

# **Review of Image Quality Measures for Solar Imaging**

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Received: 24 April 2017 / Accepted: 16 November 2017 / Published online: 5 December 2017 © The Author(s) 2017. This article is published with open access at Springerlink.com

Abstract Observations of the solar photosphere from the ground encounter significant problems caused by Earth's turbulent atmosphere. Before image reconstruction techniques can be applied, the frames obtained in the most favorable atmospheric conditions (the socalled lucky frames) have to be carefully selected. However, estimating the quality of images containing complex photospheric structures is not a trivial task, and the standard routines applied in nighttime lucky imaging observations are not applicable. In this paper we evaluate 36 methods dedicated to the assessment of image quality, which were presented in the literature over the past 40 years. We compare their effectiveness on simulated solar observations of both active regions and granulation patches, using reference data obtained by the Solar Optical Telescope on the Hinode satellite. To create images that are affected by a known degree of atmospheric degradation, we employed the random wave vector method, which faithfully models all the seeing characteristics. The results provide useful information about the method performances, depending on the average seeing conditions expressed by the ratio of the telescope's aperture to the Fried parameter,  $D/r_0$ . The comparison identifies three methods for consideration by observers: Helmli and Scherer's mean, the median filter gradient similarity, and the discrete cosine transform energy ratio. While the first method requires less computational effort and can be used effectively in virtually any atmospheric conditions, the second method shows its superiority at good seeing  $(D/r_0 < 4)$ . The third method should mainly be considered for the post-processing of strongly blurred images.

**Keywords** Earth's atmosphere: atmospheric seeing · Instrumentation and data management · Instrumental effects · Turbulence

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## 1. Introduction

Ground-based telescopes suffer from the degradation of image quality caused by the turbulent nature of Earth's atmosphere. This phenomenon, frequently termed "seeing", prevents large-aperture telescopes from achieving their theoretical angular resolution. Even the best observing sites do not allow for observations in the visible with a resolution higher than the diffraction limit of a 20 cm telescope. This means that long exposures of both very small and extremely large telescopes show the same angular resolution.

The Fried parameter,  $r_0$ , is a quantity that describes the average atmospheric conditions. The Fried parameter is the distance across which the expected change of the wavefront phase is exactly  $1/2\pi$ . It may also be understood as the size of the telescope's aperture over which the theoretical diffraction limit may be easily achieved. Since at the best observational sites  $r_0$  rarely reaches 20 cm in the visible ( $\lambda = 0.5 \mu m$ ; Socas-Navarro *et al.*, 2005), the long exposures obtained from any telescope do not expose a resolution higher than is reached by a 20 cm telescope. Importantly, the  $D/r_0$  ratio is frequently used to determine how far away the resolution of images obtained by a telescope of D diameter is from its theoretical diffraction limit.

So far, numerous techniques, both hardware and software based, have been developed to enhance the resolution of astronomical observations. Probably the most prominent hardware-based approach is adaptive optics (AO; Hardy, 1998), in which the compensation of wavefront distortions is performed directly by a deformable mirror. The AO for solar imaging differs from the method used in nighttime observations (Rimmele and Marino, 2011; Rimmele, 2004). There is no point-like object for wavefront sensing, which is usually performed with a Shack–Hartmann sensor. Instead, the cross correlation between images observed in individual sub-apertures has to be calculated to estimate the shape of the wavefront (Löfdahl, 2010). Significantly poorer daytime atmospheric conditions place much higher demands on the updating frequency of a deformable mirror. Fortunately, there is also more light available for the sensors, which enables these observations.

A popular example of a software-based approach to improve the quality of images is the method called lucky imaging (LI; Scharmer, 1989; Law, Mackay, and Baldwin, 2006). Owing to the availability of very fast and low-noise cameras, this method has recently become a very popular high-resolution acquisition technique in the visible. However, it is dedicated to smaller telescopes (< 2 m), since it relies on the fact that there is only a small chance to obtain a diffraction-limited image in a series of very short exposures (*i.e.* shorter than the coherence time of the atmosphere – usually up to several milliseconds). This chance, estimated by Fried (1978), is relatively high for smaller apertures (*e.g.*  $D/r_0 < 2$ ), while it quickly becomes negligible for greater mirrors.

There are many combinations of software and hardware techniques of high-resolution imaging. As an example, Colodro-Conde *et al.* (2017) or Mackay *et al.* (2012) presented the fusion of LI and adaptive optics (AOLI). In Schödel and Girard (2012), the deconvolution of a series of short exposures was shown as another possible way to enhance the quality of astronomical images. A wide range of speckle-interferometry methods is also available (Saha, 2007; Tokovinin and Cantarutti, 2008). They involve approaches such as aperture masking (Monnier *et al.*, 2004; Ireland, 2013) or speckle bispectral reconstructions (Lohmann, Weigelt, and Wirnitzer, 1983; Hofmann and Weigelt, 1993). Some of them have been successfully used for a long time in solar imaging (von der Lühe, 1993).

Whether with or without AO, the observer acquires a series of images and then applies several post-processing steps (*e.g.*, Denker *et al.*, 2005). One step is always the selection of best exposures, *i.e.* those with the highest image quality. Such LI has been very popular

for a long time in ground-based solar observatories because of its apparent simplicity and very low hardware requirements (only a fast camera is necessary; Beckers, 1989). However, the most advanced imagers that use lucky exposures are far from being simple (Ferayorni *et al.*, 2016). The rejection of less useful frames is possible as a result of the high intensity of the observed object, which allows for acquiring thousands of exposures *per* second at relatively low resolution or tens of frames if large-format cameras are used. The selection is also essential to reach the high quality of final outcomes, regardless of the complexity of the succeeding image reconstruction (*e.g.* simple stacking, deconvolution, or bispectral analysis).

The assessment of the temporal quality of the registered solar images becomes challenging because the character of the observed scene is complex. It is impossible to use a basic quality metric that is frequently used in LI – the intensity of the brightest pixel in a speckle pattern – as it requires a well-isolated point-like object (star). Instead, a widely employed method for the quality assessment of solar images is the root-mean-square contrast (rms contrast), which assumes the uniform isotropic properties of granulation (Danilovic *et al.*, 2008; Denker *et al.*, 2005; Scharmer *et al.*, 2010). Unfortunately, the method has several drawbacks, such as a significant dependency of its effectiveness on the wavelength (Albregtsen and Hansen, 1977) and the sensitivity to the structural contents of the image (Deng *et al.*, 2015). This implies that the tip-tilt effects, which move the observed patch and thus slightly change its contents, will also introduce additional noise into the quality estimation because image features such as sunspots or pores will move in and out of the analyzed region.

Motivated by a recent work by Deng *et al.* (2015), who introduced an objective image quality metric to solar observations, we decided to explore which of the numerous quality metrics (QMs) available in the literature can be employed to select solar frames. This was carried out by investigating the correlation between the outcomes of QMs and the known strength of the simulated turbulence. Our review includes 36 QMs with many varying implementations. Implementations refer to different gradient operators, kernel sizes, thresholding techniques, *etc.*, without implying conceptual changes. We use reference images from the *Solar Optical Telescope* (SOT: Tsuneta *et al.*, 2008) on board the *Hinode* satellite and use an advanced method for modeling atmospheric turbulences, the random wave vector (RWV, Voitsekhovich *et al.*, 1999) method. The scintillation noise is also included to faithfully reflect all the seeing characteristics. Moreover, we check the computational efficiency of the QMs to indicate which methods are more suitable for application in high-speed real-time image processing.

# 2. Experiment

# 2.1. Turbulence Simulation

Since observations from space are not disturbed by the atmosphere, we used images obtained with the SOT as reference data for our experiments. From a wide range of registered images in the *Hinode* database,<sup>1</sup> we selected a range that contained several regions of enhanced magnetic field (sunspots). The image was originally obtained at the green continuum wavelength, on 29 November 2015 at 21:19:44 UT. In Figure 1 we show the selected reference image and indicate the positions of six extracted  $100 \times 100$ -pixel patches, (roughly

<sup>&</sup>lt;sup>1</sup>*Hinode* database query form is available at http://darts.isas.jaxa.jp/solar/hinode/query.php.

Figure 1 Part of the solar photosphere imaged by the *Hinode* satellite. The six patches  $(W1-W6, 100 \times 100 \text{ pixels})$ extracted for the experiment are indicated. Three of them (W1, W2, W3) contain parts of active regions, while the remaining ones (W4, W5, W6) include only granulation. The image was obtained in the green continuum on 29 November 2015 at 21:19:44 UT.



 $5'' \times 5''$  each, image scale of 0.054'' pixel<sup>-1</sup>). Patches W1, W2, and W3 include sunspots, while W4, W5, and W6 contain granulation.

To investigate the response of various QMs for a given turbulence strength, we modeled the transfer function of the atmosphere using the RVW method. The method allows for reliable modeling of amplitude and phase fluctuations of the incoming optical wavefront. Since a patch of the solar photosphere that is used for quality assessment can be arbitrarily small, we assumed that it is within the isoplanatic angle. Thus, anisoplanatic effects, which are more complicated to simulate, were neglected in this study. Using the RVW, we generated 1000 blurring kernels (speckles patterns) for ten distinctive seeing condition scenarios:  $D/r_0 = 1, 2, \dots, 10$ . We assumed that this range is representative for observations at the best observing sites. Each generated kernel consisted of  $1024 \times 1024$  pixels, and the resolution was twice higher than required by the Nyquist limit, *i.e.* a single pixel corresponded to an angular size of  $\lambda/4D$  ( $\lambda$  – wavelength, D – telescope diameter). We opted for this oversampling to be able to combine simulated speckle kernels with reference *Hinode* images. Each blurring kernel was normalized so that the summed intensity over all pixels was unity. Exemplary kernels with the corresponding long-exposure seeing disks are presented in Figure 2. Evidently, the poorer the seeing conditions (higher  $D/r_0$ ), the more complex the kernel shape. The simulated tip-tilt effect is also visible as a displacement of the kernel centroid.

Atmospheric scintillation results in a varying attenuation of the flux that is collected by a telescope. This type of noise was recently investigated by Osborn *et al.* (2015). The authors presented the following formula for estimating the relative variance of the total intensity of the observed object:

$$\sigma_s = \sqrt{10^{-5} C_{\gamma}^2 D^{-4/3} t_e^{-1} (\cos \gamma)^{-3} \exp(-2h_{\rm obs}/H)},\tag{1}$$



**Figure 2** Exemplary blurring kernels (negatives) employed in the experiment. The rows correspond to various  $D/r_0$  relative atmospheric conditions, while the last column exposes the simulated long-exposure seeing disk (*i.e.* an ensemble average over all the kernels for a given  $D/r_0$ ). Each kernel is presented in a box with a side length of  $40\lambda/D$ . The auxiliary *gray lines* indicate the box center, highlighting the simulated tip-tilt effect.

where *D* is telescope diameter,  $\gamma$  is the zenith distance,  $h_{obs}$  is the altitude of the observatory, *H* is the scale height of the atmospheric turbulence, generally assumed to be ~ 8000 m, and  $C_Y$  is the scaling coefficient, which can be determined from turbulence profilers (SCIDARs) and was estimated to lie between 1.30–1.67 for the best observing sites (see Table 1 in Osborn *et al.*, 2015).

To include these fluctuations in our simulated images, we multiplied each kernel by a random variable with an expected value of unity and a standard deviation equal to  $\sigma_s$ . We assumed that 1) a telescope size D = 0.5 m according to the size of *Hinode/SOT* instrument, 2) observations made at a zenith distance of  $\gamma = 60^\circ$ , and 3) a low scintillation index,  $C_y = 1.5$ , which is expected for 4) a high-altitude observatory,  $h_{obs} = 3000$  m. For these conditions, the relative scintillation noise is  $\sigma_s = 0.032$ .

To properly convolve a blurring kernel with a reference patch, the scale of a kernel has to be the same as the image scale. For the assumptions given above, *i.e.* a D = 0.5 m telescope observing at  $\lambda = 550$  nm, we obtain an image scale of 0.055'' pixel<sup>-1</sup>. This means that the sampling of the blurring kernels  $(D/4\lambda)$  and the assumed telescope size allow for convolving kernels with the *Hinode* images without any prescaling. Several examples of solar images degraded by simulated blurring kernels are presented in Figure 3.

The time-dependent quality, when observing stellar objects, can be determined from the relative intensity of the brightest pixel in the normalized kernel. This is a widely accepted approach to select the sharpest frames in nighttime LI (Law, Mackay, and Baldwin, 2006). However, in our case, the object is not point-like and shows complex structures. Thus, we decided to use the quality measure based on the amount of energy preserved from the original frequency spectrum. Since the original image is convolved with a blurring kernel and the original amplitudes in the frequency spectrum are multiplied by the amplitudes of a kernel, the value of the proposed quality measure can be calculated by summing squared amplitudes

Figure 3 Exemplary simulated images for all six patches (*rows*) and four selected degrees of atmospheric turbulence,  $D/r_0 = 1, 4, 7$ , and 10 (*columns*).



in a 2D Fourier transform of a kernel. According to Parseval's theorem, this is also equal to the sum of squared intensities of a kernel directly in the image plane.

Since turbulence is a random process, it is also possible that the temporal seeing conditions will become much better or much worse than indicated by the average  $D/r_0$  (Fried, 1978). This is in fact what we also observed in our data. For all ten sets of simulated kernels ( $D/r_0 = 1, 2, ..., 10$ ), the spread of temporal quality is shown in the histograms in Figure 4. In the right part of Figure 4, we plot the amount of preserved energy of the original image over all 1000 kernels for four values of  $D/r_0$ . Clearly, the quality for the average  $D/r_0 = 3$  can sometimes outperform the conditions registered at  $D/r_0 = 1$ . Therefore,  $D/r_0$ expresses only the average blurring strength, while it cannot be taken as a reliable estimator of the quality of individual frames.

#### 2.2. Methods

A set of 35 state-of-the-art QMs was provided in the review of Pertuz, Puig, and Garcia (2013). The authors considered the most popular methods dedicated to the assessment of the focus in complex scenes by means of contrast measurement. The methods can be categorized into six families of operators, based on gradients (GRA), Laplacians (LAP), wavelets (WAV), intensity statistics (STA), discrete-cosine transform (DCT), and the miscellaneous methods (MIS), *i.e.* those that cannot be categorized into any other group. An overview of the methods with their abbreviations and references is given in Table 1.

Within the set of techniques, we can find the most popular method used in solar image processing, *i.e.* the rms-contrast measure, which was called normalized gray-level variance and is abbreviated STA5 (we follow this nomenclature). The most recent QM proposed



**Figure 4** Dependencies of temporal turbulence strength expressed by the maximum intensity in a normalized blurring kernel on the average seeing conditions  $D/r_0$ . *Left*: amount of preserved image energy for four 1000-kernel sets  $D/r_0 = 1, 3, 5, \text{ and } 7$ . *Right*: histograms of the preserved image energy over all the simulated kernels.

by Deng *et al.* (2015), the median filter gradient similarity (GRA8), was included in our comparison as well.

To improve the effectiveness of QMs for solar observations, we had to adjust the parameters of many techniques. This was carried out experimentally by tuning the parameter, considering the properties of the observed solar scene and analyzing the algorithm details. Moreover, for some of the methods, we proposed major, but still simple, modifications, which allowed enhancing their effectiveness. This resulted in the creation of various implementations of most of the methods (labeled versions A, B, *etc.*). The set of investigated parameter values and/or the details of the applied modifications are given in Table 2. The distance parameters, such as radius or size of the local filtering window, are expressed in pixels (in our case, 1 pixel = 0.055''). The thresholds are given in relative values, which means that before applying thresholding, the intensities in a patch were normalized such that the intensities cover the range from zero to unity. Several methods have two adjustable parameters, therefore we evaluated various combinations of their values. Including all the modifications, we obtained a total number of 105 implementations of 36 techniques, which are included in our comparison.

#### 2.3. Data Analysis

To assess the performance of all methods, we investigated the correlation between the results of QMs and the actual expected quality Q. As stated before, the quality was estimated by the total preserved energy with respect to the reference undisturbed image. We observed that the relation between these two quantities is almost always nonlinear. Fortunately, it is sufficient that the dependency is monotonic as it allows us to distinguish between better and poorer atmospheric conditions. To estimate the effectiveness of the methods, instead of Pearson's correlation coefficient, we therefore used the Spearman rank-order correlation  $C_s$ . This coefficient is insensitive to any nonlinearities in the observed dependencies.

As an example, we show in the upper panel of Figure 6 the significantly different dependencies between the expected quality Q and the outcomes of two QMs (LAP1 and MISB, on the left and right side, respectively) calculated for image patch W1. Each set of  $D/r_0$  is presented with a different marker/color. We decided to calculate the Spearman correlation Table 1Overview of quality measures.

Abbr.	Operator name	Citation			
Miscellaneous	operators (MIS*)				
MIS1	Absolute central moment	Shirvaikar (2004)			
MIS2	Brenner's focus measure	Brenner et al. (1976)			
MIS3	Image contrast	Nanda and Cutler (2001)			
MIS4	Image curvature measure	Helmli and Scherer (2001)			
MIS5	Helmli and Scherer's mean	Helmli and Scherer (2001)			
MIS6	Local binary pattern measure	Lorenzo et al. (2008)			
MIS7	Steerable filter-based measure	Minhas et al. (2009)			
MIS8	Spatial frequency measure	Malik and Choi (2008)			
MIS9	Vollath's autocorrelation	Vollath (1987)			
Gradient-based	l operators (GRA*)				
GRA1	Gaussian derivative	Geusebroek et al. (2000)			
GRA2	Gradient energy	Subbarao, Choi, and Nikzad (1993)			
GRA3	Thresholded gradient	Santos (1997), Chern, Neow, and Ang (2001)			
GRA4	Squared gradient	Geusebroek et al. (2000)			
GRA5	3D gradient	Ahmad and Choi (2007)			
GRA6	Tenengrad	Tenenbaum (1971), Schlag et al. (1983)			
GRA7	Tenengrad variance	Pech-Pacheco et al. (2000)			
GRA8	Median filter gradient similarity	Deng et al. (2015)			
Laplacian-base	ed operators (LAP*)				
LAP1	Energy of Laplacian	Subbarao, Choi, and Nikzad (1993)			
LAP2	Modified Laplacian	Nayar and Nakagawa (1994)			
LAP3	Diagonal Laplacian	Thelen <i>et al.</i> (2009)			
LAP4	Variance of Laplacian	Pech-Pacheco et al. (2000)			
Wavelet-based	operators (WAV*)				
WAV1	Sum of wavelet coefficients	Yang and Nelson (2003)			
WAV2	Variance of wavelet coefficients	Yang and Nelson (2003)			
WAV3	Ratio of wavelet coefficients	Xie, Rong, and Sun (2006)			
WAV4	Ratio of curvelet coefficients	Minhas et al. (2009)			
Statistics-base	d operators (STA*)				
STA1	Chebyshev moment-based	Yap and Raveendran (2004)			
STA2	Eigenvalue-based	Wee and Paramesran (2007)			
STA3	Gray-level variance	Groen, Young, and Ligthart (1985)			
STA4	Gray-level local variance	Pech-Pacheco et al. (2000)			
STA5	Normalized gray-level variance	Groen, Young, and Ligthart (1985)			
STA6	Modified gray-level variance	Pertuz, Puig, and Garcia (2013)			
STA7	Histogram entropy	Firestone et al. (1991)			
STA8	Histogram range	Firestone et al. (1991)			
DCT-based op	erators (DCT*)				
DCT1	DCT energy ratio	Shen and Chen (2006)			
DCT2	DCT reduced energy ratio	Lee <i>et al.</i> (2009)			
DCT3	Modified DCT	Lee et al. (2008)			

Method	Variants	Description	
Miscellaneous op	perators (MIS*)		
MIS1	A-D	number of bins in a histogram of image intensities (L) $L = \{50, 100, 256, 1000\}$	
MIS2	А	only horizontal gradient	
	В	only vertical gradient	
	С	maximum of the vertical and horizontal gradients	
	D-G	sum of vertical and horizontal gradients with thresholding ( <i>T</i> ) $T = \{0, 0.01, 0.1, 0.5\}$	
MIS3	-	-	
MIS4	-	-	
MIS5	A-C	window size $(w)$ $w = \{3, 7, 15\}$	
MIS6	A-D	radius of the circle in LBP operator $(r)$ number of equally spaced pixels on the circle $(n)$ $(r, n) = \{(1, 8), (1, 16), (2, 8), (2, 16)\}$	
MIS7	A-H	size of the Gaussian mask $(N)$ standard deviation of the Gaussian $(\sigma)$	
		$(N, \sigma) = \{(7, 2), (7, 5), (7, 10), (7, 15), (15, 2), (15, 5), $	
		(15, 10), (15, 15)}	
MIS8-9	-	-	
Gradient-based o	perators (GRA*)		
GRA1	A-F	size of the Gaussian mask (N) standard deviation of the Gaussian ( $\sigma$ ) (N, $\sigma$ ) = {(7, 2), (7, 5), (7, 10), (15, 2), (15, 5), (15, 10)}	
GRA2	_	-	
GRA3	А	maximum of the horizontal and vertical gradients	
	B - F	horizontal gradient bigger than a threshold $(T)$ $T = \{0.0, 0.01, 0.05, 0.1, 0.5\}$	
	G-K	horizontal and vertical gradients bigger than a threshold $(T)$ $T = \{0.0, 0.01, 0.05, 0.1, 0.5\}$	
GRA4-7	_	-	
GRA8	А	horizontal gradient and constant window size $(w = 3)$	
GRA8	В	vertical gradient and constant window size ( $w = 3$ )	
GRA8	C-F	horizontal and vertical gradient and window size $w = \{3, 5, 7, 11\}$	
Laplacian-based	operators (LAP*)		
LAP1-4	_	-	
Wavelet-based or	perators (WAV*)		
WAV1	А	1-level DWT with Daubechies-6 filters	
	В	2-level DWT and Daubechies-10 filters	
WAV2	А	1-level DWT with Daubechies-6 filters	
	В	2-level DWT and Daubechies-10 filters	
WAV3-4	_	-	

 Table 2
 Parameters and modifications of the quality measures compared in the experiment. Some methods do not have any parameters, thus they were left blank.

Method	Variants	Description	
Statistics-base	d operators (STA*)		
STA1	A-E	order of Chebyshev polynomials $(p)$ $p = \{2, 3, 4, 5, 6\}$	
STA2	A-E	number of diagonal elements from the matrix of eigenvalues (k) $k = \{1, 3, 5, 7, 9\}$	
STA3	_	-	
STA4	A-E	size of the window in which the local variance is computed ( <i>w</i> ) $w = \{3, 5, 7, 11, 15\}$	
STA5	_	-	
STA6	A-E	size of the window in which the local mean is computed (w) $w = \{3, 5, 7, 11, 15\}$	
STA7	A-D	number of bins in image intensity histogram (L) $L = \{50, 100, 256, 1000\}$	
STA8	A-D	percent of pixels removed from the histogram ( $\alpha$ ) $\alpha = \{0, 0.01, 0.02, 0.05\}$	
DCT-based op	erators (DCT*)		
DCT1	A-C	size of image sub-block $w = \{4, 8, 16\}$	
DCT2	A-C	size of image sub-block $w = \{4, 8, 16\}$	
DCT3	_	-	

 Table 2 (Continued)

coefficient in two ways: 1) within a set of observations for each  $D/r_0$ , and 2) across all the simulated conditions  $D/r_0 = 1-10$ . We present the corresponding results of  $C_s$  in each  $D/r_0$  subset in the bar plots of Figure 6. The correlation depends on  $D/r_0$  so that it becomes apparent which range of atmospheric conditions is most suitable for a given method. For example, the LAP1 method allows for an effective estimation of the image quality in  $D/r_0 = 1$ , while MIS1B is completely useless in this range. The proposed approach to calculate the correlation coefficient permitted estimating the performance of each method for a range of typical atmospheric conditions.

In the example presented in Figure 6, the superiority of LAP1 over MIS1B is also visible for  $C_s$  calculated over the whole set of  $D/r_0$ . However, the difference is significantly smaller than in particular groups as both methods achieve  $C_s > 0.9$  (0.98 and 0.90 for LAP1 and MIS1B, respectively). This is due to the wide range of considered Q values, which makes the correlation between the quantities more evident and leads to the higher value of the  $C_s$ coefficient. Although the differences are not so significant, the correlation for such a wide range of Q values still allows for a comparison of the overall effectiveness of QMs, but within a much narrower range of  $C_s$  values.

#### 2.4. Results and Discussion

The results of the comparison are presented in Figure 5 and Figure 7. While in Figure 5 we present only the best four methods for each  $D/r_0$ , the average performance obtained for whole QM families is summarized in Figure 7. We divided the results into two categories, according to the contents of the observed image: W1, W2, and W3 show active regions, and W4, W5, and W6 have granulation.



**Figure 5** Ranking of the best-quality measures for various  $D/r_0$  seeing conditions and six analyzed patches: W1, W2, and W3 show active regions, and W4, W5, and W6 have granulation areas. The lower bar plots show the rankings for wide-range correlation across all atmospheric conditions  $D/r_0 = 1-10$ .



**Figure 6** Examples of the correlation between the measured and expected image quality for two distinct methods: LAP1 on the *left side*, and MIS1B on the *right side*. The analysis was performed for image patch W1. The calculated correlation coefficients in each  $D/r_0$  set and over the whole data set  $(D/r_0 = 1-10)$  are presented in the lower bar plots.



Figure 7 Average correlation coefficients obtained for the QM families. The *left panel* corresponds to the results for active regions, while the *right panel* shows the outcomes for granulation patches.

According to the results presented in Figure 5, there is no single winner that would cover all possible atmospheric conditions and scene characteristics. However, three techniques performed distinctively better, and they are therefore discussed below.

One of the methods with a very impressive performance is Helmli and Scherer's mean method (MIS5), proposed by Helmli and Scherer (2001). This technique provided very good results for the whole range of  $D/r_0$  conditions and both types of observed solar regions. For all atmospheric conditions it was always among the four best methods. As indicated by the distinctively higher correlation coefficients calculated over  $D/r_0 = 1-10$ , its usefulness should be considered when the seeing varies strongly or is unknown. In summary, this method should be the first choice of all techniques we tested.

The second noteworthy method is the median filter gradient similarity (GRA8) method, which was recently proposed by Deng *et al.* (2015). It shows the best performance for very good atmospheric conditions ( $D/r_0 < 4$ ). However, to achieve high effectiveness, we had to slightly modify the method by 1) combining both horizontal and vertical gradients, and 2) changing the window size. The superiority of the method is evident especially for active regions (W1–W3), while it is slightly less efficient when assessing only granulation patches (W4–W6), especially for  $D/r_0 > 2$ . Interestingly, this technique was not included in the best 12 methods indicated by wide-range correlations,  $D/r_0 = 1-10$ , which indicates that it should not be applied for observations with poor or unknown atmospheric conditions. The results of the GRA8 method recommend it to be used in AO-assisted observations since in this case the image quality is significantly higher and the effective  $D/r_0$  is small.

The last method that provides good results is the DCT energy ratio proposed by Shen and Chen (2006). Its performance is the highest for moderate and poor atmospheric conditions when observing granulation regions. This method is the second best method when the whole range of  $D/r_0$  is taken into account for patches W4–W6. The parameter of this method, that is, the size of the sub-block, should be selected according to the blurring strength, *i.e.*, the larger  $D/r_0$ , the larger the sub-block.

The method that is frequently used in solar observations, rms contrast or normalized gray-level variance (STA5), showed a surprisingly poor performance. Since the rms-contrast measure was originally developed for granulation regions, with isotropic and uniform characteristics, we investigated how the method performed for this scenario. The results presented in Figure 8 indicate that the technique indeed allows achieving significantly higher correlation values for granulation. Still, the outcomes based on rms contrast were much less correlated with the expected image quality than the results achieved by the best techniques. Therefore, it did not appear in any ranking presented in Figure 5. Our conclusions agree with the observations made by Deng *et al.* (2015), who also indicate a relatively low efficiency of the common rms-contrast measure.

Some interesting conclusions can be drawn from the average performance of each QM family presented in Figure 7. The Laplacian-based methods (LAP) show very good average correlation with  $D/r_0$  for both types of observed scenarios. While the LAP-based methods are indicated only several times in the rankings presented in Figure 5, they should still be considered as a base for new and better techniques. The greatest difference between the efficiency when changing from granulation to active regions can be observed in statistical methods (STA). This agrees well with the results shown in Figure 8 and appears to be due to the assumption made in STA methods that regions expose uniform properties across the observed field. The strange shape of the GRA dependency visible in the right plot of Figure 7 arises as a result of the characteristics of GRA8. As we stated before, the performance of this method increases significantly as  $D/r_0$  decrease. This behavior biases the average efficiency of the GRA family.





The possibility of using a method in real-time image selection can be especially important, as it allows for recording only the most useful data. For completeness of our comparison, we therefore measured the time required for processing a single image patch by each method. The evaluations were performed on a single core of IntelCore i7-3930K operating at 3.2 Ghz. The procedures were repeated  $10^4$  times to obtain the average execution time. The results are presented in Table 3, which lists the methods and their average computation time (single-image analysis) in seconds, alternately.

The results show that real-time frame selection for the assumed size of an image patch is possible for frame rates of more than 1000 fps for most of the analyzed methods. This can be not true, however, when large full-resolution frames need to be processed and/or when several image calibration steps have to be applied. For this case, the usage of graphics processing units (GPU) and accompanying optimization of a code should be considered. However, in our comparison we decided to perform measurements on a single CPU core, so that the further reduction of the execution time with a multi-core machine can be estimated. For most of the included methods, the analysis was performed independently in local subregions of the whole image, which makes them easily parallelized.

We observed that GRA8 requires visibly more computation time (> 0.01 s) than MIS5 (< 0.002 s). This is mostly due to the median filtering, which requires sorting pixels in a sliding window. This indicates that GRA8, compared to MIS5, would require more computing resources and/or better code optimization to operate at the high frame rates that are frequently used in solar observations. Unfortunately, the discrete cosine transform techniques (DCT1 and DCT2) have significantly higher execution times, which makes them useless for real-time computation. These methods should be considered only in post-processing. The fastest method was the one most frequently used in solar observations, STA5. Unfortunately, its mediocre performance is not compensated by the distinctively higher computational efficiency.

## 3. Conclusions

Image quality assessment is an integral part of observations of the solar photosphere and chromosphere. It is essential to precisely select only highest fidelity images before performing consecutive image reconstruction. Unfortunately, the complexity and variety of the

MIS1A         0.0020         MIS7H         0.0114         GRA8C         0.0388         STA6C         0.0026           MIS1B         0.0025         MIS8         0.0011         GRA8D         0.0752         STA6D         0.0021           MIS1C         0.0029         MIS9         0.0013         GRA8E         0.0082         STA6E         0.0023           MIS1D         0.0039         GRA1A         0.0050         GRA8F         0.0081         STA7A         0.0013           MIS2A         0.0010         GRA1B         0.0041         LAP1         0.0017         STA7D         0.0018           MIS2B         0.0011         GRA1C         0.0038         LAP2         0.0027         STA7C         0.0031           MIS2D         0.0023         GRA1E         0.0046         LAP4         0.0014         STA8A         0.00021           MIS2E         0.0024         GRA1F         0.0044         STA1A         0.0012         STA8B         0.0020           MIS2G         0.0017         GRA3A         0.0009         STA1C         0.0012         STA8D         0.0020           MIS3         0.0160         GRA3B         0.012         STA7A         0.562         MIS2G         0.0								
MIS1B         0.0025         MIS8         0.0011         GRA8D         0.0752         STA6D         0.0021           MIS1C         0.0029         MIS9         0.0013         GRA8E         0.0082         STA6E         0.0023           MIS1D         0.0039         GRA1A         0.0050         GRA8F         0.0081         STA7A         0.0013           MIS2A         0.0010         GRA1B         0.0041         LAP1         0.0017         STA7B         0.0018           MIS2B         0.0011         GRA1C         0.0038         LAP2         0.0027         STA7C         0.0031           MIS2D         0.0023         GRA1E         0.0046         LAP3         0.0014         STA8A         0.0006           MIS2E         0.0024         GRA1F         0.0044         STA1A         0.0012         STA8B         0.0021           MIS2E         0.0026         GRA2         0.0012         STA1B         0.0012         STA8D         0.0020           MIS3         0.0160         GRA3B         0.0012         STA1B         0.0012         DCT1A         7.8562           MIS4         0.0065         GRA3C         0.0013         STA2A         0.0060         DCT2A         5.56	MIS1A	0.0020	MIS7H	0.0114	GRA8C	0.0388	STA6C	0.0026
MIS1C         0.0029         MIS9         0.0013         GRA8E         0.0082         STA6E         0.0023           MIS1D         0.0039         GRA1A         0.0050         GRA8F         0.0081         STA7A         0.0013           MIS2A         0.0010         GRA1B         0.0041         LAP1         0.0017         STA7B         0.0018           MIS2B         0.0011         GRA1C         0.0038         LAP2         0.0027         STA7C         0.0031           MIS2D         0.0023         GRA1E         0.0046         LAP3         0.0014         STA8A         0.0006           MIS2E         0.0024         GRA1F         0.0046         LAP4         0.0012         STA8B         0.0021           MIS2F         0.0026         GRA2         0.0012         STA1B         0.0012         STA8D         0.0020           MIS3         0.0160         GRA3B         0.0012         STA1C         0.0012         DCT1A         7.8562           MIS4         0.0065         GRA3C         0.0013         STA2A         0.0060         DCT1C         8.0760           MIS58         0.0031         GRA3E         0.0011         STA2A         0.0058         DCT2A         5.56	MIS1B	0.0025	MIS8	0.0011	GRA8D	0.0752	STA6D	0.0021
MIS1D       0.0039       GRA1A       0.0050       GRA8F       0.0081       STA7A       0.0013         MIS2A       0.0010       GRA1B       0.0041       LAP1       0.0017       STA7B       0.0018         MIS2B       0.0011       GRA1C       0.0038       LAP2       0.0027       STA7C       0.0031         MIS2C       0.0006       GRA1D       0.0050       LAP3       0.0014       STA8A       0.0006         MIS2D       0.0023       GRA1E       0.0046       LAP4       0.0014       STA8A       0.0002         MIS2E       0.0024       GRA1F       0.0044       STA1A       0.0012       STA8B       0.0021         MIS2G       0.0017       GRA3A       0.0009       STA1C       0.0012       STA8D       0.0020         MIS3       0.0160       GRA3B       0.0012       STA1D       0.0012       DCT1A       7.8562         MIS4       0.0065       GRA3C       0.0013       STA2A       0.0060       DCT1C       8.0760         MIS5B       0.0013       GRA3E       0.0011       STA2B       0.0058       DCT2A       5.5642         MIS6A       0.0768       GRA3G       0.0020       STA2D       0.00	MIS1C	0.0029	MIS9	0.0013	GRA8E	0.0082	STA6E	0.0023
MIS2A       0.0010       GRA1B       0.0041       LAP1       0.0017       STA7B       0.0018         MIS2B       0.0011       GRA1C       0.0038       LAP2       0.0027       STA7C       0.0031         MIS2C       0.0006       GRA1D       0.0050       LAP3       0.0039       STA7D       0.0046         MIS2D       0.0023       GRA1E       0.0046       LAP4       0.0014       STA8A       0.0006         MIS2E       0.0024       GRA1F       0.0044       STA1A       0.0012       STA8B       0.0022         MIS2G       0.0017       GRA3A       0.0009       STA1C       0.0012       STA8D       0.0020         MIS3       0.0160       GRA3B       0.0012       STA1D       0.0012       DCT1A       7.8562         MIS4       0.0065       GRA3C       0.0013       STA1E       0.0012       DCT1B       6.5742         MIS5A       0.0027       GRA3F       0.0010       STA2A       0.0060       DCT1C       8.0760         MIS5B       0.0011       GRA3G       0.0011       STA2C       0.0058       DCT2A       5.5642         MIS6A       0.0768       GRA3G       0.0020       STA2D       0.00	MIS1D	0.0039	GRA1A	0.0050	GRA8F	0.0081	STA7A	0.0013
MIS2B       0.0011       GRA1C       0.0038       LAP2       0.0027       STA7C       0.0031         MIS2C       0.0006       GRA1D       0.0050       LAP3       0.0039       STA7D       0.0046         MIS2D       0.0023       GRA1E       0.0046       LAP4       0.0014       STA8A       0.0006         MIS2E       0.0024       GRA1F       0.0044       STA1A       0.0012       STA8B       0.0021         MIS2F       0.0026       GRA2       0.0012       STA1B       0.0012       STA8D       0.0020         MIS2G       0.0017       GRA3A       0.0099       STA1C       0.0012       DCT1A       7.8562         MIS4       0.0065       GRA3C       0.0013       STA1E       0.0012       DCT1A       7.8562         MIS5       0.0027       GRA3F       0.0013       STA2A       0.0060       DCT1C       8.0760         MIS55       0.0031       GRA3F       0.0011       STA2B       0.0058       DCT2A       5.5642         MIS6A       0.0768       GRA3F       0.0010       STA2C       0.0058       DCT3       0.0011         MIS6B       0.0855       GRA3H       0.0021       STA2B       0.005	MIS2A	0.0010	GRA1B	0.0041	LAP1	0.0017	STA7B	0.0018
MIS2C         0.0006         GRA1D         0.0050         LAP3         0.0039         STA7D         0.0046           MIS2D         0.0023         GRA1E         0.0046         LAP4         0.0014         STA8A         0.0006           MIS2E         0.0024         GRA1F         0.0044         STA1A         0.0012         STA8B         0.0022           MIS2F         0.0026         GRA2         0.0012         STA1B         0.0012         STA8D         0.0020           MIS2G         0.0017         GRA3A         0.0009         STA1C         0.0012         STA8D         0.0020           MIS3         0.0160         GRA3B         0.0012         STA1D         0.0012         DCT1A         7.8562           MIS4         0.0065         GRA3C         0.0013         STA2A         0.0060         DCT1C         8.0760           MIS5B         0.0031         GRA3E         0.0011         STA2B         0.0058         DCT2A         5.5642           MIS6A         0.0768         GRA3G         0.0020         STA2D         0.0056         DCT2C         7.7149           MIS6B         0.0855         GRA3I         0.0021         STA4E         0.0058         DCT3         0.	MIS2B	0.0011	GRA1C	0.0038	LAP2	0.0027	STA7C	0.0031
MIS2D       0.0023       GRA1E       0.0046       LAP4       0.0014       STA8A       0.0006         MIS2E       0.0024       GRA1F       0.0044       STA1A       0.0012       STA8B       0.0021         MIS2F       0.0026       GRA2       0.0012       STA1B       0.0012       STA8D       0.0022         MIS2G       0.0017       GRA3A       0.0009       STA1C       0.0012       STA8D       0.0020         MIS3       0.0160       GRA3B       0.0012       STA1D       0.0012       DCT1A       7.8562         MIS4       0.0065       GRA3C       0.0013       STA1E       0.0012       DCT1B       6.5742         MIS5A       0.0028       GRA3D       0.0013       STA2A       0.0060       DCT1C       8.0760         MIS5B       0.0031       GRA3E       0.0011       STA2B       0.0058       DCT2A       5.5642         MIS6A       0.0768       GRA3G       0.0020       STA2D       0.0056       DCT2C       7.7149         MIS6B       0.0855       GRA3H       0.0021       STA4B       0.0010       WAV1A       0.0099         MIS6D       0.8066       GRA3I       0.0025       STA3       0.0	MIS2C	0.0006	GRA1D	0.0050	LAP3	0.0039	STA7D	0.0046
MIS2E       0.0024       GRA1F       0.0044       STA1A       0.0012       STA8B       0.0021         MIS2F       0.0026       GRA2       0.0012       STA1B       0.0012       STA8C       0.0022         MIS2G       0.0017       GRA3A       0.0009       STA1C       0.0012       STA8D       0.0020         MIS3       0.0160       GRA3B       0.0012       STA1D       0.0012       DCT1A       7.8562         MIS4       0.0065       GRA3C       0.0013       STA1E       0.0012       DCT1B       6.5742         MIS5A       0.0028       GRA3D       0.0013       STA2A       0.0060       DCT1C       8.0760         MIS5B       0.0031       GRA3E       0.0011       STA2B       0.0058       DCT2A       5.5642         MIS5C       0.0027       GRA3F       0.0010       STA2C       0.0058       DCT2C       7.7149         MIS6B       0.0855       GRA3I       0.0021       STA2E       0.0056       DCT2C       7.7149         MIS6D       0.0806       GRA3I       0.0021       STA4B       0.0010       WAV1A       0.0099         MIS6D       0.0809       GRA3I       0.0025       STA3       0.	MIS2D	0.0023	GRA1E	0.0046	LAP4	0.0014	STA8A	0.0006
MIS2F       0.0026       GRA2       0.0012       STA1B       0.0012       STA8C       0.0022         MIS2G       0.0017       GRA3A       0.0009       STA1C       0.0012       STA8D       0.0020         MIS3       0.0160       GRA3B       0.0012       STA1D       0.0012       DCT1A       7.8562         MIS4       0.0065       GRA3C       0.0013       STA1E       0.0012       DCT1B       6.5742         MIS5A       0.0028       GRA3D       0.0013       STA2A       0.0060       DCT1C       8.0760         MIS5B       0.0031       GRA3E       0.0011       STA2B       0.0058       DCT2A       5.5642         MIS5C       0.0027       GRA3F       0.0010       STA2D       0.0056       DCT2C       7.7149         MIS6B       0.0855       GRA3H       0.0025       STA3       0.0010       WAV1A       0.0099         MIS6D       0.809       GRA3I       0.0021       STA4B       0.0040       WAV1A       0.0099         MIS6D       0.809       GRA3I       0.0021       STA4B       0.0040       WAV1A       0.0099         MIS7A       0.0135       GRA3K       0.0021       STA4B       0.00	MIS2E	0.0024	GRA1F	0.0044	STA1A	0.0012	STA8B	0.0021
MIS2G       0.0017       GRA3A       0.0009       STA1C       0.0012       STA8D       0.0020         MIS3       0.0160       GRA3B       0.0012       STA1D       0.0012       DCT1A       7.8562         MIS4       0.0065       GRA3C       0.0013       STA1E       0.0012       DCT1B       6.5742         MIS5A       0.0028       GRA3D       0.0013       STA2A       0.0060       DCT1C       8.0760         MIS5B       0.0021       GRA3E       0.0011       STA2B       0.0058       DCT2A       5.5642         MIS5C       0.0027       GRA3F       0.0010       STA2C       0.0058       DCT2C       7.7149         MIS6B       0.0855       GRA3H       0.0021       STA2E       0.0058       DCT3       0.0011         MIS6C       0.0806       GRA3I       0.0025       STA3       0.0010       WAV1A       0.0099         MIS6D       0.0809       GRA3K       0.0021       STA4B       0.0040       WAV1A       0.0015         MIS7A       0.0135       GRA3K       0.0021       STA4B       0.0040       WAV2A       0.016         MIS7D       0.036       GRA3I       0.0021       STA4B       0.00	MIS2F	0.0026	GRA2	0.0012	STA1B	0.0012	STA8C	0.0022
MIS3         0.0160         GRA3B         0.0012         STA1D         0.0012         DCT1A         7.8562           MIS4         0.0065         GRA3C         0.0013         STA1E         0.0012         DCT1B         6.5742           MIS5A         0.0028         GRA3D         0.0013         STA2A         0.0060         DCT1C         8.0760           MIS5B         0.0031         GRA3E         0.0011         STA2B         0.0058         DCT2A         5.5642           MIS5C         0.0027         GRA3F         0.0010         STA2C         0.0058         DCT2B         5.7970           MIS6A         0.0768         GRA3G         0.0020         STA2D         0.0056         DCT2C         7.7149           MIS6B         0.0855         GRA3H         0.0021         STA2E         0.0058         DCT3         0.0011           MIS6D         0.0809         GRA3I         0.0025         STA3         0.0010         WAV1A         0.0099           MIS6D         0.0809         GRA3I         0.0021         STA4B         0.0040         WAV2A         0.0150           MIS7A         0.0135         GRA4         0.0011         STA4B         0.0040         WAV2A         0	MIS2G	0.0017	GRA3A	0.0009	STA1C	0.0012	STA8D	0.0020
MIS4         0.0065         GRA3C         0.0013         STA1E         0.0012         DCT1B         6.5742           MIS5A         0.0028         GRA3D         0.0013         STA2A         0.0060         DCT1C         8.0760           MIS5B         0.0031         GRA3E         0.0011         STA2B         0.0058         DCT2A         5.5642           MIS5C         0.0027         GRA3F         0.0010         STA2C         0.0058         DCT2B         5.7970           MIS6A         0.0768         GRA3G         0.0020         STA2D         0.0056         DCT2C         7.7149           MIS6B         0.0855         GRA3H         0.0021         STA2E         0.0058         DCT3         0.0011           MIS6C         0.0806         GRA3I         0.0025         STA3         0.0010         WAV1A         0.0099           MIS6D         0.0809         GRA3J         0.0019         STA4A         0.0037         WAV1B         0.0143           MIS7A         0.0136         GRA4         0.0011         STA4B         0.0040         WAV2A         0.0150           MIS7B         0.0136         GRA4         0.0011         STA4D         0.0036         WAV3         0.	MIS3	0.0160	GRA3B	0.0012	STA1D	0.0012	DCT1A	7.8562
MIS5A         0.0028         GRA3D         0.0013         STA2A         0.0060         DCT1C         8.0760           MIS5B         0.0031         GRA3E         0.0011         STA2B         0.0058         DCT2A         5.5642           MIS5C         0.0027         GRA3F         0.0010         STA2C         0.0058         DCT2B         5.7970           MIS6A         0.0768         GRA3G         0.0020         STA2D         0.0056         DCT2C         7.7149           MIS6B         0.0855         GRA3H         0.0021         STA2E         0.0058         DCT3         0.0011           MIS6C         0.0806         GRA3I         0.0025         STA3         0.0010         WAV1A         0.0099           MIS7A         0.0135         GRA3K         0.0021         STA4B         0.0040         WAV1A         0.0099           MIS7A         0.0135         GRA3K         0.0021         STA4B         0.0040         WAV2A         0.0105           MIS7B         0.0136         GRA4         0.0011         STA4C         0.0047         WAV2B         0.0150           MIS7C         0.0141         GRA5         0.0079         STA4D         0.0036         WAV3         0	MIS4	0.0065	GRA3C	0.0013	STA1E	0.0012	DCT1B	6.5742
MIS5B         0.0031         GRA3E         0.0011         STA2B         0.0058         DCT2A         5.5642           MIS5C         0.0027         GRA3F         0.0010         STA2C         0.0058         DCT2B         5.7970           MIS6A         0.0768         GRA3G         0.0020         STA2D         0.0056         DCT2C         7.7149           MIS6B         0.0855         GRA3H         0.0021         STA2E         0.0058         DCT3         0.0011           MIS6D         0.0806         GRA3I         0.0025         STA3         0.0010         WAV1A         0.0099           MIS6D         0.0809         GRA3I         0.0021         STA4A         0.0037         WAV1B         0.0143           MIS7A         0.0135         GRA3K         0.0021         STA4B         0.0040         WAV2A         0.0105           MIS7B         0.0136         GRA4         0.0011         STA4C         0.0047         WAV2B         0.0150           MIS7C         0.0141         GRA5         0.0079         STA4D         0.0045         WAV2         0.0265           MIS7D         0.0129         GRA6         0.0030         STA4E         0.0045         WAVC         0.0	MIS5A	0.0028	GRA3D	0.0013	STA2A	0.0060	DCT1C	8.0760
MIS5C         0.0027         GRA3F         0.0010         STA2C         0.0058         DCT2B         5.7970           MIS6A         0.0768         GRA3G         0.0020         STA2D         0.0056         DCT2C         7.7149           MIS6B         0.0855         GRA3H         0.0021         STA2D         0.0058         DCT3         0.0011           MIS6C         0.0806         GRA3I         0.0025         STA3         0.0010         WAV1A         0.0099           MIS6D         0.0809         GRA3J         0.0019         STA4A         0.0037         WAV1B         0.0143           MIS7A         0.0135         GRA4         0.0021         STA4B         0.0040         WAV2A         0.0105           MIS7B         0.0136         GRA4         0.0011         STA4C         0.0047         WAV2B         0.0150           MIS7C         0.0141         GRA5         0.0079         STA4D         0.0045         WAV2         0.0265           MIS7D         0.0129         GRA6         0.0030         STA4E         0.0045         WAVC         0.0848           MIS7E         0.0107         GRA7         0.0023         STA6A         0.0019         MIS7F         0.010	MIS5B	0.0031	GRA3E	0.0011	STA2B	0.0058	DCT2A	5.5642
MIS6A         0.0768         GRA3G         0.0020         STA2D         0.0056         DCT2C         7.7149           MIS6B         0.0855         GRA3H         0.0021         STA2E         0.0058         DCT3         0.0011           MIS6C         0.0806         GRA3I         0.0025         STA3         0.0010         WAV1A         0.0099           MIS6D         0.0809         GRA3J         0.0019         STA4A         0.0037         WAV1B         0.0143           MIS7A         0.0135         GRA3K         0.0021         STA4B         0.0040         WAV2A         0.0105           MIS7B         0.0136         GRA4         0.0011         STA4C         0.0047         WAV2B         0.0150           MIS7C         0.0141         GRA5         0.0079         STA4D         0.0045         WAV3         0.0265           MIS7D         0.0129         GRA6         0.0030         STA4E         0.0045         WAVC         0.0848           MIS7E         0.0107         GRA7         0.0023         STA5         0.0005         MAVC         0.0848           MIS7F         0.0108         GRA8A         0.0072         STA6A         0.0016         MAVC         0.0848<	MIS5C	0.0027	GRA3F	0.0010	STA2C	0.0058	DCT2B	5.7970
MIS6B         0.0855         GRA3H         0.0021         STA2E         0.0058         DCT3         0.0011           MIS6C         0.0806         GRA3I         0.0025         STA3         0.0010         WAV1A         0.0099           MIS6D         0.0809         GRA3J         0.0019         STA4A         0.0037         WAV1B         0.0143           MIS7A         0.0135         GRA3K         0.0021         STA4B         0.0040         WAV2A         0.0105           MIS7B         0.0136         GRA4         0.0011         STA4C         0.0047         WAV2B         0.0150           MIS7C         0.0141         GRA5         0.0079         STA4D         0.0036         WAV3         0.0265           MIS7D         0.0129         GRA6         0.0030         STA4E         0.0045         WAVC         0.0848           MIS7E         0.0107         GRA7         0.0023         STA5         0.0005         VAVC         0.0848           MIS7F         0.0108         GRA8A         0.0072         STA6A         0.0019         VAVC         0.0848           MIS7G         0.0106         GRA8B         0.0204         STA6B         0.0016         VAV2	MIS6A	0.0768	GRA3G	0.0020	STA2D	0.0056	DCT2C	7.7149
MIS6C         0.0806         GRA3I         0.0025         STA3         0.0010         WAV1A         0.0099           MIS6D         0.0809         GRA3J         0.0019         STA4A         0.0037         WAV1B         0.0143           MIS7A         0.0135         GRA3K         0.0021         STA4B         0.0040         WAV2A         0.0105           MIS7B         0.0136         GRA4         0.0011         STA4C         0.0047         WAV2B         0.0150           MIS7C         0.0141         GRA5         0.0079         STA4D         0.0036         WAV3         0.0265           MIS7D         0.0129         GRA6         0.0030         STA4E         0.0045         WAVC         0.0848           MIS7E         0.0107         GRA7         0.0023         STA5         0.0005         WAVC         0.0848           MIS7F         0.0108         GRA8A         0.0072         STA6A         0.0019         WAVC         0.0848           MIS7G         0.0106         GRA8B         0.0204         STA6B         0.0016         WAVC	MIS6B	0.0855	GRA3H	0.0021	STA2E	0.0058	DCT3	0.0011
MIS6D         0.0809         GRA3J         0.0019         STA4A         0.0037         WAV1B         0.0143           MIS7A         0.0135         GRA3K         0.0021         STA4B         0.0040         WAV2A         0.0105           MIS7B         0.0136         GRA4         0.0011         STA4B         0.0047         WAV2B         0.0150           MIS7C         0.0141         GRA5         0.0079         STA4D         0.0036         WAV3         0.0265           MIS7D         0.0129         GRA6         0.0030         STA4E         0.0045         WAVC         0.0848           MIS7E         0.0107         GRA7         0.0023         STA5         0.0005             MIS7F         0.0108         GRA8A         0.0072         STA6A         0.0019             MIS7G         0.0106         GRA8B         0.0204         STA6B         0.0016	MIS6C	0.0806	GRA3I	0.0025	STA3	0.0010	WAV1A	0.0099
MIS7A         0.0135         GRA3K         0.0021         STA4B         0.0040         WAV2A         0.0105           MIS7B         0.0136         GRA4         0.0011         STA4C         0.0047         WAV2B         0.0150           MIS7C         0.0141         GRA5         0.0079         STA4D         0.0036         WAV3         0.0265           MIS7D         0.0129         GRA6         0.0030         STA4E         0.0045         WAVC         0.0848           MIS7E         0.0107         GRA7         0.0023         STA5         0.0005         WAVC         0.0848           MIS7F         0.0108         GRA8A         0.0072         STA6A         0.0019         WAVC         0.0848           MIS7G         0.0106         GRA8B         0.0204         STA6B         0.0016         WAVC         0.0848	MIS6D	0.0809	GRA3J	0.0019	STA4A	0.0037	WAV1B	0.0143
MIS7B         0.0136         GRA4         0.0011         STA4C         0.0047         WAV2B         0.0150           MIS7C         0.0141         GRA5         0.0079         STA4D         0.0036         WAV3         0.0265           MIS7D         0.0129         GRA6         0.0030         STA4E         0.0045         WAVC         0.0848           MIS7E         0.0107         GRA7         0.0023         STA5         0.0005             MIS7F         0.0108         GRA8A         0.0072         STA6A         0.0019                MIS7G         0.0106         GRA8B         0.0204         STA6B         0.0016	MIS7A	0.0135	GRA3K	0.0021	STA4B	0.0040	WAV2A	0.0105
MIS7C         0.0141         GRA5         0.0079         STA4D         0.0036         WAV3         0.0265           MIS7D         0.0129         GRA6         0.0030         STA4E         0.0045         WAVC         0.0848           MIS7E         0.0107         GRA7         0.0023         STA5         0.0005         VAVC         0.0848           MIS7F         0.0108         GRA8A         0.0072         STA6A         0.0019         VAVC         VAVC           MIS7G         0.0106         GRA8B         0.0204         STA6B         0.0016         VAVC         VAVC	MIS7B	0.0136	GRA4	0.0011	STA4C	0.0047	WAV2B	0.0150
MIS7D         0.0129         GRA6         0.0030         STA4E         0.0045         WAVC         0.0848           MIS7E         0.0107         GRA7         0.0023         STA5         0.0005	MIS7C	0.0141	GRA5	0.0079	STA4D	0.0036	WAV3	0.0265
MIS7E         0.0107         GRA7         0.0023         STA5         0.0005           MIS7F         0.0108         GRA8A         0.0072         STA6A         0.0019           MIS7G         0.0106         GRA8B         0.0204         STA6B         0.0016	MIS7D	0.0129	GRA6	0.0030	STA4E	0.0045	WAVC	0.0848
MIS7F         0.0108         GRA8A         0.0072         STA6A         0.0019           MIS7G         0.0106         GRA8B         0.0204         STA6B         0.0016	MIS7E	0.0107	GRA7	0.0023	STA5	0.0005		
MIS7G 0.0106 GRA8B 0.0204 STA6B 0.0016	MIS7F	0.0108	GRA8A	0.0072	STA6A	0.0019		
	MIS7G	0.0106	GRA8B	0.0204	STA6B	0.0016		

 Table 3
 Computation efficiency of the methods. In each consecutive column we show the method abbreviation and execution time in seconds, alternately. The three fastest methods are indicated in *bold*.

observed structures make estimating the image quality a challenging task. There is no single point-like object available, therefore the selection techniques used in nighttime LI are not applicable.

In this study we decided to employ 36 techniques with various implementations and evaluated their precision in selecting the best exposures. The methods were based on various principles (gradients, intensity statistics, wavelets, Laplacians, and discrete cosine transforms) and were published over the past 40 years. Additionally, we enhanced their performance by applying simple modifications and by adjusting their tunable parameters.

In the comparison we employed reference images that contained both active regions and granulation areas, obtained by the *Hinode* satellite. The selected patches were degraded by convolving them with blurring kernels generated by the RWV method, which faithfully reflects the seeing characteristics. We assumed a wide range of relative atmospheric conditions, starting from nearly undisturbed observations at  $D/r_0 = 1$  to mediocre seeing at  $D/r_0 = 10$ . The reference quality of each simulated image was objectively estimated by measuring the amount of energy preserved in the Fourier spectrum of the original image. To assess the efficiency of the compared techniques, we finally calculated Spearman's correlation coefficient between the outcomes of each method and the expected image quality.

The results of our comparison showed that the efficiency depends on the strength of the atmospheric turbulence. For good seeing,  $D/r_0 < 4$ , the best method is the median filter gradient similarity (Deng *et al.*, 2015), (GRA8), the most recent technique proposed for solar observations. It is noteworthy that, the original idea had to be slightly modified to enhance the method performance. On the other hand, when the seeing conditions cover a wide range, the most efficient method is Helmli and Scherer's mean (Helmli and Scherer, 2001), (MIS5). This method should be considered when observing without AO or when the seeing conditions are unknown. The third outstanding method was the DCT energy ratio (Shen and Chen, 2006), which showed high performance in poor atmospheric conditions when observing granulation regions. The measurements of the execution time indicated that of the three mentioned techniques, Helmli and Scherer's mean has a significantly higher computational efficiency, which recommends it to be used with extremely high frame rates and/or larger image patches.

**Acknowledgements** We would like to thank for the numerous important comments, a thorough review, and the great help in polishing the English provided by the anonymous referee. This research was supported by the Polish National Science Centre grants 2016/21/D/ST9/00656 and (A. Popowicz) and 2015/17/N/ST7/03720 (K. Bernacki). We would also like to acknowledge the support from the Polish Ministry of Science and Higher Education funding for statutory activities.

Disclosure of Potential Conflicts of Interest The authors declare that they have no conflicts of interest.

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