



The stability of 3-DOF triple-rigid-body pendulum system near resonances

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Abstract In this article, the motion of three degree-of-freedom (DOF) dynamical system consisting of a triple rigid body pendulum (TRBP) in the presence of three harmonically external moments is studied. In view of the generalized coordinates of the system, Lagrange's equations are used to obtain the governing system of equations of motion (EOM). The analytic approximate solutions are gained up to the third approximation utilizing the approach of multiple scales (AMS) as novel solutions. The solvability conditions are determined in accordance with the elimination of secular terms. Therefore, the arising various resonances cases have been categorized and the equations of modulation have been achieved. The temporal histories of the obtained approximate solutions, as well as the resonance curves, are visually

displayed to reveal the positive effects of the various parameters on the dynamical motion. The numerical results of the governing system are achieved using the fourth-order Runge–Kutta method. The visually depicted comparison of asymptotic and numerical solutions demonstrates high accuracy of the employed perturbation approach. The criteria of Routh–Hurwitz are used to investigate the stability and instability zones, which are then analyzed in terms of steady-state solutions. The strength of this work stems from its uses in engineering vibrational control applications which carry the investigated system a huge amount of importance.

Keywords Nonlinear dynamics · Vibrating systems · Resonance · Perturbation approaches · Stability

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1 Introduction

Due to their widespread applicability in everyday life, pendulum models have piqued the curiosity of many scholars in recent decades, particularly the first two decades of this century. However, the dynamics of many different types of pendulums were examined using various methods whether they are analytical or numerical.

In [1], the authors examined the instability positions of an inverted pendulum, in which if its pivot is harmonically pushed up and down with suitable frequency and amplitude, then its instability position can be abolished. The parametric pendulum is used in [2] to show how non-harmonic perturbations can be used to flip from one dynamic state to the other without changing the system's intrinsic characteristics. In [3], the authors investigated the motion of a simple pendulum as a dynamical model with single generalized coordinate to examine its periodic movement on an elliptic route. On the other hand, the chaotic motion of 2-DOF weakly nonlinear spring pendulum system for a fixed and moving suspension point is examined in [4] and [5], respectively, to reveal their chaotic behaviors near resonance with respect to the used parameters. The ASM [6] is used in [7] to explore the stability of a nonlinear spring pendulum, in which the improvement of this work is investigated in [8] when the pendulum is subjected to an external force.

Numerous publications, such as [9–13], have investigated various routes of the suspension points for the linear and nonlinear elastic pendulums with various DOFs. In [9], the suspension point of a damped elastic pendulum (EP) moves in a circular path. The obtained results are generalized in [10] for an elliptic route of this point, in which the approximate solutions (AS) of some special cases are obtained. In [11], the authors considered such a problem when the pivot point has a trajectory of Lissajous curve, while the general outcomes of this work are found in [12] for the planar motion of an EP connected with a rigid body to produce a dynamical model with 3 DOFs on the same route of its suspension point. A special case of these results is found in [13] for a fixed point of suspension. The cases of linear and nonlinear damped EP carrying a rigid body, when the pivot point has a path of ellipse, is examined in [14, 15], respectively. The AMS is used in these works to gain the AS of the governing system of motion. Therefore, the requirements of solvability are obtained through the conditions of eliminating secular terms and the possible resonance cases are characterized. The vibrational motion of a rigid body regarding the equilibrium position is investigated numerically in [16] using the framework of ode45 solver of the Runge–Kutta method [17] from fourth order. Recently, a comparison between numerical solutions (NS) and the AS for the motions of rigid bodies pendulum is examined in [18, 19] to highlight

the good reliability between them and to explore the high accuracy of the adopted perturbation approach. Moreover, the conditions of Routh–Hurwitz [20] have been used to ensure that steady-state solutions are stable and to evaluate their different stability regions.

On the other hand, the employment of the absorbers in the configuration of various constructions of dynamical models has piqued the interest of many researchers, e.g., [21–26] due to their applications in the vibrational control of engineering industries. In [21], the authors investigated how a longitudinal absorber may stabilize and regulate the vibration of a ship roll motion through the examination of the behavior of 3-DOF nonlinear spring pendulum. The behavior of a 2-DOF tuned absorber has been studied in [22] when the rotation of its suspension point is on an elliptic trajectory. The frequency response's equations are used to analyze the steady-state solutions around the chosen resonance situation, in which the conditions of stability have been established. The influence of the existence of a damped nonlinear EP on the behavior of this problem is regulated in [23]. The stability analysis for the motion of a transverse absorber linked with a nonlinear elastic spring, according to the examined three cases of the system's resonance, is presented in [24]. The vibrational analysis problem of a connected inverted pendulum with a passive mass for a spring absorber is addressed in [25]. In [26], the authors demonstrated how to modify automatically the rotating speed of a 2-DOF pendulum absorber by determining the phase between the primary structure's vibration and the absorber vibration, in which the response of absorber's speed has been implemented.

Furthermore, there are other types of pendulums that have been studied in [27–32]. The motion of a double pendulum under the influence of a vibrating force and a gravity one in the situation of a vibrating point of suspension is investigated in [27]. The parametrically driven double pendulum and its bifurcation structure at tiny oscillation amplitudes are investigated in [28], while the resonance and non-resonance cases of a double pendulum are discussed in [29]. However, the motion of a system comprising of two attached physical pendulums swinging along horizontal axes is investigated in [30]. Examinations of the experimental and numerical results for the motion of a triple pendulum were investigated in [31–34]. In [31], numerical simulation of generic

mechanical model with rigid motion limiters as well as the stability and bifurcation analysis is presented. On the other hand, the experimental rig and its corresponding dynamical model of the triple pendulum are provided in [32]. The piston-connecting rod–crankshaft system of a single-cylinder combustion engine is described in [33] as a particular case of a triple pendulum with barriers. High consistency between the experimental results and the numerical one for the motion of the same model is presented in [34]. The bifurcations and stability of high-frequency periodic motions with limited amplitude are also addressed, as well as the stability criteria. Recently, the stability analysis of un-stretched double pendulum and triple one when they are subjected to external harmonic moments and force are investigated in [35] and [36], respectively. The stability and instability zones for different parameters of the frequency responses are estimated.

This paper focuses on the motion of a plane dynamical system consisting of a TRBP with 3 DOFs under the impact of three harmonic external moments as a novel dynamical model. The governing system of motion, which is made up of a set of three second-order nonlinear differential equations, is derived using Lagrange’s equations. The analytic approximation solutions strategy of this system, as novel solutions, is based on the use of the AMS. The prerequisites for solvability are met by removing secular terms. As a result, the arising resonance cases are identified, and the equations modulation are obtained. The frequency responses curves and the time histories of the derived solutions are drawn to highlight the good effects of various parameters on the motion. The fourth-order Runge–Kutta method is utilized to obtain the numerical results of the governing system. The juxtaposition of the analytical and numerical results demonstrates that the perturbation technique used is extremely accurate. The stability and instability domains are evaluated using Routh–Hurwitz conditions, and the steady-state solutions are analyzed.

2 Dynamical modeling

The investigated dynamical model in this work consists of three rigid bodies attached with each other and moving in a vertical plane under the influence of a gravity field with acceleration g as shown in Fig. 1.

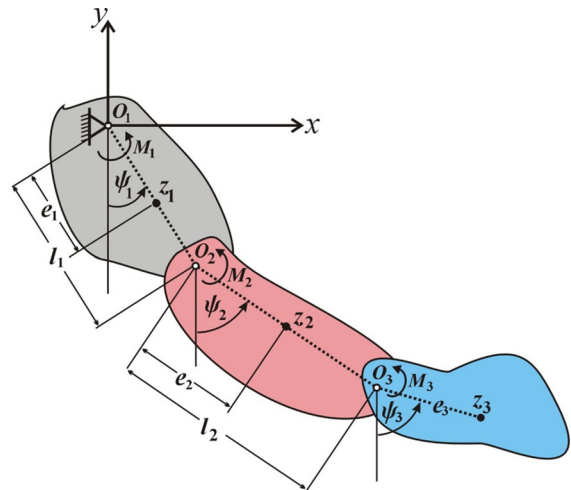


Fig. 1 Dynamical motion

The physical quantities e_j ($j = 1, 2, 3$) and l_k ($k = 1, 2$) refer to the distance between the bodies gravity centers z_j and the rotation centers O_j , and the link lengths of the first two pendulums, respectively. Furthermore, the mass and the moments of inertia of j th links regarding to z_j (orthogonal to the movement xy plane) are represented by m_j and J_j , respectively. The excitation moments operating on the links of the pendulums at O_j are denoted by $M_j(t) = f_j \cos \Omega_j t$ (where f_j and Ω_j are the amplitudes and frequencies of these moments), and the angular position’s variables are denoted by ψ_j ($j = 1, 2, 3$). It is supposed that the resistance moments at O_j have a viscous damping with coefficients c_j .

Based on the above description, the kinetic energy T and the potential one V of the system can be stated as follows

$$\begin{aligned}
 T = & \frac{1}{2} m_1 e_1^2 \dot{\psi}_1^2 + \frac{1}{2} m_2 [l_1^2 \dot{\psi}_1^2 + e_2^2 \dot{\psi}_2^2 + 2l_1 e_2 \dot{\psi}_1 \dot{\psi}_2 \cos(\psi_1 - \psi_2)] \\
 & + \frac{1}{2} m_3 [l_1^2 \dot{\psi}_1^2 + l_2^2 \dot{\psi}_2^2 + e_3^2 \dot{\psi}_3^2 + 2l_2 e_3 \dot{\psi}_2 \dot{\psi}_3 \cos(\psi_2 - \psi_3) \\
 & + 2l_1 l_2 \dot{\psi}_1 \dot{\psi}_2 \cos(\psi_1 - \psi_2) + 2l_1 e_3 \dot{\psi}_1 \dot{\psi}_3 \cos(\psi_1 - \psi_3)] \\
 & + \frac{1}{2} J_1 \dot{\psi}_1^2 + \frac{1}{2} J_2 \dot{\psi}_2^2 + \frac{1}{2} J_3 \dot{\psi}_3^2, \\
 V = & -m_1 g e_1 \cos \psi_1 - m_2 g (e_2 \cos \psi_2 + l_1 \cos \psi_1) \\
 & - m_3 g (e_3 \cos \psi_3 + l_1 \cos \psi_1 + l_2 \cos \psi_2).
 \end{aligned}
 \tag{1}$$

The governing system of EOM can be constructed using the below Lagrange’s equations [37]

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{\psi}_j} \right) - \frac{\partial L}{\partial \psi_j} = Q_j; \quad L = T - V \quad (j = 1, 2, 3), \tag{2}$$

where ψ_j and $\dot{\psi}_j$ are the generalized coordinates and their corresponding velocities, while the generalized forces Q_j have the forms

$$\begin{aligned} Q_1 &= f_1 \cos(\Omega_1 t) - c_1 \dot{\psi}_1 - c_2 (\dot{\psi}_1 - \dot{\psi}_2), \\ Q_2 &= f_2 \cos(\Omega_2 t) + c_2 \dot{\psi}_1 - (c_2 + c_3) \dot{\psi}_2 + c_3 \dot{\psi}_3, \\ Q_3 &= f_3 \cos(\Omega_3 t) + c_3 \dot{\psi}_2 - c_3 \dot{\psi}_3. \end{aligned} \tag{3}$$

Let us proceed with the dimensionless representations of the parameters we will be using

$$\begin{aligned} B_1 &= \frac{m_1 e_1^2 + (m_2 + m_3) l_1^2}{J_{z_1}}, & B_2 &= \frac{m_2 e_2^2 + m_3 l_2^2}{J_{z_2}}, \\ B_3 &= \frac{m_3 e_3^2}{J_{z_3}}, & N_1 &= \frac{m_2 e_2 l_1 + m_3 l_1 l_2}{J_{z_1}}, \\ N_2 &= \frac{m_2 e_2 l_1 + m_3 l_1 l_2}{J_{z_2}}, & N_3 &= \frac{m_3 e_3 l_2}{J_{z_3}}, & M_1 &= \frac{m_3 e_3 l_1}{J_{z_1}}, \\ M_2 &= \frac{m_3 e_3 l_2}{J_{z_2}}, & M_3 &= \frac{m_3 e_3 l_1}{J_{z_3}}, \\ \omega_1^2 &= \frac{m_1 g e_1}{J_{z_1}}, & \omega_2^2 &= \frac{m_2 g e_2}{J_{z_2}}, & \omega_3^2 &= \frac{m_3 g e_3}{J_{z_3}}, \\ \omega^2 &= \frac{\omega_2^2}{\omega_1^2}, & \tilde{\omega}^2 &= \frac{\omega_3^2}{\omega_1^2}, & S_1 &= \frac{(m_3 + m_2) g l_1}{J_{z_1} \omega_1^2}, \\ S_2 &= \frac{m_3 g l_2}{J_{z_2} \omega_1^2}, & P_1 &= \frac{\Omega_1}{\omega_1}, & P_2 &= \frac{\Omega_2}{\omega_1}, \\ P_3 &= \frac{\Omega_3}{\omega_1}, & F_1 &= \frac{F e_1}{J_{z_1} \omega_1^2}, & C_1 &= \frac{c_1}{J_{z_1} \omega_1}, \\ C_2 &= \frac{c_2}{J_{z_1} \omega_1}, & C_3 &= \frac{c_3}{J_{z_2} \omega_1}, & \mu_1 &= \frac{c_2}{J_{z_2} \omega_1}, \\ \mu_2 &= \frac{c_3}{J_{z_3} \omega_1}, & \tau &= \omega_1 t. \end{aligned} \tag{4}$$

Making use of (1), (2), (3), and (4), we can get the following EOM in its dimensionless forms

$$A\psi'' + B\psi' + C\psi^2 + D = F, \tag{5}$$

where

$$\psi'' = \begin{pmatrix} \psi_1'' \\ \psi_2'' \\ \psi_3'' \end{pmatrix}, \quad \psi' = \begin{pmatrix} \dot{\psi}_1 \\ \dot{\psi}_2 \\ \dot{\psi}_3 \end{pmatrix}, \quad \psi^2 = \begin{pmatrix} \psi_1'^2 \\ \psi_2'^2 \\ \psi_3'^2 \end{pmatrix}, \tag{6}$$

$$A = \begin{pmatrix} 1 + B_1 & N_1 \cos(\psi_1 - \psi_2) & M_1 \cos(\psi_1 - \psi_3) \\ N_2 \cos(\psi_2 - \psi_1) & 1 + B_2 & M_2 \cos(\psi_2 - \psi_3) \\ M_3 \cos(\psi_1 - \psi_3) & N_3 \cos(\psi_3 - \psi_2) & 1 + B_3 \end{pmatrix},$$

$$B = \begin{pmatrix} C_1 + C_2 & -C_2 & 0 \\ -\mu_1 & C_3 + \mu_1 & -C_3 \\ 0 & -\mu_2 & \mu_2 \end{pmatrix},$$

$$C = \begin{pmatrix} 0 & N_1 \sin(\psi_1 - \psi_2) & M_1 \sin(\psi_1 - \psi_3) \\ N_2 \sin(\psi_2 - \psi_1) & 0 & M_2 \sin(\psi_2 - \psi_3) \\ M_3 \sin(\psi_3 - \psi_1) & N_3 \sin(\psi_3 - \psi_2) & 0 \end{pmatrix},$$

$$D = \begin{pmatrix} (1 + S_1) \sin \psi_1 \\ (\omega^2 + S_2) \sin \psi_2 \\ \tilde{\omega}^2 \sin \psi_3 \end{pmatrix}, \quad F = \begin{pmatrix} f_1 \cos P_1 \tau \\ f_2 \cos P_2 \tau \\ f_3 \cos P_3 \tau \end{pmatrix}. \tag{7}$$

The foregoing set of Eq. (5) provides three second-order nonlinear differential equations in terms of ψ_j ($j = 1, 2, 3$).

3 The recommended method

The goal of the present section is to use the AMS to acquire the AS of the preceding governing EOM and to classify the different resonances cases. To achieve this aim, the trigonometric function of ψ_j ($j = 1, 2, 3$) can be approximated in the neighborhood of static equilibrium position up to the third order. Therefore, the system of EOM (5) can be rewritten as follows

$$\begin{aligned} &(1 + B_1)\psi_1'' + \frac{1}{36} [9(\psi_1^2 - 2)(\psi_2^2 - 2) + \psi_1\psi_2(\psi_1^2 - 6)(\psi_2^2 - 6)]N_1\psi_2'' \\ &+ \frac{1}{36} [9(\psi_1^2 - 2) \times (\psi_3^2 - 2) + \psi_1\psi_3(\psi_1^2 - 6)(\psi_3^2 - 6)]M_1\psi_3'' \\ &+ \frac{1}{12} [\psi_1(\psi_1^2 - 6)(\psi_2^2 - 2) - \psi_2(\psi_1^2 - 2)(\psi_2^2 - 6)]N_1\psi_2'^2 \\ &+ \frac{1}{12} [\psi_1(\psi_1^2 - 6)(\psi_3^2 - 2) - \psi_3(\psi_1^2 - 2)(\psi_3^2 - 6)]M_1\psi_3'^2 \\ &+ (1 + S_1) \times \left(\psi_1 - \frac{\psi_1^3}{6} \right) + (C_1 + C_2)\psi_1' - C_2\psi_2' = f_1 \cos P_1 \tau, \end{aligned} \tag{8}$$

$$\begin{aligned}
 & (1 + B_2)\psi_2'' + \frac{1}{36}[9(\psi_1^2 - 2)(\psi_2^2 - 2) + \psi_1\psi_2(\psi_1^2 - 6)(\psi_2^2 - 6)]N_2\psi_1'' \\
 & + \frac{1}{36}[9(\psi_2^2 - 2) \times (\psi_3^2 - 2) + \psi_2\psi_3(\psi_2^2 - 6)(\psi_3^2 - 6)]M_2\psi_3'' \\
 & - \frac{1}{12}[\psi_1(\psi_1^2 - 6)(\psi_2^2 - 2) - \psi_2(\psi_1^2 - 2) \times (\psi_2^2 - 6)]N_2\psi_1'^2 \\
 & + \frac{1}{12}[\psi_2(\psi_2^2 - 6)(\psi_3^2 - 2) - \psi_3(\psi_2^2 - 2)(\psi_3^2 - 6)]M_2\psi_3'^2 + (\omega^2 + S_1) \\
 & \times \left(\psi_2 - \frac{\psi_2^3}{6}\right) + (C_3 + \mu_1)\psi_2' - \mu_1\psi_1' + C_3\psi_3' = f_2 \cos P_2\tau,
 \end{aligned} \tag{9}$$

$$\begin{aligned}
 & (1 + B_3)\psi_3'' + \frac{1}{36}[9(\psi_3^2 - 2)(\psi_2^2 - 2) + \psi_3\psi_2(\psi_3^2 - 6)(\psi_2^2 - 6)]N_3\psi_2'' \\
 & + \frac{1}{36}[9(\psi_1^2 - 2) \times (\psi_3^2 - 2) + \psi_1\psi_3(\psi_1^2 - 6)(\psi_3^2 - 6)]M_3\psi_1'' \\
 & - \frac{1}{12}[\psi_2(\psi_2^2 - 6)(\psi_3^2 - 2) - \psi_3(\psi_2^2 - 2) \times (\psi_3^2 - 6)]N_3\psi_2'^2 \\
 & - \frac{1}{12}[\psi_1(\psi_1^2 - 6)(\psi_3^2 - 2) - \psi_3(\psi_1^2 - 2)(\psi_3^2 - 6)]M_3\psi_1'^2 \\
 & + \tilde{\omega} \left(\psi_3 - \frac{\psi_3^3}{6}\right) - \mu_2(\psi_2' - \psi_3') = f_3 \cos P_3\tau.
 \end{aligned} \tag{10}$$

It is crucial to realize that the vibration amplitudes; specially the generalized coordinates must be formulated in terms of a tiny parameter $0 < \varepsilon < 1$. Therefore, new variables θ , ϕ , and χ can be introduced as follows

$$\begin{aligned}
 \psi_1 &= \varepsilon\theta(\tau; \varepsilon), \\
 \psi_2 &= \varepsilon\phi(\tau; \varepsilon), \\
 \psi_3 &= \varepsilon\chi(\tau; \varepsilon).
 \end{aligned} \tag{11}$$

Now, we can seek for these variables as power series of ε according to the following series [6]

$$\begin{aligned}
 \theta(\tau, \varepsilon) &= \sum_{k=1}^3 \varepsilon^{k-1} \theta_k(\tau_0, \tau_1, \tau_2) + O(\varepsilon^3), \\
 \phi(\tau, \varepsilon) &= \sum_{k=1}^3 \varepsilon^{k-1} \phi_k(\tau_0, \tau_1, \tau_2) + O(\varepsilon^3), \\
 \chi(\tau, \varepsilon) &= \sum_{k=1}^3 \varepsilon^{k-1} \chi_k(\tau_0, \tau_1, \tau_2) + O(\varepsilon^3).
 \end{aligned} \tag{12}$$

Here, $\tau_0 = t$, $\tau_1 = \varepsilon t$, and $\tau_2 = \varepsilon^2 t$ are distinct timescales in which τ_0 represent a fast scale while τ_1 and τ_2 are the slow ones. Consequently, the derivatives regarding t can be transformed into the scales τ_0 , τ_1 , and τ_2 using the following operators

$$\begin{aligned} \frac{d}{dt} &= \frac{\partial}{\partial \tau_0} + \varepsilon \frac{\partial}{\partial \tau_1} + \varepsilon^2 \frac{\partial}{\partial \tau_2}, \\ \frac{d^2}{dt^2} &= \frac{\partial^2}{\partial \tau_0^2} + 2\varepsilon \frac{\partial^2}{\partial \tau_0 \partial \tau_1} + \varepsilon^2 \left(\frac{\partial^2}{\partial \tau_1^2} + 2 \frac{\partial^2}{\partial \tau_0 \partial \tau_2} \right) + O(\varepsilon^3). \end{aligned} \tag{13}$$

Taking into account the smallness of the parameters $B_j, N_j, M_j, S_1, S_2, f_j$, and C_j as below

$$\begin{aligned} B_j &= \varepsilon \tilde{B}_j, \quad N_j = \varepsilon \tilde{N}_j, \quad M_j = \varepsilon \tilde{M}_j, \quad S_1 = \varepsilon \tilde{S}_1, \quad S_2 = \varepsilon \tilde{S}_2, \\ f_j &= \varepsilon^3 \tilde{f}_j, \quad C_j = \varepsilon \tilde{C}_j, \quad \mu_1 = \tilde{\mu}_1, \quad \mu_2 = \tilde{\mu}_2 \quad (j = 1, 2, 3) \end{aligned} \tag{14}$$

where the parameters $\tilde{B}_j, \tilde{N}_j, \tilde{M}_j, \tilde{S}_1, \tilde{S}_2, \tilde{f}_j, \tilde{\mu}_1, \tilde{\mu}_2$, and \tilde{C}_j are unity-order parameters.

Making use of (11)–(14) into (8)–(10), and then equaling the coefficients of equal powers of ε to construct the sets of the following partial differential equations (PDE):

Order of ε :

$$\frac{\partial^2 \theta_1}{\partial \tau_0^2} + \theta_1 = 0, \tag{15}$$

$$\frac{\partial^2 \phi_1}{\partial \tau_0^2} + \omega^2 \phi_1 = 0, \tag{16}$$

$$\frac{\partial^2 \chi_1}{\partial \tau_0^2} + \varpi^2 \chi_1 = 0. \tag{17}$$

Order of ε^2 :

$$\begin{aligned} \frac{\partial^2 \theta_2}{\partial \tau_0^2} + \theta_2 &= -2 \frac{\partial^2 \theta_1}{\partial \tau_0 \partial \tau_1} - \tilde{B}_1 \frac{\partial^2 \theta_1}{\partial \tau_0^2} - \tilde{N}_1 \frac{\partial^2 \phi_1}{\partial \tau_0^2} \\ &\quad - \tilde{M}_1 \frac{\partial^2 \chi_1}{\partial \tau_0^2} - \tilde{S}_1 \theta_1 + \tilde{C}_2 \frac{\partial \phi_1}{\partial \tau_0} \\ &\quad - (\tilde{C}_1 + \tilde{C}_2) \frac{\partial \theta_1}{\partial \tau_0}, \end{aligned} \tag{18}$$

$$\begin{aligned} \frac{\partial^2 \phi_2}{\partial \tau_0^2} + \omega^2 \phi_2 &= -2 \frac{\partial^2 \phi_1}{\partial \tau_0 \partial \tau_1} - \tilde{B}_2 \frac{\partial^2 \phi_1}{\partial \tau_0^2} - \tilde{N}_2 \frac{\partial^2 \theta_1}{\partial \tau_0^2} \\ &\quad - \tilde{M}_2 \frac{\partial^2 \chi_1}{\partial \tau_0^2} - \tilde{S}_2 \phi_1 + \tilde{\mu}_1 \frac{\partial \theta_1}{\partial \tau_0} \\ &\quad - (\tilde{\mu}_1 + \tilde{C}_3) \frac{\partial \phi_1}{\partial \tau_0} + \tilde{C}_3 \frac{\partial \chi_1}{\partial \tau_0}, \end{aligned} \tag{19}$$

$$\begin{aligned} \frac{\partial^2 \chi_2}{\partial \tau_0^2} + \varpi^2 \chi_2 &= -2 \frac{\partial^2 \chi_1}{\partial \tau_0 \partial \tau_1} - \tilde{B}_3 \frac{\partial^2 \chi_1}{\partial \tau_0^2} - \tilde{N}_3 \frac{\partial^2 \phi_1}{\partial \tau_0^2} \\ &\quad - \tilde{M}_2 \frac{\partial^2 \theta_1}{\partial \tau_0^2} + \tilde{\mu}_2 \frac{\partial \phi_1}{\partial \tau_0} - \tilde{\mu}_2 \frac{\partial \chi_1}{\partial \tau_0}. \end{aligned} \tag{20}$$

Order of ε^3 :

$$\begin{aligned} \frac{\partial^2 \theta_3}{\partial \tau_0^2} + \theta_3 &= -\frac{\partial^2 \theta_1}{\partial \tau_1^2} - 2 \frac{\partial^2 \theta_1}{\partial \tau_0 \partial \tau_2} - 2 \frac{\partial^2 \theta_2}{\partial \tau_0 \partial \tau_1} \\ &\quad - 2 \tilde{B}_1 \frac{\partial^2 \theta_1}{\partial \tau_0 \partial \tau_1} - \tilde{B}_1 \frac{\partial^2 \theta_2}{\partial \tau_0^2} - \tilde{N}_1 \frac{\partial^2 \phi_2}{\partial \tau_0^2} \\ &\quad - 2 \tilde{N}_1 \frac{\partial^2 \phi_1}{\partial \tau_0 \partial \tau_1} - \tilde{M}_1 \frac{\partial^2 \chi_2}{\partial \tau_0^2} - 2 \tilde{M}_1 \frac{\partial^2 \chi_1}{\partial \tau_0 \partial \tau_1} \\ &\quad + \frac{1}{6} \theta_1^3 - \tilde{S}_1 \theta_2 \\ &\quad - (\tilde{C}_1 + \tilde{C}_2) \left(\frac{\partial \theta_1}{\partial \tau_1} + \frac{\partial \theta_2}{\partial \tau_0} \right) \\ &\quad + \tilde{C}_2 \left(\frac{\partial \phi_1}{\partial \tau_1} + \frac{\partial \phi_2}{\partial \tau_0} \right) + \tilde{f}_1 \cos P_1 \tau, \end{aligned} \tag{21}$$

$$\begin{aligned} \frac{\partial^2 \phi_3}{\partial \tau_0^2} + \omega^2 \phi_3 &= -\frac{\partial^2 \phi_1}{\partial \tau_1^2} - 2 \frac{\partial^2 \phi_1}{\partial \tau_0 \partial \tau_2} - 2 \frac{\partial^2 \phi_2}{\partial \tau_0 \partial \tau_1} \\ &\quad - 2 \tilde{B}_2 \frac{\partial^2 \phi_1}{\partial \tau_0 \partial \tau_1} - \tilde{B}_2 \frac{\partial^2 \phi_2}{\partial \tau_0^2} - \tilde{N}_2 \frac{\partial^2 \phi_2}{\partial \tau_0^2} \\ &\quad - 2 \tilde{N}_2 \frac{\partial^2 \theta_1}{\partial \tau_0 \partial \tau_1} - \tilde{M}_2 \frac{\partial^2 \chi_2}{\partial \tau_0^2} \\ &\quad - 2 \tilde{M}_2 \frac{\partial^2 \chi_1}{\partial \tau_0 \partial \tau_1} + \frac{1}{6} \omega^2 \phi_1^3 \\ &\quad - \tilde{S}_2 \phi_2 + \tilde{\mu}_1 \left(\frac{\partial \theta_1}{\partial \tau_1} + \frac{\partial \theta_2}{\partial \tau_0} \right) \\ &\quad + (\tilde{\mu}_1 + \tilde{C}_3) \left(\frac{\partial \phi_1}{\partial \tau_1} + \frac{\partial \phi_2}{\partial \tau_0} \right) \\ &\quad + \tilde{C}_3 \left(\frac{\partial \chi_1}{\partial \tau_1} + \frac{\partial \chi_2}{\partial \tau_0} \right) + \tilde{f}_2 \cos P_2 \tau, \end{aligned} \tag{22}$$

$$\begin{aligned} \frac{\partial^2 \chi_3}{\partial \tau_0^2} + \varpi^2 \chi_3 = & -\frac{\partial^2 \chi_1}{\partial \tau_1^2} - 2\frac{\partial^2 \chi_1}{\partial \tau_0 \partial \tau_2} - 2\frac{\partial^2 \chi_2}{\partial \tau_0 \partial \tau_1} \\ & - 2\tilde{B}_3 \frac{\partial^2 \chi_1}{\partial \tau_0 \partial \tau_1} - \tilde{B}_3 \frac{\partial^2 \chi_2}{\partial \tau_0^2} - \tilde{N}_3 \frac{\partial^2 \phi_2}{\partial \tau_0^2} \\ & - 2\tilde{N}_3 \frac{\partial^2 \phi_1}{\partial \tau_0 \partial \tau_1} - \tilde{M}_3 \frac{\partial^2 \theta_2}{\partial \tau_0^2} - 2\tilde{M}_3 \frac{\partial^2 \theta_1}{\partial \tau_0 \partial \tau_1} \\ & + \frac{1}{6} \varpi^2 \chi_1^3 - \tilde{\mu}_2 \left(\frac{\partial \chi_1}{\partial \tau_1} + \frac{\partial \chi_2}{\partial \tau_0} \right) \\ & - \tilde{\mu}_2 \left(\frac{\partial \phi_1}{\partial \tau_1} + \frac{\partial \phi_2}{\partial \tau_0} \right) + \tilde{f}_3 \cos P_3 \tau. \end{aligned} \tag{23}$$

The preceding Eqs. (15)-(23) constitute a system of nine linear PDE, which can be solved in the order they appeared. Therefore, the first group of Eqs. (15)–(17) have the general solutions that can be represented in the following ways

$$\theta_1 = A_1 e^{i\tau_0} + \bar{A}_1 e^{-i\tau_0}, \tag{24}$$

$$\phi_1 = A_2 e^{i\omega\tau_0} + \bar{A}_2 e^{-i\omega\tau_0}, \tag{25}$$

$$\chi_1 = A_3 e^{i\varpi\tau_0} + \bar{A}_3 e^{-i\varpi\tau_0}. \tag{26}$$

Here A_j ($j = 1, 2, 3$) and \bar{A}_j are unknown complex functions and the corresponding complex conjugate, respectively.

Inserting (24)–(26) into (18)–(20) and canceling the terms that lead to secular ones to get the following conditions

$$2i \frac{\partial A_1}{\partial \tau_1} + [\tilde{S}_1 - \tilde{B}_1 + i(\tilde{C}_1 + \tilde{C}_2)] A_1 = 0, \tag{27}$$

$$2i\omega \frac{\partial A_2}{\partial \tau_1} + [\tilde{S}_2 - \tilde{B}_2 \omega^2 + i\omega(\tilde{\mu}_1 + \tilde{C}_3)] A_2 = 0, \tag{28}$$

$$2i\varpi \frac{\partial A_3}{\partial \tau_1} + (i\varpi \tilde{C}_3 - \tilde{B}_3 \varpi^2) A_3 = 0. \tag{29}$$

As a result, the solutions of second order can be written as follows

$$\theta_2 = \frac{(\tilde{N}_1 \omega + i \tilde{C}_1) \omega A_2}{1 - \omega^2} e^{i\omega\tau_0} + \frac{\tilde{M}_1 \varpi^2 A_3}{1 - \varpi^2} e^{i\varpi\tau_0} + cc, \tag{30}$$

$$\begin{aligned} \phi_2 = & \frac{(\tilde{N}_2 + i \tilde{\mu}_1) A_1}{\omega^2 - 1} e^{i\tau_0} + \frac{(\tilde{M}_2 \varpi + i \tilde{C}_3) \varpi A_3}{\omega^2 - \varpi^2} e^{i\varpi\tau_0} \\ & + cc, \end{aligned} \tag{31}$$

$$\chi_2 = \frac{(\tilde{N}_3 \omega + i \tilde{\mu}_2) \omega A_2}{\varpi^2 - \omega^2} e^{i\omega\tau_0} + \frac{\tilde{M}_3 A_1}{\varpi^2 - 1} e^{i\tau_0} + cc, \tag{32}$$

where cc denotes the preceding terms' complex conjugates.

Making use of the solutions (24)–(26) and (30)–(32) into Eqs. (21)–(23), one obtains the requirements for deleting secular terms from the approximation of order three in the forms

$$\begin{aligned} \frac{\partial^2 A_1}{\partial \tau_1^2} + 2i \frac{\partial A_1}{\partial \tau_2} + 2i\tilde{B}_1 \frac{\partial A_1}{\partial \tau_1} \\ - \left[\frac{(\tilde{N}_1 \tilde{N}_2 + \tilde{N}_1 \tilde{\mu}_1 + i\tilde{N}_2 \tilde{C}_2 - \tilde{C}_2 \tilde{\mu}_1)}{\omega^2 - 1} \right. \\ \left. + \frac{\tilde{M}_1 \tilde{M}_3}{\varpi^2 - 1} + \frac{1}{2} A_1 \bar{A}_1 + (\tilde{C}_1 + \tilde{C}_2) \frac{\partial A_1}{\partial \tau_1} \right] A_1 = 0, \end{aligned} \tag{33}$$

$$\begin{aligned} \frac{\partial^2 A_2}{\partial \tau_1^2} + 2i\omega \frac{\partial A_2}{\partial \tau_2} + 2i\omega \tilde{B}_2 \frac{\partial A_2}{\partial \tau_1} \\ - \left[\frac{(\tilde{N}_1 \tilde{N}_2 \omega^2 + i\omega \tilde{N}_2 \tilde{C}_2 + \tilde{C}_2 \tilde{\mu}_1 + i\tilde{N}_1 \tilde{\mu}_1 \omega) \omega^2}{1 - \omega^2} \right. \\ \left. + \frac{(\tilde{M}_2 \tilde{N}_3 \omega + i\tilde{M}_2 \tilde{\mu}_2 + i\tilde{N}_3 \tilde{C}_3) \omega^3}{\varpi^2 - \omega^2} \right. \\ \left. + \frac{1}{2} \omega^2 A_2 \bar{A}_2 + (\tilde{\mu}_1 + \tilde{C}_3) \frac{\partial A_2}{\partial \tau_1} \right] A_2 = 0, \end{aligned} \tag{34}$$

$$\begin{aligned} \frac{\partial^2 A_3}{\partial \tau_1^2} + 2i\varpi \tilde{B}_3 \frac{\partial A_3}{\partial \tau_2} + 2i\varpi \tilde{B}_3 \frac{\partial A_3}{\partial \tau_1} + \tilde{\mu}_2 \frac{\partial A_3}{\partial \tau_1} \\ - \left[\frac{\tilde{M}_1 \tilde{M}_3 \omega^4}{1 - \varpi^2} + \frac{1}{2} \varpi^2 A_3 \bar{A}_3 \right. \\ \left. + \frac{(i\varpi \tilde{N}_3 \tilde{C}_3 + \tilde{M}_2 \tilde{N}_3 \varpi^2 + i\varpi \tilde{\mu}_2 \tilde{M}_2 - \tilde{C}_3 \tilde{\mu}_2) \varpi^2}{\omega^2 - \varpi^2} \right] A_3 = 0. \end{aligned} \tag{35}$$

Thus, the third-order approximations θ_3 , ϕ_3 , and χ_3 have the forms

$$\begin{aligned}
\theta_3 = & 2 \left[\frac{i\tilde{N}_1\omega^3}{(1-\omega^2)^2} \frac{\partial A_2}{\partial \tau_1} e^{i\omega\tau_0} + \frac{\tilde{M}_1\varpi^3}{(1-\varpi^2)^2} \frac{\partial A_3}{\partial \tau_1} e^{i\varpi\tau_0} - \frac{\tilde{C}_2\omega^2 A_2}{(1-\omega^2)^2} e^{i\omega\tau_0} \right] \\
& - \tilde{B}_1 \left[\frac{\omega^3 A_2}{(1-\omega^2)^2} \times (\tilde{N}_1\omega + \tilde{C}_2) e^{i\omega\tau_0} + \frac{\tilde{M}_1\varpi^4 A_3}{(1-\varpi^2)^2} e^{i\varpi\tau_0} \right] \\
& + 2 \frac{i\omega\tilde{N}_1}{(1-\omega^2)} \frac{\partial A_2}{\partial \tau_1} e^{i\omega\tau_0} \\
& + 2 \frac{i\varpi\tilde{M}_1}{(1-\varpi^2)} \frac{\partial A_3}{\partial \tau_1} e^{i\varpi\tau_0} - \frac{\omega^3 A_2 \tilde{M}_1 (\tilde{N}_3\omega + i\tilde{\mu}_2)}{(1-\omega^2)(\varpi^2 - \omega^2)} e^{i\omega\tau_0} \\
& + \tilde{S}_1 \left[\frac{\tilde{M}_1\varpi^2 A_3}{(1-\varpi^2)^2} e^{i\varpi\tau_0} + \frac{(\tilde{N}_1\omega + i\tilde{C}_2)\omega A_2}{(1-\omega^2)^2} e^{i\omega\tau_0} \right] \\
& + \frac{1}{48} A_1^3 e^{3i\tau_0} - (\tilde{C}_1 + \tilde{C}_2) \left[\frac{(i\tilde{N}_1\omega - \tilde{C}_2)\omega^2 A_2}{(1-\omega^2)^2} e^{i\omega\tau_0} + \frac{i\tilde{M}_1\varpi^3 A_3}{(1-\varpi^2)^2} e^{i\varpi\tau_0} \right] \\
& - \tilde{C}_2 \left[\frac{1}{(1-\omega^2)} \frac{\partial A_2}{\partial \tau_1} e^{i\omega\tau_0} + \frac{(\tilde{M}_2\varpi - \tilde{C}_3)i\varpi^2 A_3}{(1-\varpi^2)(\omega^2 - \varpi^2)} e^{i\varpi\tau_0} \right] + \frac{\tilde{f}_1}{2(1-P_1^2)} e^{iP_1\tau_0},
\end{aligned} \tag{36}$$

$$\begin{aligned}
\phi_3 = & 2 \left[\frac{(i\tilde{N}_2 - \tilde{\mu}_1)\partial A_1}{(\omega^2 - 1)^2} e^{i\tau_0} + \frac{(i\tilde{M}_2\varpi - \tilde{C}_3)\varpi^2 \partial A_3}{(\omega^2 - \varpi^2)^2} e^{i\varpi\tau_0} \right] \\
& - \tilde{B}_2 \left[\frac{(\tilde{N}_2 + i\tilde{\mu}_1)A_1}{(\omega^2 - 1)^2} e^{i\tau_0} + \frac{(\tilde{M}_2\varpi + i\tilde{C}_3)\varpi^3 A_3}{(\omega^2 - \varpi^2)^2} e^{i\varpi\tau_0} \right] \\
& - \frac{\tilde{N}_2\tilde{M}_1\varpi^4 A_3}{(1-\varpi^2)(\omega^2 - \varpi^2)} e^{i\varpi\tau_0} \\
& + \frac{2i\tilde{N}_2}{(\omega^2 - 1)} \frac{\partial A_1}{\partial \tau_1} e^{i\tau_0} + \frac{2i\varpi\tilde{M}_2}{(\omega^2 - \varpi^2)} \frac{\partial A_3}{\partial \tau_1} e^{i\varpi\tau_0} - \frac{\tilde{M}_2\tilde{M}_3 A_1}{(\omega^2 - 1)(\varpi^2 - 1)} e^{i\tau_0} \\
& + \frac{1}{48} A_2^3 e^{3i\omega\tau_0} + \tilde{S}_2 \left[\frac{(\tilde{N}_2 + i\tilde{\mu}_1)A_1}{(\omega^2 - 1)^2} e^{i\tau_0} + \frac{(\tilde{M}_2\varpi + i\tilde{C}_3)\varpi A_3}{(\omega^2 - \varpi^2)^2} e^{i\varpi\tau_0} \right] \\
& - \tilde{\mu}_1 \left[\frac{1}{(\omega^2 - 1)} \frac{\partial A_1}{\partial \tau_1} e^{i\tau_0} + \frac{i\tilde{M}_1\varpi^3 A_3}{(1-\varpi^2)(\omega^2 - \varpi^2)} e^{i\varpi\tau_0} \right] \\
& - \tilde{\mu}_2 \left[\frac{1}{(\omega^2 - \varpi^2)} \frac{\partial A_3}{\partial \tau_1} e^{i\varpi\tau_0} + \frac{i\tilde{M}_3 A_1}{(\varpi^2 - 1)(\omega^2 - 1)} e^{i\tau_0} \right] \\
& + \frac{\tilde{f}_2}{2(\omega^2 - P_2^2)} e^{iP_2\tau_0} \\
& - (\tilde{\mu}_1 + \tilde{C}_3) \left[\frac{(i\tilde{N}_2 - \tilde{\mu}_1)A_1}{(\omega^2 - 1)^2} e^{i\tau_0} + \frac{(i\tilde{M}_2\varpi - \tilde{C}_3)\varpi A_3}{(\omega^2 - \varpi^2)^2} e^{i\varpi\tau_0} \right],
\end{aligned} \tag{37}$$

$$\begin{aligned}
\chi_3 = & \frac{2i\tilde{N}_3\omega}{(\varpi^2 - \omega^2)} \frac{\partial A_2}{\partial \tau_1} e^{i\omega\tau_0} + \frac{2i\tilde{M}_3}{(\varpi^2 - 1)} \frac{\partial A_1}{\partial \tau_1} e^{i\tau_0} + \frac{1}{48} A_3^3 e^{3i\varpi\tau_0} \\
& - \frac{(\tilde{N}_3\omega - \tilde{\mu}_2)\tilde{B}_3\omega^3 A_2}{(\varpi^2 - \omega^2)^2} e^{i\omega\tau_0} - \frac{\tilde{B}_3\tilde{M}_3 A_1}{(\varpi^2 - 1)^2} e^{i\tau_0} \\
& + 2 \left[\frac{(i\omega\tilde{N}_3 - \tilde{\mu}_2)\omega^2 \partial A_2}{(\varpi^2 - \omega^2)^2} e^{i\omega\tau_0} + \frac{i\tilde{M}_3}{(\varpi^2 - 1)^2} \frac{\partial A_1}{\partial \tau_1} e^{i\tau_0} \right] \\
& - \frac{(\tilde{N}_2 + i\tilde{\mu}_1)\tilde{N}_3}{(\omega^2 - 1)(\varpi^2 - 1)} A_1 e^{i\tau_0} \\
& - \tilde{\mu}_2 \left[\frac{1}{(\varpi^2 - \omega^2)} \frac{\partial A_2}{\partial \tau_1} e^{i\omega\tau_0} + \frac{(i\tilde{N}_2 - \tilde{\mu}_1)A_1 e^{i\tau_0}}{(\omega^2 - 1)(\varpi^2 - 1)} \right] \\
& + \tilde{\mu}_2 \left[\frac{(i\tilde{N}_3\omega - \tilde{\mu}_1)\omega^2 A_2}{(\varpi^2 - \omega^2)^2} e^{i\omega\tau_0} + \frac{i\tilde{M}_3 A_1 e^{i\tau_0}}{(\varpi^2 - 1)^2} \right] \\
& - \frac{\tilde{f}_3 e^{iP_3\tau_0}}{2(\varpi^2 - P_3^2)} - \frac{(\tilde{M}_3\tilde{N}_1\omega + i\tilde{C}_2)\omega^3}{(1-\omega^2)(\varpi^2 - \omega^2)} A_2 e^{i\omega\tau_0}.
\end{aligned} \tag{38}$$

The unknown functions A_j ($j = 1, 2, 3$) can be determined by looking at the conditions (27)–(29)

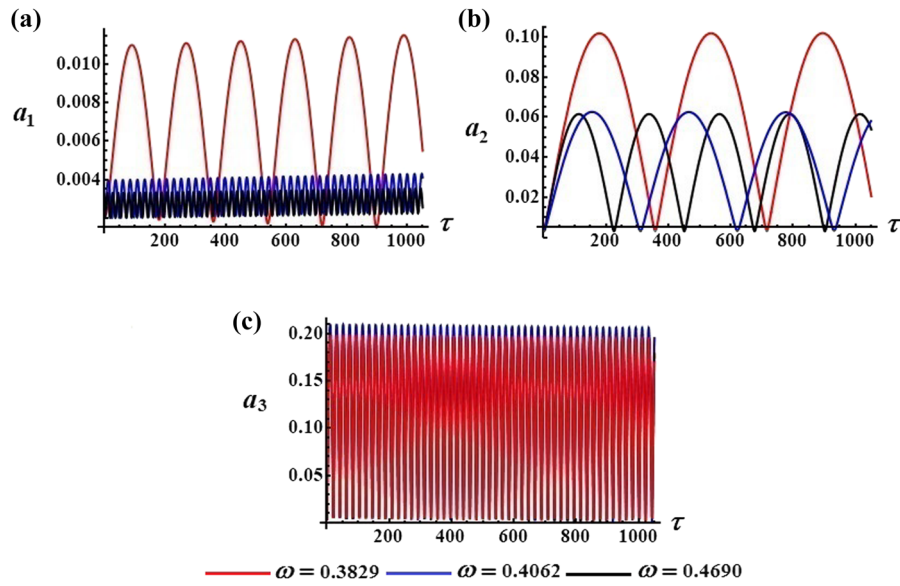


Fig. 2 Temporal variation of the amplitude $a_1, a_2,$ and a_3 , **a** a_1 at $\omega(= 0.3829, 0.4062, 0.4690)$, **b** a_2 at $\omega(= 0.3829, 0.4062, 0.4690)$, **c** a_3 at $\omega(= 0.3829, 0.4062, 0.4690)$

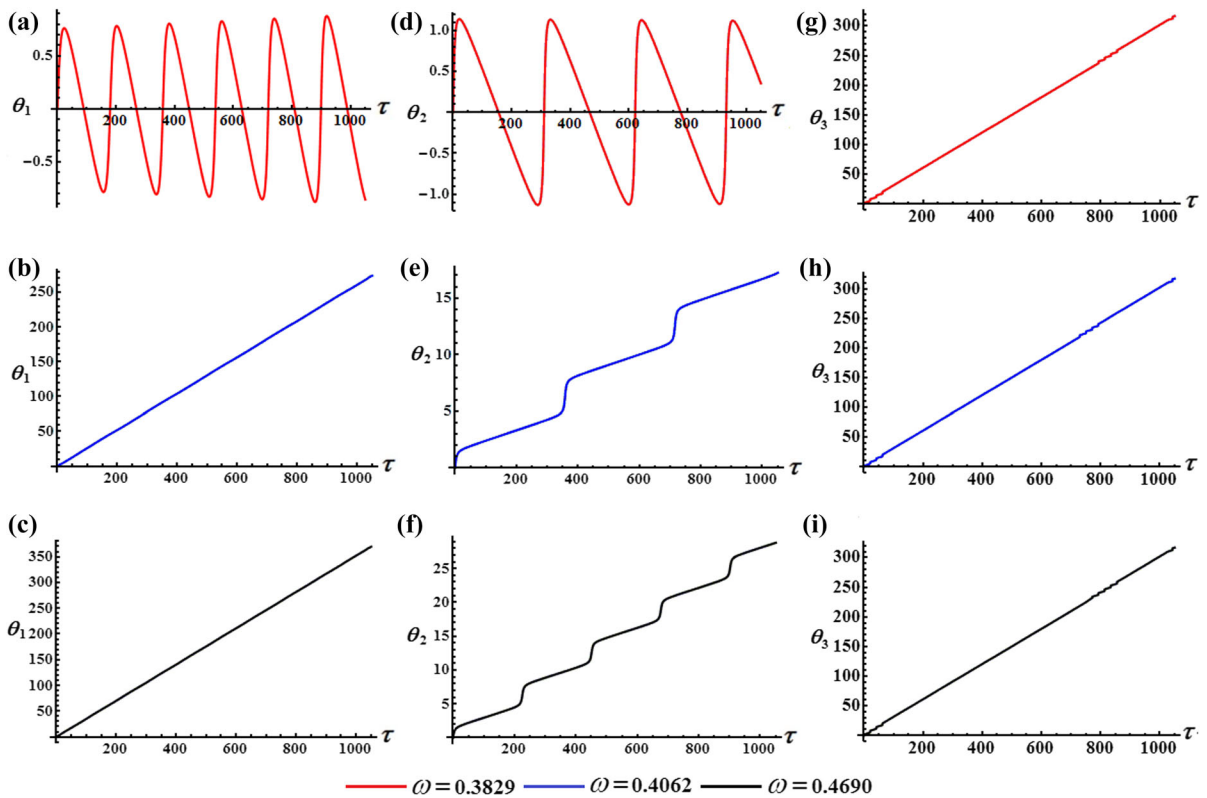


Fig. 3 Temporal variation of the modified phase $\theta_1, \theta_2,$ and θ_3 when **a-c** θ_1 at $\omega(= 0.3829, 0.4062, 0.4690)$, **d-f** θ_2 at $\omega(= 0.3829, 0.4062, 0.4690)$, **g-i** θ_3 at $\omega(= 0.3829, 0.4062, 0.4690)$

and (33)–(35). Therefore, the required AS can be obtained easily after substituting the solutions (24)–(26), (30)–(32), (36)–(38), and series (12) into hypothesis (11).

As previously stated, dealing with the AMS necessitates the employment of an unlimited number of separate timescales rather than a single time variable. The solvability constraints, which demand the removal of secular elements from fast time variables, are regarded as the appropriate tax for this flexibility. The fast timescale constrains the structure of the estimated solutions. It is also crucial to double-check that the requirements of the solvability for different orders are consistent. The amplitudes of “free” resonant phrases that emerge in each expansion order are limited by these requirements. The analysis may provide inaccurate results or only allow simple solutions if the restrictions are not fulfilled. It should be noted that alternative free amplitude options may yield contradicting findings [38].

4 Resonance requirements and equations of modulation

The categorizations of resonance cases that may emerge in the second or third-order solutions, as well as the consideration three of these cases, are both significant aspects of this section. It is well known that

the resonance cases occur if the denominators of these parts tend to zero [39]. Therefore, it might be categorized as:

- (i) When $p_1 \approx 1, p_2 \approx \omega$, and $p_3 \approx \varpi$, there is a main primary external resonance.
- (ii) When $\omega \approx 1, \varpi \approx \omega$, and $\varpi \approx 1$, there is an internal resonance.

It is noted that, if any one of the resonance cases is met, we should expect that the studied model’s behavior will be challenging. Furthermore, the approach described above is valid if the vibrations have values other than that of the resonance. Therefore, we will investigate the three primary external resonances that occur at the same instant to remedy this problem. To pursuit of this objective, it is critical to employ the dimensionless detuning parameters $\sigma_j (j = 1, 2, 3)$ that detect the distance between the oscillations and the stern resonance. Then we will be able to write

$$P_1 = 1 + \sigma_1, \quad P_2 = \omega + \sigma_2, \quad P_3 = \varpi + \sigma_3, \quad (39)$$

Then, we can formulate these parameters in terms of ε according to

$$\sigma_j = \varepsilon \tilde{\sigma}_j \quad (j = 1, 2, 3). \quad (40)$$

Inserting (39) and (40) into (18)–(23) and deleting the terms that yield secular ones, to gain the conditions of solvability as follows.

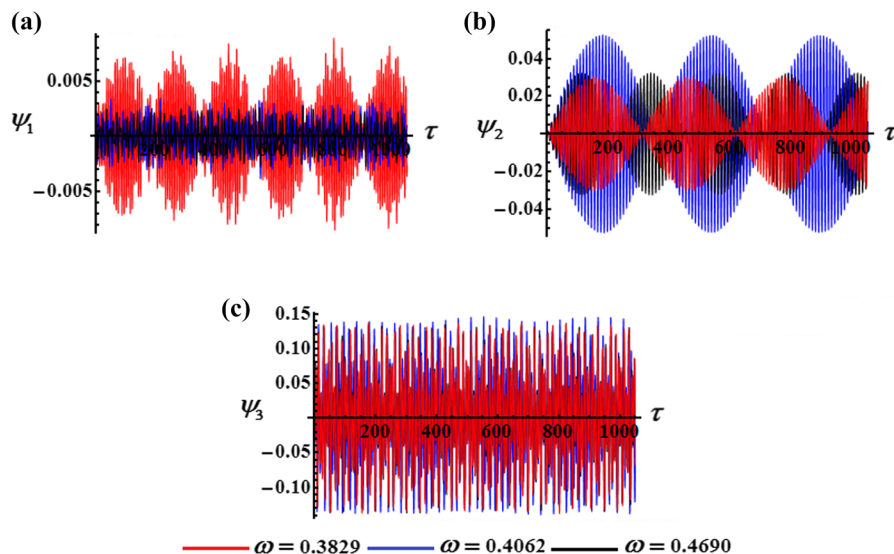


Fig. 4 Time histories of the AS ψ_1, ψ_2 , and ψ_3 when **a** ψ_1 at $\omega(= 0.3829, 0.4062, 0.4690)$, **b** ψ_2 at $\omega(= 0.3829, 0.4062, 0.4690)$, **c** ψ_3 at $\omega(= 0.3829, 0.4062, 0.4690)$

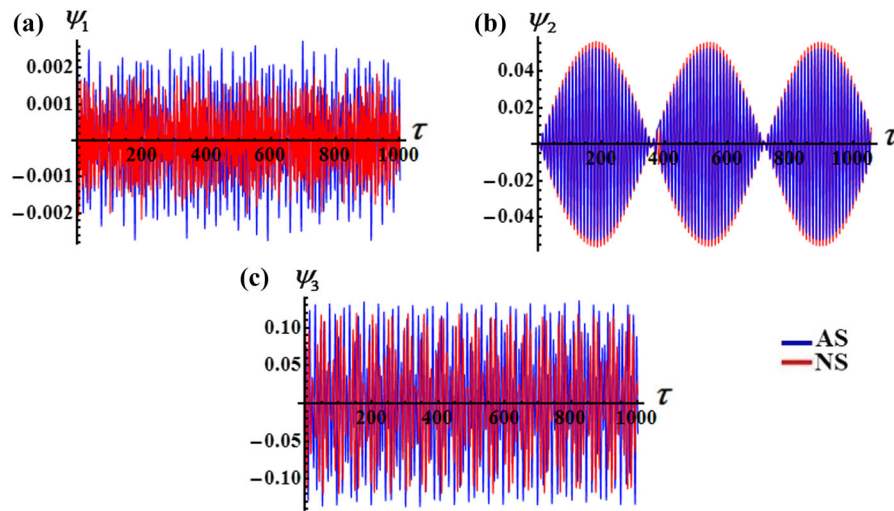
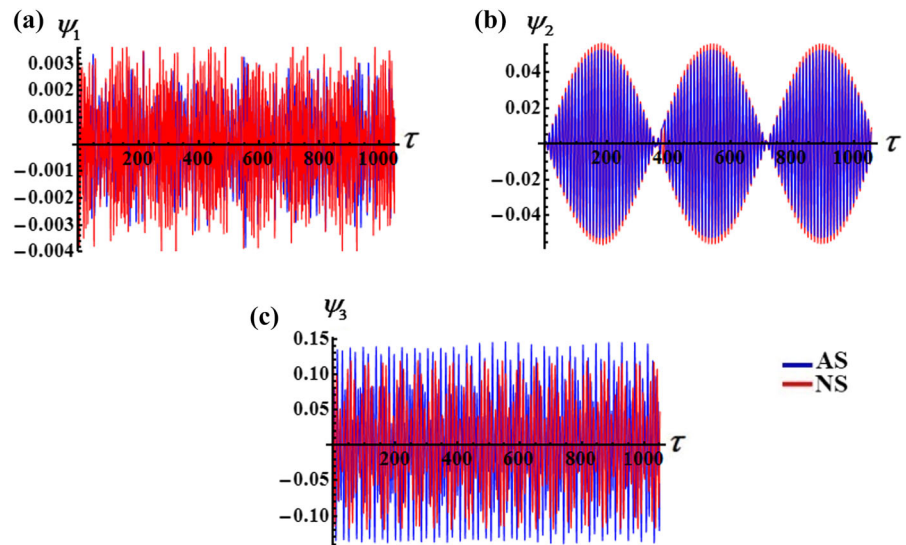


Fig. 5 Comparison between the AS and the NS of the variable $\psi_1, \psi_2,$ and ψ_3 when $\omega = 0.3829$

Fig. 6 Comparison between the AS and the NS of the variable $\psi_1, \psi_2,$ and ψ_3 when $\omega = 0.4062$



– Conditions of the second-order approximation

$$\frac{\partial A_1}{\partial \tau_1} = \frac{1}{2i} [\tilde{B}_1 - \tilde{S}_1 - i(\tilde{C}_1 + \tilde{C}_2)] A_1, \quad (41)$$

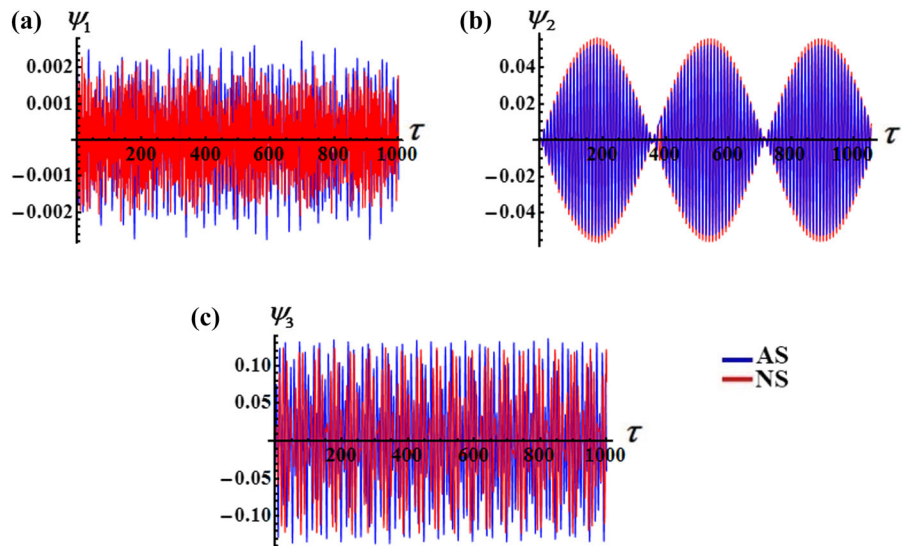
$$\frac{\partial A_2}{\partial \tau_1} = \frac{1}{2i\omega} [\tilde{B}_2 \omega^2 - \tilde{S}_2 - i\omega(\tilde{\mu}_1 + \tilde{C}_3)] A_2, \quad (42)$$

$$\frac{\partial A_3}{\partial \tau_1} = \frac{1}{2i\omega} (\tilde{B}_3 \omega - i\tilde{\mu}_2) A_3. \quad (43)$$

– Conditions of the third-order approximation

$$\begin{aligned} & 2i \frac{\partial A_1}{\partial \tau_2} - \frac{1}{4} \{ \tilde{S}_1^2 + 2\tilde{B}_1 \left(\tilde{S}_1 - \frac{3}{2} \tilde{B}_1 \right) \\ & + (\tilde{C}_1 + \tilde{C}_2) [4i\tilde{S}_1 - 3(\tilde{C}_1 + \tilde{C}_2)] + \frac{4\tilde{M}_1\tilde{M}_3}{\omega^2 - 1} \\ & + \frac{4}{\omega^2 - 1} [\tilde{N}_1(\tilde{N}_2 + i\tilde{\mu}_1) + i\tilde{N}_2\tilde{C}_2 - \tilde{C}_2\tilde{\mu}_1] \\ & - 2A_1\bar{A}_1 \} A_1 - \frac{\tilde{f}_1}{2} e^{i\tilde{\sigma}_1\tau_1} = 0, \end{aligned} \quad (44)$$

Fig. 7 Consistency between the AS and the NS of the variable ψ_1, ψ_2 , and ψ_3 when $\omega = 0.4690$



$$\begin{aligned}
 &2i\omega \frac{\partial A_2}{\partial \tau_2} - \frac{1}{4} \left\{ 2\tilde{B}_2(\tilde{S}_2 - \frac{3}{2}\tilde{B}_2\omega^2) + \frac{1}{\omega^2}\tilde{S}_2^2 \right. \\
 &+ (\tilde{\mu}_1 + \tilde{C}_3) \left[\frac{4i\tilde{S}_2}{\omega} - 3(\tilde{\mu}_1 + \tilde{C}_3) \right] \\
 &+ \frac{4\omega^3}{\omega^2 - \omega^2} [(\tilde{M}_2(\tilde{N}_3\omega + i\tilde{\mu}_2) + (i\omega^3\tilde{N}_3 - \omega^3\tilde{C}_3)\tilde{\mu}_2)] \\
 &- \frac{4[(\tilde{C}_2 + i\omega\tilde{N}_1)\omega^2\tilde{\mu}_1 - i\tilde{N}_2\tilde{C}_2]}{1 - \omega^2} \\
 &\left. - 2\omega^2 A_2 \bar{A}_2 \right\} A_2 - \frac{\tilde{f}_2}{2} e^{i\tilde{\sigma}_2 \tau_2} = 0,
 \end{aligned} \tag{45}$$

$$\begin{aligned}
 &2i\omega \frac{\partial A_3}{\partial \tau_2} - \frac{1}{4} \left\{ \tilde{B}_3(4i\omega\tilde{\mu}_2 - 3\tilde{B}_3\omega^2) \right. \\
 &+ 3\tilde{\mu}_2^2 + \frac{4\omega^4 \tilde{M}_1 \tilde{N}_3 \tilde{C}_2}{1 - \omega^2} \\
 &+ \frac{4}{\omega^2 - \omega^2} [\tilde{M}_2\omega^3(\tilde{N}_3\omega + i\tilde{\mu}_2) \\
 &+ \omega^3\tilde{C}_3(i\tilde{N}_3 - \tilde{\mu}_2)] - 2\omega^2 A_3 \bar{A}_3 \left. \right\} A_3 \\
 &- \frac{\tilde{f}_3}{2} e^{i\tilde{\sigma}_3 \tau_3} = 0.
 \end{aligned} \tag{46}$$

It is clear that the functions A_j ($j = 1, 2, 3$) can be determined using the forgoing criteria (41)–(46) which can be represented in the following polar form [40]

$$\begin{aligned}
 A_j(\tau_1, \tau_2) &= \frac{1}{2} \tilde{a}_j(\tau_1, \tau_2) e^{i\psi_j(\tau_1, \tau_2)}; \quad a_j = \varepsilon \tilde{a}_j, \\
 \theta_j(\tau_1, \tau_2) &= \tilde{\sigma}_j \tau_1 - \psi_j(\tau_1, \tau_2); \\
 \sigma_j &= \varepsilon \tilde{\sigma}_j \quad (j = 1, 2, 3),
 \end{aligned} \tag{47}$$

where θ_j are the modified phases, ψ_j are the phase angles and a_j are the amplitudes.

Making use of (47) into (41)–(46), and then distinguishing the real parts and the imaginary ones of the resulted equations to acquire the following modulation equations of six ordinary differential equations from first order

$$\begin{aligned}
 \frac{d\theta_1}{d\tau} &= \frac{a_1}{8} \left[\frac{4(N_1N_2 + M_1M_2 - \mu_1C_2)}{\omega^2 - 1} - 8\sigma_1 + \frac{a_1^2}{2} \right. \\
 &\quad \left. - B_1(4 - 3B_1) + S_1(2B_1 + S_1 - 4) + 3(C_1 + C_2)^2 \right] + \frac{f_1}{2} \cos \theta_1, \\
 \frac{da_1}{d\tau} &= \frac{a_1}{2} \left[\frac{C_1N_2 + N_1\mu_1 + N_2C_2}{\omega^2 - 1} + (S_1 - 1)(C_1 + C_2) \right] + \frac{f_1}{2} \sin \theta_1, \\
 \frac{d\theta_2}{d\tau} &= \frac{a_2}{8} \left[\frac{4(N_1N_2\omega^2 + C_2\mu_1)\omega^2}{\omega^2 - 1} + \frac{4(\omega^2M_3M_2 - C_3\mu_2)\omega^2}{\omega^2 - \omega^2} \right. \\
 &\quad \left. + \frac{a_2^2\omega^2}{2} - 8\omega\sigma_2 + n_1 + n_2 - 3(C_3 + \mu_1)^2 \right] + \frac{f_2}{2} \cos \theta_2, \\
 \frac{da_2}{d\tau} &= \frac{a_2}{2} \left[\frac{(C_2N_2 + N_1\mu_1)\omega^2}{1 - \omega^2} + \left(\frac{S_2}{\omega} - 1 \right) (C_3 + \tilde{C}_2) + \frac{(M_2 + N_3)\mu_2\omega^2}{\omega^2 - \omega^2} \right] \\
 &\quad + \frac{f_2}{2\omega} \sin \theta_2, \\
 \frac{d\theta_3}{d\tau} &= \frac{a_3}{8} \left[\frac{4M_1M_3\omega^4}{1 - \omega^2} + \frac{4(\omega^2N_3M_2 - C_3\mu_2)\omega^2}{\omega^2 - \omega^2} + \frac{a_3^2\omega^2}{2} \right. \\
 &\quad \left. + B_3\omega^2(4 - 3B_3) + 3\mu_2^2 - 8\omega\sigma_3 \right] + \frac{f_3}{2} \cos \theta_3, \\
 \frac{da_3}{d\tau} &= \frac{a_3}{2\omega} [n_3 + (B_3 - \omega)\mu_2] + \frac{f_3}{2\omega} \sin \theta_3,
 \end{aligned} \tag{48}$$

where

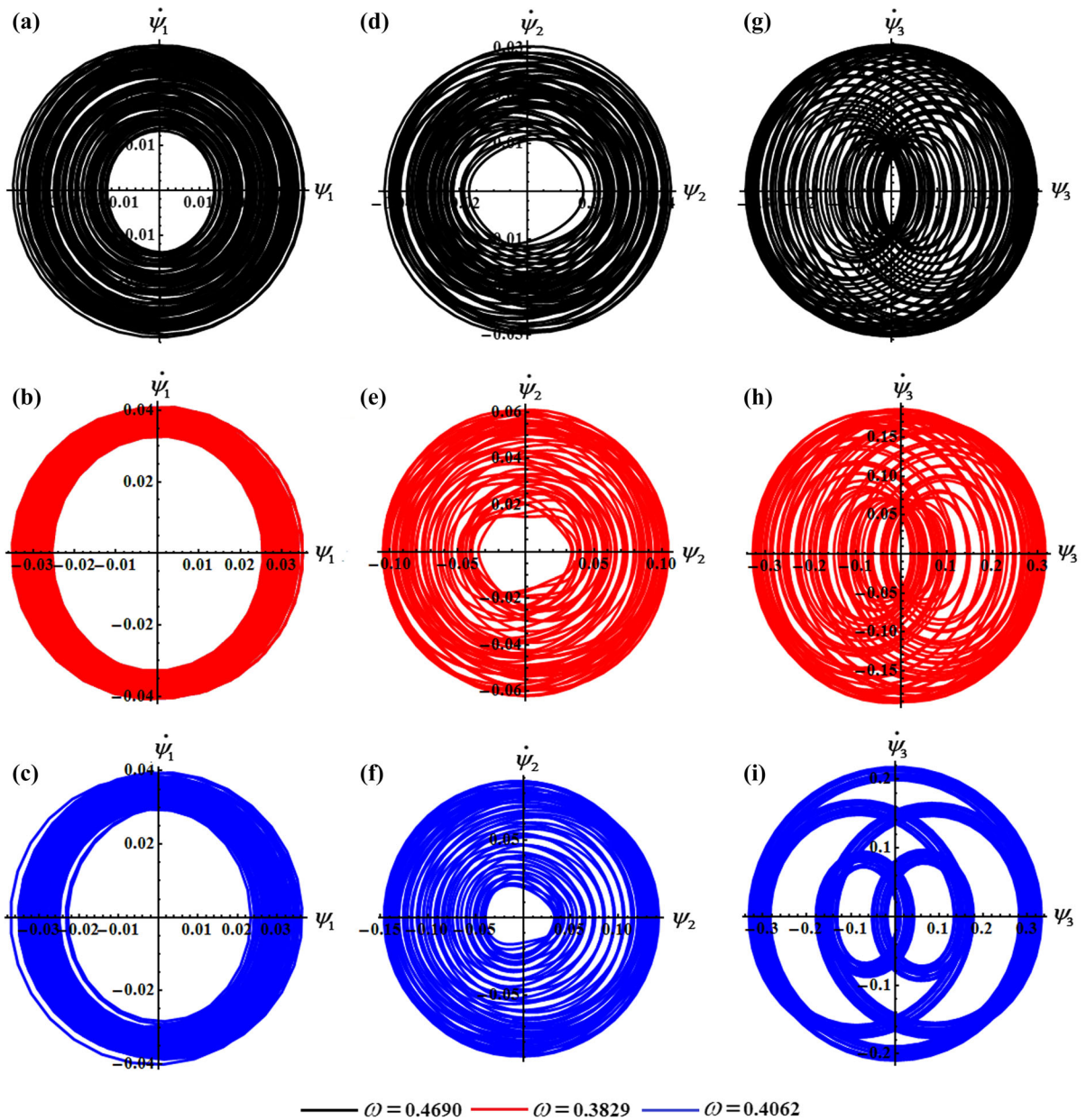


Fig. 8 Phase planes for the solutions $\psi_1, \psi_2,$ and ψ_3 when $\omega(= 0.3829, 0.4062, 0.4690)$

$$n_1 = B_2\omega^2 \left(1 - \frac{3}{4}B_2 \right),$$

$$n_2 = S_2 \left(\frac{S_2}{4\omega^2} + \frac{B_2}{2} - 1 \right),$$

$$n_3 = \frac{(N_3C_3 + \mu_2M_2)\varpi^3}{\omega^2 - \varpi^2}.$$

Referring to the preceding system (48), the time histories of its solutions a_j ($j = 1, 2, 3$) and θ_j are graphed in Figs. 2 and 3, respectively. These figures are calculated at $\omega(= 0.3829, 0.4062, 0.4690)$ and according to the following data

$$\begin{aligned}
 B_1 &= 0.202, & B_2 &= 0.0168, & B_3 &= 0.00187, \\
 N_1 &= 0.649, & N_2 &= 0.0357, & N_3 &= 0.0075, \\
 M_1 &= 0.1159, & M_2 &= 0.00375, & M_3 &= 0.01275, \\
 C_1 &= 0.0000761, & C_2 &= 0.0000304, \\
 C_3 &= 0.0000609, & f_1 &= 0.02, & f_2 &= 0.05, \\
 f_3 &= 1, & \mu_1 &= 0.0000167, & \mu_2 &= 0.0000670, \\
 \sigma_1 &= -0.1, & \sigma_2 &= 0.2, & \sigma_3 &= 0.3.
 \end{aligned}$$

Periodic waves can be seen while looking at the potions (a), (b), and (c) of Fig. 2, where the amplitudes of these waves decrease and the number of oscillations increase in addition to the increasing of their wave-lengths with the increment of the values of ω . The variation of θ_j has an increasing manner when time goes on as shown in parts of Fig. 3. These observations are constituting with the nature of the equations of the previous system (48). Therefore, the behavior of a_j and θ_j is influenced with the distinct values of ω .

The variation of the obtained AS for ψ_j ($j = 1, 2, 3$) via dimensionless time τ is plotted in portions (a), (b), and (c) of Fig. 4. Periodic waves are produced which encapsulates the characteristics of the obtained stable solutions. Some wave packets, characterizing the behavior of these solutions, have been obtained. These solutions are verified through the comparison with the NS of the original regulating system of Eqs. (8)–(10) using the fourth-order Runge–Kutta

method when $\omega = 0.3829, \omega = 0.4062, \omega = 0.4690, \psi_1(0) = 0.0001, \psi_1'(0) = 0, \psi_2(0) = 0.0002, \psi_2'(0) = 0.00001, \psi_3(0) = 0.3,$ and $\psi_3'(0) = 0$ (with the consideration of the same values of other parameters) as graphed in parts of Figs. 5, 6, and 7, respectively. The good matching between them explores the high precision of the used perturbation method. The relations between the AS and their first-order derivatives are plotted in Fig. 8 to graph the phase planes figures when ω takes different values. It is notable that we have closed trajectories which confirm that the gained AS have a stable behavior, which is predicted before, during the tested interval of time.

5 Steady-state solutions

The goal of this section is to investigate the dynamical system’s vibrations under examination the steady-state case. To accomplish this purpose, we consider the null value of the first derivatives of the modified phases θ_j and amplitudes a_j in Eq. (48), i.e., $\frac{d\theta_j}{d\tau} = \frac{da_j}{d\tau} = 0$ ($j = 1, 2, 3$) [41]. Therefore, the next set of six algebraic equations regarding the variables θ_j and a_j is yielded

Fig. 9 Amplitudes’ resonance curves a_j ($j = 1, 2, 3$) as a function of σ_3 at $\omega = 0.4062$

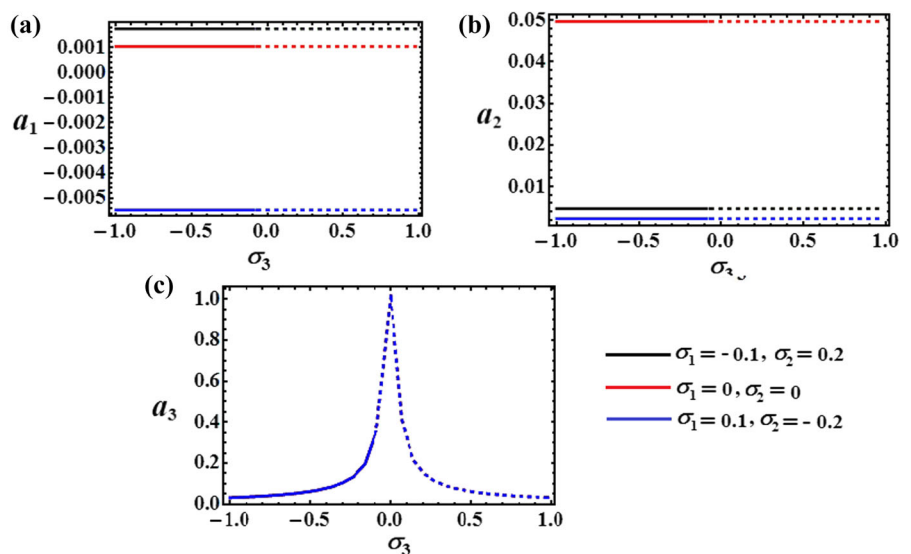


Fig. 10 Curves of $a_j(\sigma_2)$; ($j = 1, 2, 3$) at $\omega = 0.4062$

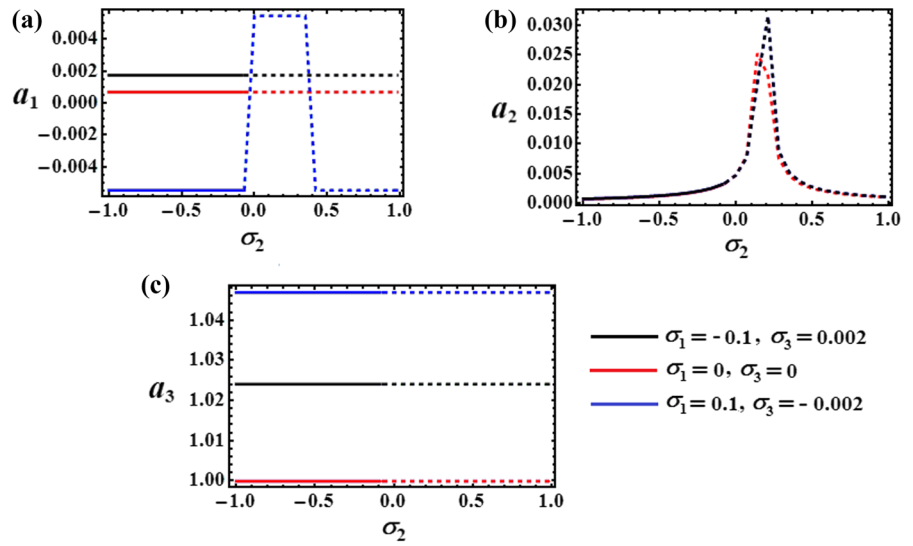


Fig. 11 Curves of $a_j(\sigma_1)$; ($j = 1, 2, 3$) at $\omega = 0.4062$

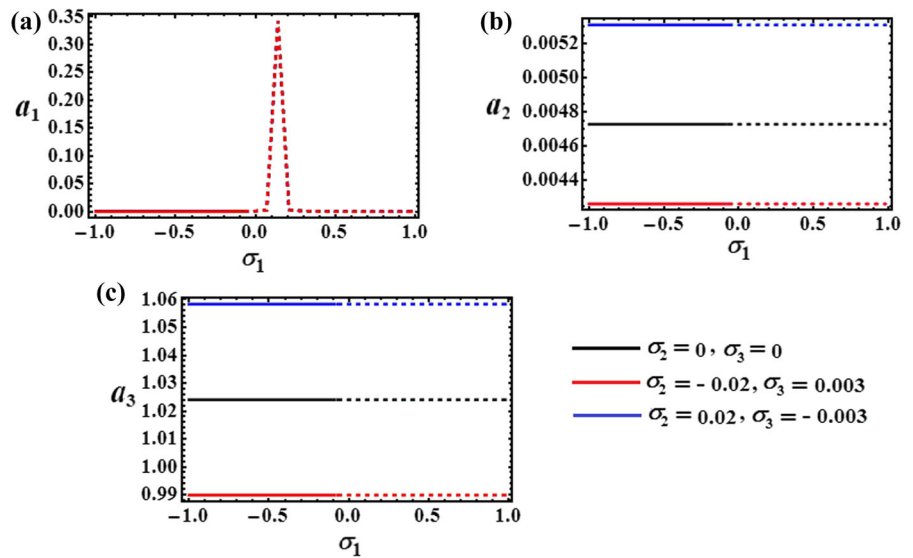


Fig. 12 Resonance curves of $a_j(\sigma_3)$; ($j = 1, 2, 3$) at $\omega = 0.4062$, $\sigma_1 = -0.1$, $\sigma_2 = 0.2$, and $C_1 = (0.005, 0.01, 0.1)$

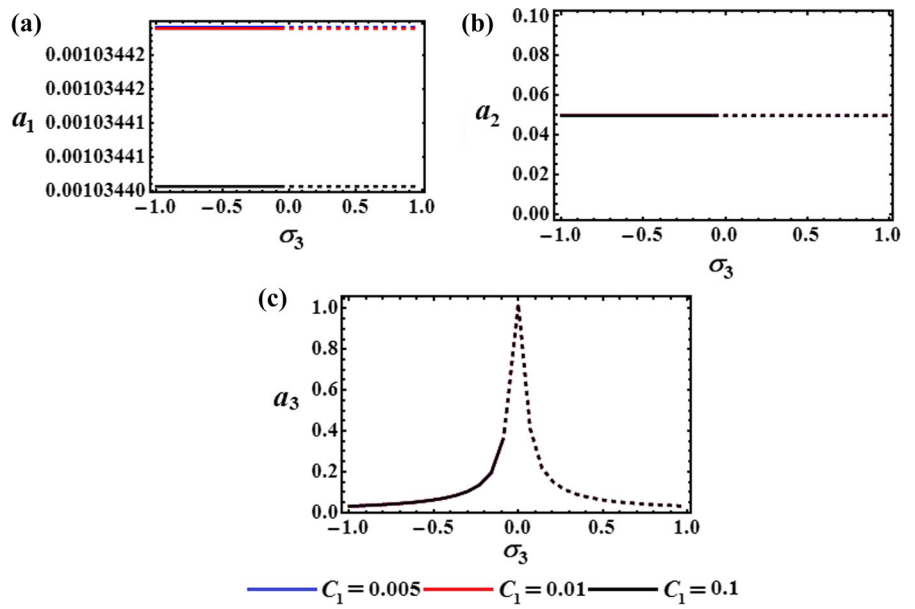
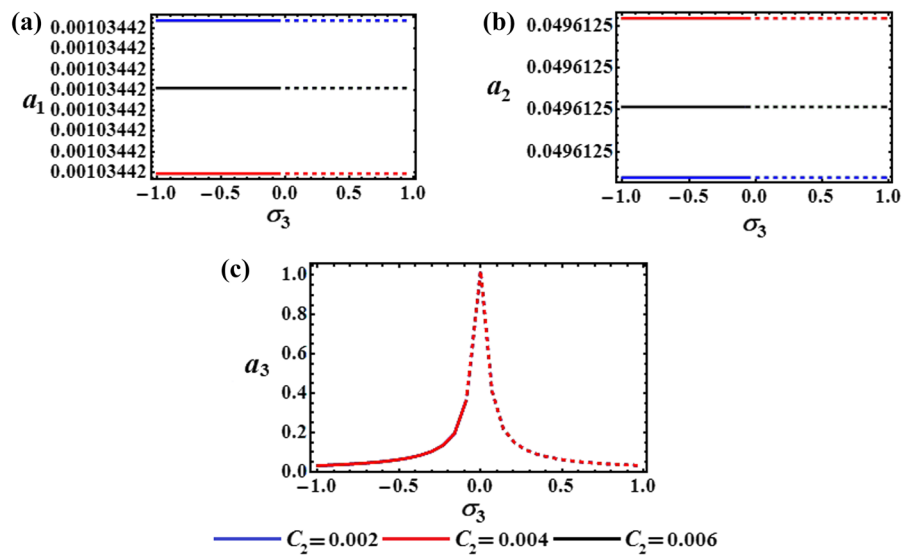


Fig. 13 Resonance curves of $a_j(\sigma_3)$; ($j = 1, 2, 3$) at $\omega = 0.4062$, $\sigma_1 = -0.1$, $\sigma_2 = 0.2$ and $C_2 = (0.002, 0.004, 0.006)$



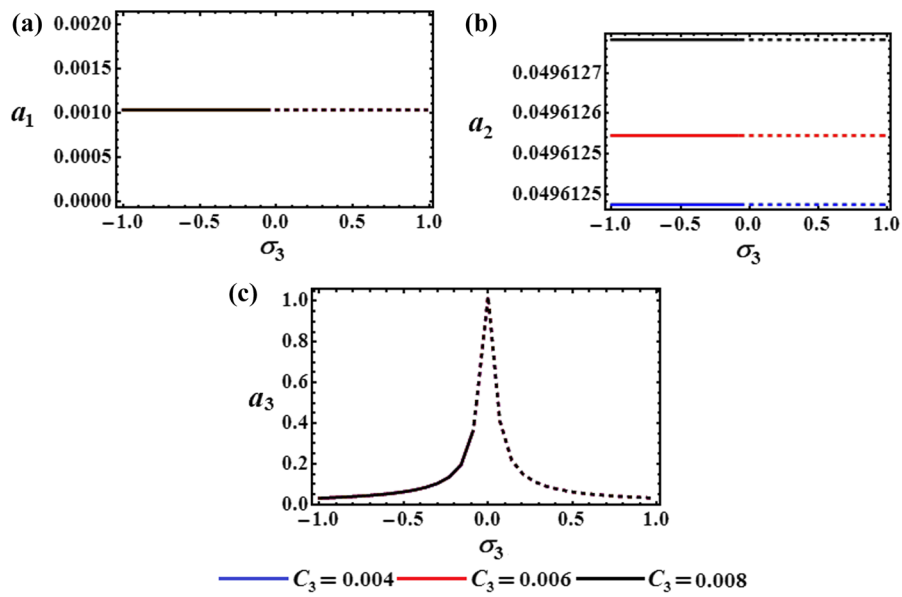


Fig. 14 Resonance curves of $a_j(\sigma_3)$; ($j = 1, 2, 3$) at $\omega = 0.4062, \sigma_1 = -0.1, \sigma_2 = 0.2$, and $C_3 (= 0.004, 0.006, 0.008)$

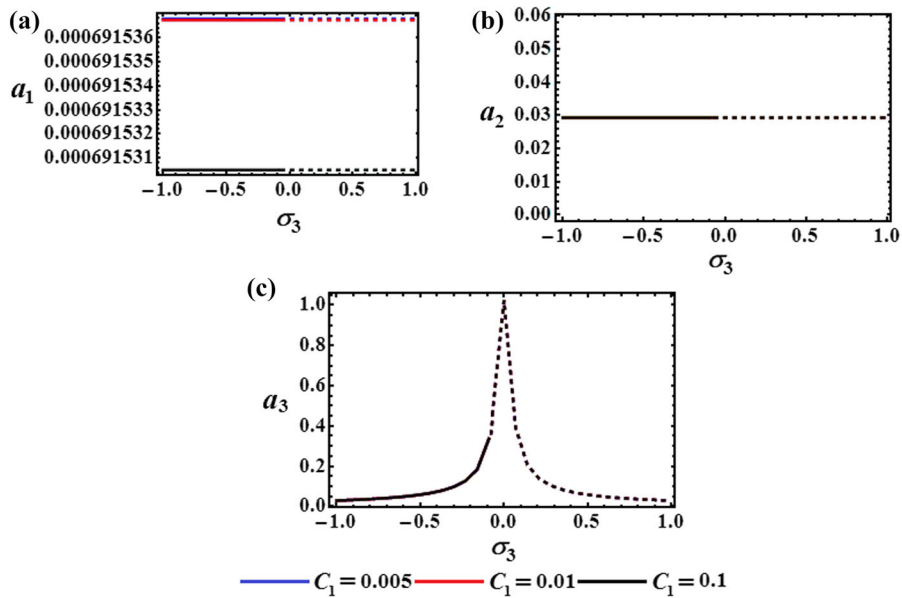


Fig. 15 Resonance curves of $a_j(\sigma_3)$; ($j = 1, 2, 3$) at $\omega = 0.3829, \sigma_1 = -0.1, \sigma_2 = 0.2$, and $C_1 (= 0.005, 0.01, 0.1)$

Fig. 16 Resonance curves of $a_j(\sigma_3)$; ($j = 1, 2, 3$) at $\omega = 0.3829$, $\sigma_1 = -0.1$, $\sigma_2 = 0.2$, and $C_2 = (0.002, 0.004, 0.006)$

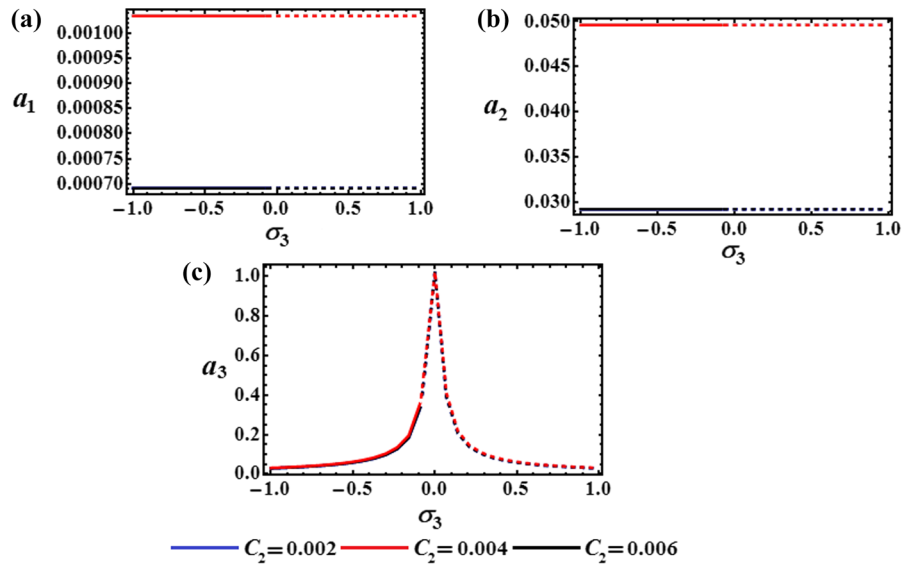
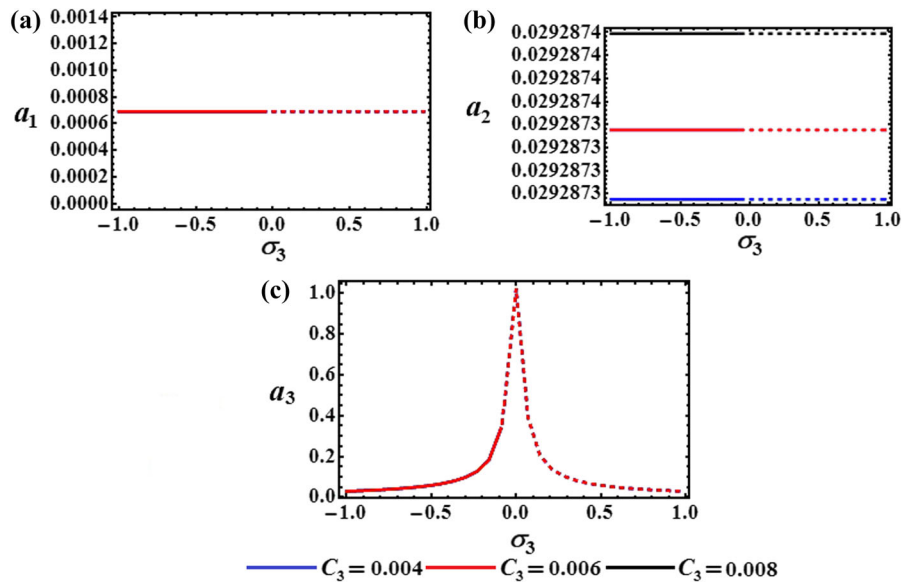


Fig. 17 Resonance curves of $a_j(\sigma_3)$; ($j = 1, 2, 3$) at $\omega = 0.3829$, $\sigma_1 = -0.1$, $\sigma_2 = 0.2$, and $C_3 = (0.004, 0.006, 0.008)$



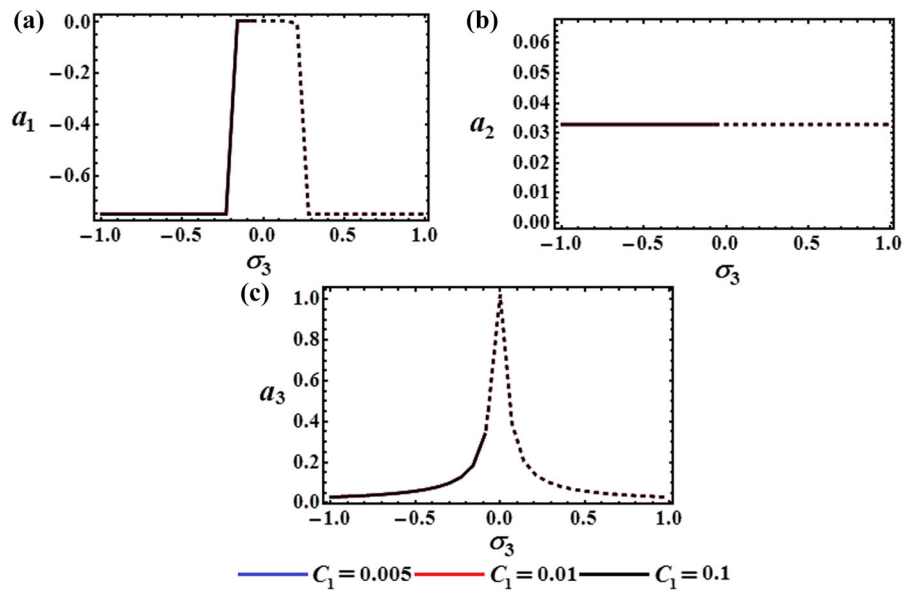


Fig. 18 Resonance curves of $a_j(\sigma_3)$; ($j = 1, 2, 3$) at $\omega = 0.4690, \sigma_1 = -0.1, \sigma_2 = 0.2$, and $C_1 (= 0.005, 0.01, 0.1)$

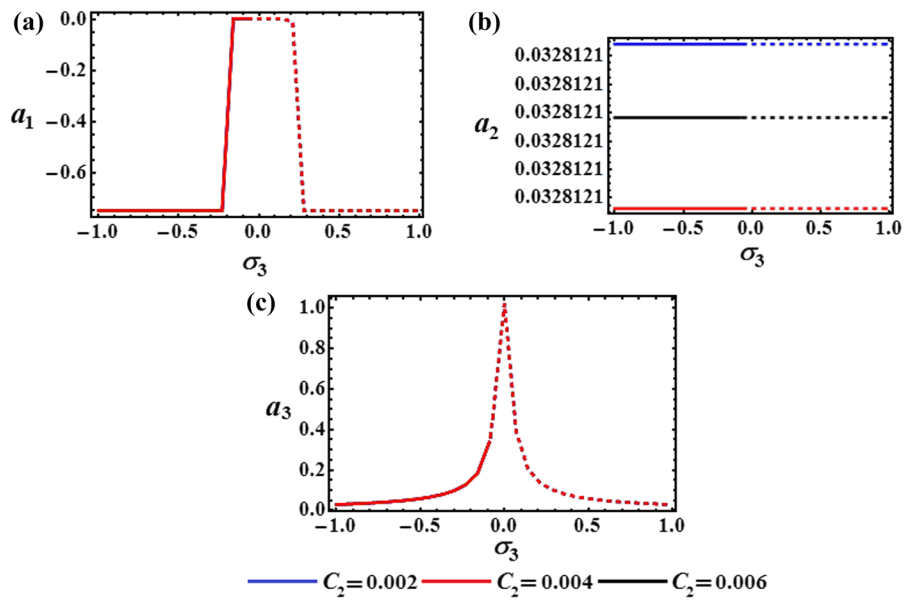


Fig. 19 Resonance curves of $a_j(\sigma_3)$; ($j = 1, 2, 3$) at $\omega = 0.4690, \sigma_1 = -0.1, \sigma_2 = 0.2$, and $C_2 (= 0.002, 0.004, 0.006)$

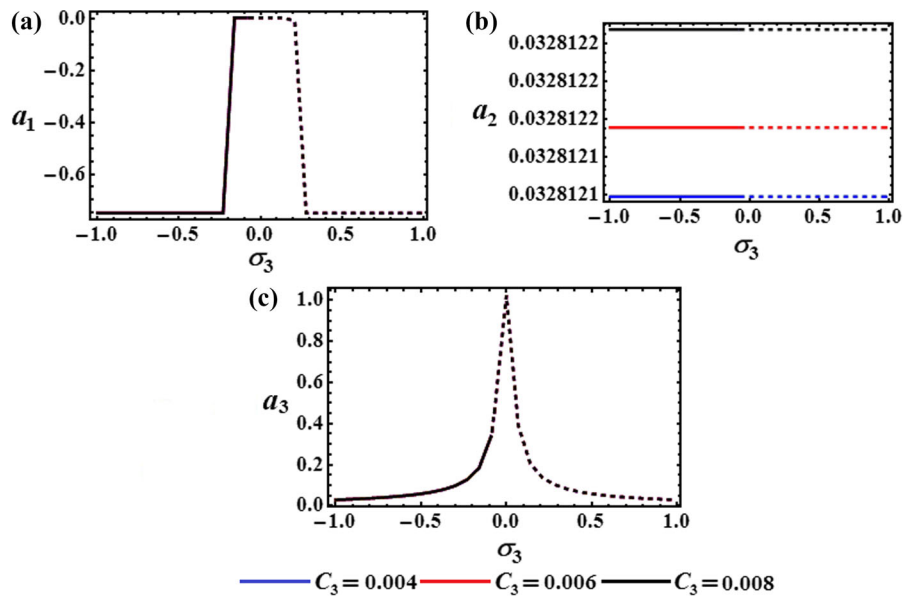


Fig. 20 Resonance curves of $a_j(\sigma_3)$; ($j = 1, 2, 3$) at $\omega = 0.4690, \sigma_1 = -0.1, \sigma_2 = 0.2$, and $C_3 (= 0.004, 0.006, 0.008)$

Fig. 21 Resonance curves of $a_j(\sigma_3)$; ($j = 1, 2, 3$) at $\omega = 0.4690$

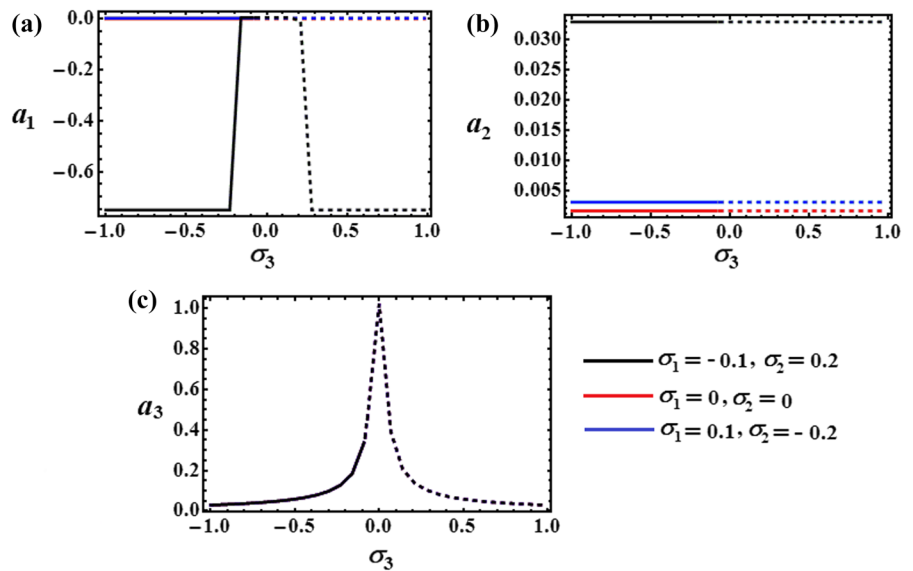


Fig. 22 Resonance curves of $a_j(\sigma_2)$; ($j = 1, 2, 3$) at $\omega = 0.4690$

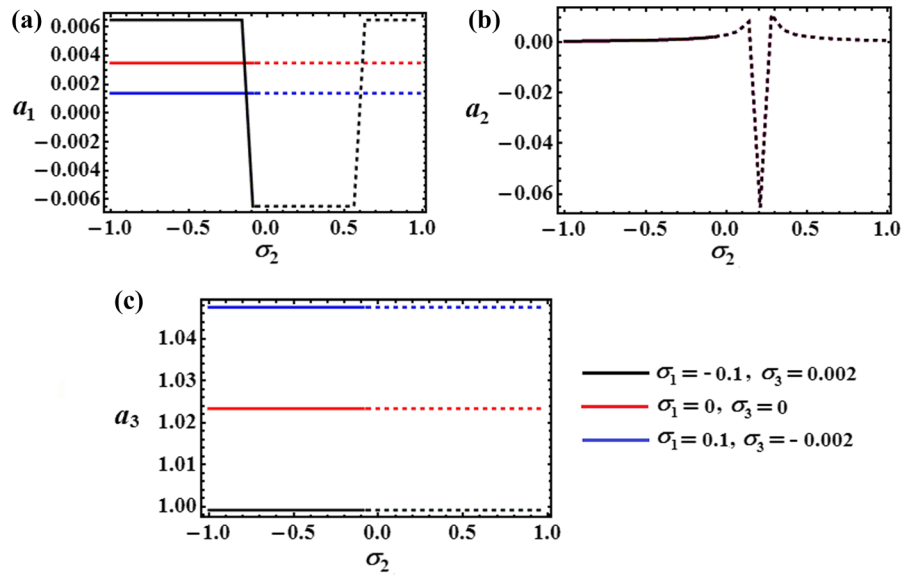


Fig. 23 Resonance curves of $a_j(\sigma_1)$; ($j = 1, 2, 3$) at $\omega = 0.4690$

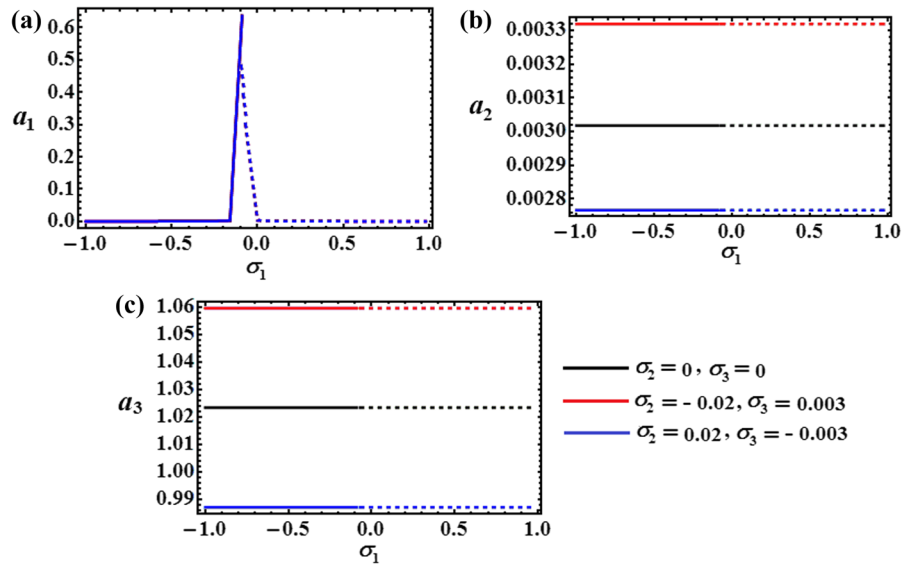


Table 1 Critical and peaks fixed points when detuning parameters σ_j have different values at $\omega = 0.4062$

Figure	Peaks points	Critical points	$\sigma_j (j = 1, 2, 3)$
Figure 9a	–	(–0.07, 0.00103442)	$\sigma_1 (= -0.1, 0, 0.1),$ $\sigma_2 (= -0.2, 0, 0.2)$
Figure 9b	–	(–0.07, 0.00173997) (–0.07, –0.00547301) (–0.07, 0.0496125) (–0.07, 0.00472759) (–0.07, 0.00225665)	
Figure 9c	(–0.0689, 1.036)	(–0.07, 0.492666)	
Figure 10a	–	(–0.07, 0.000691537)	$\sigma_1 (= -0.1, 0, 0.1),$ $\sigma_3 (= -0.002, 0, 0.002)$
Figure 10b	(0.1287, 0.0253)	(–0.07, 0.00173997) (–0.07, –0.00547301) (–0.07, 0.0336113)	
Figure 10c	–	(–0.07, 0.999864), (–0.07, 1.02406), (–0.07, 1.04689)	
Figure 11a	(0.1004, 0.3401)	(–0.07, 0.00117769)	$\sigma_2 (= -0.02, 0, 0.02),$ $\sigma_3 (= -0.003, 0, 0.003)$
Figure 11b	–	(–0.07, 0.00472759), (–0.07, 0.00530889), (–0.07, 0.00426102)	
Figure 11c	–	(–0.07, 1.02406), (–0.07, 1.0583), (–0.07, 0.98983)	

Table 2 Critical and peaks fixed points when damping coefficients C_j have different values at $\omega = 0.4062$

Figure	Peaks points	Critical points	$C_j (j = 1, 2, 3)$
Figure 12a	–	(–0.07, 0.00103440)(–0.07, 0.00103442)	$C_1 (= 0.005, 0.01, 0.1)$
Figure 12b	–	(–0.07, 0.0496125)	
Figure 12c	(–0.02203, 1.026)	(–0.07, 0.492666)	
Figure 13a	–	(–0.07, 0.00103442)	$C_2 (= 0.002, 0.004, 0.006)$
Figure 13b	–	(–0.07, 0.0496125)	
Figure 13a	(–0.02203, 1.026)	(–0.07, 0.492666)	
Figure 14a	–	(–0.07, 0.00103442)	$C_3 (= 0.004, 0.006, 0.008)$
Figure 14b	–	(–0.07, 0.0496125), (–0.07, 0.0496126), (–0.07, 0.0496127)	
Figure 14c	(–0.02203, 1.026)	(–0.07, 0.492666)	

Table 3 Critical and peaks fixed points when damping coefficients C_j have different values at $\omega = 0.3829$

Figure	Peaks points	Critical points	$C_j (j = 1, 2, 3)$
Figure 15a	–	(–0.07, 0.000691537), (–0.07, 0.000691553)	$C_1 (= 0.005, 0.01, 0.1)$
Figure 15b	–	(–0.07, 0.0292873)	
Figure 15c	(–0.02203, 1.026)	(–0.07, 0.454438)	
Figure 16a	–	(–0.07, 0.000691537)	$C_2 (= 0.002, 0.004, 0.006)$
Figure 16b	–	(–0.07, 0.029873)	
Figure 16c	(–0.02203, 1.026)	(–0.07, 0.454438)	
Figure 17a	–	(–0.07, 0.000691537)	$C_3 (= 0.004, 0.006, 0.008)$
Figure 17b	–	(–0.07, 0.0292873), (–0.07, 0.0292874)	
Figure 17c	(–0.02203, 1.026)	(–0.07, 0.454439)	

Table 4 Critical and peaks fixed points when damping coefficients C_j have different values at $\omega = 0.4690$

Figure	Peaks points	Critical points	$C_j (j = 1, 2, 3)$
Figure 18a	–	(–0.07, 0.00648686), (–0.07, 0.00648444)	$C_1 (= 0.005, 0.01, 0.1)$
Figure 18b	–	(–0.07, 0.328121)	
Figure 18c	(–0.02138, 1.026)	(–0.07, 0.454438)	
Figure 19a	–	(–0.07, 0.00648688)	$C_2 (= 0.002, 0.004, 0.006)$
Figure 19b	–	(–0.07, 0.0328121)	
Figure 19c	(–0.02138, 1.026)	(–0.07, 0.454955)	
Figure 20a	–	(–0.07, 0.0648693)	$C_3 (= 0.004, 0.006, 0.008)$
Figure 20b	–	(–0.07, 0.0328121), (–0.07, 0.0328122)	
Figure 20c	(–0.02138, 1.026)	(–0.07, 0.454654), (–0.07, 0.454655)	

$$\begin{aligned}
 f_1 \cos \theta_1 &= -a_1 \left[2\sigma_1 + n_4 + \frac{a_1^2}{8} + B_1 \left(1 - \frac{3}{4} B_1 \right) + S_1 \left(\frac{S_1}{4} + \frac{B_1}{2} - 1 \right) \right. \\
 &\quad \left. - \frac{3}{4} (C_1 + C_2)^2 \right], \\
 f_1 \sin \theta_1 &= -a_1 \left[\frac{C_2 N_2}{\omega^2 - 1} + (S_1 - 1)(C_1 + C_2) \right], \\
 f_2 \cos \theta_2 &= -a_2 \left[2\omega\sigma_2 + n_5 + n_6 + \frac{a_2^2}{8} \omega^2 + n_1 + n_2 - \frac{3}{4} (C_3 + \mu_1)^2 \right], \\
 f_2 \sin \theta_2 &= -a_2 \left[2\omega\sigma_2 + n_5 + n_6 + \frac{a_2^2}{8} \omega^2 + n_1 + n_2 - \frac{3}{4} (C_3 + \mu_1)^2 \right], \\
 f_3 \cos \theta_3 &= -a_3 \left[2\varpi\sigma_3 + \frac{M_1 M_3 \varpi^4}{1 - \varpi^2} + n_6 + \frac{a_3^2}{8} \varpi^2 + \frac{3}{4} \mu_2^2 + B_3 \varpi^2 \left(1 - \frac{3}{4} B_3 \right) \right], \\
 f_3 \sin \theta_3 &= -a_3 (n_3 + \mu_2 B_3 - \mu_2 \varpi),
 \end{aligned}
 \tag{49}$$

$$\begin{aligned}
 n_4 &= \frac{N_1 N_2 + M_1 M_2 - C_1 C_2}{\omega^2 - 1}, \\
 n_5 &= \frac{(N_1 N_2 \omega^2 - \mu_1 C_2) \omega^2}{1 - \omega^2}, \\
 n_6 &= \frac{(N_3 M_2 \omega^2 - \mu_2 C_3) \omega^2}{\varpi^2 - \omega^2}.
 \end{aligned}$$

Elimination of the modified phases θ_j from the previous system produces three nonlinear algebraic equations of amplitudes a_j and the frequency response functions that are clarified by the detuning parameters σ_j as follows

where

Table 5 Critical and peaks fixed points when detuning parameters σ_j have different values at $\omega = 0.4690$

Figure	Peaks points	Critical points	$\sigma_j (j = 1, 2, 3)$
Figure 21a	–	(−0.07, 0.00648693), (−0.07, 0.00648663), (−0.07, 0.00137394)	$\sigma_1 (= -0.1, 0, 0.1),$ $\sigma_2 (= -0.2, 0, 0.2)$
Figure 21b	–	(−0.07, 0.328121), (−0.07, 0.00301757), (−0.07, 0.00158162)	
Figure 21c	(−0.02138, 1.026)	(−0.07, 0.454955)	
Figure 22a	–	(−0.07, 0.00137394), (−0.07, 0.0034863), (−0.07, 0.00648693)	$\sigma_1 (= -0.1, 0, 0.1),$ $\sigma_3 (= -0.002, 0, 0.002)$
Figure 22ab	(0.2329, −0.06461), (0.3093, 0.01063)	(−0.07, 0.00228992)	
Figure 22ac	–	(−0.07, 1.04756), (−0.07, 1.02335), (0.07, 0.999136)	
Figure 23a	(−0.06815, 0.3073)	(−0.07, 0.301986)	$\sigma_2 (= -0.02, 0, 0.02),$ $\sigma_3 (= -0.003, 0, 0.003)$
Figure 23b	–	(−0.07, 0.00301757), (−0.07, 0.00331889), (−0.07, 0.00276641)	
Figure 23c	–	(−0.07, 1.02335), (−0.07, 1.05966), (−0.07, 0.987042)	

$$\begin{aligned}
 f_1^2 &= a_1^2 \left\{ 2\sigma_1 + n_4 + \frac{a_1^2}{8} + B_1 \left(1 - \frac{3}{4} B_1 \right) + S_1 \left(\frac{S_1}{4} + \frac{B_1}{2} - 1 \right) \right. \\
 &\quad \left. - \frac{3}{4} (C_1 + C_2)^2 \right\}^2 + \left[\frac{C_2 N_2}{\omega^2 - 1} + (S_1 - 1)(C_1 + C_2) \right]^2, \\
 f_2^2 &= a_2^2 \left\{ 2\omega\sigma_2 + n_1 + n_2 + n_5 + n_6 + \frac{a_2^2}{8} \omega^2 - \frac{3}{4} (C_3 + \mu_1)^2 \right\}^2 \\
 &\quad + \left[2\omega\sigma_2 + n_1 + n_2 + n_5 + n_6 - \frac{3}{4} (C_3 + \mu_1)^2 \right]^2, \\
 f_3^2 &= a_3^2 \left\{ 2\varpi\sigma_3 + \frac{M_1 M_3 \varpi^4}{1 - \varpi^2} + n_6 + \frac{a_3^2}{8} \varpi^2 + \frac{3}{4} \mu_2^2 + B_3 \varpi^2 \left(1 - \frac{3}{4} B_3 \right) \right\}^2 \\
 &\quad + (n_1 + \mu_2 B_3 - \mu_2 \varpi)^2.
 \end{aligned}
 \tag{50}$$

It is important to note that the case of steady-state solutions is considered an important part for the

stability’s examination. Therefore, to study the behavior near a neighborhood region of fixed points, let us consider the following substitutions into the above system of Eqs. (48) [42, 43]

$$\begin{aligned}
 a_1 &= a_{10} + a_{11}, & a_2 &= a_{20} + a_{21}, \\
 a_3 &= a_{30} + a_{31}, \\
 \theta_1 &= \theta_{10} + \theta_{11}, & \theta_2 &= \theta_{20} + \theta_{21}, \\
 \theta_3 &= \theta_{30} + \theta_{31},
 \end{aligned}
 \tag{51}$$

where a_{j0}, θ_{j0} are the solutions at the steady state of (49) and a_{j1}, θ_{j1} are the corresponding tiny perturbations. Therefore, the linearized system of (48) has the form

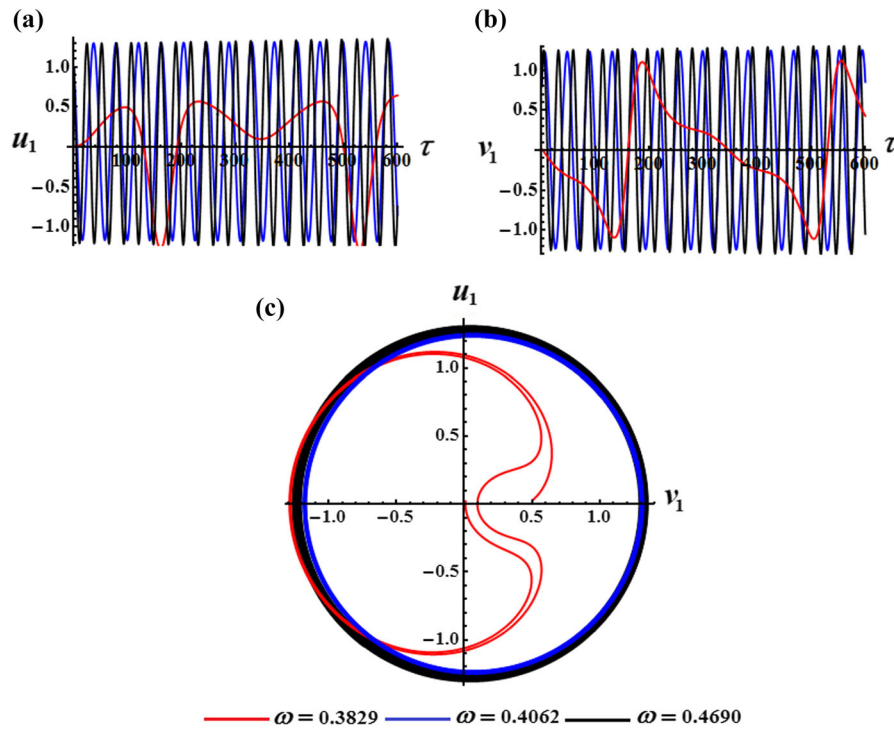


Fig. 24 **a** Variation of u_1 via time τ , **b** variation of v_1 versus time τ , **c** projections of the modulation equations’ paths on the $u_1 v_1$ plane when $\omega(= 0.3829, 0.4062, 0.4690)$

$$\begin{aligned}
 a_{10} \frac{d\theta_{11}}{d\tau} &= \frac{a_{11}}{2} \left[2\sigma_1 + n_1 + B_1 \left(1 - \frac{3}{4} B_1 \right) \right. \\
 &\quad \left. + S_1 \left(-1 + \frac{1}{2} B_1 + \frac{1}{4} S_1 \right) - \frac{3}{4} (C_1 + C_2)^2 + \frac{3}{8} a_{10}^2 a_{11} \right] \\
 &\quad - \frac{f_1}{2} \theta_{11} \sin \theta_{10}, \\
 \frac{da_{11}}{d\tau} &= \frac{a_{11}}{2} \left[\frac{C_2 N_2}{\omega^2 - 1} + (C_1 + C_2)(S_1 - 1) \right] \\
 &\quad + \frac{f_1}{2} \theta_{11} \cos \theta_{10}, \\
 a_{20} \frac{d\theta_{21}}{d\tau} &= \frac{a_{21}}{2} \left[2\sigma_2 + \frac{1}{\omega} (n_2 + n_3 + n_4) + \frac{a_{20}^2}{8} \omega - \frac{3}{4\omega} (C_3 + \mu_1)^2 \right], \\
 \frac{da_{21}}{d\tau} &= \frac{a_{21}}{2} \left[\frac{\omega^2 (C_2 N_2 + \mu_1 N_1)}{1 - \omega^2} + \frac{\mu_2 \omega^2 (M_2 + N_3)}{\omega^2 - \omega^2} \right. \\
 &\quad \left. + (C_3 + \mu_1) \left(\frac{S_2}{\omega} - 1 \right) \right] + \frac{f_2}{2\omega} \theta_{21} \cos \theta_{20}, \\
 a_{30} \frac{d\theta_{31}}{d\tau} &= \frac{a_{31}}{2} \left[2\sigma_3 + \frac{M_1 M_3 \omega^3}{1 - \omega^2} + \frac{n_3}{\omega} + \frac{3a_{30}^2}{8} + B_3 \omega \left(1 - \frac{3}{4} B_3 \right) \right. \\
 &\quad \left. + \frac{3}{4\omega} \mu_2^2 \right] - \frac{f_3}{2\omega} \theta_{31} \sin \theta_{30}, \\
 \frac{da_{31}}{d\tau} &= \frac{a_{31}}{2} \left[\frac{n_6}{\omega} + \mu_2 \left(\frac{B_3}{\omega} - 1 \right) \right] + \frac{f_3}{2\omega} \theta_{31} \cos \theta_{30}.
 \end{aligned}
 \tag{52}$$

The solutions of the previous system can be achieved if we represent a_{j1} and θ_{j1} exponentially as in the forms $q_k e^{\lambda T}$, where q_k ($k = 1, 2, \dots, 6$) are constants and λ denotes the unknown perturbations’ associated with their eigenvalues. The roots’ real parts of the following characteristic equations should not be positive value, if the solutions at steady state a_{j0} and θ_{j0} are stable asymptotically [44]

$$\lambda^6 + \Gamma_1 \lambda^5 + \Gamma_2 \lambda^4 + \Gamma_3 \lambda^3 + \Gamma_4 \lambda^2 + \Gamma_5 \lambda + \Gamma_6 = 0. \tag{53}$$

Here Γ_k are functions of the unperturbed parameters a_{j0} , θ_{j0} , and g_j (see Appendix 1).

The Routh–Hurwitz criteria [20] provide the necessary and sufficient requirements for steady-state solutions that can be expressed as follows

$$\begin{aligned}
 &\Gamma_1 > 0, \\
 &\Gamma_1\Gamma_2 - \Gamma_3 > 0, \\
 &\Gamma_1\Gamma_2\Gamma_3 - \Gamma_3^2 - \Gamma_1^2\Gamma_4 + \Gamma_1\Gamma_5 > 0, \\
 &\Gamma_1\Gamma_2\Gamma_3\Gamma_4 - \Gamma_3^2\Gamma_4 - \Gamma_1^2\Gamma_4^2 - \Gamma_1\Gamma_2^2\Gamma_5 + \Gamma_5\Gamma_2\Gamma_3 \\
 &\quad + 2\Gamma_1\Gamma_4\Gamma_5 - \Gamma_5^2 + \Gamma_1^2\Gamma_2\Gamma_6 - \Gamma_1\Gamma_6\Gamma_3 > 0, \\
 &\Gamma_1\Gamma_2\Gamma_3\Gamma_4\Gamma_5 - \Gamma_4\Gamma_5\Gamma_3^2 - \Gamma_1^2\Gamma_4^2\Gamma_5 \\
 &\quad - \Gamma_1\Gamma_2^2\Gamma_5^2 + \Gamma_5^2\Gamma_2\Gamma_3 + 2\Gamma_1\Gamma_4\Gamma_5^2 - \Gamma_5^3 - \Gamma_1\Gamma_2\Gamma_3^2\Gamma_6 \\
 &\quad + \Gamma_3^3\Gamma_6 + \Gamma_1^2\Gamma_6\Gamma_3\Gamma_4 + 2\Gamma_1^2\Gamma_2\Gamma_5\Gamma_6 \\
 &\quad - 3\Gamma_1\Gamma_5\Gamma_3\Gamma_6 - \Gamma_1^3\Gamma_6^2 > 0, \\
 &\Gamma_6(\Gamma_1\Gamma_2\Gamma_3\Gamma_4\Gamma_5 - \Gamma_4\Gamma_5\Gamma_3^2 - \Gamma_1^2\Gamma_4^2\Gamma_5 - \Gamma_1\Gamma_2^2\Gamma_5^2 \\
 &\quad + \Gamma_2\Gamma_3\Gamma_5^2 + 2\Gamma_1\Gamma_4\Gamma_5^2 - \Gamma_5^3 - \Gamma_1\Gamma_2\Gamma_3^2\Gamma_6 \\
 &\quad + \Gamma_3^3\Gamma_6 + \Gamma_1^2\Gamma_6\Gamma_3\Gamma_4 + 2\Gamma_1\Gamma_2\Gamma_5\Gamma_6 \\
 &\quad - 3\Gamma_1\Gamma_5\Gamma_3\Gamma_6 - \Gamma_1^3\Gamma_6^2) > 0.
 \end{aligned}
 \tag{54}$$

6 Analysis of system’s stability

In the present part of this section, the dynamical motion of the considered TRBP system in the presence of external moments M_j ($j = 1, 2, 3$) is examined using the linear stability analysis. The stability requirements are performed besides the modeling of the nonlinear system’s equations. Some parameters, such as detuning parameters σ_j and the natural frequencies $1, \varpi$, have been discovered to play a key role in undermining the stability requirements. A customized process with different system parameters has been used to plot the stability graphs of the system (48). The amplitudes a_j of the fluctuations versus time are plotted for distinct parametric regions, see Figs. 9, 10, 11, 12, 13, 14, 15, 16, 17, 18, 19, 20, 21, 22, and 23 that are drawn to show the impact of the σ_j values on the possible fixed points.

Overall, the areas of stable and unstable fixed points under the present constraints of the selected values of the impacted parameters, lie in the range $\sigma_j \leq -0.07$ and $-0.07 < \sigma_j$, respectively. It is important to note that the solid curves reflect the domain of stable fixed points, whereas the dashed curves denote the unstable ranges.

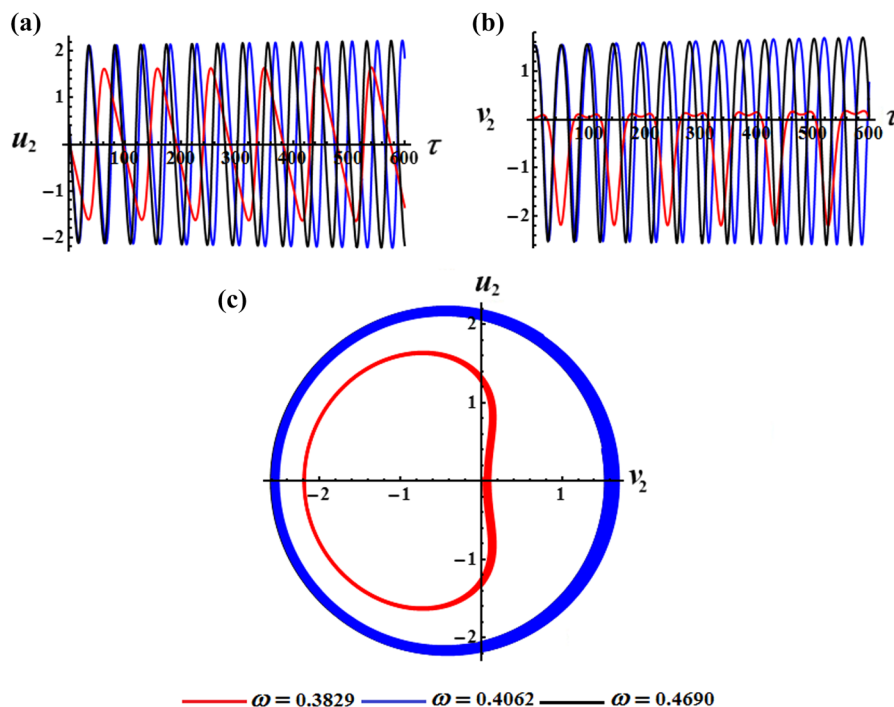


Fig. 25 a and b Variation of u_2 and v_2 via time τ , c projections of the modulation equations’ paths on the u_2v_2 plane when $\omega(= 0.3829, 0.4062, 0.4690)$

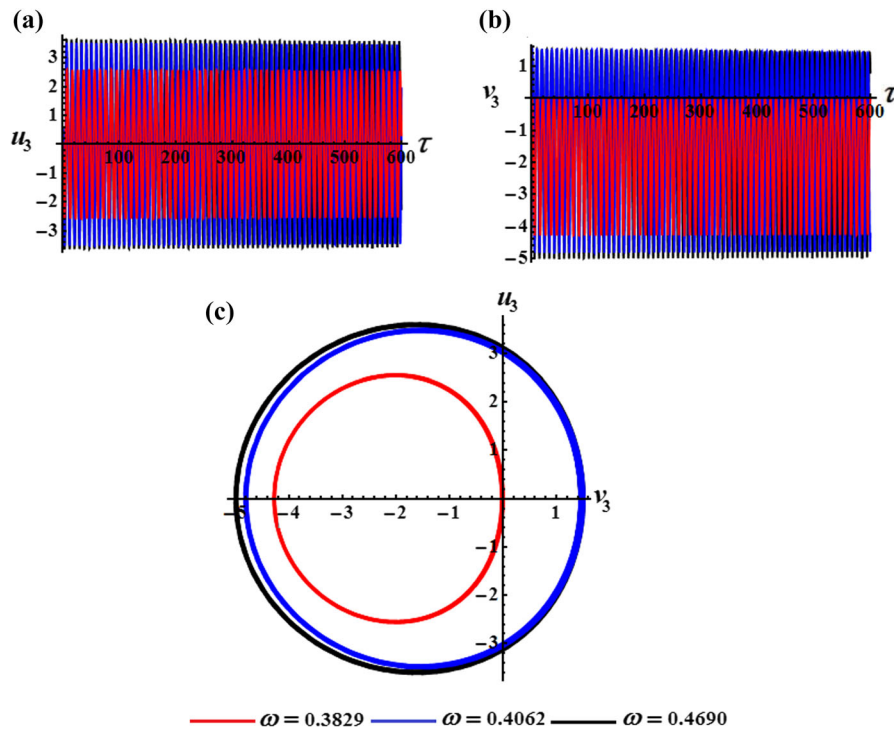


Fig. 26 a and b Variation of u_3 and v_3 via time τ , c projections of the modulation equations' paths on the u_3v_3 plane when $\omega(= 0.3829, 0.4062, 0.4690)$

No peaks are observed in the planes $a_1\sigma_3$ and $a_2\sigma_3$ except for three critical fixed points, as shown in parts (a) and (b) of Fig. 9, while there exist one peak and one critical fixed points in the plane $a_3\sigma_3$ when $\omega = 0.4062$ at $(\sigma_1 = -0.1, \sigma_3 = 0.2)$, $(\sigma_1 = \sigma_3 = 0)$, and $(\sigma_1 = 0.1, \sigma_3 = -0.2)$. It is clear from the third equation in the system (50) that a_3 is a function of σ_3 , so we get a curve as shown in Fig. 9c, this means that a_3 changes with σ_3 , while we get straight lines as shown in Fig. 9a and b. This means that the value of a_1 , a_2 are invariant with respect to σ_3 because they are functions of σ_1 and σ_2 as observed in the first and second equations of the system (50), respectively. A closer look at Fig. 10 reveals that it is graphed when $(\sigma_1 = 0.1, \sigma_3 = -0.002)$, $(\sigma_1 = -0.1, \sigma_3 = 0.002)$, and $(\sigma_1 = \sigma_3 = 0)$. Several critical points are drawn in part (a). The drawn curve in part (b) includes one peak at the point $(0.1287, 0.0253)$ and one critical fixed point in the plane $a_2\sigma_2$ at $\omega = 0.4062$. On the other hand, there exist three critical fixed points in Fig. 10c at the same considered values of the detuning parameters.

Curves of Fig. 11 are plotted when $(\sigma_2 = 0.02, \sigma_3 = -0.003)$, $(\sigma_2 = -0.02, \sigma_3 = 0.003)$, and $(\sigma_2 = \sigma_3$

$= 0)$, the peak fixed point appears in the plane $a_1\sigma_1$ of frequency response as in part (a). There are three critical fixed points are observed in the planes of frequency responses $a_2\sigma_1$ and $a_3\sigma_1$ as shown in Fig. 11b and c.

No peaks are observed in the planes $a_1\sigma_3$ and $a_2\sigma_3$ except for two and one critical fixed points, as shown in portions (a) and (b), respectively, of Fig. 12. In Fig. 13, there is one critical fixed point in the plane $a_1\sigma_3$ and $a_2\sigma_3$ while there exist one peak and one critical fixed points in the plane $a_3\sigma_3$ of Figs. 12, 13, 14. Moreover, three critical fixed points are observed in the plane $a_2\sigma_3$ of Fig. 14 when $\omega = 0.4062$ at $C_1(= 0.005, 0.01, 0.1), C_2(= 0.002, 0.004, 0.006), -\sigma_1 = -0.1$, and $\sigma_2 = 0.2$.

Several critical points are drawn in the planes $a_1\sigma_3$ and $a_2\sigma_3$, as shown in portions (a) and (b), respectively, of Figs. 15, 16 and 17, while there exists one peak and one critical fixed points in the plane $a_3\sigma_3$ when $\omega = 0.3829$ at $C_1(= 0.005, 0.01, 0.1), C_2(= -0.002, 0.004, 0.006), -\sigma_1 = -0.1$, and $\sigma_2 = 0.2$.

There are two critical fixed points in the plane $a_1\sigma_3$ of Fig. 18 while there exists one critical fixed point in

part (b) and one peak and one critical fixed points in part (c) at $\omega = 0.4690$, $C_1(= 0.005, 0.01, 0.1)$. In Fig. 19, the one peak and one critical fixed points exist in the plane $a_3\sigma_3$ while there is one critical fixed point in the plane $a_2\sigma_3$ and $a_1\sigma_3$ when $\omega = 0.4690$, $C_2(= -0.002, 0.004, 0.006)$. There are one and two critical points in parts (a) and (b) of Fig. 20, respectively. There exists two critical points and one peak in part (c) at $\omega = 0.4690$ and $C_3(= 0.004, 0.006, 0.008)$.

No peaks are observed in the planes $a_1\sigma_3$ and $a_2\sigma_3$ except for three critical fixed points, as drawn in parts (a) and (b) of Fig. 21, while there exists essential one peak and one critical fixed points in the plane $a_3\sigma_3$ when $\omega = 0.4690$ at $(\sigma_1 = -0.1, \sigma_3 = 0.2)$, $(\sigma_1 = \sigma_3 = 0)$, and $(\sigma_1 = 0.1, \sigma_3 = -0.2)$. A closer examination of the curves of Fig. 22 shows that it is graphed when $(\sigma_1 = 0.1, \sigma_3 = -0.002)$, $(\sigma_1 = -0.1, \sigma_3 = 0.002)$, and $(\sigma_1 = \sigma_3 = 0)$. Several critical are drawn in part (a). The drawn curve in part (b) includes two peaks and one critical fixed point in the plane $a_2\sigma_2$ at $\omega = 0.4690$. On the other hand, there are three crucial critical fixed points in Fig. 22c at the same considered values of the detuning parameters.

Curves of Fig. 23 are drawn when $(\sigma_2 = 0.02, \sigma_3 = -0.003)$, $(\sigma_2 = -0.02, \sigma_3 = 0.003)$, and $(\sigma_2 = \sigma_3 = 0)$, the peak fixed point appears in the plane $a_1\sigma_1$ of frequency response as in part (a). There are three observed fundamental critical fixed points in the planes of frequency responses $a_2\sigma_1$ and $a_3\sigma_1$ as shown in Fig. 23b and c. Tables 1 and 5 show the relation between the critical and peaks fixed points and the values of the parameters σ_j , and ω , while Tables 2, 3, 4 show the relation between the critical and peaks fixed points at the considered values of the parameters C_j and ω , respectively (Table 5).

7 Nonlinear analysis

This section examines the stability of the nonlinear amplitude of Eq. (48) as well as exhibiting its characteristics. Therefore, the following transformations are considered [45, 46]

$$A_j = \frac{1}{2} [\tilde{u}_j(\tau_1, \tau_2) + i \tilde{v}_j(\tau_1, \tau_2)] e^{-i\tilde{\sigma}_j \tau_1} \quad (j = 1, 2, 3);$$

$$u_j = \varepsilon \tilde{u}_j, \quad v_j = \varepsilon \tilde{v}_j, \tag{55}$$

where u_j and v_j are the real and imaginary parts of the amplitudes A_j , respectively.

Substituting (14) and (87) into (33)–(35), and consequently separating real and imaginary part to yield

$$\begin{aligned} \frac{dv_1}{d\tau} + \frac{1}{16}(u_1^3 + u_1 v_1^2) + \frac{1}{2}[\sigma_1 - \frac{3}{4}B_1^2 + \frac{1}{4}S_1^2 \\ + \frac{1}{2}(B_1 - S_1) + \frac{1}{2}B_1S_1 - \frac{3}{4}(C_1 + C_2)^2 \\ + \frac{1}{\omega^2 - 1}(M_1M_3 + N_1N_2 - C_2\mu_1)] u_1 \\ - \frac{1}{2} [S_1(C_1 + C_2) + \frac{N_1\mu_1 + N_2C_2}{\omega^2 - 1} + \frac{1}{2}(C_1 + C_2)] \\ v_1 + \frac{f_1}{2} = 0, \end{aligned}$$

$$\begin{aligned} \frac{du_1}{d\tau} + \sigma_1 v_1 + \frac{1}{2}(B_1 - S_1) v_1 - \frac{1}{2}(C_1 + C_2) u_1 \\ + \frac{1}{16}(v_1^3 + v_1 u_1^2) \\ + \frac{1}{2} [\frac{1}{4}S_1^2 - \frac{3}{4}B_1^2 + \frac{1}{2}B_1S_1 - \frac{3}{4}(C_1 + C_2)^2 \\ + \frac{M_1M_3 + N_1N_2 - C_2\mu_1}{\omega^2 - 1}] v_1 \\ + \frac{1}{2} [S_1(C_1 + C_2) + \frac{N_1\mu_1 + N_2C_2}{\omega^2 - 1}] u_1 = 0, \end{aligned}$$

$$\begin{aligned} \omega \frac{dv_2}{d\tau} + \sigma_2 u_2 \omega + \frac{1}{2}(B_2\omega^2 - S_2) u_2 + \frac{1}{2}\omega(C_3 + \mu_1) v_2 \\ + \frac{1}{16}\omega^2(u_2^3 + u_2 v_2^2) + \frac{1}{2}[\frac{1}{4\omega^2}S_2^2 - \frac{3}{4}B_2^2\omega^2 + \frac{1}{2}B_2S_2 \\ - \frac{3}{4}(C_3 + \mu_1)^2 + \frac{\omega^2(N_1N_2\omega^2 - C_2\mu_1)}{1 - \omega^2} + \frac{\omega^2(M_2N_3\omega^2 - C_3\mu_2)}{\omega^2 - \omega^2}] u_2 \\ - \frac{1}{2} [\frac{S_2}{\omega}(C_3 + \mu_1) + \frac{\omega^3(N_1\mu_1 + N_2C_2)}{1 - \omega^2} + \frac{\omega^3(N_3\mu_2 + M_2\mu_2)}{\omega^2 - \omega^2}] v_2 + \frac{f_2}{2} = 0, \end{aligned}$$

$$\begin{aligned}
 &\omega \frac{du_2}{d\tau} - \sigma_2 v_2 \omega + \frac{1}{2}(B_2 \omega^2 - S_2) v_2 \\
 &\quad - \frac{1}{2} \omega (C_3 + \mu_1) u_2 - \frac{1}{16} \omega^2 (v_2^3 + v_2 u_2^2) \\
 &\quad - \frac{1}{2} \left[\frac{1}{4\omega^2} S_2^2 - \frac{3}{4} B_2^2 \omega^2 + \frac{1}{2} B_2 S_2 - \frac{3}{4} (C_3 + \mu_1)^2 \right. \\
 &\quad \left. + \frac{\omega^2 (N_1 N_2 \omega^2 - C_2 \mu_1)}{1 - \omega^2} + \frac{\omega^2 (M_2 N_3 \omega^2 - C_3 \mu_2)}{\omega^2 - \omega^2} \right] v_2 \\
 &\quad + \frac{1}{2} \left[\frac{S_2}{\omega} (C_3 + \mu_1) + \frac{\omega^3 (N_1 \mu_1 + N_2 C_2)}{1 - \omega^2} + \frac{\omega^3 (N_3 \mu_2 + M_2 \mu_2)}{\omega^2 - \omega^2} \right] \\
 &u_2 = 0, \\
 &\omega \frac{dv_3}{d\tau} + \frac{1}{2} \omega \mu_2 v_3 + \frac{1}{16} \omega^2 (u_3^3 + u_3 v_3^2) \\
 &\quad + \frac{1}{2} \left[\frac{3}{4} \mu_2^2 - \frac{1}{4} B_3^2 \omega^2 + \frac{\omega^4 M_1 M_3}{1 - \omega^2} + \frac{\omega^2}{\omega^2 - \omega^2} (M_2 N_3 \omega^2 - C_3 \mu_2) + \sigma_3 \omega \right] u_3 \\
 &\quad - \frac{1}{2} \left[B_3 \omega \mu_2 + \frac{\omega^3 (M_2 \mu_2 + N_3 C_3)}{\omega^2 - \omega^2} \right] v_3 + \frac{f_3}{2} = 0, \\
 &\omega \frac{du_3}{d\tau} + \frac{1}{2} \omega \mu_2 u_3 - \frac{1}{16} \omega^2 (v_3^3 + v_3 u_3^2) \\
 &\quad - \frac{1}{2} \left[\frac{3}{4} \mu_2^2 - \frac{5}{4} B_3^2 \omega^2 + \frac{\omega^4 M_1 M_3}{1 - \omega^2} + \frac{\omega^2 (M_2 N_3 \omega^2 - C_3 \mu_2)}{\omega^2 - \omega^2} - \sigma_3 \omega \right] v_3 \\
 &\quad - \frac{1}{2} \left[(B_3 \omega \mu_2 + \frac{\omega^3 (M_2 \mu_2 + N_3 C_3)}{\omega^2 - \omega^2}) \right] u_3 = 0. \tag{56}
 \end{aligned}$$

The adjusted amplitudes were then verified over time in various parametric zones, and the amplitudes’ characteristics are depicted in phase plane curves as illustrated in Figs. 24, 25 and 26. The values of the parameters are set to the values listed below

$$\begin{aligned}
 &\sigma_1 = -0.1, \quad \sigma_2 = 0.2, \quad \sigma_3 = 0.3, \\
 &\omega (= 0.3829, 0.4062, 0.4690), \quad u_1(0) = 1, \\
 &v_1(0) = 0.8, \quad u_2(0) = 1.5, \\
 &v_2(0) = 0.4, \quad u_3(0) = 1.5, \quad v_3(0) = 0.5.
 \end{aligned}$$

Portions (a) and (b) of Figs. 24, 25 and 26 describe the variation of the adjusted phases via the dimensionless time τ , while parts (c) of the same figures represent the projections of the modulation equation trajectories on the plane $u_j v_j$ when ω have the above different values. The plotted curves of the waves

illustrating the time histories of u_j and v_j behave periodic attitudes. The oscillation number increases with the increase in the frequency value ω , while the wavelengths decrease. However, the raising of ω values leads to increase in the amplitudes behavior as shown in Fig. 26. The plotted closed curves in parts (c) indicate that the above modulation system behaves in a stable manner.

8 Conclusion

An externally influenced TRBP dynamical system with 3 DOFs has been investigated as a novel model. The regulating nonlinear differential equations are derived using Lagrange’s equations from second kind. The strategy of the approximate analytic solutions up to the

third-order of approximation is investigated using the MSA. The prerequisites for solvability are met by removing secular terms. The emerging resonance cases are detected, and the equations of modulation are achieved. The frequency responses curves and time histories of the obtained new results are visually displayed to emphasize the beneficial effects of the various parameters on the motion. The numerical results of the motion's governing system are gained using the Runge–Kutta fourth-order method. The comparison between both results demonstrates that the used perturbation technique is extremely accurate. The steady-state solutions are investigated, and the zones of stability and instability are evaluated using Routh–Hurwitz conditions. This work is significant because of its applications in engineering vibrational control, which gives the researched system a lot of weight.

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Author contributions **T.S. Amer:** Conceptualization, Methodology, Data curation, Supervision, Validation, Visualization and Reviewing. **F.M. El-Sabaa:** Resources, Conceptualization, Formal analysis, Supervision, Visualization and Reviewing. **S.K. Zakria:** Visualization, Conceptualization, Investigation, Writing- Original draft preparation. **A.A. Galal:** Supervision,

Resources, Conceptualization, Methodology, Visualization, Reviewing and editing.

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Declarations

Conflict of Interest The authors have reported that there is no conflict of interest.

Data Availability Data sharing is not appropriate for this research because no datasets were created or analyzed.

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Appendix 1

$$\Gamma_1 = \frac{1}{2} \left[-2(d_2 + d_5 + d_8) + \frac{\sin \theta_{10} f_1}{a_{10}} + \frac{\sin \theta_{20} f_2}{\omega a_{20}} + \frac{\sin \theta_{30} f_3}{\varpi a_{30}} \right],$$

$$\Gamma_2 = \frac{1}{4\omega\varpi a_{10}a_{20}a_{30}} [2\omega\varpi(-2a_{10}a_{30}d_4d_6 - a_{20}a_{30}(d_7d_9 + d_2d_5 + (d_2 + d_5)d_8 - 2d_1d_3 - (d_2 + d_5 + d_8) \sin \theta_{10}f_1)) + \varpi \sin \theta_{20}a_{30}(-2(d_2 + d_5 + d_8)a_{10} + \sin \theta_{10}f_1)f_2 + \sin \theta_{30}(\omega a_{20}(-2(d_2 + d_5 + d_8)a_{10} + \sin \theta_{10}f_1) \sin \theta_{20}a_{10}f_2)f_3],$$

$$\Gamma_3 = \frac{1}{8\omega\varpi a_{10}a_{20}a_{30}} [4\omega\varpi(2d_1d_3(d_5 + d_8)a_{20}a_{30} + \sin \theta_{10}(-d_4d_6a_{30} + a_{20}(-d_7d_9 + d_2d_5(1 + d_8)a_{30})f_1 + 2\varpi \sin \theta_{20}a_{30}(-2d_1d_3 - (d_2 + d_5 + d_8) \sin \theta_{10}f_1)f_2 + \sin \theta_{30}(2\omega a_{20}(-2d_1d_3 - (d_2 + d_5 + d_8) \sin \theta_{10}f_1) + \sin \theta_{10} \sin \theta_{20}f_1f_2)f_3 + 2a_{10}(4\varpi\omega(d_4d_6(d_2 + d_8)a_{30} + a_{20}((d_2 + d_5)d_7d_9 - d_2d_5d_8a_{30}))) + 2\varpi \sin \theta_{20}(-d_7d_9 + d_2d_5(1 + d_8)a_{30})f_2 + \sin \theta_{30}(-2d_4d_6\omega + 2(d_5d_2 + d_8(d_2 + d_5)\omega a_{20} - (d_2 + d_5 + d_8) \sin \theta_{20}f_2)f_3)],$$

$$\Gamma_4 = \frac{1}{8\omega\varpi a_{10}a_{20}a_{30}} [4\omega\varpi d_4d_6a_{30}(2d_1d_3 + (d_2 + d_8) \sin \theta_{10}f_1) + 2\varpi \sin \theta_{20}(2d_1d_3(d_5 + d_8)a_{30} + \sin \theta_{10}(-d_7d_9 + (d_2d_5 + (d_2 + d_5)d_8)a_{30})f_1)f_2 + \sin \theta_{30}(-2d_4d_6\omega \sin \theta_{10}f_1 + \sin \theta_{20}(-2d_1d_3 - (d_2 + d_5 + d_8) \sin \theta_{10}f_1)f_2)f_3 + 2\omega a_{20}(4d_1d_3\varpi(d_7d_9 - d_5d_8a_{30}) + 2\varpi \sin \theta_{10}((d_2 + d_5)d_7d_9 - d_2d_5d_8a_{30})f_1 + \sin \theta_{30}(2d_1d_3(d_5 + d_8) + (d_2d_5 + (d_2 + d_5)d_8) \sin \theta_{10}f_1)f_3) + 2a_{10}(4\omega\varpi(d_4d_6d_7d_9 - d_2(d_5d_7d_9a_{20} + d_4d_6d_8a_{30})) + 2\varpi \sin \theta_{20}((d_2 + d_5)d_7d_9 - d_2d_5d_8a_{30})f_2 + \sin \theta_{30}(2d_4d_6(d_2 + d_8)\omega - 2d_2d_5d_8\omega a_{20} - 2d_2d_5d_8\omega a_{20} + (d_2d_5 + (d_2 + d_5)d_8) \sin \theta_{20}f_2)f_3)],$$

$$\Gamma_5 = \frac{1}{8\omega\varpi a_{10}a_{20}a_{30}} [4\omega\varpi d_4d_6(-2d_1d_3d_8a_{30} + \sin \theta_{10}(d_7d_9 - d_2d_8a_{30})f_1) + 2\varpi \sin \theta_{20}(2d_1d_3(d_7d_9 - d_5d_8a_{30}) + \sin \theta_{10}((d_2 + d_5)d_7d_9 - d_2d_5d_8a_{30})f_1)f_2 + \sin \theta_{30}(2d_4d_6\omega(2d_1d_3 + (d_2 + d_8) \sin \theta_{10}f_1) + \sin \theta_{20}(2d_1d_3(d_5 + d_8) + (d_2d_5 + (d_2 + d_5)d_8) \sin \theta_{10}f_1)f_2)f_3 - 2d_5\omega a_{20}(2d_1d_3 + d_2 \sin \theta_{10}f_1)(2d_7d_9\varpi + d_8 \sin \theta_{30}f_3) - 2d_2a_{10}(2d_4d_6\omega + d_5 \sin \theta_{20}f_2)(2d_7d_9\varpi + d_8 \sin \theta_{30}f_3)],$$

$$\Gamma_6 = \frac{-1}{8\omega\varpi a_{10}a_{20}a_{30}} [(2d_1d_3 + d_2 \sin \theta_{10}f_1)(2d_4d_6\omega + d_5 \sin \theta_{20}f_2)(2d_7d_9\varpi + d_8 \sin \theta_{30}f_3)]$$

where

$$d_3 = \frac{1}{2}f_1 \cos \theta_{10},$$

$$d_1 = \sigma_1 + \frac{n_4}{2} + \frac{3a_{10}^2}{16} + \frac{1}{2}B_1 \left(1 - \frac{3}{4}B_1 \right) + \frac{S_1}{2} \left(-1 + \frac{B_1}{2} + \frac{S_1}{4} \right) - \frac{3}{8}(C_1 + C_2)^2,$$

$$d_4 = \sigma_2 + \frac{1}{2\omega}(n_1 + n_2 + n_5 + n_6) - \frac{3}{8\omega}(C_3 + \mu_1)^2 + \frac{3\omega a_{20}^2}{16},$$

$$d_2 = \frac{N_2C_2}{2(\omega^2 - 1)} + \frac{1}{2}(C_1 + C_2)(S_1 - 1),$$

$$d_5 = \frac{1}{2} \left(-1 + \frac{S_2}{\omega} \right) (\mu_1 + C_3) + \frac{\omega^2 (C_2 N_2 + \mu_1 N_1)}{2(1 - \omega^2)} + \frac{\mu_2 \omega^2 (M_2 + N_3)}{2(\varpi^2 - \omega^2)},$$

$$d_6 = \frac{f_2 \cos \theta_{20}}{2\omega},$$

$$d_7 = \sigma_3 + \frac{3\varpi a_{30}^2}{16} + \frac{1}{2} \varpi B_3 \left(1 - \frac{3}{4} B_3 \right) + \frac{3}{8\varpi} \mu_2^2 + \frac{M_1 M_3 \varpi^3}{2(1 - \varpi^2)} + \frac{N_3 M_2 \varpi^3 - \mu_2 C_3 \varpi}{2(\omega^2 - \varpi^2)},$$

$$d_8 = \frac{-\mu_2}{2} \left(1 - \frac{B_3}{\varpi} \right) + \frac{n_3}{2\varpi},$$

$$d_9 = \frac{f_3}{2\varpi} \cos \theta_{30}.$$

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