#### **ORIGINAL ARTICLE**



# Efficacy of persulfate-based advanced oxidation process (US/PS/Fe<sub>3</sub>O<sub>4</sub>) for ciprofloxacin removal from aqueous solutions

Shahin Ahmadi<sup>1</sup> · Christian Osagie<sup>2</sup> · Somayeh Rahdar<sup>1</sup> · Nadeem A. Khan<sup>3</sup> · Sirajuddin Ahmed<sup>3</sup> · Hamideh Hajini<sup>1</sup>

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#### Abstract

Research evidence has shown that pollution of surface and underground waters is the leading sources of environmental and health-related problems. Disposed unused therapeutic drugs have been known to contaminate underground water and also offer drug resistance to infection-causing bacterial. This research seeks to evaluate the use of US/PS/Fe<sub>3</sub>O<sub>4</sub> for the removal of ciprofloxacin (CIP-F) from aqueous solutions. The research also seeks to obtain the optimum set of conditions about which the highest removal efficiency of CIP-F is obtained by monitoring the used pH, Fe<sub>3</sub>O<sub>4</sub> nanoparticles (NPs) concentration, PS concentration, CIP-F concentration, and contact time. The analysis was done using a UV–Vis spectrophotometer (Cecil model CE102) set at 280 nm. The result shows that a 98.43% removal efficiency is achievable after optimization if the separation parameters were set to the optimum conditions (pH=5, CIP-F concentration=200 mg/L, PS concentration=0.15 mol/L, Fe<sub>3</sub>O<sub>4</sub> concentration=0.01 g/L and contact time=45 min). The reaction was also observed to follow the pseudo-first-order reaction model. Since the results obtained show that US/PS/Fe<sub>3</sub>O<sub>4</sub> can effectively and efficiently aid the surface adsorption of CIP-F from aqueous solutions, it is therefore recommended based on experimental findings that US/PS/Fe<sub>3</sub>O<sub>4</sub> be used for removing CIP-F from effluents.

Keywords Ciprofloxacin · US · Persulfate · Nanoparticles · Water treatment · Optimization

# Introduction

Research evidence has shown that pollution of surface and underground water is leading sources of environmental and health-related problems. Continuous usage of antibiotics to mitigate the resulting health issues could result in drug resistance even in low concentrations because they provided resistance to the causative bacteria (Choi et al. 2008). Drugs are generally used for treatment and prevention of bacterial infections (Ahmadi et al. 2017) and, as such, may either kill or inhibit the growth of the bacteria (Choi et al. 2008).

- <sup>2</sup> Environmental and Natural Sciences, Brandenburg University of Technology, Cottbus-Senftenberg, Senftenberg, Germany
- <sup>3</sup> Civil Engineering Department, Jamia Millia Islamia, New Delhi, India

Unused therapeutic drugs are sometimes disposed of into the sewage system. If these drugs are not degraded during sewage treatment, in soil or other environmental compartments, they may reach the surface water and groundwater and, potentially contaminate drinking water (Ahmadi et al. 2017). One of such antibiotics is ciprofloxacin (CIP-F). Ciprofloxacin (CIP-F) is a common antibiotic of fluoroquinolone class (Onyechi and Igwegbe 2018) that is widely prescribed for the treatment of intra-abdominal infections; this type of infection is associated with diarrhea, respiratory tract infections, and urinary tract infection (Zhang et al. 2011; Igwegbe et al. 2020). The antibiotic is classified into the fluoroquinolone class, which has a stable naphthol ring and is toxic to microorganisms, and their stability in the environment (Martinez 2009).

Many treatment methods have been proposed for the removal of CIP-F from contaminated waters, which include photodecomposition (Don et al. 2010), adsorption (Kho-shnamvand et al. 2017; Rahdar et al. 2019; Dhiman and Sharma 2018), oxidation (Bader and Hoigné 1981), and flotation (Mostafapour et al. 2017). The advanced oxidation process (AOP) is one of the most effective methods



Shahin Ahmadi sh.ahmadi398@gmail.com

Christian Osagie osagichr@b-tu.de

<sup>&</sup>lt;sup>1</sup> Department of Environmental Health, Zabol University of Medical Sciences, Zabol, Iran

of decomposing and removing dangerous, resistive, and biological irresolvable organic pollutants (Ren et al. 2010). This process is based on the production of hydroxyl radicals (Arsene et al. 2011; Poulopoulos et al. 2006; Khan et al. 2019b; Balarak et al. 2019). These radicals oxidize organic compounds swiftly and non-selectively (Arsene et al. 2011). The use of ultrasonic waves has also attracted attention owing to their cheapness, environmentally friendliness, and lack of sludge production. The ultrasonic process is based on the development of pore or micro-bubbles from acoustic cavitation in water (Nelson et al. 2002).

However, the use of advanced oxidation cycle processes alone has not been efficient, its efficiency can be increased by using a sonochemical oxidation process, which is achieved by the addition of chemicals such as Persulfate, nanoparticles, and catalytic particles (Chen and Su 2012). Persulfate oxidation with a redox potential of 2.01 has proven to be more effective when compared with hydrogen peroxide and ozone since the produced radicals are more cost-efficient, soluble, and stable when applied to toxic and resistive materials (Epold et al. 2015). Persulfate (PS) salt dissolved in water will be produced  $S_2O_8^2$  anion with low oxidation capacity. Chemical and thermal methods can be used to increase the oxidative capacity and production of SO<sub>4</sub> from the aforementioned anion (Chen and Su 2012). The rate of persulfate reaction has been observed to increased significantly when heat, light, or specific metallic ions were used as a catalyst (Epold et al. 2015). Ions from cobalt or Iron are commonly used metallic ions for the activation of Persulfate (Taimoory et al. 2017). Metallic ions from Iron ( $Fe^{2+}$ ) are the most preferred but are associated with problems such as substantial volume requirements and high sludge production. To curb this excess, iron oxides nanoparticles can be used as a perfect substitute for Fe<sup>2+</sup> as they are non-toxic, readily available, and cost-effective. Iron oxide nanoparticle produced by green synthesis has been used to replace  $Fe^{2+}$  in this study to investigate its effectiveness.

This paper presents the removal of (CIP-F) from aqueous solution by the application of US/PS/Fe<sub>3</sub>O<sub>4</sub>. During this study, process parameters like pH, persulfate (PS) concentration, Fe<sub>3</sub>O<sub>4</sub> nanoparticles concentration, and time were varied and optimized, to access the optimal removal during the batch studies. The final concentration of CIP-F was investigated using the UV–Vis spectrophotometer Cecil model CE1021 at 280 nm.

# **Materials and methods**

#### Materials

CIP-F with the chemical formulae:  $C_{16}H_{17}KN_2O_4S$  has a molecular weight of 385.8 g/mol. Figure 1 shows the molecular structure of CIP-F.

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#### **Pilot ultrasonic**

A reactor with a known surface area is used for the pilot test. The reactor is a digital ultrasonic apparatus (Elma CD-Germany, 4820) made from Plexiglas. It has 3.7 L capacity in volume with a 2.5 w/cm<sup>2</sup> per unit of energy input and a power input of 500 w per 100 ml samples in the bath with US waves.

### Synthesis of Iron (II) sulfate heptahydrate (Fe<sub>3</sub>O<sub>4</sub>)

Analytical grade Iron (II) sulfate heptahydrate ( $FeSO_4.7H_2O$ ) and sodium hydroxide used in this research were also supplied by Sigma-Aldrich. Also, the magnetite nanoparticles used in this research were synthesized based on earlier published research on the use of a green surfactant-free electrochemical method (Taimoory et al. 2017).

#### **Experimental methods**

The pH of the water sample used for the research was adjusted by adding 0.1 mol of HCl into each flask. The final pH of the water sample was measured using a MIT65 pH meter. A stock solution of CIP-F was prepared with a concentration of 1000 ppm in double-distilled water. The prepared CIP-F solution was then poured into the Erlenmeyer flask, and Fe<sub>3</sub>O<sub>4</sub>–NPs were subsequently added. The Erlenmeyer flask with its contents was then placed inside the ultrasonic apparatus with the ultrasound waves regulated to 60 kHz at a set time. After the reaction, the residual concentrations were measured using a UV-visible spectrophotometer (Shimadzu Model: CE-1021-UK). The readings were taken at 280 nm with the spectrophotometer. The removal efficiency (%*R*) was then calculated using the equation below (Ahmadi and Mostafapour 2017a, b, c):

$$\%R = \frac{\left(C_0 - C_f\right)}{C_0} 100 \tag{1}$$

where  $C_o$  and  $C_f$  are the initial and equilibrium liquid-phase concentration of CIP-F(mg/L), respectively.



Ciprofloxacin (CIP-F) with 100% purity was used for this research; the CIP-F used was supplied by Sigma–Aldrich.



Fig. 1 The chemical structure of CIP-F

The four process variables monitored in this study were the initial pH of the solution (varied between 3 and 8), the concentration of the nanoparticles (varied between 0.01 and 0.08 g/L), the contact time (varied between 10 and 120 min), the concentration of PS (varied between 0.01 and 1.2 mol/L), and the initial concentration of CIP-F (varied between 50 and 250 mg/L).

# **Result and discussion**

# Effect of pH

The effect of pH is one of the parameters being monitored in this research. It directly influences the amount and type of radicals used for the advanced oxidation process. Figure 2 presents the results of varying the pH of 100 mg/L of ciprofloxacin (CIP-F) from 3 to 8 while monitoring its removal efficiency on US/PS/Fe<sub>3</sub>O<sub>4</sub>. The results showed that CIP-F removal efficiency increases with increasing pH. The removal efficiency showed a decline after pH 5 was exceeded. The highest possible efficiency was observed at pH 5, showing that CIP-F is better removed in an acidic environment. Also, since the advanced oxidation process works on the principle of hydroxyl production, removing it in an acidic medium encourages a neutralization reaction, thus enhancing the decomposition of the pollutant (Shemer et al. 2006).

#### Effect of Fe<sub>3</sub>O<sub>4</sub>–NPs concentration

Figure 3 presents the result obtained from monitoring the effect of change in concentration of  $Fe_3O_4$ -NPs on the removal efficiency, the optimum conditions were obtained at pH of 5 and  $Fe_3O_4$ -NPs concentration of 0.01 g/L.





**Fig. 3** Effect of  $Fe_3O_4$ –NPs concentration on the removal efficiency of CIP-F via the US/PS/Fe<sub>3</sub>O<sub>4</sub> process (Frequency: 60 kHz, PS: 0.02 mol/L, CIP-F: 100 mg/L and pH 5)

Increasing the  $Fe_3O_4$ -NPs concentrations from 0.01 to 0.08 g/L had a decreasing effect on the removal efficiency; the increased production of kernel resulted from the increase in  $Fe_3O_4$ -NPs concentration, thereby reducing the number of bubbles and radicals produced, i.e., nanoparticles provide extra surfaces for cavitation (Cheng et al. 2013).

## **Effects of PS concentration**

Figure 4 shows the effect of varying the concentration of persulfate on CIP-F removal efficiency. This was achieved by maintaining the pH at 5. The result shows that the removal efficiency increased when the PS concentration increased from 0.01 to 0.15 mol/L but subsequently reduces with further increase in PS concentration. The reaction mechanism is as shown by Eqs. 2 to 5. PS is converted to sulfate radical (one of the strongest oxidative agents), and it decomposes the organic compounds to water,  $CO_2$  and mineral acids. Also, the produced persulfate radical reacts with water and hydroxyl ions indirectly to produce hydroxyl radical which



Fig. 2 Effect of pH on the removal efficiency of CIP-F via the US/PS/  $Fe_3O_4$  process (Frequency: 60 kHz, PS: 0.02 mol/L, CIP-F: 100 mg/L and  $Fe_3O_4$ –NPs: 0.25 g/L)

Fig. 4 Effect of persulfate concentration on the removal efficiency of CIP-F via the US/PS/Fe<sub>3</sub>O<sub>4</sub> process (Frequency: 60 kHz, pH 5 and Fe<sub>3</sub>O<sub>4</sub>–NPs: 0.01 g/L, CIP-F: 100 mg/L)



decomposes organic materials. (Ta et al. 2006; Shiying et al. 2009).

$$S_2 O_8^{2-} \to 2S^{4-}$$
 (2)

$$SO^{4-} + M \rightarrow Product$$
 (3)

$$SO^{4-} + H_2O \rightarrow HO^- \tag{4}$$

$$HO^- + M \rightarrow Product$$
 (5)

Given the preceding, increasing the concentration of the PS used makes the radicals act as a scavenger and converted persulfate radical to sulfate (Eq. 6) (Li et al. 2011).

$$S_2 O_8^{2-} + SO^{4-} \rightarrow S_2 O_8^{-} + SO_4^{2-}$$
 (6)

#### Effect of time and CIP-F concentration

This was used to monitor the time effect of varying the concentration of CIP-F concentration on the removal efficiency of CIP-F. The CIP-F concentrations used were 50, 200, and 250 mg/L for a varied duration between 10 and 120 min. The pH and PS concentrations used were set at 5 and 0.15 mol/L, respectively. The results obtained are presented in Fig. 5. Based on the concentration of CIP-F used, the removal efficiency decreased with an increase in concentration, as observed in Fig. 5. The removal efficiency initially increased as the concentration of CIP-F used increased from 50 to 200 mg/L but subsequently reduces as the concentration of CIP-F used was increased to 250 mg/L. This subsequent decrease in the removal efficiency associated with an increase in CIP-F concentration may be attributed to increased production of by-products during the reaction (AsI et al. 2015). It is,



Fig.5 Effect of time on the removal efficiency of CIP-F via the US/ PS/Fe<sub>3</sub>O<sub>4</sub> process (Frequency: 60 kHz, pH: 5, PS: 0.15 mol/L and Fe<sub>3</sub>O<sub>4</sub>–NPs: 0.01 g/L)



therefore, safe to infer that the removal efficiency decreased with an increase in the concentration of US/PS/Fe<sub>3</sub>O<sub>4</sub>.

Considering the time effect per concentration, an initial increase in removal efficiency was observed for 45 min, after which a gradual decline began to emerge. It was observed from the research that the optimum removal efficiency was obtained at 45 min. Although a similar study by Khan et al. (2019a) indicated that the optimal resident time was 30 min, their study investigated the catalytic ozonation process for the removal of ciprofloxacin with modified active carbon with MgO in aqueous solution using a fluidized bed reactor (Guo et al. 2014).

#### **Kinetics study**

The kinetic study was carried out to investigate the rate of disintegration of CIP-F using the US/PS/Fe<sub>3</sub>O<sub>4</sub> process and to classify the reaction into the appropriate order. Organic chemical compound reactions are either classified into the pseudo-first-order or pseudo-second-order categories and, as such, the research tests to see which category the chemical reaction falls into. The equations for the pseudo-first-order and pseudo-second-order reactions are given below as Eqs. 7 and 8, respectively (Li et al. 2011; Ahmadi et al. 2019; Hemmati et al. 2017):

$$\ln\left(\frac{c}{c_0}\right) = -k_1 t \tag{7}$$

$$\frac{1}{C} - \frac{1}{C_0} = -k_2 t \tag{8}$$

where  $C_0$  = Initial concentration in milligrams per liter and C = Final concentration in milligrams per liter at time t.

The test variables were set to the optimum condition (contact time = 10 min, pH = 7, PS concentration = 0.02 mol/L and nanoparticles concentration = 0.25 g/L) for perfect modeling of the rate of reaction. The result obtained for the rate of disintegration and the calculated results from Eqs. 7 and 8 are presented in Fig. 6 and Table 1. From the result, it can be observed that the rate constant obtained is similar to the value obtained from the slope of the plot of  $\ln\left(\frac{c}{c_0}\right)$  against the time. It is, therefore, safe to conclude that the reaction follows the pseudo-first-order scheme. The associated loss of CIP-F in the reaction was observed to be a function of time and correctly models the pseudo-second-order scheme (Asl et al. 2015).

# Conclusion

The results obtained from this research have shown that the  $US/PS/Fe_3O_4$  process can effectively and efficiently aid the surface adsorption of CIP-F from aqueous solutions with





Fig. 6 Pseudo first-order plot for the CIP-F degradation process

Table 1 Kinetics for the CIP-F degradation via the US/PS/Fe $_{3}O_{4}$  process

<i>C</i> <sub>0</sub> (mg/L)	Pseudo-first-order		Pseudo-second-order	
	$\overline{K_1}$	$R^2$	$\overline{K_2}$	$R^2$
50	0.007	0.5061	0.006	0.5517
200	0.0052	0.8723	0.0057	0.305
250	0.0065	0.5869	0.0024	0.2126

a 98.43% removal efficiency. This was achieved by carrying out the degradation at the optimum conditions set to pH=5, CIP-F concentration=200 mg/L, PS concentration=0.15 mol/L and Fe<sub>3</sub>O<sub>4</sub> concentration=0.01 g/L at a resident time of 45 min. The reaction was also observed to follow the pseudo-first-order reaction model rather than the pseudo-second-order reaction. It is therefore recommended based on experimental findings that US/PS/Fe<sub>3</sub>O<sub>4</sub> be used for the removal of CIP-F from effluents.

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## **Compliance with ethical standards**

Conflict of interest The authors declare no conflict of interest.

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