

Non‑conventional Stabilization for Fruit and Vegetable Juices: Overview, Technological Constraints, and Energy Cost Comparison

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Abstract

This study will provide an overview and a description of the most promising alternatives to *conventional thermal treatments* for juice stabilization, as well as a review of the literature data on fruit and vegetable juice processing in terms of three key parameters in juice production, which are microbial reduction, enzyme inactivation, and nutrient-compound retention. The alternatives taken into consideration in this work can be divided, according to the action mechanism upon which these are based, in *non-conventional thermal* treatments, among which microwave heating (MWH) and ohmic heating (OH), and *nonthermal treatments*, among which electrical treatments, i.e., pulsed electric felds (PEF), high-pressure processing (HPP), radiation treatments such as ultraviolet light (UVL) and high-intensity pulsed light (PL), and sonication (HIUS) treatment, and inert-gas treatments, i.e., the pressure change technology (PCT) and supercritical carbon dioxide (SC-CO₂) treatments. For each technology, a list of the main critical process parameters (CPP), advantages (PROS), and disadvantages (CONS) will be provided. In addition, for the non-thermal technologies, a summary of the most relevant published result of their application on fruit and vegetable juices will be presented. On top of that, a comparison of typical specifc working energy costs for the main efective and considered technologies will be reported in terms of KJ per kilograms of processed product.

Keywords Non-conventional technologies · Food processing · Energy cost · Technological constraints · Vegetable and fruit juices

Introduction

Fruit and vegetable juices, beverages, juice blends, smoothies, and purees are an increasingly popular way of consuming fruit and fresh-like vegetables and may contribute to a healthy diet and healthy life. Over the last few years, the consumption of fruit and vegetable juices has been rapidly increasing, making the juice and beverage industry among the largest agro-based industries worldwide (Walkling-Ribeiro et al., [2010](#page-18-0)).

Vegetable and fruit juices are traditionally preserved by thermal processing. Unfortunately, they might have some

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detrimental effects on the nutritional quality, impacting negatively on the fresh-like characteristics. Therefore, recent consumer demand for safe and minimally processed foods with high-quality attributes have encouraged food industry and scientifc researchers to design alternative technologies to produce food with a minimum of changes induced by the technologies themselves (Jiménez-Sánchez et al., [2017a](#page-16-0)).

For this reason, recently there has been a growing interest in the design of non-conventional and novel non-thermal processing systems that minimally modify sensory, nutritional, and functional properties of fruit and vegetable juices and beverages. The non-conventional and non-thermal technologies that will be presented in this paper could meet industry and consumer expectations. Anyway, although nonconventional treatment seems less detrimental than the conventional thermal ones, the efects are strongly dependent on the food matrix (Alves Filho et al., [2016](#page-15-0)). Therefore, the main motivation for food processors is to select the most appropriate thermal or non-thermal technology along with validated processing conditions to retain nutritive constituents, color, and flavor attributes (Koutchma et al., [2016](#page-17-0)).

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In the last few years, many studies and research about comparison among diferent technologies for fruit and vegetable juice treatment have been carried out (Bevilacqua et al., [2018;](#page-15-1) Jiménez-Sánchez et al., [2017a,](#page-16-0) [b](#page-16-1); Qazalbash et al., [2018](#page-17-1); Timmermans et al., [2011;](#page-18-1) Van Impe et al., [2018](#page-18-2); Vervoort et al., [2011](#page-18-3)), but to the best of our knowledge no report gives a comprehensive overview of the advantages, disadvantages, and technological constraints for their application, or provide a comparison of their specifc energy consumption with the conventional thermal treatment.

Based on the above premises, as an input to processor choice, this paper will provide an overview of the most promising non-conventional technologies, specifying their mechanisms of action and critical process parameters, reporting the results of their application, and lastly, comparing their specifc working energy costs.

Non‑conventional Technologies

Thermal Technologies

Microwave heating (MWH) and *ohmic heating* (OH) are processes based on temperature increasing into the product to which they are applied, but not related to conventional heat transmission methods (conduction and convection). Therefore since their effect on microbial reduction, enzymatic deactivation, and nutrient deterioration is still related to heat, they can be classifed as non-conventional thermal technologies.

Microwave Heating

Microwave heating is a sub-category of electrical treatments, where electromagnetic waves are emitted by a smalldimension magnetron and guided through space to the target. Microwaves are electromagnetic waves whose frequency varies from 300 MHz to 300 GHz. The industrial microwave systems typically operate at frequencies from 915 MHz to 2.45 GHz (Datta & Davidson, [2000](#page-16-2)).

MWH is caused by the ability of the materials to absorb microwave energy and convert it into heat. Microwave heating of food materials mainly occurs due to dipolar and ionic mechanisms. The presence of moisture or water causes dielectric heating due to the dipolar nature of water. There are many factors afecting microwave heating and its heat distribution, but the most important of them are the dielectric properties and penetration depth (Chandrasekaran et al., [2013](#page-16-3)).

MWH is a promising way for juice stabilization because of some advantages, like the reduced processing time, a good process control, and space savings (Salazar-González et al., [2014](#page-17-2)). Destruction of microbes or enzymes by microwave or radio frequency waves at sublethal temperatures was explained by one or more of the following theories: selective heating, electroporation, cell membrane rupture, and magnetic feld coupling.

The selective heating theory suggests that the microorganisms are selectively heated due to microwaves and reach a temperature higher than that of the surrounding fuid. This causes the microorganisms to be destroyed more quickly. According to the electroporation theory, the electrical potential across the cell membrane causes pores, which results in the leakage of cellular materials. In the cell membrane rupture theory, the cell membrane is ruptured due to the voltage applied across the cell membrane. According to the magnetic feld coupling theory, the internal components of the cell are disrupted due to the coupling of electromagnetic energy with critical molecules such as protein or DNA (Kozempel et al., [1998](#page-17-3)). Although various theories suggest the non-thermal efect of microwaves, it was further observed that in the absence of other stresses such as pH or heat, microwave energy did not inactivate microorganisms (Chandrasekaran et al., [2013\)](#page-16-3).

MWH treatments are nowadays applied by some food industries and were found to save some costs and time compared to indirect heating methods. Also, food quality is maximized and better retained using electromagnetic energy rather than conventional heating. Microwave heating processes used on fruit and vegetable juices can achieve high processing temperatures in shorter times; therefore, more nutritional and sensory properties are conserved.

Ohmic Heating

Ohmic heating (OH) applied to food products involves the passage of high-frequency alternating electric current through them, generating internal heat as a result of electrical resistance — Joule efect — of the food matrix (Valero et al., [2010\)](#page-18-4).

As outlined in Fig. [1](#page-2-0), in the typical industrial design for liquid food OH treatment involves the application of a high electrical potential (typically around 5000 V) between the two fanges at the extremities of each module, using the food product fowing through as a resistor. The high-frequency electrical current (typically between 20 and 30 kHz) therefore passes through the food, increasing its temperature fast and uniformly thanks to the Joule efect, thus bypassing conventional heat transfer mechanisms such as conduction and convection.

The heating rate is directly proportional to the square of the electric feld strength, and the electrical conductivity of the product (Jiménez-Sánchez et al., [2017a](#page-16-0)).

For this reason, the efficiency of the application of OH for the stabilization of liquid foods strongly depends on the conductivity of the product to be treated. Typical conductivity

Fig. 1 OH application mechanism scheme

value of fruit and vegetable juices is between 0.2 and 1 S/m at 20 °C with lower value for raw water and honey sugar and higher values for meat products and seafood (Zhang, [2007](#page-18-5)).

The ohmic heating technology has many benefts: for example, compared to the conventional heating, it reduces the problems of surface fouling, or over heating of the product, it has low maintenance costs and high energy conversion efficiencies (Pereira & Vincente, 2010), and retain higher nutritional value of food product (Debbarma et al., [2021](#page-16-4)), but the diferent electrode materials during OH at diferent electrical frequencies have an infuence on protein structural aspects (Ferreira et al., [2021](#page-16-5)).

OH is very efective in fruit and vegetable juices that contain water and ionic salts in abundance (Miller & Silva, [2012\)](#page-17-5). In these kinds of products OH provides uniform and rapid heating, resulting very efficacious for microbial reduction and enzyme inactivation, with a beneficial effect on the nutritional and organoleptic properties of processed products (Mercali et al., [2015](#page-17-6)). Additionally, compared to conventional thermal technologies, OH offers better energy efficiency, lower capital cost, and shorter treatment time. In addition, it results to be an environmentally friendly process, since around 97% of electrical energy provided is converted into heat (Lee et al., [2015](#page-17-7)). Figure [2](#page-2-1) provides a typical example of liquid food product heating curves on a temperature over time chart, showing the faster temperature rising with OH in comparison with conventional indirect heating technologies.

Non‑thermal Technologies

The technologies that will be described in this section are defined as non-thermal because their effect of microbial reduction is not due to the increase of temperature, in contrast to the technologies seen so far, but is a result of diferent action mechanisms, specifc for each technology.

Fig. 2 Example of temperature rising curves for product under conventional thermal and OH

Pulsed Electric Fields

Pulsed electric feld (PEF) is one of the most extensively studied non-thermal technologies that had been applied to fruit and vegetable juices for microorganism inactivation as well as for maintaining organoleptic and nutritional qualities similar to those of fresh juice.

This treatment involves the application of high-intensity electric feld (typically between 10 and 40 kV/cm), in form of very short pulses (usually $5-30 \mu s$), to a product placed between two electrodes. The application of PEF pulses induces microscopic pores — called electropores — in the microbiological membranes, resulting in an increase in their permeability. The plasma membranes of cells become hence permeable to small molecules, ions, and water, which will be able to pass from one side of the membrane to the other. This phenomenon is called electroporation and induces swelling and the rupture of the cell membrane leading to cell death (Jiménez-Sánchez et al., [2017a\)](#page-16-0).

Although a temperature might rise due to the electric current fowing through the liquid food (as it happens during ohmic heating), PEF is intended to be a non-thermal technique (Jiménez-Sánchez et al., [2017a\)](#page-16-0).

In addition, even if the application of PEF at relatively lower temperatures to inactivate pathogens and food spoilage bacteria, as well as enzymes, has already been described in the literature, a better understanding and accurate prediction of inactivation levels are necessary to achieve enzymatically stable products without overprocessing (Bevilacqua et al., [2018](#page-15-1)).

High‑Pressure Processing

High-pressure processing (HPP) refers to the application of hydrostatic pressure in the range from 100 to over 900 MPa on pre-packaged food. During this process, the pressurization is applied isostatically, i.e., equally in all for the duration of the treatment and then released (Jiménez-Sánchez et al., [2017a](#page-16-0)).

High pressure causes unfolding of proteins or enzymes, as well as considerable damage to the genetic material of microorganisms, due to phase transition fuidity change of the cell membrane, an intracellular pH change, and breakdown of ribosomes, ultimately resulting in injury and death of vegetative microorganisms (Qazalbash et al., [2018](#page-17-1)). On the other hand, this technology exerts limited efects on small molecules such as volatile compounds, pigments, vitamins, and antioxidant compounds (Stefanini et al., [2021](#page-18-6)), owing to its limited impacts on the covalent bonds and its low processing temperature (Chen et al., [2015\)](#page-16-6). This led to the commercial adoption of this treatment for increasing the shelf life of juices and for manufacturing of high-quality products.

Figure [3](#page-3-0) shows a schematic example of HPP technology application: HPP is typically applied as a batch process in which pre-packed products are loaded into the pressure vessel. As soon as they are loaded and closed, the vessel is flled with pressure-transmitting fuid, by using a pressuregenerating mean. A pressure medium, water in most current HPP equipment (Rastogi, [2013](#page-17-8)), is pumped isostatically from its tank into the pressure vessel and once the desired pressure is reached, the pump is stopped by closing the inlet valves (Elamin et al., [2015](#page-16-7)). The desired pressure can be maintained with no more energy needed to hold it (Huang et al., [2014\)](#page-16-8). After holding the product for the required time, the pressure is released from the vessel by freeing out the pressure-transmitting fuid to return to its initial tank reservoir (Farkas & Hoover, [2000](#page-16-9)).

It is also important to notice that although HHP is intended to be a cold (totally non-thermal) technology, an inherent mild increase in pressurized water temperature does occur.

Fig. 3 Example scheme of HPP process application

Fig. 4 Example scheme of continuous PCT process fow diagram

The temperature increasing during compression is reported to be approximately 3 °C every 100 MPa (Timmermans et al., [2011](#page-18-1)).

Pressure Change Technology

process fow diagram

Pressure change technology (PCT) is an emerging process which has been recently proposed as an innovative approach for the non-thermal inactivation of microorganisms and sta-bilization of liquid foods (Aschoff et al., [2016](#page-15-2)).

A schematic representation of PCT process application is provided in Fig. [4](#page-4-0). When pressure change technology (PCT) is applied, the liquid product is pressurized with a high-pressure pump at a maximum pressure of 50 MPa and subsequently mixed with an inert gas (such as nitrogen, helium, or argon) at a slightly higher pressure (approximately 1 MPa) using an inline static mixer. During the subsequent holding time, the inert gas dissolves and difuses in the liquid medium in high amounts, penetrating into intracellular microbial liquids until reaching saturation. After the retention time, the pressurized product saturated with gas is quickly released to atmospheric pressure by a relief valve.

This fash decompression causes a sudden outgassing of the inert gas, which damages all the microbial cell structures into which it has penetrated but minimizes the impact on enzyme activity and nutritional compounds. Thus, in contrast to static technologies such as high-pressure processing, the lethal effect of PCT is achieved at the dynamic decompression step instead of during the retention time (Aschof et al., [2016\)](#page-15-2). Therefore, the stabilization mechanism of PCT can be called *dynamic decompression*.

Ultraviolet Light Radiation

Among the non-thermal technologies developed in the last few decades, *ultraviolet light* (UVL) processing is one of the most promising because it is easy to use, lethal to most microorganisms, and it is a cold process that can be efective at low cost in comparison with other preservation methods (Gayán et al., [2012](#page-16-10)). A schematic example of industrial UVL technology application is provided in Fig. [5.](#page-4-1)

The wavelength range for UVL for food processing varies from 100 to 400 nm and is categorized as UV-A (320–400 nm), UV-B (280–320), and UV-C (200–280 nm). UV-C radiation, especially the wavelength of 254 nm, is considered the *germicidal region* in which the main bactericidal efect occurs (Gayán et al., [2012\)](#page-16-10).

The inactivation of microorganisms starts with the microorganism's DNA absorbing UV radiation, and then cross-linked pyrimidine nucleoside bases are formed causing a mutation in the DNA, mainly thymine dimmers. The structural damage caused by the formation of these dimmers inhibits the formation of new DNA, resulting in the inactivation of the afected microorganism. This reaction has been called the *photochemical efect* (Gómez-López et al., [2012](#page-16-11)).

Pulsed Light Radiation

Recently, *pulsed light* (PL) has been intensely investigated as an alternative to thermal treatments for killing pathogenic and spoilage microorganisms (Maftei et al., [2014\)](#page-17-9). It is based on application of very short intense fashes of light. The equipment used consists of a high-energy electrical energy capacitor that discharges pulses of electrical energy to *fash lamps* which produce fashes of broad-spectrum light. The spectrum of emitted light is in the range of 200–1100 nm. The emitted fashes are very intense but have an extremely short duration (0.2–0.4 ms).

In addition to the *photochemical efect* previously mentioned for the UVL technology, exposure to PL also causes a membrane disruption as a result of a momentous overheating. This phenomenon is attributed to a diference in UV light absorption between the microorganism and its surrounding environment, called *photothermal efect*. Besides, structural damage in microbial cells like cytoplasmic membrane shrinkage was also reported, called *photophysical efect* (Ferrario et al., [2014\)](#page-16-12).

Also in this case, the outline for PL treatment application has been provided in Fig. [6](#page-5-0).

Supercritical Carbon Dioxide

Among the non-thermal process for liquid foods such as fresh juices, there is also a method called dense phase carbon dioxide (DPCD) or supercritical carbon dioxide $(SC\text{-}CO_2)$ that is able to inactivate microorganisms and enzymes using $CO₂$ in the supercritical state (Deng et al., [2020\)](#page-16-13). Foods are subject to sub-critical or supercritical (i.e., pressurized) $CO₂$ at low temperature (20–50 °C) under moderate pressure (below 50 MPa) for 5–30 min (Ferrentino & Spilimbergo, 2011). CO₂ has many advantages: it is inert to oxidation

reactions, non-fammable, non-corrosive, non-toxic, safe solvent, and has low critical temperature, which allows the development of non-thermal process, therefore minimizing the infuence on sensorial and nutritional characteristics of foods (Silva et al., [2020\)](#page-18-7).

The equipment for $SC\text{-}CO₂$ processing of liquid foods is specifc to each application and the process may be operated in batch, semicontinuous, or pseudo-continuous and continuous operating mode (Perrut, [2012\)](#page-17-10).

This technology has been investigated over the past 50 years: its efects on various microorganisms including pathogens, spoilage bacteria, yeasts and molds, and diferent enzymes have been demonstrated (Fleury et al., [2018](#page-16-15)). Several studies have been performed on the efficiency of $SCCO₂$ processing in the preservation of juices, such as mango (Tang et al., [2021\)](#page-18-8), tomato (Zhao et al., [2019\)](#page-18-9), orange (Niu et al., [2019](#page-17-11)), apple (Gasperi et al., [2009](#page-16-16)), guava (Plaza et al., [2015\)](#page-17-12), and melon (Pei et al., [2018\)](#page-17-13). Few studies evaluated the shelf life of natural juices processed by $SC\text{-}CO₂$ technology, regarding microbial quality and other parameters (Torabian et al., [2018;](#page-18-10) Zou et al., [2016\)](#page-18-11). Moreover, the literature regarding the effects of $SCCO₂$ technology on the sensory properties as well as the acceptance of the nonthermally processed juices by the consumers is still scarce (Silva et al., [2020](#page-18-7)). This type of process, although known to the applied research sector, still fnds little attention in the food industry today.

High‑Intensity Ultrasound

High-intensity ultrasound (HIUS) refers to ultrasound operating at frequency higher than 20 kHz: this technology gained success in the feld of food disinfection (Afari et al., [2016](#page-15-3)). To get the ultrasound, an electric current alternating is applied to a piezoelectric material fxed to the wall of a

Fig. 6 Example scheme of PL process fow diagram

container. A sonicator consists of an electricity generator, a converter to transform electrical energy into mechanical energy, and probes that amplify the produced vibration.

The mechanism of operation of the sonication is based on the phenomenon of cavitation, with the formation of small bubbles in the liquid medium that quickly alternates compression and expansion and cause violent collapse. Shock waves with high energy densities can radiate from collapsing bubbles that are strong enough to shear and break cell walls and membrane structures, as well as depolymerize large molecules (Deng et al., [2020\)](#page-16-13). Therefore, this process is able to guarantee a bactericide effect (Gómez et al., [2011](#page-16-17)). Moreover, hydroxyl radicals can be formed due to the rise of temperature at a localized position inside a collapsing bubble: they can react with the DNA chain and break the double-strand microbial DNA (Bilek & Turantaş, [2013](#page-16-18)).

However, even if HIUS is generally considered safe, non-toxic, and environmentally friendly (Deng et al., [2020](#page-16-13)), information on its commercial application is scarce and more efforts are needed to develop large-scale inexpensive equipment for their application in the food industry.

Fruit and Vegetable Juice Stabilization Effectiveness

Although the efectiveness of heat treatments is well known and does not change signifcantly depending on the technology used to apply the heat (conventional or non-conventional), the results of non-thermal technologies are often uncertain and may difer depending on the variation in process parameters.

In Table [1,](#page-7-0) what we consider to be the most representative data found in the scientifc literature regarding the efectiveness of the main non-thermal technologies has been summarized, in terms of the three key aspects of microbial reduction, enzymatic inactivation, and nutrient-compound retention for each standpoint. The results obtained and the process conditions applied have been reported.

Technological Constraints

Following the description and the effects of the various stabilization technologies reported in the previous sections of this work, it is possible to summarize a list of the principal critical process parameters (CPP), advantages (PROS), and disadvantages (CONS) associated with each of these processes.

In Table [2,](#page-10-0) an overview of the above aspects is provided for each technology, reporting also the data source.

Working Energy Cost Comparison

Starting from the technical features, the process fow diagrams, and the operating mechanism of the technologies taken into account in this paper, the energy consumption per mass unit of treated product has been estimated in order to perform a comparison of the specifc energy cost required by each of them. For this comparison, also an estimation for the *conventional indirect thermal treatment* (CITT) has been considered.

The estimation of the specifc working energy consumption for each technology has been carried out starting from the method reported by Rodriguez-Gonzalez et al. ([2015](#page-17-14)), with the following further assumptions:

- The components of working costs considered are those for product stabilization treatment (i.e., energy for heating and pumping), other service fuid pumping, heat dissipation (i.e., for equipment cooling), and for product cooling.
- The evaluation of energy consumption per unit mass of juice processed has been carried on a system boundary going from inlet untreated product to outlet stabilized product, considering both with the same temperature value equal to 20 °C.
- In the cases of thermal treatments, the use of a process temperature not exceeding 68 °C were assumed.

This latter condition was assumed in order to make the comparison between diferent technologies as fair as possible. In fact, thermal processes reaching temperatures higher than the herein imposed are able to reach levels of product stability, i.e., shelf life, often inaccessible with non-thermal technologies, which would nevertheless penalize them from an energy point of view.

Approximately 5-log reduction of *Escherichia coli* in apple-derived products was taken into consideration as target for all the stabilization technologies under consideration. The treatment conditions to achieve such *E. coli* inactivation levels and, therefore, utilized for specifc energy cost estimation for the diferent technologies are the following:

CITT/OH/MWH:A treatment at 68 °C for 15 s has been considered, since more than 5-log reduction of nonadapted and acid-adapted *E. coli O157:H7* was obtained at 68.1 °C for 14 s in apple cider at pH 4.1 and 11 °Brix (Mak et al., [2001\)](#page-17-15).

HPP:A treatment at 600 MPa for 2 min has been considered, since for high-pressure treatment, literature reports 1–5 min at 350–600 MPa to inactivate *E. coli* in apple juice (Daher et al., [2017\)](#page-16-19). Also, 3 min for pressure fuid to come up to the desired pressure was estimated.

Table 1 Overview of reported non-thermal technologies effects in terms of microbial reduction, enzymes inactivation, and nutrients retention

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Table 2 (continued)

Table 2 (continued)

PEF:A treatment with monopolar pulses of 2-μs duration at electric feld strength of 23 kV/cm has been considered. In addition, it was estimated a preheating of the product to 44 °C and a post PEF treatment temperature of 56 °C at a repetition rate of 90 Hz and a fow rate of 130 L/h. Also energy for product preheating and cooling have been taken into account.

UVL/PL:For both technologies, a treatment module made of 24 lamps with 65-W output power each has been considered. In this study, pilot modules with a flow rate of approximately 20 L/min were chosen. Such parameters are able to achieve the desired bacterial inactivation in clear apple cider according to industries.

PCT:Since no data on *E. coli* inactivation in apple juice have been found in scientifc literature, the energy cost estimation in this case has been done starting from the process parameters described by Aschoff et al. (2016) (2016) (2016) , i.e., product pressure of 50 MPa, $T_{\text{max}} < 40 \degree \text{C}$, and 1.3min holding time.

As far as the SC - $CO₂$ and HIUS treatments are concerned, the literature is scarce and the data available for microbial inactivation are very low in comparison to the other technologies: for example, only 1.3 log reduction of *E. coli* was reached in orange juice treated with HIUS (42 kHz, 60 min) (Kernou et al., [2021](#page-16-24)). Therefore, since the established target of 5-log reduction of *E. coli* in apple-derived products is not achieved, these two treatments cannot be considered in this evaluation.

For thermal treatments, i.e., CITT, OH, and MW, the most commonly used equation is the one related to heat content which considers a physical property (specifc heat capacity or C_p) to estimate the energy required to change the temperature of a material. This equation is utilized in food materials as well as equipment materials and is an indicator of heat transfer by conduction (Singh & Heldman, [2001](#page-18-23); Toledo, [2007\)](#page-18-24):

$E_h = (C_n \times m \times \Delta T) \times \eta$

where E_h is the specific energy for heating, C_p is the specific heat capacity, *m* is the mass to be heated, ΔT is the temperature differential, and η is the system efficiency.

This equation can be used for a valid prediction of heating costs also for non-conventional thermal technologies, i.e., OH and MWH. In this study, the efficiency values of 90% , 97%, and 85%, respectively, for CITT, OH, and MW have been considered. The same equation has been referred to also for cooling energy cost estimation.

In addition, for the non-conventional thermal technologies, in which the product is heated without direct contact with hot surfaces, the electric energy not converted in food heating need to be dissipated. For this reason, an additional energy cost for electric equipment's cooling system (E_d) has been considered:

$$
E_{\rm d} = (C_{\rm p} \times m \times \Delta T) \times (1 - \eta)
$$

The basic equation used for estimating the energy required to pump fuids through pipes is the following:

$$
E_{\rm p} = (P \times V) \times \eta
$$

where E_p is the specific energy for pumping, *V* is the volumetric flow rate, and η is the pump efficiency.

The total amount of working energy consumption for thermal treatments has therefore been calculated by summing the three contributes above described:

$$
E_{\text{tot}} = E_{\text{h}} + E_{\text{d}} + E_{\text{p}}
$$

In the case of 65% of heat recovery, the energy savings are considerable in terms of both product warming and cooling, as well as heat dissipation.

The internal energy requirement for HPP can be estimated basing on process control metrics using the pressure head component of pump power calculation equations (Rodriguez-Gonzalez et al., [2015](#page-17-14)):

$$
E_{\rm s} = (P_{\rm f} - P_{\rm i})/\rho
$$

where E_s is the specific energy, *P* is the pressure, and ρ is the density. The same equation has been utilized also for PCT running cost estimations, being the fuids (product and inert gas) pumping the only energy requiring contribute.

A measure of the specifc energy input for PEF process can be estimated using the following equation (in a thermodynamic system is enthalpy, and its change as a function of temperature is also applicable to PEF (Heinz et al., [2003](#page-16-29)):

$$
E_{\rm s} = f \frac{1}{\dot{\rm m}} \int_{0}^{\infty} k(T) E(t)^2 dt
$$

where E_s is the specific energy for heating and $E, k(T), f$, and *m* denotes the electric field strength, the media conductivity, the repetition rate, and the mass fow rate, respectively (Toepf et al., [2007\)](#page-18-21).

For both UVL and PL processes, lastly, the total applied UV energy for treatment of a liter of liquid product in a continuous-fow unit can be calculated using the following equation, as UV output power of the *n* number of the UV sources divided by volumetric fow rate (*V̇*) of the treated fuid (Keyser et al., [2008\)](#page-17-26) in (J/L).

$$
E_{\rm s} = (P_{UV} \times L_N)/V
$$

where E_s is the specific energy for heating, P_{UV} is the output power, L_N is the number of lamps, and *V* is the is the volumetric fow rate. The results have than been divided by the estimated product density ρ in order to evaluate the specific energy per kg.

Any eventual data missing or to be integrated have been obtained from the scientifc papers by Gómez-López et al. ([2012\)](#page-16-11), Cacace et al. [\(2020\)](#page-16-30), and Vollmer et al. ([2020\)](#page-18-26). In addition, information from the literature has been crosschecked with experts from leading companies in the feld of fruit and vegetable juice processing technology, such as CFT (Catelli Food Technology) and Elea Vertriebs- und Vermarktungsgesellschaft mbH.

All the results of the estimates have been expressed in kJ over kg of treated product. Both cases of no heat recovery and 65% of heat recovery have been reported in Tables [3](#page-13-0) and [4](#page-14-0), as well as in the subsequent Figs. [7](#page-14-1) and [8.](#page-14-2) The specifc working energy costs resulted very high for the microwave heating, followed by the conventional indirect thermal treatment, the ohmic heating, the high-pressure processing, and pulsed electric felds. On the other hand, it resulted very low for ultraviolet light radiation, pulsed light radiation, and pressure change technology. However, considering the 65% of heat recovery, the estimated results change: HPP is characterized by the highest specifc working energy costs, followed by MHW, OH, CITT, and PEF, while UVL, PL, and PCT continue to result as the lowest ones.

In the second graph, the specifc energy consumption estimated for the thermal technologies and those technologies that involve a product pre-heating such as PEF are much

Table 3 Specifc working energy cost estimations for thermal and non-thermal technologies with no heat recovery

Technology	Treatment (heating / pressurizing) $+$ pumping) (kJ/kg)	Product cooling (kJ/kg)	Heat dissipation (kJ/kg)	Total (kJ/kg)
Conventional indirect thermal treatment (CITT)	211.39	186.15	Ω	397.54
Ohmic heating (OH)	193.41	171.96	5.80	371.16
Microwave heating (MHW)	217.68	196.23	32.65	446.57
High-pressure processing (HPP)	339.94	$\mathbf{0}$	0	339.94
Pulsed electric fields (PEF)	161.81	140.0	0	301.81
Ultraviolet light radiation (UVL)	26.24	Ω	0	26.24
Pulsed light radiation (PL)	25.15	Ω		25.15
Pressure change technology (PCT)	26.28	Ω	0	26.28

ENERGY CONSUMPTION WITHOUT HEAT RECOVERY

ENERGY CONSUMPTION WITH HEAT RECOVERY

lower than in the second, since the energy recovery system allows energy saving of around 36% on the total process. This comparison was made by fully including the energy for product cooling, but cheaper alternatives (in terms of energy) could also be considered such as well cooling-towers to be recovered somewhere else in the process.

Furthermore, for OH and MWH technologies, the heat recovery system allows a lower overheating of the electrodes and magnetrons since the thermal increase that must be provided to the product would be lower. This therefore reduces heat dissipation and thus the energy costs for cooling the equipment.

Even the PEF technology, although not thermal, involves, as previously mentioned, a temperature increases of the product and therefore gains benefts in terms of energy consumptions from the heat recovery system.

Completely non-thermal processes such as HPP, UVL, and PCT, as can be seen, do not involve any energy costs for product and equipment cooling, so their specifc energy consumption is still constant in both graphs. In contrast, for the PL technology, a minimal energy cost for the lamps cooling should always be taken into account. The high-energy requirements of HPP technology are due to the achievement of the high pressures for product treatment; therefore, no benefts in terms of energy consumptions could come from a heat recovery system.

Conclusions

This work provides an overview of some of the existing alternatives to conventional thermal treatments, currently utilized to achieve the safety and improved quality of fruit and vegetable juices. Thermal treatments are still the most commonly used methods and the only ones capable of efectively inactivating spores and enzymes for the production of low-acid shelf stable products. Non-conventional thermal treatments such as OH and MWH are gaining great success among the producers, since they allow to reach very quickly the high temperatures for stabilization processes, leading in many cases to a better retention of the nutritional and sensory properties of products.

Non-thermal approaches seem to offer the most effective alternative in terms of nutrients and fresh-like characteristics preservation as well as working energy costs saving, but they also have many limits. In fact, targeting pathogen microorganism only, they are often able to obtain exclusively the sanitary treatment, with variable effects on spoilage microorganisms and enzymes, leading to fnal products requiring refrigerated storage. In addition, some non-thermal approaches, such as PEF, HPP, and UVL, are currently used for industrial applications, while others, like PCT, PL, HIUS, and $SC\text{-}CO₂$, are still at pilot-scale level and their scale-up represents a challenge.

Therefore, it is fundamental for each producer aiming to choose the best technology for achieving or improving the desired fnal product or production process, to take into consideration, compare, and possibly to further investigate all the various critical parameters and technical aspects presented in this overview.

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Declarations

Conflict of Interest The authors declare no competing interests.

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