

Microstructured Reactor as a Pre-Turbo Catalytic Converter

M. Iwaniszyn · J. Ochońska · P. Jodłowski ·
J. Łojewska · A. Matuszek-Chmurowska ·
A. Kołodziej

Published online: 27 February 2013

© The Author(s) 2013. This article is published with open access at Springerlink.com

Abstract The idea of a structured catalytic converter placed immediately after engine exhaust valves, thus operating on high gas temperature and velocity, is explored. The assumption is that major part of the reactor operates in the entry region where Nusselt and Sherwood numbers are highly enhanced. In this work, flow resistances as well as heat and mass transfer coefficients were studied for gas velocities exceeding 50 m/s. Consequently, the transition range (between laminar and turbulent flows) was reached. The comparison with classic monolith has shown significant improvement in heat or mass transfer paid by slight increase in flow resistance.

Keywords Heat transfer · Mass transfer · Flow resistance · Catalytic converter · High velocity

List of Symbol

a Specific surface area, m^{-1}
 A, B Constants
 C_D Drag coefficient

D_A Kinematic diffusivity, $m^2 s^{-1}$
 D_h $4\varepsilon/a$, hydraulic diameter, m
 D_p Grains diameter, m
 f Fanning friction factor
 G_Z Graetz number
 k_C Mass transfer coefficient, m/s
 k_r Kinetic rate constant, m/s
 L Channel length, m
 L_R Reactor length, m
 L^+ $L/(D_h \cdot Re)$, hydraulic dimensionless channel length
 L^* $L/(D_h \cdot Re \cdot Pr)$, heat dimensionless channel length
 L^{*M} $L/(D_h \cdot Re \cdot Sc)$, mass dimensionless channel length
 Nu $\alpha \cdot D_h/\lambda$, Nusselt number
 Pr $C_p \cdot \eta/\lambda$, Prandtl number
 Re $w_0 \cdot \rho \cdot D_h/(\varepsilon \cdot \eta)$, Reynolds number
 Sc $\eta/(\rho \cdot D_A)$, Schmidt number
 Sh $k_c D_h/D_A$, Sherwood number
 W_0 Superficial gas velocity, m/s
 α Heat transfer coefficient, $W m^{-2} K^{-1}$
 ΔP Pressure drop (flow resistance), Pa
 ε Void volume
 η Dynamic viscosity, Pa s
 λ Thermal conductivity, $W m^{-1} K^{-1}$
 ρ Density, $kg m^{-3}$
 χ Efficiency criterion, eqs. (9) and (10)

M. Iwaniszyn (✉) · A. Kołodziej
Institute of Chemical Engineering, Polish Academy of Sciences,
Bałtycka 5, 44-100 Gliwice, Poland
e-mail: miwaniszyn@iich.gliwice.pl

J. Ochońska · P. Jodłowski · J. Łojewska
Faculty of Chemistry, Jagiellonian University, Ingardena 3,
30-060 Kraków, Poland

A. Matuszek-Chmurowska · A. Kołodziej
Faculty of Civil Engineering, Opole University of Technology,
Katowicka 48, 45-061 Opole, Poland

List of Subscripts

fd Fully developed flow
H Boundary condition of constant heat flux
T Boundary condition of constant surface temperature
tr Triangular structure
sn Sinusoidal structure

1 Introduction

Effective control of vehicle engine emission, especially that of Diesel engines, constitutes a serious problem because of lean combustion conditions, high amount of nitrogen oxides and production of particulate matter. Therefore, novel methods of controlling CO/NO_x emissions are still proposed to enhance the effectiveness of classic monolithic converters. For example, More et al. [1] suggested preliminary pollution reduction in a small converter placed before the turbocharger. Assumed gas velocity may reach 100 m/s. The authors [1] postulated that up to 70 % of pollution may be neutralized within this small reactor. The above idea is a challenge for all: catalysis, material and chemical engineering. This pre-turbo converter should be designed to operate at high gas temperature and velocity. This may bring about erosion of catalyst and even converter substrate (usually ceramic or metallic monolith).

Few years ago, Kołodziej and Łojewska [2] and Kołodziej et al. [3] designed and modeled metallic short-channel structures, which base on the assumption of developing laminar flow [4]. The short monolith proposed in [1] follows the idea of the short-channel reactor [2, 3] for much higher flow velocities with possibility to reach the transition or even turbulent flow regime. For this reason, heat and mass transfer coefficients should be much higher than in classic monolithic converters.

As excessive heat and mass transfer resistances may significantly reduce the yield of catalytic reactor, particularly monolithic one, the idea of small converter operating in very severe flow regime seems attractive, however, very difficult to achieve. In fact, velocity suggested in [1] exceeds many times that commonly applied in chemical reactors and to our knowledge there is no information on the functioning the structured reactors in the literature.

The purpose of this work was to test the short-channel structures described in [2, 3] for very high gas velocities, about 50 m/s, to meet and experimentally check the demands presented in [1].

2 Experimental

Two types of structures were tested: of sinusoidal and triangular channel cross-section. The structures were made of

metal—Kanthal, steel containing 20 % Cr and 3–5 % Al. Each structure was composed of two type strips stacked alternately and welded: straight strips and wavy (sinusoidal structure) or zigzag (triangular structure) strips. Both strips displayed very close electrical resistance. Table 1 contains the parameters of the tested structures and of the ceramic monolith and packed bed taken for comparison.

Heat transfer and flow resistance experiments were performed using the same methodology as described by Kołodziej and Łojewska [2]. Electric current that heated the structures flowing directly through them reached up to 150 A. Air fed to the reactor was used under ambient temperature and temperatures slightly above the ambient ones (till 50 °C). Air velocity reached slightly above 50 m/s (limit of the apparatus). Temperatures of the flowing air and of the structure surface were measured using several thermocouples. Special composite glue providing good heat conduction and no electric conduction was used to fix the thermocouples to the channel walls. During the flow resistance experiment, the Recknagel micromanometer was used that ensured resolution of 0.05 Pa and reproducibility of 0.2 Pa.

The experiments were performed at ambient conditions for a velocity of 50 m/s. However, usual temperature of the exhaust gases (catalytic combustion or deNO_x process) amounts to 400 °C at least. The Reynolds numbers reached during the experiments (cf. Table 1) correspond, at 400 °C, to a velocity of ~150 m/s.

3 Results and Discussion

The main purpose of this study was to determine the flow resistance, heat and mass transfer in the short-channel triangular and sinusoidal structures under very high gas velocities. The range of Reynolds numbers used (cf. Table 1) proved that not only the laminar, but also the transition flow occurred in the channels.

In short capillary channels the developing laminar flow lead to enhanced transport coefficients, even more within the transient flow range. Unfortunately, in this developing region (or entrance channel section) the flow resistance is also higher comparing with the fully developed flow.

Fanning friction factors, f , defined by Darcy–Weisbach equation:

Table 1 Parameters of the short-channel structures studied

Structure	Channel length L, (mm)	Specific surface a, (m ⁻¹)	Void volume (ε)	Hydraulic diameter D _h , (mm)	Reynolds range studied
Triangular (base 5.26 mm; height 4.72 mm)	5	1314.4	0.945	2.876	59.8–6810.6
Sinusoidal (base 4.06 mm; height 2.19 mm)	5	2382.7	0.904	1.518	38.2–4232.3
Monolith 100 cpsi	200	1339	0.72	2.15	–
Packed bed of 2 mm spheres	–	1570	0.48	2.0 (D _p)	–

$$\frac{\Delta P}{L} = 2f \frac{w_0^2 \rho}{\varepsilon^2 D_h} \tag{1}$$

depends on hydraulic dimensionless channel length, L^+ :

$$L^+ = \frac{L}{D_h Re} \tag{2}$$

The correlations for triangular and sinusoidal structures are, respectively:

$$(f \cdot Re)_{tr} = 2.044L^{+(-0.631)} \tag{3}$$

$$(f \cdot Re)_{sn} = 0.774L^{+(-0.687)} \tag{4}$$

78 experiments were executed for each structure. The average error does not exceed 1 % for both cases. Figure 1 compares both experimental and theoretical results: flow resistance results, correlations derived, theoretical solution of Fleming and Sparow [5] for laminar developing flow in short triangular (equilateral) channel and the dependence proposed by Shah [6] for fully developed laminar flow in triangular and sinusoidal channel.

In the case of triangular structure the experimental points lie close to the theoretical solution of Fleming and Sparow [5] (line 1 and eq. 3 in Fig. 1). However, the results obtained for sinusoidal structure lie below the theoretical solutions of Fleming and Sparow [5] (line 1 and eq. 4, in fact, for the triangular channel) and even below the solution for fully developed laminar flow (line 3—Shah [6]).

As the independent mass transfer experiments were not performed, the heat and mass transfer analogy was used to derive the mass transfer characteristics. This approach was applied and experimentally proved in [7]; a wide discussion of the problem is presented in [8]. The correlations for

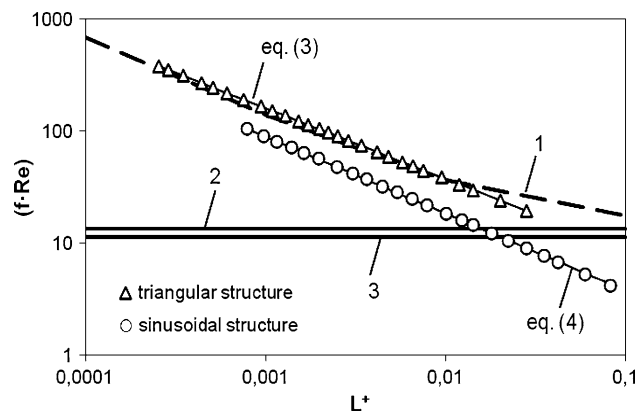


Fig. 1 Flow resistance results in terms of the $(f \cdot Re)$ product vs. dimensionless channel length L^+ (selected experimental points). 1 theoretical solution of Fleming and Sparow [5] (developing flow); theoretical solutions of Shah [6] for fully developed laminar flow: 2 triangular structure ($f \cdot Re = 13,333$); 3 sinusoidal structure ($f \cdot Re = 11,256$)

heat (mass) transfer for triangular and sinusoidal structures are:

$$Nu_{tr} = Nu_H \left[0, 532(\text{Pr} \cdot L^*)^{-0,161} \right] \tag{5}$$

$$Sh_{tr} = Sh_H \left[0, 532(\text{Sc} \cdot L^{*M})^{-0,161} \right]$$

$$Nu_{sn} = Nu_T \left[1, 399(\text{Pr} \cdot L^*)^{-0,209} \right] \tag{6}$$

$$Sh_{sn} = Sh_T \left[1, 399(\text{Sc} \cdot L^{*M})^{-0,209} \right]$$

The number of experimental points was 258 for both, triangular and sinusoidal structures. The average error for triangular structure amounts to 6 % while for sinusoidal structure—7 %. Nu_H and Nu_T (analogically Sh_H and Sh_T) are Wibulswas’ [9] theoretical solutions for $\langle H \rangle$ (constant heat flux) and $\langle T \rangle$ (constant wall temperature) boundary conditions:

$$Nu_H = 3, 111 + 0, 448 \cdot (L^*)^{-0,608} \tag{7}$$

$$Sh_H = 3, 111 + 0, 448 \cdot (L^{*M})^{-0,608}$$

$$Nu_T = 2, 47 + 0, 299 \cdot (L^*)^{-0,598} \tag{8}$$

$$Sh_T = 2, 47 + 0, 299 \cdot (L^{*M})^{-0,598}$$

The heat transfer results and correlations with theoretical solutions of Wibulswas [9] are presented in Fig. 2. The mass transfer description is analogical.

Figure 2 shows that, for large Reynolds numbers (small L^*), Nusselt numbers are higher than theoretical solution of Wibulswas found for triangular structures [9] (line 2 in Fig. 2). This is because the Wibulswas’ [9] solution applies to laminar flow, while the experiments achieved the transition flow regime. The discrepancy between the experiments and the theory is not big in the case of triangular structure. For the sinusoidal structure the differences

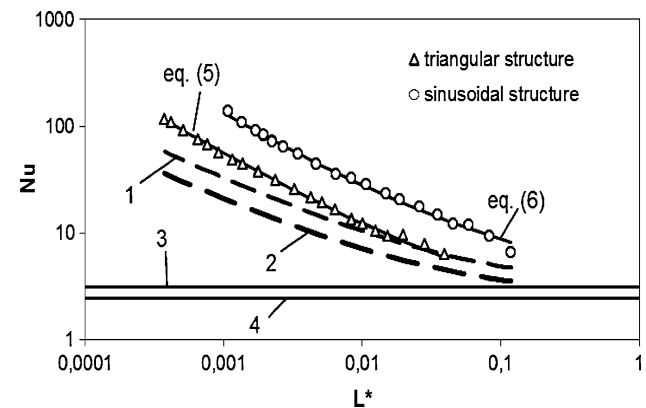


Fig. 2 Heat transfer results in terms of the Nusselt number versus dimensionless channel length L^* (selected experimental points). Theoretical solutions of Wibulswas [9] for developing flow: 1 $\langle H \rangle$ boundary solution; 2 $\langle T \rangle$ boundary solution. Theoretical values for fully developed flow [4]: 3 triangular structure ($Nu = 3,111$); 4 sinusoidal structure ($Nu = 2,47$)

Table 2 Pressure drop for different types of pre-turbo reactor filling

Reactor structure	Re	ΔP [kPa]	
		$L_R = 10$ mm	$L_R = 20$ mm
Triangular short-channel structure	2,300	0.78	1.56
Sinusoidal short-channel structure	1,300	0.67	1.34
Monolith 100 cpsi	1,630	0.81	1.17
Packed bed of 2 mm spheres	1,520	53	106

Temperature 400 °C, atmospheric pressure, superficial gas velocity $w_0 = 50$ m/s

between the experiments and the Wilulswas’ [9] prediction for triangular channel are significant. However, the theoretical solution for laminar flow developing in a sinusoidal channel is not available in the literature. Therefore, Wilulswas’ [9] solution is the only possibility to compare the experiments with theoretical prediction. Sinusoidal channel slightly resemble the triangular one with rounded corners.

The experimentally obtained ranges of Nusselt numbers drop into the range from 5.2 to 122 ($Sh = 8.4\text{--}264$) for the triangular structure and—from 6.6 to 139.8 ($Sh = 9.0\text{--}288$) for the sinusoidal structure, which agrees well with the Nu and Sh range from 4 to 100 postulated by More et al. [1].

A question arises whether the pressure drop is acceptable for a reactor working with such a large velocity. The reactor (pre-turbo converter) length L_R assumed was 10 or 20 mm. This is in accordance with the concept of pre-turbo converter presented by More et al. [1] as this reactor type is expected to realise 50–70 % of total conversion at very short distance. Resulting pressure drop for the structures considered are presented in Table 2.

As visible, the pressure drop of structures is almost two orders of magnitude lower than that of packed bed. The pressure drop of short-channel structures is close to the monolith. Such a short monolith (10–20 mm) may be regarded as a short-channel structure as well. The flow resistance seems acceptable for very short reactors considering high temperature near to the exhaust valve, very intense mass transfer and large available pressure of the exhaust gas in this region of an engine (near to the exhaust valve).

A comparison of the short-channel structures studied with the ceramic monolith 100 cpsi and packed bed, in terms of mass transfer and flow resistance, is presented in Figs. 3 and 4, respectively. Hawthorn [10] correlations were used to calculate Sherwood numbers and Fanning friction factors of the monolith. Sherwood numbers of the packed bed was calculated using Wakao and Kagueli [11] correlation and flow resistance was calculated using Ergun

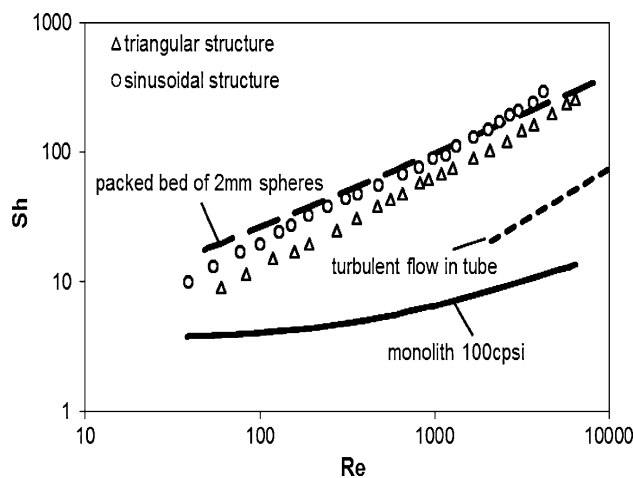


Fig. 3 Mass transfer for short-channel structures (selected experimental points) and monolith *tr* triangular structure, *sn* sinusoidal structure, *1* packed bed of 2 mm spheres, *2* monolith 100cps, *3* turbulent flow in tube

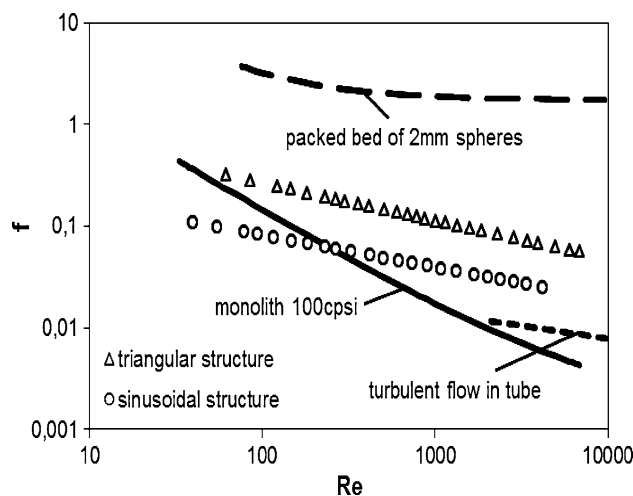


Fig. 4 Flow resistance for short-channel structures (selected experimental points) and monolith (selected experimental points) and monolith. *tr* triangular structure, *sn* sinusoidal structure, *1* packed bed of 2 mm spheres (Ergun model), *2* monolith 100cps (Hawthorne model [10]), *3* turbulent flow in tube (Blasius formula)

equation. In the case of the turbulent flow, the flow resistance results were obtained using Blasius equation and the mass transfer results were calculated using the classic equation applied for the turbulent flow in tube: $Sh = 0.023Re^{0.83}Sc^{0.44}$ [12] (similar formula, known as McAdams equation, operated for heat transfer).

As it is shown in Fig. 3 mass transfer for triangular and sinusoidal structures is one order of magnitude higher than those of monolith and comparable with the packed bed. It is noticeable that shortening the channel length (40 times) improved the mass transfer coefficient (Sherwood number) 2 till 30 times. The flow resistance for short-channel structures almost comparable with monolith was rated as a success.

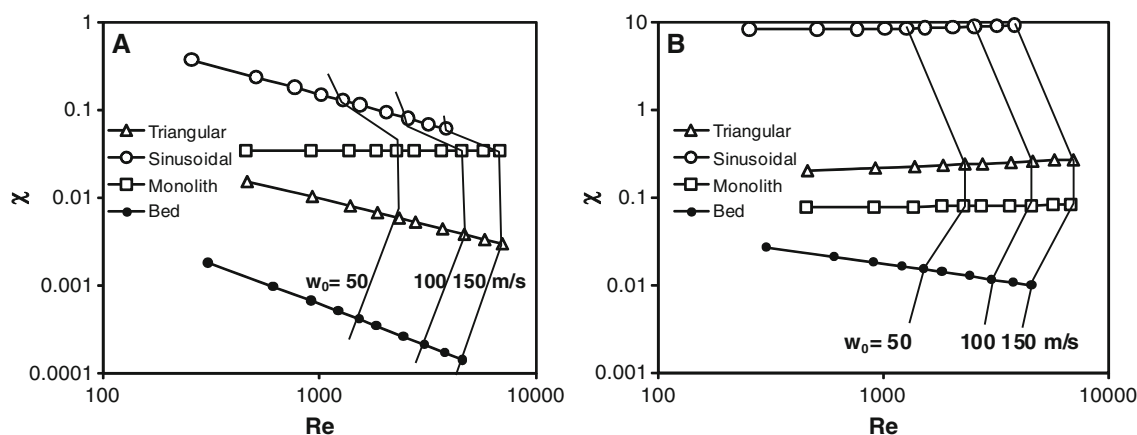


Fig. 5 Efficiency criterion χ versus Re number: **a** for the kinetics of Bennet et al. [13], χ defined by eq. (9), **b** for very fast kinetics, χ defined by eq. (10). Thin solid lines connect points of specified gas velocity w_0

It is not easy to compare the particular solutions considering both transfer properties and pressure drop. The efficiency criteria proposed in [2] enable to compare structure taking into account flow resistance, mass transfer and reaction kinetics. For an arbitrary kinetics, the criterion χ is defined:

$$\chi = \frac{k_c a}{1 + k_c/k_r} \frac{D_h}{4w_0 f} \quad (9)$$

and for very fast kinetics ($k_r \rightarrow \infty$)

$$\chi = \frac{k_c \varepsilon}{w_0 f} \quad (10)$$

The details are presented in [2]. The comparison of the efficiencies for the both cases presented above is shown in Fig. 5. In the Figure, the corresponding gas velocities are shown in the form of diagram. The experiments were performed at temperature close to the ambient one and with gas velocities up to 50 m/s. When considering typical engine exhaust conditions (400 °C), the experimentally studied Re range (Table 1) covers linear velocities up to 150 m/s.

For the kinetics of Bennett et al. [13], sinusoidal short-channel structure displays the highest efficiency, next classic monolith and triangular structure. However, for very fast kinetics kinetics ($k_r \rightarrow \infty$) the best in again sinusoidal structure, next the triangular one and monolith. Fast reaction kinetics is advantageous to short-channel structures. The packed bed displays the worst efficiency for both cases considered.

4 Conclusions

Pioneering transfer and friction experimental study was performed on short-channel structures that operated at very

high gas velocities, about 50 m/s (laminar and transient flow). Friction factors and Nusselt (Sherwood) numbers were experimentally measured and correlated as functions of dimensionless channel length. The correlations covered both laminar developing flow and transient flow ranges with satisfactory accuracy. The heat (mass) transfer correlations were based on the theoretically derived solutions for developing laminar flow supplemented by experimentally derived correction terms.

Short-channel structures display highly enhanced transfer properties in comparison with classic monoliths under high gas velocities. Nusselt (Sherwood) numbers are over one order of magnitude higher. Particularly, heat (or mass) transfer properties of sinusoidal structure are promising within transient region. The transfer properties enhanced by up to 30 times are paid by only moderate increase in flow resistance.

The efficiencies of the short-channel structures, particularly of the sinusoidal ones, are excellent, especially for very fast kinetics. The short-channel structures seem very efficient solution for the pre-turbo catalytic converter.

Acknowledgments This study was supported by the grants from the Polish National Science Centre (Grants N N523 556638 and N N209 119137) and by the project from Polish Science Foundation financed by EU structural funds (BRIDGE).

Open Access This article is distributed under the terms of the Creative Commons Attribution License which permits any use, distribution, and reproduction in any medium, provided the original author(s) and the source are credited.

References

1. More H, Mmbaga J, Hayes RE, Votsmeier M, Checkel MD (2007) Top Catal 42–43:429
2. Kołodziej K, Łojewska J (2007) Chem Eng Process 46:637

3. Kołodziej K, Łojewska J, Ochońska J, Łojewski T (2011) *Chem Eng Process* 50:869
4. Shah RK, London AL (1978) *Laminar flow forced convection in ducts*. Academic Press, New York
5. Fleming DP, Sparow EM (1969) *J Heat Transf* 91:345
6. Shah RK (1975) *Int J Heat Mass Transf* 18:849
7. Kołodziej A, Łojewska J (2009) *Catal Today* 147S(suppl):S120
8. Iwaniszyn M, Jaroszyński M, Ochońska J, Łojewska J, Kołodziej A (2011) *Scientific Publications of ICh PAN* 15:37 (available at: [http://www.iich.gliwice.pl/files/303/Zeszyt%2015%20\(2011\).pdf](http://www.iich.gliwice.pl/files/303/Zeszyt%2015%20(2011).pdf) pages 37–46) Accessed 5 Feb 2013
9. Wibulswas P (1966) *Laminar-Flow Heat-Transfer in Non-Circular Ducts*. Ph.D. Thesis, London University, London, 1966
10. Hawthorn RD (1974) Afterburner catalysis—effects of heat and mass transfer between gas and catalyst surface, *AIChE Symp. Ser.* 70(137):428
11. Wakao N, Kaguei S (1982) *Heat and mass transfer in packed beds*. Girdon and Breach Science Publisher, New York
12. Gilliland ER, Sherwood TK (1934) *Ind Eng Chem* 26:516, 26:1093
13. Bennett CJ, Kolaczowski AT, Thomas WJ (1991) *Trans Inst Chem Eng B* 69:209