.15	0.31	0.22	0.13	0.58	0.07
5413.5 8.25 0.00 88.91 92.72 2.86 0.24 2.37 Average 8.20 -0.01 78.83 95.22 2.64 0.25 2.31 5425.5 $Zone C$ 8.32 -0.01 83.72 99.04 2.70 0.26 2.32 5426.5 8.21 -0.01 76.99 103.00 2.55 0.27 2.24 5426.5 8.21 -0.01 76.99 103.00 2.55 0.27 2.24 5427.5 8.21 -0.01 79.18 104.54 2.45 0.27 2.20 5427.5 8.21 -0.01 79.18 102.23 2.44 0.27 2.20 5427.5 8.21 -0.01 79.18 102.23 2.44 0.26 2.26 5428.5 8.18 -0.01 79.18 101.29 2.44 0.26 2.26 5429.5 8.23 -0.01 77.32 98.98 2.45 0.26 2.26 5429.5 8.21 -0.01 77.32 98.18 0.26 2.26 5429.5 8.21 -0.01 80.34 98.13 2.50 0.26 2.26 5429.5 8.21 -0.01 81.12 98.30 2.55 0.26 2.26 5429.5 8.21 -0.01 81.12 98.30 2.56 0.26 2.26 5430.5 8.21 -0.01 81.12 99.71 2.50 0.26 2.26 5430.5	5413		8.16	0.00	86.33	94.48	2.84	0.25	2.36	0.94	3.39	3.39	0.30	0.23	0.14	0.52	0.07
Average 8.20 -0.01 78.83 95.22 2.64 0.25 2.31 5425.5 Zone C 8.32 -0.01 83.72 99.04 2.70 0.26 2.32 5426.5 8.21 -0.01 76.99 103.00 2.55 0.27 2.24 5426.5 8.21 -0.01 74.39 104.54 2.45 0.27 2.20 5426.5 8.21 -0.01 79.15 103.06 2.55 0.27 2.20 5427 8.21 -0.01 79.18 104.54 2.45 0.27 2.20 5427.5 8.21 -0.01 79.18 102.23 2.44 0.26 2.23 5428.5 8.23 -0.01 79.18 101.29 2.44 0.26 2.26 5428.5 8.23 -0.01 77.32 98.98 2.45 0.26 2.26 5429.5 8.21 -0.01 77.32 98.91 2.50 0.26 2.26	5413.5		8.25	0.00	88.91	92.72	2.86	0.24	2.37	0.93	3.67	3.72	0.26	0.22	0.14	0.50	0.07
5425.5 Zone C 8.32 -0.01 83.72 99.04 2.70 0.26 2.32 5426. 8.21 -0.01 76.99 103.00 2.55 0.27 2.24 5426.5 8.21 -0.01 74.39 104.54 2.45 0.27 2.20 5426.5 8.21 -0.01 79.15 103.06 2.55 0.27 2.20 5427 8.21 -0.01 79.18 103.26 2.42 0.27 2.19 5427.5 8.21 -0.01 79.18 102.23 2.44 0.27 2.20 5428.5 8.18 -0.01 79.18 101.29 2.44 0.26 2.25 5429 8.18 -0.01 77.32 98.98 2.45 0.26 2.26 5429 8.21 -0.01 80.34 98.13 2.50 0.26 2.28 5429.5 8.21 -0.01 83.37 97.70 2.54 0.26 2.28 5429.5 8.21 -0.01 81.12 98.30 2.55 0.27 2.26	Average		8.20	-0.01	78.83	95.22	2.64	0.25	2.31	1.26	4.29	4.26	0.19	0.25	0.19	0.39	0.07
5426 8.21 -0.01 76.99 103.00 2.55 0.27 2.24 5426.5 8.21 -0.01 74.39 104.54 2.45 0.27 2.20 5427 8.21 -0.01 79.15 103.26 2.42 0.27 2.20 5427.5 8.21 -0.01 79.18 102.23 2.44 0.27 2.20 5428.5 8.18 -0.01 79.18 101.29 2.44 0.26 2.22 5429 8.18 -0.01 77.32 98.98 2.45 0.26 2.26 5429 8.21 -0.01 77.32 98.13 2.50 0.26 2.26 5429.5 8.21 -0.01 80.34 98.13 2.50 0.26 2.26 5429.5 8.18 -0.01 81.12 98.30 2.55 0.26 2.28 5429.5 8.21 -0.01 81.12 98.13 2.50 0.26 2.26 5430 8.21 -0.01 81.12 98.30 2.55 0.27 2.26 5430.5 8.21 -0.01 79.37 99.71 2.50 0.29 2.24	5425.5	Zone C	8.32	-0.01	83.72	99.04	2.70	0.26	2.32	1.43	2.90	3.21	0.26	0.25	0.17	0.46	0.08
5426.5 8.21 -0.01 74.39 104.54 2.45 0.27 2.20 5427 8.21 -0.01 79.15 103.26 2.42 0.27 2.19 5427.5 8.21 -0.01 79.15 103.26 2.42 0.27 2.19 5427.5 8.21 -0.01 79.18 102.23 2.44 0.27 2.20 5428.5 8.18 -0.01 77.32 98.98 2.45 0.26 2.25 5429 8.21 -0.01 77.32 98.13 2.50 0.26 2.26 5429 8.21 -0.01 8.337 97.70 2.54 0.26 2.28 5429.5 8.18 -0.01 81.12 98.30 2.55 0.26 2.28 5429.5 8.21 -0.01 81.12 98.30 2.55 0.26 2.28 5430 8.21 -0.01 79.37 99.71 2.50 0.27 2.26 5430.5 8.21 -0.01 79.37 99.71 2.50 0.29 2.24 <td>5426</td> <td></td> <td>8.21</td> <td>-0.01</td> <td>76.99</td> <td>103.00</td> <td>2.55</td> <td>0.27</td> <td>2.24</td> <td>1.14</td> <td>3.57</td> <td>4.06</td> <td>0.09</td> <td>0.27</td> <td>0.24</td> <td>0.31</td> <td>0.08</td>	5426		8.21	-0.01	76.99	103.00	2.55	0.27	2.24	1.14	3.57	4.06	0.09	0.27	0.24	0.31	0.08
5427 8.21 -0.01 79.15 103.26 2.42 0.27 2.19 5427.5 8.21 -0.01 79.18 102.23 2.44 0.27 2.20 5428 8.18 -0.01 79.18 101.29 2.44 0.27 2.20 5428 8.18 -0.01 79.18 101.29 2.44 0.26 2.22 5429 8.13 -0.01 77.32 98.98 2.45 0.26 2.26 5429 8.21 -0.01 80.34 98.13 2.50 0.26 2.28 5429.5 8.18 -0.01 81.32 97.70 2.54 0.26 2.28 5430 8.21 -0.01 81.12 98.30 2.55 0.27 2.26 5430.5 8.21 -0.01 79.37 99.71 2.50 0.27 2.26	5426.5		8.21	-0.01	74.39	104.54	2.45	0.27	2.20	1.07	4.45	5.13	0.00	0.29	0.29	0.24	0.07
5427.5 8.21 -0.01 79.18 102.23 2.44 0.27 2.20 5428 8.18 -0.01 79.18 101.29 2.44 0.26 2.22 5428.5 8.23 -0.01 77.32 98.98 2.45 0.26 2.26 5429.5 8.21 -0.01 80.34 98.13 2.50 0.26 2.28 5429.5 8.18 -0.01 80.34 98.13 2.50 0.26 2.28 5430 8.21 -0.01 81.12 98.30 2.55 0.27 2.29 5430 8.21 -0.01 81.12 98.30 2.55 0.27 2.26 5430 8.21 -0.01 79.37 99.71 2.50 0.29 2.24	5427		8.21	-0.01	79.15	103.26	2.42	0.27	2.19	1.10	5.09	5.89	0.00	0.29	0.29	0.22	0.07
5428 8.18 -0.01 79.18 101.29 2.44 0.26 2.22 5428.5 8.23 -0.01 77.32 98.98 2.45 0.26 2.26 5429 8.21 -0.01 87.32 98.98 2.45 0.26 2.26 5429 8.21 -0.01 80.34 98.13 2.50 0.26 2.28 5429.5 8.18 -0.01 83.37 97.70 2.54 0.26 2.29 5430 8.21 -0.01 81.12 98.30 2.55 0.27 2.26 5430.5 8.21 -0.01 79.37 99.71 2.50 0.29 2.26	5427.5		8.21	-0.01	79.18	102.23	2.44	0.27	2.20	1.16	5.14	5.92	0.00	0.29	0.29	0.23	0.07
5428.5 8.23 -0.01 77.32 98.98 2.45 0.26 2.26 5429 8.21 -0.01 80.34 98.13 2.50 0.26 2.28 5429.5 8.18 -0.01 80.34 98.13 2.50 0.26 2.28 5429.5 8.18 -0.01 83.37 97.70 2.54 0.26 2.29 5430 8.21 -0.01 81.12 98.30 2.55 0.27 2.26 5430.5 8.21 -0.01 79.37 99.71 2.50 0.29 2.24	5428		8.18	-0.01	79.18	101.29	2.44	0.26	2.22	1.18	4.94	5.53	0.00	0.27	0.27	0.24	0.07
5429 8.21 -0.01 80.34 98.13 2.50 0.26 2.28 5429.5 8.18 -0.01 83.37 97.70 2.54 0.26 2.29 5430 8.21 -0.01 81.12 98.30 2.55 0.27 2.26 5430 8.21 -0.01 81.12 98.30 2.55 0.27 2.26 5430.5 8.21 -0.01 79.37 99.71 2.50 0.29 2.24	5428.5		8.23	-0.01	77.32	98.98	2.45	0.26	2.26	1.20	4.87	5.36	0.07	0.26	0.24	0.28	0.07
5429.5 8.18 -0.01 83.37 97.70 2.54 0.26 2.29 5430 8.21 -0.01 81.12 98.30 2.55 0.27 2.26 5430.5 8.21 -0.01 81.12 98.30 2.55 0.27 2.26 5430.5 8.21 -0.01 79.37 99.71 2.50 0.29 2.24	5429		8.21	-0.01	80.34	98.13	2.50	0.26	2.28	1.21	4.86	5.34	0.14	0.25	0.21	0.31	0.06
5430 8.21 -0.01 81.12 98.30 2.55 0.27 2.26 5430.5 8.21 -0.01 79.37 99.71 2.50 0.29 2.24	5429.5		8.18	-0.01	83.37	97.70	2.54	0.26	2.29	1.21	5.00	5.50	0.16	0.26	0.21	0.31	0.06
5430.5 8.21 -0.01 79.37 99.71 2.50 0.29 2.24	5430		8.21	-0.01	81.12	98.30	2.55	0.27	2.26	1.15	5.49	5.99	0.15	0.27	0.22	0.28	0.06
	5430.5		8.21	-0.01	79.37	99.71	2.50	0.29	2.24	1.10	6.24	6.79	0.16	0.28	0.23	0.25	0.06

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يزيز KAC	Table 2	continued)															
مدينة الملك عبداك عند العلوم والتقنية ST	Depth (ft)	Zone name	Calliper (IN)	Density correc- tion (G/ C3)	Gamma ray (API)	Sonic (US/F)	Photo- electric (B/E)	Neutron porosity	Density (G/C3)	Micro- spherical resistivity (\Omegam2/m)	Shallow resistivity (Ωm2/m)	Deep resistivity (Ωm2/m)	VSH_ ND	_TIHP UN	PHIE_ ND	SW_ INDO	BVW
<u>)</u> SF	5431		8.21	-0.01	77.21	100.83	2.48	0.28	2.21	1.06	7.23	7.90	0.06	0.29	0.27	0.20	0.06
oring	5431.5		8.18	-0.01	80.67	101.98	2.49	0.27	2.20	1.07	8.29	9.10	0.00	0.29	0.29	0.18	0.05
ger	5432		8.18	-0.01	85.67	100.52	2.57	0.27	2.21	1.06	8.28	8.96	0.00	0.29	0.29	0.19	0.05
	5432.5		8.18	-0.01	93.11	97.65	2.71	0.28	2.25	1.11	7.95	8.46	0.15	0.27	0.23	0.23	0.05
	5433		8.18	-0.01	97.65	95.95	2.83	0.26	2.31	1.28	6.48	6.77	0.23	0.25	0.18	0.30	0.05
	5433.5		8.19	0.00	102.20	96.63	2.87	0.25	2.33	1.35	5.05	5.15	0.22	0.24	0.17	0.37	0.06
	5434		8.18	-0.01	104.71	96.65	2.78	0.26	2.30	1.22	5.00	5.04	0.20	0.25	0.19	0.34	0.06
	5434.5		8.21	-0.01	103.35	101.42	2.67	0.26	2.26	1.13	5.71	5.66	0.10	0.26	0.23	0.28	0.06
	5435		8.21	-0.01	99.46	102.35	2.63	0.25	2.25	1.10	5.89	5.73	0.01	0.26	0.26	0.26	0.07
	5435.5		8.19	-0.01	91.23	93.89	2.68	0.25	2.28	1.14	6.27	6.03	0.10	0.25	0.22	0.28	0.06
	5436		8.21	-0.01	94.54	92.12	2.79	0.24	2.36	1.45	5.26	5.25	0.26	0.22	0.14	0.42	0.06
	Average		8.20	-0.01	86.54	99.37	2.59	0.26	2.26	1.18	5.63	6.04	0.11	0.27	0.23	0.28	0.06
	5488	Zone D	8.26	-0.01	76.15	98.84	2.80	0.29	2.33	0.95	1.95	2.03	0.37	0.26	0.14	0.63	0.09
	5488.5		8.23	-0.01	72.45	100.95	2.77	0.30	2.31	0.93	2.25	2.36	0.39	0.27	0.16	0.54	0.09
	5489		8.21	-0.01	72.67	102.34	2.72	0.34	2.29	0.84	2.32	2.44	0.50	0.30	0.15	0.53	0.08
	5489.5		8.18	-0.01	73.53	103.14	2.68	0.32	2.27	0.78	2.39	2.53	0.37	0.29	0.18	0.47	0.08
	5490		8.25	-0.01	73.98	105.05	2.63	0.30	2.25	0.67	2.25	2.37	0.23	0.28	0.21	0.44	0.09
	5490.5		8.23	-0.01	79.18	103.09	2.59	0.28	2.26	0.64	2.57	2.76	0.17	0.27	0.22	0.41	0.09
	5491		8.28	0.00	81.77	103.44	2.58	0.29	2.28	0.75	3.48	3.75	0.24	0.27	0.20	0.37	0.07
	5491.5		8.29	0.00	81.18	102.14	2.57	0.28	2.29	0.83	2.91	3.13	0.26	0.26	0.18	0.43	0.08
	5492		8.22	0.00	72.31	100.86	2.56	0.27	2.27	0.97	2.97	3.18	0.18	0.27	0.21	0.39	0.08
	5492.5		8.19	0.00	70.15	101.96	2.53	0.29	2.24	0.80	2.70	2.90	0.17	0.28	0.23	0.38	0.09
	5493		8.19	-0.01	76.77	98.96	2.50	0.30	2.24	0.79	2.85	3.02	0.19	0.29	0.23	0.37	0.09
	5493.5		8.22	0.00	84.56	95.78	2.53	0.27	2.27	0.84	2.97	3.10	0.16	0.26	0.21	0.40	0.08
	5494		8.24	0.00	95.37	92.58	2.59	0.26	2.33	1.11	2.96	3.06	0.26	0.24	0.16	0.49	0.08
	5494.5		8.25	0.00	102.11	91.78	2.67	0.25	2.37	1.54	3.16	3.26	0.35	0.23	0.12	0.58	0.07
	5495		8.28	0.00	106.43	93.54	2.70	0.29	2.37	1.75	2.47	2.57	0.48	0.24	0.10	0.70	0.07
	5495.5		8.25	0.00	95.18	94.90	2.70	0.26	2.34	1.23	1.89	1.97	0.28	0.24	0.16	0.63	0.10
	5496		8.23	-0.01	91.07	95.83	2.65	0.24	2.32	1.06	2.32	2.41	0.18	0.24	0.18	0.52	0.09
	5496.5		8.23	-0.01	88.25	94.23	2.66	0.21	2.33	1.13	2.31	2.40	0.08	0.22	0.19	0.51	0.10
	5497		8.25	0.00	90.39	93.84	2.70	0.23	2.35	1.35	1.96	2.00	0.19	0.22	0.16	0.62	0.10
	5497.5		8.23	-0.01	88.88	92.99	2.80	0.24	2.34	1.22	1.84	1.86	0.23	0.23	0.16	0.65	0.10
	5498		8.25	-0.01	93.21	94.44	2.91	0.25	2.34	1.22	1.98	1.99	0.24	0.23	0.16	0.63	0.10
	Average		8.24	0.00	83.62	98.31	2.65	0.28	2.30	1.01	2.53	2.66	0.27	0.26	0.18	0.50	0.09

Table 2 ((continued)															
Depth (ft)	Zone name	Calliper (IN)	Density correc- tion (G/ C3)	Gamma ray (API)	Sonic (US/F)	Photo- electric (B/E)	Neutron porosity	Density (G/C3)	Micro- spherical resistivity (Ωm2/m)	Shallow resistivity (Ωm2/m)	Deep resistivity (Ωm2/m)	UN	PHIT_ ND	PHIE_ ND	SW_ INDO	BVW
5558.5	Zone E	8.39	0.01	49.76	103.15	2.95	0.34	2.32	0.92	2.20	2.25	0.56	0.29	0.12	0.64	0.08
5559		8.25	0.00	47.17	102.08	2.69	0.28	2.27	0.97	2.71	2.82	0.23	0.27	0.20	0.42	0.09
5559.5		8.24	-0.01	51.39	101.26	2.50	0.27	2.24	1.09	2.35	2.48	0.08	0.27	0.25	0.39	0.10
5560		8.25	-0.01	57.32	101.29	2.47	0.26	2.24	1.08	2.26	2.38	0.04	0.27	0.26	0.39	0.10
5560.5		8.23	-0.01	59.26	101.08	2.52	0.28	2.25	1.01	2.40	2.52	0.16	0.28	0.23	0.41	0.09
5561		8.21	-0.01	51.14	101.72	2.60	0.28	2.26	1.13	2.01	2.11	0.20	0.27	0.22	0.47	0.10
5561.5		8.21	-0.01	50.40	102.05	2.68	0.32	2.26	1.08	1.72	1.84	0.35	0.29	0.19	0.53	0.10
5562		8.22	-0.01	49.54	102.41	2.75	0.31	2.26	1.00	1.63	1.71	0.28	0.29	0.20	0.53	0.11
5562.5		8.21	-0.01	55.16	101.93	2.83	0.31	2.24	0.91	1.86	1.95	0.26	0.30	0.22	0.47	0.10
5563		8.21	0.01	66.41	107.35	3.01	0.29	2.23	0.78	1.72	1.78	0.12	0.28	0.25	0.46	0.11
5563.5		8.16	0.04	80.69	110.26	3.30	0.34	2.27	0.43	1.32	1.38	0.45	0.31	0.17	0.64	0.11
Average		8.23	0.00	56.20	103.14	2.76	0.30	2.26	0.95	2.02	2.11	0.25	0.28	0.21	0.49	0.10

the efficiency of Zone A to be a favourable potential oil reservoir in Rabeh East Field.

The calculated water saturation has been displayed in track twelve in Fig. 5 and track ten in Figs. 6–8, shading with blue colour, while the green colour in the same track refers to the hydrocarbon saturation. The highest average water saturation of 50% (i.e. the hydrocarbon saturation equals 50%) was recorded in Zone D, while water saturation was low in Zone A (23%) (Tables 1 and 2).

The constructed Pickett plot (Pickett, 1972) for the studied zones shows that most of the plotted points are clustered below line of Sw = 50% confirming the hydrocarbon potentiality of these intervals. This reflects that the hydrocarbon saturation in the examined zones expected to be more than 50% as shown in Fig. 10. This result demonstrates the correctness of the mathematical calculations for the calculated water saturation values as well as the significance of these zones as oil-bearing zones.

The calculated BVW values have been presented in the last track in Figs. 5-8 shading with blue colour. The maximum bulk volume of water (0.10) was documented in Zone E, and the minimum value (0.03) was noted in Zone A (Tables 1 and 2).

The bulk volume of water at the irreducible case in sandstone reservoirs (i.e. expectable to yield water-free oil) depends on the grain size. If sand grains are fine-grained and graded to siltstones as the sand grains in the examined zones within the Mutulla Formation, the BVW values should vary between 0.035 and 0.09 (Asquith and Gibson 1982; Fertl and Vercellino 1978; Asquith 1985). Accordingly, since the BVW values in Zones; B, C and D vary between 0.06 and 0.09 (Table 2), it is expected that these zones will produce oil without water. However, Zone E that exhibits the highest BVW of 0.10 will produce oil with water.

Conclusions

The explanation of the well log data for the sandstone of the Mutulla Formation as well as the limestone of the Thebes Formation in Rabeh East Field at Gulf of Suez Basin exposed that these formations are superior oil reservoirs. The comprehensive petrophysical assessment for the well log data of RE-25 Well revealed five oil-bearing zones (A, B, C, D and E). These promising intervals represent total net pay thickness of 51.5 ft and display relatively low shale volume (0.07–0.27), high effective porosity (0.14–0.23), low water saturation (0.23–0.50) and low bulk volume of water (0.03–0.10). Zone A represents the promising limestone interval of Thebes Formation with 16 ft thick. This zone includes primary and secondary porosity types supporting the effectiveness of this limestone to be a valuable oil reservoir in the Rabeh East Field. However, the sandstone





Fig. 9 Neutron-density cross-plot for Zone A in Thebes Formation and Zones B, C, D, E within Mutulla Formation in RE-25 Well



Fig. 10 Pickett cross-plot for the promising Zones A, B, C, D, E in RE-25 Well. Note that the all points locate less than Sw = 75% line confirming the oil potentiality of these zones

reservoirs within the Mutulla Formation in RE-25 Well represented by zones B (10 ft thick), C (10.5 ft thick), D (10 ft thick) and E (5 ft thick). Consequently, drilling new wells close to the RE-25 Well in Rabeh East Field is highly indorsed to examine the Mutulla and the Thebes formations as supplementary oil reservoirs beside the main targets including the Nubia, Rudies and Nukhul formations. Acknowledgements Many thanks for Ganoub El-Wadi Petroleum Company and the Egyptian General Petroleum Corporation (EGPC) for providing the raw geophysical data used in this paper.

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Declarations

Conflict of interest Here, I confirm that there is no conflict of interest.

Ethical approval Hereby, I assure that this paper has not been previously published and the manuscript reflects my own research and analysis in a truthful and complete manner.

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