**Doi**: 10.1007/s11589-010-0735-5

# Contemporary tectonic stress field in China\*

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**Abstract** The contemporary tectonic stress field in China is obtained on the basis of Chinese stress field database and Harvard CMT catalogue. Result of the inverted tectonic stresses shows that the maximum principal stress axis strikes nearly north-south direction in the west part of Tibet plateau, ENE direction in North China. In Central China, its strikes show a radiated pattern, i.e., NNE in north part and NNW in south part. The detailed stress field parameters of nearly whole China are given and can be used in geodynamic stress field simulation and earthquake prediction.

Key words: tectonic stress field; focal mechanism; stress measurement

CLC number: P315.72<sup>+</sup>7 **Document code**: A

### 1 Introduction

Study of tectonic stress field, a major branch of Earth science, plays an important role in the studies of geodynamics. The World Stress Map Plan started in 1980s was led by M. L. Zoback. Lots of scientists participated in this plan. The plan collected global tectonic stress measurements and research results to establish global stress database. The world stress map was edited based on the global stress database. The world stress map reflects feature of global lithosphere stress field both in total and in subareas, and thus can explain the tectonic stress interaction in lithosphere (Zoback, 1992).

Tectonic stress field study has achieved significant development in China. In the early of 1970s, Li et al (1973) studied the stress field near a seismic station by synthetic first motion pattern of multi earthquakes (Aki, 1966). Xu et al (1983) extended this idea to stress determination by using multi-micro-earthquake and multi-station, further applied it to North China area. This method was also used to determine the tectonic stress field around Ordos block (Xue and Yan, 1984), East China (Wang and Xu, 1985) and Southwest China (Xu et al, 1987). Xu et al (1992) obtained the fundamental features of stress field in Chinese mainland by

Another stress field determination method is using fault slip data and focal mechanism data (Angelier, 1979; Gephart and Forsyth, 1984; Michael, 1987). Based on stress determination method of Angelier (1979), Xu and Ge (1984) improved it and applied it to the 1931 *M*8.0 Fuyun, Xinjiang, earthquake. Using the similar method, the tectonic stress field in Southwest China (Xie et al, 1993; Cui and Xie, 1999) and in Guangdong and its adjacent areas (Kang et al, 2008) have been obtained. By using focal mechanism data in Chinese mainland, Du and Shao (1999) derived the tectonic stress field and principal stress ratio.

Nevertheless, neither Xu et al (1992) nor Du and Shao (1999) could cover their stress analysis on the whole China. For example, their stress analysis did not

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summarizing the stress field directions of previous studies, which reflects the close relationship between the motion of each block and that of the adjacent blocks. According to focal mechanism data and deep hole breakouts, Xu (2001) gave the present-day tectonic stress map for eastern Asia region. The maps of orientation of principal stress axes show that, apart from the strong influence of the collision between the Indian plate and the Eurasian plate, the present-day tectonic stress in eastern Asia is significantly affected by the back-arc extension of the subduction zones. The joint effect of the continental collision at Himalaya arc and back-arc extension in Myanmar arc region may be responsible for the remarkable rotation of principal stress orientations in southeastern part of Tibet plateau.

<sup>\*</sup> Received 9 April 2010; accepted in revised form 12 June 2010; published 10 August 2010.

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cover most of Tarim basin, Ningxia Hui autonomous region, most part of Inner Mongolia autonomous region, Hubei and Hunan provinces, etc. However, the tectonic stress field in whole China is needed in some geodynamic and earthquake prediction study. For example, the load/unload response ratio method used to earthquake prediction needs to know the tectonic stress field in advance (Peng et al, 2000; Wan, 2004). In recent years, accumulation of stress measurement, fault slip measurement and focal mechanism data, especially establishment of crustal stress database in China and its adjacent areas (Xie et al, 2003), lays a solid foundation for the study on determination of Chinese tectonic stress field. By using this database, Xie et al (2004) summarized the fundamental features of Chinese tectonic stress field and divided the Chinese mainland into different tectonic stress blocks. In this study, we will divide the whole China into 2°×2° subregions and determine the tectonic stress direction and stress ratio in each subregion by using this database and CMT catalogue from 1976 to 2005.

# 2 Tectonic stress inversion method

Studying the state of stress in the Earth's crust and upper mantle is helpful in understanding plate motion and regional deformation (Hardebeck and Hauksson, 2001). Earthquake focal mechanisms are indicators of stress; thus, we will use earthquake focal mechanisms to detect stress state that cannot be directly measured. Several authors have proposed methods to determine orientations of stress axes of seismotectonic regime in spite of complicated tectonic settings (e.g., Gephart and Forsyth, 1984; Michael, 1984; Angelier, 1989; Horiuchi et al, 1995). For tectonic stress inversion is a nonlinear problem, Michael's method linearly determines the stress tensor by using least squares method and has a probability to trap in local minimum. So, in this paper, the focal mechanism stress inversion (short for FMSI) (Gephart and Forsyth, 1984) program by grid searching stress field parameters is used to determine the orientations of principal stress axes in China.

FMSI method has three basic assumptions (Gephart and Forsyth, 1984; Gephart, 1990): ① slip on the fault plane occurs in the direction of resolved shear stress, ② stress orientation is uniform in the calculated area, and ③ earthquakes are shear dislocations and can occur on preexisting faults. The FMSI method uses a grid search over stress field parameter space to find the best-fitting

model that minimizes the average of the individual misfits between possible models and real data (Gephart and Forsyth, 1984; Gephart, 1990).

In FMSI, the individual misfit calculated for each earthquake is defined as the least rotation angle about any axis of general orientation which is needed to match the observed slip direction with one consistent with a given stress model (Gephart and Forsyth, 1984). We obtained the azimuths and plunges of three principal stresses axes  $\sigma_1$ ,  $\sigma_2$  and  $\sigma_3$  ( $\sigma_1 \ge \sigma_2 \ge \sigma_3$ ) and the ratio  $R = (\sigma_2 - \sigma_1)/(\sigma_3 - \sigma_1)$  ( $0 \le R \le 1$ ) by the best-fitting model. This may help us to distinguish the stress filed type.

There are four stress parameters ( $\sigma_1$ ,  $\sigma_2$ ,  $\sigma_3$  and R) in the FMSI inversion algorithm, and the minimum number of events used to inversion is four. Moreover, diverse data set can give better constrains to find out the suitable stress tensor orientation. For above reasons, we used all the earthquake focal mechanisms within each data set to obtain an average local stress field without separating fault types in a region.

The procedure of FMSI to determine best-fitting stress model is as follows. We first perform a coarse initial grid search (with 10° spacing in stress orientations) covering the whole range of possible models for each data set by the approximate FMSI method (short for FMSIA, Gephart, 1990). We then take the best resulting stress model as a starting model to perform a fine grid search (with 5° spacing in stress orientations) by the exact FMSI method (short for FMSIE, Gephart, 1990).

In FMSI, the size of the average misfit corresponding to the best fitting stress model could be an indicator of the homogeneity degree of stress. According to a series of tests carried out by Wyss et al (1992) and Gillard et al (1996), for the real earthquake, focal mechanisms with errors of 15° (average of the uncertainties in strike, dip and rake) cannot obtain the average misfit of the stress inversion larger than 6°, thus the average misfit smaller than 6° may represent a homogeneous stress field. In contrast, the average misfit larger than 9° could be attributed to heterogeneity of stress. In the case of average misfit in the range between 6° and 9°, the stress solution is acceptable, but may reflect some heterogeneity (e.g., Wyss and Lu, 1995; Lu et al, 1997).

#### 3 Data

The data used in Chinese tectonic field determination include: © 918 focal mechanism data from 1920 to 2003 determined by Chinese scholars, © 240 fault stria-

tion data from Quaternary fault slip measurements, ③ 72 stress relief data with all three axis directions at measured depth range of 50–363 m, and ④ 7 hydraulic fracturing stress data with all three axis directions at measured depth range from 400 m to 1 620 m. All the above data are from database of crustal stress in China and its adjacent areas (Xie et al, 2003). We also search the focal mechanism data from Harvard CMT solutions for the earthquakes in 1976–2005, which are not overlapped with the 918 focal mechanism data during 1920–2003 (Xie et al, 2003).

We divide the whole China into  $2^{\circ}\times2^{\circ}$  grids. In order to cover the whole study region and get the smoothing stress field, we select the data within the square areas of  $5^{\circ}\times5^{\circ}$  with the center of grid point. The stress field is smoothed by repeated selection of the focal mechanism data at different grid point, which looks more reasonable for stress field continuation. For the crust stress field has a probability different from the mantle stress field, we only select the data with depth less than 60 km. We cannot invert stress field in the areas less than four focal mechanism data, and use the stress direction determined by composite focal mechanism

nism solution of Wang and Xu (1985) instead (Figures 1 and 2 quivers without color filled).

## 4 Results

Basing on the data above mentioned, we get the stress field nearly covering the whole China (Figures 1 and 2) by the stress field determination method (Gephart and Forsyth, 1984; Gephart, 1990) and the results are listed in Table 1. From Figure 1, we can see that the bigger misfit angles are distributed in east part of Tibet plateau, Tianshan and its west area, Taiwan and south-east costal region of China, showing larger heterogeneity of stress field (e.g., Wyss and Lu, 1995; Lu and Wyss, 1996; Lu et al, 1997). But the continuity of stress field with other areas shows the overall pattern may be accepted. From Figure 2, we can see larger number of focal mechanisms used in the inversion in Taiwan region, south-east coastal region of China, west to Tianshan region and central region of the Tibet plateau, which shows more constraint to these stress field results.

Table 1 Results of stress field inverted in this study

Lat. /°N	Long.	$\sigma_{l}$ axis		$\sigma_2$ axis		$\sigma_3$ axis		D	Misfit angle	Number of
	/°E	Az/°	Pl/°	Az/°	Pl/°	Az/°	Pl/°	R	/°	earthquakes
22	99	212	7	97	73	304	15	0.45	6.926	78
22	101	194	26	42	60	290	12	0.25	8.633	69
22	103	354	26	145	60	258	12	0.25	5.129	48
22	105	344	26	144	62	250	8	0.30	3.931	27
22	107	337	25	138	63	243	7	0.40	1.550	10
22	109	330	4	151	85	61	0			0
22	111	330	4	151	85	61	0			0
22	113	112	12	21	4	272	77	0.55	1.960	4
22	115	84	17	298	69	177	11	0.20	4.012	11
24	99	190	35	36	52	289	13	0.35	9.034	90
24	101	18	9	257	72	110	15	0.65	10.973	81
24	103	359	10	127	74	267	12	0.55	7.574	62
24	105	339	30	141	58	245	8	0.30	4.853	40
24	107	331	25	132	63	237	7	0.45	3.729	13
24	109	330	4	151	85	61	0			0
24	111	330	4	151	85	61	0			0
24	113	108	13	16	7	258	75	0.60	1.843	4
24	115	71	13	310	65	166	20	0.50	1.226	7
24	117	292	6	177	75	24	13	0.40	10.524	210
24	119	112	3	206	58	20	31	0.65	10.459	318
24	121	292	3	189	76	23	13	0.40	9.989	351
26	99	190	35	29	53	287	9	0.15	11.605	99
26	101	10	35	177	54	276	6	0.40	11.245	90
26	103	10	35	163	52	271	13	0.25	9.879	69
26	105	158	14	310	74	66	7	0.40	7.871	41
26	107	306	10	172	75	38	10	0.20	3.904	11
26	111	80	3	175	60	353	29			0
26	113	80	3	175	60	353	29			0
26	115	75	24	292	60	172	16	0.30	2.099	8

Pro										Contin	ued from Table 1
26 117 112 4 221 78 21 11 0.45 10.029 143 26 119 99 9 213 68 6 19 0.40 10.914 248 28 85 178 148 34 343 53 90 12 0.40 5.393 440 28 87 188 34 20 55 222 6 0.50 7.722 58 28 91 25 14 205 76 295 0 0.70 9.115 66 28 93 39 7 144 64 306 24 0.95 10.821 81 28 95 39 30 205 59 306 6 0.75 10.589 88 28 99 182 55 40 28 300 18 0.50 12.105 88 28 99 182 55 40 28 300 18 0.50 12.105 88 28 101 10 35 179 54 277 5 0.40 12.726 79 28 103 10 35 157 50 268 16 0.35 13.290 58 28 107 293 18 49 53 192 30 0.65 2.790 10 28 107 293 18 49 53 192 30 0.65 2.790 10 28 111 80 3 175 60 333 89 60 0.10 0.738 44 28 111 80 3 175 60 333 89 60 0.10 0.738 44 28 111 80 3 175 60 333 89 60 0.10 0.738 44 28 111 80 3 175 60 333 89 60 0.10 0.738 44 28 111 9 10 9 211 50 13 38 0.60 9.889 220 30 81 15 5 225 84 105 12 3 3 0.60 8 35 29 30 81 15 5 225 84 114 330 29 181 37 0.50 9.889 182 38 117 4 26 317 88 49 33 18 3 0.60 9.889 220 30 81 15 5 225 84 105 12 3 3 0.60 8 33 29 30 0.60 8 30 30 30 30 0.65 2.790 10 38 11 10 9 211 50 13 33 30 0.60 9.889 220 30 81 15 5 225 84 105 3 3 0.60 8 9.482 9.90 10 30 81 15 5 225 84 105 3 3 0.60 8 9.482 9.90 10 30 81 15 5 225 84 105 3 3 0.60 9.889 220 30 81 15 6 0.35 114 9 0.05 114 9 0.85 5.429 9.00 10 30 81 15 5 225 84 105 3 0.50 3.869 27 3 30 83 174 26 317 88 76 16 0.20 4795 34 30 85 186 30 354 59 93 5 0.35 5.666 0.00 10 0.73 84 30 85 186 30 354 59 93 5 0.35 5.666 0.00 10 0.73 84 30 93 203 81 23 0 114 9 0.85 5.429 9.431 39 0.00 85 186 30 39 91 12.00 88 31 23 0 0.65 2.799 12.00 9.433 30 0.00 85 186 30 354 59 93 5 0.35 5.666 0.00 10 0.75 5.787 0.00 9.483 44 9.53 19.20 9.90 9.90 9.90 9.90 9.90 9.90 9.90									- R		Number of
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30	30	81	15	5	225	84	105	3	0.50	3.869	27
30 87 348 61 191 27 96 10 0.50 5.787 62 30 89 293 81 23 0 114 9 0.85 5.429 70 30 91 269 81 13 2 104 9 0.50 6.788 78 30 93 203 66 32 23 301 3 0.50 9.463 88 30 95 48 43 200 43 304 14 0.65 9.660 68 30 97 240 85 27 4 118 3 0.70 9.484 81 30 99 248 55 93 32 356 12 0.10 9.413 72 30 101 79 66 291 20 197 12 0.60 12.469 66 30 101 79 66 291 20 197 12 0.60 12.469 66 30 103 293 39 119 50 26 3 0.65 9.951 48 30 105 118 32 278 56 22 9 0.50 9.313 37 30 107 293 18 49 53 192 30 0.65 2.769 12 30 100 272 7 181 0 86 83 0.70 1.189 55 30 111 273 1 1 4 84 187 5 30 115 69 7 233 82 339 2 30 115 69 7 233 82 339 2 30 117 47 14 311 19 170 66 0.75 0.996 44 30 117 47 14 311 19 170 66 0.75 0.996 44 30 119 249 38 96 48 350 14 0.40 5.530 10 30 117 47 14 311 19 170 66 0.55 0.996 44 30 121 282 83 94 6 185 1 0.40 5.488 21 32 79 17 7 227 81 108 4 0.40 5.530 10 30 121 282 83 94 6 185 1 0.40 5.488 21 32 81 183 19 338 69 90 8 0.20 6.646 40 32 83 178 14 315 71 85 12 0.40 6.004 47 32 89 200 60 1 28 99 8 0.20 6.646 40 32 87 186 30 341 57 89 11 0.40 6.194 70 32 89 200 60 1 28 96 8 0.30 7.183 84 32 93 240 80 30 41 57 89 11 0.40 6.194 70 32 89 200 60 1 28 96 8 0.30 7.183 84 32 93 240 80 30 81 12 5 0.60 7.675 88 32 99 69 35 245 54 338 2 0.00 0.00 9.176 63 32 107 297 19 51 49 194 34 0.60 3.140 12 32 107 297 19 51 49 194 34 0.60 3.140 12 32 107 297 19 51 49 194 34 0.60 3.140 12	30	83	174	26	317		76	16	0.20	4.795	34
30         89         293         81         23         0         114         9         0.85         5.429         70           30         91         269         81         13         2         104         9         0.50         6.758         78           30         93         203         66         32         23         301         3         0.50         9.463         88           30         95         48         43         200         43         304         14         0.65         9.660         68           30         97         240         85         27         4         118         3         0.70         9.484         81           30         101         79         66         291         20         197         12         0.60         12.469         66           30         103         293         39         119         50         26         3         0.65         9.951         48           30         107         293         18         49         53         192         30         0.65         2.769         12           30         107         293         <		85								5.566	60
30 91 269 81 13 2 104 9 0.50 6.758 78 30 93 203 66 32 23 301 3 0.50 9.463 88 30 95 48 43 200 43 304 14 0.65 9.660 68 30 97 240 85 27 4 118 3 0.70 9.484 81 30 99 248 55 93 32 356 12 0.10 9.413 72 30 101 79 66 291 20 197 12 0.60 12.469 66 30 103 293 39 119 50 26 3 0.65 9.951 48 30 107 293 18 49 53 192 30 0.65 2.769 12 30 107 293 18 49 53 192 30 0.65 2.769 12 30 109 272 7 181 0 86 83 0.70 1.189 5 30 111 273 1 14 84 187 5 30 113 77 66 249 23 159 0 30 111 273 1 14 84 187 5 30 115 69 7 233 82 339 2 030 117 47 14 311 19 170 66 0.75 0.996 4 30 117 47 14 311 19 170 66 0.75 0.996 4 30 119 249 38 96 48 350 14 0.40 5.530 10 30 121 282 83 94 6 185 1 0.40 5.488 21 32 79 17 7 7 227 81 108 4 0.40 5.530 10 30 121 282 83 94 6 185 1 0.40 5.888 21 32 79 17 7 7 227 81 108 4 0.40 5.530 10 32 81 183 19 338 69 90 8 0.20 6.646 40 32 83 178 14 315 71 85 12 0.40 6.004 47 32 88 183 23 357 66 92 2 0.35 6.170 70 32 87 186 30 341 57 89 11 0.40 6.194 70 32 87 186 30 341 57 89 11 0.40 6.194 70 32 88 183 23 357 66 92 2 0.35 6.170 70 32 89 200 60 1 28 96 8 0.30 7.183 84 32 93 240 80 30 8 121 5 0.60 7.675 88 32 93 240 80 30 8 121 5 0.60 7.675 88 32 99 69 35 245 54 338 2 0.30 12.522 59 32 101 69 35 245 54 338 2 0.30 12.522 59 32 101 69 35 245 54 338 2 0.30 12.522 59 32 105 294 2 266 47 202 42 0.50 9.529 36 32 105 294 2 266 47 202 42 0.50 9.529 36 32 107 297 19 51 49 194 34 0.60 3.140 12.50											62
30 93 203 66 32 23 301 3 0.50 9.463 88 30 95 48 43 200 43 304 14 0.65 9.660 68 30 97 240 85 27 4 118 3 0.70 9.484 81 30 99 248 55 93 32 356 12 0.10 9.413 72 30 101 79 66 291 20 197 12 0.60 12.469 66 30 103 293 39 119 50 26 3 0.65 9.951 48 30 105 118 32 278 56 22 9 0.50 9.313 37 30 107 293 18 49 53 192 30 0.65 2.769 12 30 109 272 7 181 0 86 83 0.70 1.189 5 30 111 273 1 14 84 187 5 30 111 273 1 14 84 187 5 30 111 5 69 7 233 82 339 2 30 115 69 7 233 82 339 2 30 117 47 14 311 19 170 66 0.75 0.996 4 30 119 249 38 96 48 350 14 0.40 5.530 10 30 121 282 83 94 6 185 1 0.40 5.488 21 32 79 17 7 227 81 108 4 0.70 8.558 47 32 81 183 19 338 69 90 8 0.20 6.646 40 32 83 178 14 315 71 85 12 0.40 6.004 47 32 85 183 23 357 66 92 2 0.35 6.170 70 32 87 186 30 341 57 89 11 0.40 6.004 47 32 85 183 23 357 66 92 2 0.35 6.170 70 32 89 200 60 1 28 96 8 0.30 7.183 84 32 91 203 66 7 23 184 47 299 21 0.60 11.555 77 32 99 69 35 245 54 338 2 0.30 10.555 77 32 99 69 35 245 54 338 2 0.30 10.841 52 32 101 69 35 245 54 338 2 0.30 10.841 52 32 101 69 35 245 54 338 2 0.30 10.841 52 32 103 281 9 20 46 183 42 0.90 12.522 59 32 101 69 35 245 54 338 2 0.30 10.841 52 32 103 281 9 20 46 183 42 0.90 12.630 46 32 105 294 2 26 47 202 42 0.50 9.529 36 32 107 297 19 51 49 194 34 0.60 3.140 12.52											70
30         95         48         43         200         43         304         14         0.65         9,660         68           30         97         240         85         27         4         1118         3         0.70         9,484         81           30         99         248         55         93         32         356         12         0.10         9,413         72           30         101         79         66         291         20         197         12         0.60         12,469         66           30         103         293         39         119         50         26         3         0.65         9,951         48           30         103         293         39         119         50         26         3         0.65         9,951         48           30         107         293         18         49         53         192         30         0.65         2,769         12           30         107         293         18         49         53         192         30         0.65         2,769         12           30         111         273											
30											
30         99         248         55         93         32         356         12         0.10         9.413         72           30         101         79         66         291         20         197         12         0.60         12.469         66           30         103         293         39         119         50         26         3         0.65         9.951         48           30         105         118         32         278         56         22         9         0.50         9.313         37           30         107         293         18         49         53         192         30         0.65         2.769         12           30         109         272         7         181         0         86         83         0.70         1.189         5           30         111         273         1         14         84         187         5         0           30         115         66         249         23         159         0         0         0           30         115         66         249         23         159         0         0											
30         101         79         66         291         20         197         12         0.60         12.469         66           30         103         293         39         119         50         26         3         0.65         9.951         48           30         105         118         32         278         56         22         9         0.50         9.313         37           30         107         293         18         49         53         192         30         0.65         2.769         12           30         109         272         7         181         0         86         83         0.70         1.189         5           30         111         273         1         14         84         187         5         0         0           30         115         69         7         233         82         339         2         0         0           30         117         47         14         311         19         170         66         0.75         0.996         4           30         119         249         38         96         48											72
30         105         118         32         278         56         22         9         0.50         9.313         37           30         107         293         18         49         53         192         30         0.65         2.769         12           30         109         272         7         181         0         86         83         0.70         1.189         5           30         111         273         1         14         84         187         5         0           30         113         77         66         249         23         159         0         0           30         115         69         7         233         82         339         2         0           30         117         47         14         311         19         170         66         0.75         0.996         4           30         119         249         38         96         48         350         14         0.40         5.530         10           30         121         282         83         94         6         185         1         0.40         5.488											66
30         107         293         18         49         53         192         30         0.65         2.769         12           30         109         272         7         181         0         86         83         0.70         1.189         5           30         111         273         1         14         84         187         5         0           30         113         77         66         249         23         159         0         0           30         115         69         7         233         82         339         2         0           30         117         47         14         311         19         170         66         0.75         0.996         4           30         119         249         38         96         48         350         14         0.40         5.530         10           30         121         282         83         94         6         185         1         0.40         5.488         21           32         81         183         19         338         69         90         8         0.20         6.646	30	103	293	39	119	50	26	3	0.65	9.951	48
30         109         272         7         181         0         86         83         0.70         1.189         5           30         111         273         1         14         84         187         5         0           30         113         77         66         249         23         159         0         0           30         115         69         7         233         82         339         2         0           30         117         47         14         311         19         170         66         0.75         0.996         4           30         119         249         38         96         48         350         14         0.40         5.530         10           30         121         282         83         94         6         185         1         0.40         5.488         21           32         79         17         7         227         81         108         4         0.70         8.558         47           32         81         183         19         338         69         90         8         0.20         6.646	30	105	118	32		56	22	9	0.50	9.313	37
30         111         273         1         14         84         187         5         0         0           30         113         77         66         249         23         159         0         0           30         115         69         7         233         82         339         2         0           30         117         47         14         311         19         170         66         0.75         0.996         4           30         119         249         38         96         48         350         14         0.40         5.530         10           30         121         282         83         94         6         185         1         0.40         5.530         10           30         121         282         83         94         6         185         1         0.40         5.588         21           32         79         17         7         227         81         108         4         0.70         8.558         47           32         81         183         19         338         69         90         8         0.20											12
30         113         77         66         249         23         159         0 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>0.70</td><td>1.189</td><td>5</td></td<>									0.70	1.189	5
30         115         69         7         233         82         339         2         0           30         117         47         14         311         19         170         66         0.75         0.996         4           30         119         249         38         96         48         350         14         0.40         5.530         10           30         121         282         83         94         6         185         1         0.40         5.530         10           32         79         17         7         227         81         108         4         0.70         8.558         47           32         81         183         19         338         69         90         8         0.20         6.646         40           32         83         178         14         315         71         85         12         0.40         6.004         47           32         85         183         23         357         66         92         2         0.35         6.170         70           32         87         186         30         341         57 </td <td></td>											
30         117         47         14         311         19         170         66         0.75         0.996         4           30         119         249         38         96         48         350         14         0.40         5.530         10           30         121         282         83         94         6         185         1         0.40         5.488         21           32         79         17         7         227         81         108         4         0.70         8.558         47           32         81         183         19         338         69         90         8         0.20         6.646         40           32         81         183         19         338         69         90         8         0.20         6.646         40           32         83         178         14         315         71         85         12         0.40         6.004         47           32         85         183         23         357         66         92         2         0.35         6.170         70           32         87         186 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>											
30         119         249         38         96         48         350         14         0.40         5.530         10           30         121         282         83         94         6         185         1         0.40         5.488         21           32         79         17         7         227         81         108         4         0.70         8.558         47           32         81         183         19         338         69         90         8         0.20         6.646         40           32         83         178         14         315         71         85         12         0.40         6.004         47           32         85         183         23         357         66         92         2         0.35         6.170         70           32         87         186         30         341         57         89         11         0.40         6.194         70           32         89         200         60         1         28         96         8         0.30         7.183         84           32         91         203         6									0.75	0.996	
30         121         282         83         94         6         185         1         0.40         5.488         21           32         79         17         7         227         81         108         4         0.70         8.558         47           32         81         183         19         338         69         90         8         0.20         6.646         40           32         83         178         14         315         71         85         12         0.40         6.004         47           32         85         183         23         357         66         92         2         0.35         6.170         70           32         87         186         30         341         57         89         11         0.40         6.194         70           32         89         200         60         1         28         96         8         0.30         7.183         84           32         91         203         66         7         23         100         6         0.35         7.693         93           32         93         240         80 </td <td></td>											
32         79         17         7         227         81         108         4         0.70         8.558         47           32         81         183         19         338         69         90         8         0.20         6.646         40           32         83         178         14         315         71         85         12         0.40         6.004         47           32         85         183         23         357         66         92         2         0.35         6.170         70           32         87         186         30         341         57         89         11         0.40         6.194         70           32         89         200         60         1         28         96         8         0.30         7.183         84           32         91         203         66         7         23         100         6         0.35         7.693         93           32         93         240         80         30         8         121         5         0.60         7.675         88           32         95         45         35 <td></td> <td>21</td>											21
32       81       183       19       338       69       90       8       0.20       6.646       40         32       83       178       14       315       71       85       12       0.40       6.004       47         32       85       183       23       357       66       92       2       0.35       6.170       70         32       87       186       30       341       57       89       11       0.40       6.194       70         32       89       200       60       1       28       96       8       0.30       7.183       84         32       91       203       66       7       23       100       6       0.35       7.693       93         32       93       240       80       30       8       121       5       0.60       7.675       88         32       95       45       35       184       47       299       21       0.60       9.177       67         32       97       45       35       184       47       299       21       0.60       11.555       77         32	32	79	17	7	227	81	108	4	0.70		47
32       83       178       14       315       71       85       12       0.40       6.004       47         32       85       183       23       357       66       92       2       0.35       6.170       70         32       87       186       30       341       57       89       11       0.40       6.194       70         32       89       200       60       1       28       96       8       0.30       7.183       84         32       91       203       66       7       23       100       6       0.35       7.693       93         32       93       240       80       30       8       121       5       0.60       7.675       88         32       95       45       35       184       47       299       21       0.60       9.177       67         32       97       45       35       184       47       299       21       0.60       11.555       77         32       99       69       35       245       54       338       2       0.30       12.522       59         32 <td></td>											
32       85       183       23       357       66       92       2       0.35       6.170       70         32       87       186       30       341       57       89       11       0.40       6.194       70         32       89       200       60       1       28       96       8       0.30       7.183       84         32       91       203       66       7       23       100       6       0.35       7.693       93         32       93       240       80       30       8       121       5       0.60       7.675       88         32       95       45       35       184       47       299       21       0.60       9.177       67         32       97       45       35       184       47       299       21       0.60       11.555       77         32       99       69       35       245       54       338       2       0.30       12.522       59         32       101       69       35       245       54       338       2       0.30       10.841       52         32 <td></td> <td>47</td>											47
32       87       186       30       341       57       89       11       0.40       6.194       70         32       89       200       60       1       28       96       8       0.30       7.183       84         32       91       203       66       7       23       100       6       0.35       7.693       93         32       93       240       80       30       8       121       5       0.60       7.675       88         32       95       45       35       184       47       299       21       0.60       9.177       67         32       97       45       35       184       47       299       21       0.60       11.555       77         32       99       69       35       245       54       338       2       0.30       12.522       59         32       101       69       35       245       54       338       2       0.30       10.841       52         32       103       281       9       20       46       183       42       0.90       12.630       46         32<											70
32       91       203       66       7       23       100       6       0.35       7.693       93         32       93       240       80       30       8       121       5       0.60       7.675       88         32       95       45       35       184       47       299       21       0.60       9.177       67         32       97       45       35       184       47       299       21       0.60       11.555       77         32       99       69       35       245       54       338       2       0.30       12.522       59         32       101       69       35       245       54       338       2       0.30       10.841       52         32       103       281       9       20       46       183       42       0.90       12.630       46         32       105       294       2       26       47       202       42       0.50       9.529       36         32       107       297       19       51       49       194       34       0.60       3.140       12 <td< td=""><td>32</td><td>87</td><td>186</td><td>30</td><td>341</td><td>57</td><td>89</td><td>11</td><td>0.40</td><td></td><td>70</td></td<>	32	87	186	30	341	57	89	11	0.40		70
32     93     240     80     30     8     121     5     0.60     7.675     88       32     95     45     35     184     47     299     21     0.60     9.177     67       32     97     45     35     184     47     299     21     0.60     11.555     77       32     99     69     35     245     54     338     2     0.30     12.522     59       32     101     69     35     245     54     338     2     0.30     10.841     52       32     103     281     9     20     46     183     42     0.90     12.630     46       32     105     294     2     26     47     202     42     0.50     9.529     36       32     107     297     19     51     49     194     34     0.60     3.140     12       32     109     96     0     5     69     186     21     0.80     0.683     6											84
32     95     45     35     184     47     299     21     0.60     9.177     67       32     97     45     35     184     47     299     21     0.60     11.555     77       32     99     69     35     245     54     338     2     0.30     12.522     59       32     101     69     35     245     54     338     2     0.30     10.841     52       32     103     281     9     20     46     183     42     0.90     12.630     46       32     105     294     2     26     47     202     42     0.50     9.529     36       32     107     297     19     51     49     194     34     0.60     3.140     12       32     109     96     0     5     69     186     21     0.80     0.683     6											
32     97     45     35     184     47     299     21     0.60     11.555     77       32     99     69     35     245     54     338     2     0.30     12.522     59       32     101     69     35     245     54     338     2     0.30     10.841     52       32     103     281     9     20     46     183     42     0.90     12.630     46       32     105     294     2     26     47     202     42     0.50     9.529     36       32     107     297     19     51     49     194     34     0.60     3.140     12       32     109     96     0     5     69     186     21     0.80     0.683     6											
32     99     69     35     245     54     338     2     0.30     12.522     59       32     101     69     35     245     54     338     2     0.30     10.841     52       32     103     281     9     20     46     183     42     0.90     12.630     46       32     105     294     2     26     47     202     42     0.50     9.529     36       32     107     297     19     51     49     194     34     0.60     3.140     12       32     109     96     0     5     69     186     21     0.80     0.683     6											
32     101     69     35     245     54     338     2     0.30     10.841     52       32     103     281     9     20     46     183     42     0.90     12.630     46       32     105     294     2     26     47     202     42     0.50     9.529     36       32     107     297     19     51     49     194     34     0.60     3.140     12       32     109     96     0     5     69     186     21     0.80     0.683     6											
32     103     281     9     20     46     183     42     0.90     12.630     46       32     105     294     2     26     47     202     42     0.50     9.529     36       32     107     297     19     51     49     194     34     0.60     3.140     12       32     109     96     0     5     69     186     21     0.80     0.683     6								2			52
32     105     294     2     26     47     202     42     0.50     9.529     36       32     107     297     19     51     49     194     34     0.60     3.140     12       32     109     96     0     5     69     186     21     0.80     0.683     6	32										46
32 109 96 0 5 69 186 21 0.80 0.683 6	32							42		9.529	36
											12
32 111 273 1 14 84 187 5									0.80	0.683	6
		111	273			84		5			0
									0.40	0.516	0
32 115 252 12 34 74 160 9 0.40 0.516 5 32 117 257 7 139 75 349 13 0.50 0.397 5											5 5
											6

									Contin	ued from Table 1
Lat.	Long.	$\sigma_{\rm l}$ 8			axis		axis	- R	Misfit angle	Number of
/°N	/°E	Az/°	Pl/°	Az/°	Pl/°	Az/°	Pl/°		/°	earthquakes
32	121	240	5	29	84	150	3	0.35	0.978	5
34	79	20	9	212	80	110	2	0.60	8.484	54
34	81	18	9	227	79	109	5	0.50	7.082	43
34	83	183	19	338	69	90	8	0.20	6.467	46
34	85	183	14	3	76	273	0	0.35	6.261	65
34	87	0	35	183	54	91	2	0.25	6.846	72
34	89	193	19	321	61	96	21	0.25	4.751	85
34	91	27	2	275	84	117	5	0.50	7.279	98
34	93	29	26	198	63	297	4	0.50	8.299	100
34 34	95 97	26 52	23 7	206 149	67 45	116 315	0 44	0.50 0.65	8.669 9.842	78 76
34	97	52 57	7		43 44	313		0.65	9.842 8.992	59
34	101	217	14	153 118	31	328	45 55	0.65	11.898	59 51
34	101	77	25	241	64	344	6	0.03	8.313	40
34	105	112	0	22	47	202	43	0.13	6.978	31
34	107	98	0	8	51	188	39	0.85	5.171	14
34	109	84	30	255	59	352	4	0.50	2.363	8
34	111	82	6	347	35	180	54	0.55	1.368	5
34	113	256	37	39	46	151	19	0.45	0.943	4
34	115	90	5	354	45	185	44	0.35	1.711	6
34	117	82	22	332	39	194	42	0.20	1.592	6
34	119	236	28	53	61	145	1	0.20	2.530	7
36	77	202	26	316	40	89	38	0.40	10.604	121
36	79	16	21	175	67	283	7	0.50	9.711	85
36	81	8	13	192	76	98	1	0.25	7.084	61
36	83	357	18	131	64	262	17	0.50	6.682	33
36	85	192	7	300	68	99	20	0.25	4.860	40
36	87	26	0	296	74	116	16	0.50	3.971	50
36	89	21	0	291	77	111	13	0.40	6.058	67
36	91	210	5	320	76	119	13	0.55	6.530	75
36	93	30	35	190	53	293	9	0.45	7.097	81
36	95 2 <b>7</b>	30	0	120	46	300	44	0.65	8.440	63
36	97	210	9	101	64	305	24	0.60	8.492	60
36	99	233	2	142	10	333	79 56	0.35	5.430	42
36	101	57 25	6	323	33	156	56	0.45	5.642	39
36 36	103 105	35 103	0 5	125 9	20 33	305 201	70 56	0.40 0.55	6.306 6.761	27 27
36	103	103	0	11	33 42	191	48	0.33	5.843	15
36	107	81	26	256	63	351	2	0.80	4.261	15
36	111	73	7	333	53	168	36	0.45	3.689	11
36	113	258	7	356	49	162	40	0.60	4.463	13
36	115	71	0	341	69	161	21	0.50	3.578	16
36	117	256	5	356	64	164	25	0.55	3.566	16
36	119	252	9	12	72	160	15	0.50	3.468	14
38	75	182	7	275	25	78	63	0.50	10.313	161
38	77	201	21	309	39	89	43	0.40	9.903	140
38	79	22	19	144	57	283	26	0.75	9.244	102
38	81	8	13	179	76	278	2	0.25	9.281	77
38	83	13	7	193	83	283	0	0.30	9.885	43
38	85	194	16	316	62	97	22	0.25	6.193	49
38	87	195	14	314	63	99	22	0.25	6.082	52
38	89	31	21	217	68	122	2	0.55	6.331	55
38	91	216	21	13	67	123	8	0.50	7.551	62
38	93	207	3	313	79	116	10	0.50	7.289	67
38	95	25	1	283	84	115	5	0.50	8.155	47
38	97	25	25	159	56	285	21	0.65	4.746	44
38	99	55	0	145	7	325	83	0.45	6.669	39
38	101	10	4	279	5	136	83	0.50	5.326	34
38	103	227	7	134	21	334	67	0.55	6.422	24
38 38	105 107	48 52	27 26	307 312	19 19	186 190	55 57	0.45 0.05	7.145 4.428	24 13
38	107	36	30	286	30	160	57 45	0.05	4.428 7.116	13
38	109	252	5	286 144	30 74	343	15	0.73	3.993	13
38	111	232	3	144	/4	343	13	0.30	3.993	14

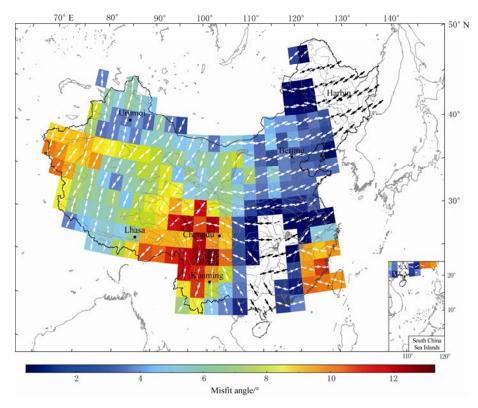
Continued from Table 1 Lat.  $\sigma_{l}$  axis  $\sigma_2$  axis  $\sigma_3$  axis Misfit angle Number of R /°E earthquakes /°N Pl/° Az/° Pl/° Az/° Az/° 2.494 0.35 0.30 4 537 0.50 4.105 0.45 4.202 0.40 2.537 0.25 3.694 0.35 2.895 6.433 0.65 5.398 0.65 0.706.632 0.70 5.905 0.60 4.864 0.05 1.115 0.05 0.978 0.75 0.7350.50 3.889 0.65 6.147 0.735 0.75 0.05 0.481 0.50 0.842 0.50 2.238 0.20 0.688 

Note: The data with Number of earthquakes of 0 are from Wang and Xu (1985).

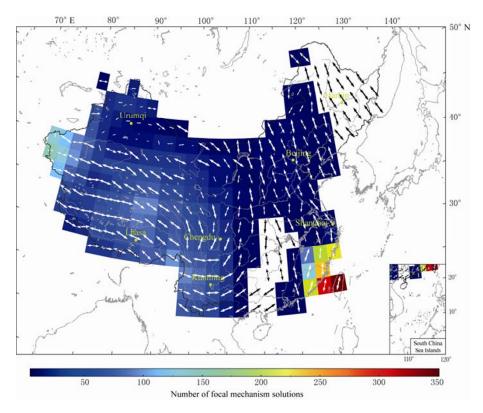
Most of  $\sigma_1$  and  $\sigma_3$  axes are horizontal (Figures 1 and 2), indicating that the seismotectonic deformation takes place primarily through strike-slip faulting. The continuous  $\sigma_1$  and  $\sigma_3$  direction showing the stress field in China and its adjacent areas has the same source which is driven by the northward indentation of the Indian plate, and subduction of the Pacific ocean plate under the Eurasia plate. The western part, i.e., Tibetan plateau, undergoes north-south compression and east-west extension, and this trend extends to Xinjiang area. The  $\sigma_1$  direction appears to curve sharply in the eastern end of Himalaya arc, showing some eddylike feature to the south of the Assam wedge (Figure 1). The principal

stress axes show a relatively uniform radial pattern. That is, the compressive horizontal stress trajectories radiate from Tibet plateau to the northern, eastern, and south-eastern parts of the mainland (Figure 1). The inferred extensional stress directions lie along arcs convex outward from the plateau (Figure 2). Despite inevitable local variations, which are often indistinguishable from the error in stress axis estimation, this overall pattern is schematically expressed in Figure 1 by horizontal stress trajectories.

In central part of Tibet plateau, there are relative vertical  $\sigma_1$  axes, horizontal  $\sigma_3$  axes in east-west direction. This may be caused by the extension of this region and



**Figure 1**  $\sigma_1$  direction and misfit angles obtained in this study. Quivers show the directions of  $\sigma_1$ , and the longer the quiver is, the more horizontal the  $\sigma_1$  will be.



**Figure 2**  $\sigma_3$  direction and number of data used in this study. Quivers show the directions of  $\sigma_3$ , and the longer the quiver is, the more horizontal the  $\sigma_3$  will be.

be validated by more lakes in this area. In the North-South Seismic Zones, we can see that the stress direction changes sharply, which indicates a dividing line of the stress field in this area.

### 5 Discussion and conclusions

The data used to infer modern stress field in the present study come from earthquakes occurred during the past several decades, stress measurements in recent years and quaternary fault slip measurements. It is interesting to notice that a similar pattern of stress axes as discovered in this study has also been found before. For example, Xu et al (1992) used a different method to get the mean principal tress axes basing on 9 621 P wave first motion polarity from 5 054 small earthquakes. Using the similar method to this study, Du and Shao (1999) also got the modern tectonic stress field. Based on the data of earthquake centroid moment tensor (CMT) solution, P-wave first motion focal mechanism solution and deep hole breakouts, Xu (2001) compiled a present-day tectonic stress map for eastern Asia region. The same stress field pattern confirms our study method and data used. But the stress filed inferred in this study covers more areas. The stress field obtained in this study is also consistent with GPS measurement (Wang et al, 2001; Wang et al, 2003) and its strain rate field (Shen et al, 2003; Zhang et al, 2004), quaternary fault slip rates and GPS observations (Holt et al, 2000), as well as GPS, geologic, and shear wave splitting data (Flesh et al, 2005).

Existence of the broad-scale radial pattern of  $\sigma_1$  directions indicates that the primary force responsible for the tectonic movement and earthquake generation in continental area of China does not come from some local sources but from an external driving force on a large scale. It is quite likely related to the indentation effect of plate collision between India and Euroasia, as studied by many authors (e.g., Tapponnier and Molnar, 1976; Houseman and England, 1986; England and Houseman, 1986).

As mentioned previously, we have studied a stress field in some crustal volume which has a thickness represented by earthquake focal depth. Due to the limited resolving capability of the method and data that we used, we can say nothing about possible variation of the stress state with depth.

Most of stress relief measurement data are measured in shallow part of the crust. Strictly speaking, they cannot be used to invert the stress field in the deep part

of the crust (e.g., Xu, 2001) for being affected by topography. In this study, we want to get the average stress field in a relatively large area, the topographic effect may be smoothed, so this sort of data can be used to constrain the stress field.

In the stress filed inversion, we select the data within the square areas of 5°×5° with the center of grid point. So the smoothing stress field can be achieved, and can be conveniently used to constrain the stress field in geodynamic process simulation, earthquake prediction (e.g., Peng et al, 2000; Wan, 2004) as well as slip property of active fault determination (Wan et al, 2008).

Acknowledgements This work is supported by the National Natural Science Foundation of China (40874022), Public Utility Research Project (200808053) and 973 program (2008CB425703). We would like to thank John Gephart for making his program available and Furen Xie for making Chinese stress field data available. Profs. Zhonghuai Xu and Zhengkang Shen provided their constructive comments and suggestions. The reviewers' comments improved the manuscript a lot.

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