



# Thermally stimulated discharge (TSD) study of low-temperature transitions in chlorine-containing polymers

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## Abstract

Thermally stimulated discharge current (TSD) tests on PVC, chlorinated polyethylene, chlorinated PVC, and chlorinated paraffins always show a relatively low-intensity transition in the  $-100$  to  $-80$  °C range. Several chlorine-containing polymers and one chlorinated paraffin were tested up to 70% chlorine content by short-circuited TSD method. The intensities of these transitions show a maximum at about 40% chlorine content except for PVC. Knowing the random nature of chlorination, it is assumed that this transition originates from the rotational movement of neighboring  $-\text{CH}_2-\text{CHCl}-$  monomeric units.

**Keywords** TSD · PVC · Chlorinated polyethylene · Relaxation process

## Abbreviations

PVC	Poly(vinyl chloride)
CPVC	Chlorinated PVC
CPE	Chlorinated polyethylene
CP	Chlorinated paraffin
DMA	Dynamic mechanical analysis
TSD	Thermally stimulated discharge

$\tau$	Relaxation time (s)
$\tau_0$	Preexponential factor (s)
$\vartheta$	Temperature in centigrades (°C)

## List of symbols

$A$	Energy of activation ( $\text{J mol}^{-1}$ ; $\text{kJ mol}^{-1}$ ; $\text{eV/molecule}$ )
$\mathcal{A}$	Area ( $\text{m}^2$ ; $\text{cm}^2$ )
$E$	Electric field ( $\text{Vm}^{-1}$ ; $\text{kV mm}^{-1}$ )
$I$	Current (in general) (A)
$I_d$	Depolarization current (pA)
$I_m$	Peak current (pA)
$Q$	Electric charge (As; pAs)
$T$	Absolute temperature (K)
$R$	Gas constant ( $8.314 \text{ J mol}^{-1} \text{ K}^{-1}$ ; $5.189 \cdot 10^{-19} \text{ eV mol}^{-1} \text{ K}^{-1}$ .)
$\epsilon_0$	Dielectric constant of vacuum ( $8.854 \cdot 10^{-12} \text{ F m}^{-1}$ )
$\Delta\epsilon$	Relaxation strength ( $\epsilon_{r0}-\epsilon_{r\infty}$ ) here ( $\sigma/E\epsilon_0$ )
$\sigma$	Charge density ( $\text{As m}^{-2}$ )

## Introduction

Chlorine-containing polymers are widely used in everyday life. The best known of them is polyvinyl chloride (PVC), the third most important commodity polymer. Chlorinated polyethylene (CPE) is used as impact modifier, flame retardant additive and in paints. Chlorinated PVC (CPVC) has high glass transition temperature and has an important role in hot-water piping. Polychloroprene (Neoprene) is an important synthetic rubber. Chlorinated paraffins (CP) are used as secondary plasticizers and flame retardants. The chlorine-containing polymers are thoroughly investigated; most of their relaxation processes are known. Some of them, in particular the randomly chlorinated polymers (CPE, CPVC), have multiple transitions. Hedvig [1] demonstrated  $\alpha$  and  $\beta$  relaxation of PVC; these are detectable by dynamic mechanical analysis (DMA), AC dielectric and TSD methods as well. Despite of the high polarity of the  $-\text{C}-\text{Cl}$  bond, few references can be found on the low-temperature peak of chlorine-containing polymers. Galop [2] used short-circuit TSD for testing polymers and stated that the frozen-in stresses also produce depolarization current. Interestingly, a low-temperature peak was found in polypropylene at  $-50$  °C and explained as “relaxation of lateral groups.” del Val [3] used the analogous mechanical method, the thermally stimulated creep (TSC) for testing PVC and

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PVC-CPE blends. Deformation rate curves were resolved by windowing technique and found low-temperature transitions at about  $-80\text{ }^{\circ}\text{C}$  for all tested polymers. This transition was assigned to  $\beta$  relaxation. However,  $\beta$  relaxation of PVC is in the range of  $-30\text{ }^{\circ}\text{C}$  [4]. Guarrotxena [5] used the TSD technique for chlorinated PVC. This material contains less  $-\text{CH}_2-\text{CHCl}-$  monomer units because of the chlorination of the neighboring carbon atoms, while the frequency of  $-\text{CHCl}-$  units increases. However, the depolarization processes below  $0\text{ }^{\circ}\text{C}$  were not investigated.

Kollár and Zsoldos [6] tested PVC-PE blends by different thermal methods but over  $-80\text{ }^{\circ}\text{C}$  and observed the  $\beta$  relaxation of PVC only. Mahrous [7] investigated CPVC-polyester blends by TSD but over room temperature only.

Nogales [8] used combined dielectric techniques (TSD and A.C. dielectric) for investigation of molecular motions in PVC without deeply analyzing the low temperature region.

Several TSD measurements on chlorine-containing polymers revealed that there is peak of low intensity in the  $-100$  to  $-75\text{ }^{\circ}\text{C}$  range and its origin is not known [9].

## Experimental

### Materials

Chlorinated polyethylene samples up to 33.8% chlorine content were taken from the BorsodChem's CPE plant reactors. During this process, additive-free high-density polyethylene powder is chlorinated in aqueous slurry. To avoid the blocking of material the reaction temperature must be kept below the melting temperature of PE, while the Cl content is less than 17–19%. Thereafter, the temperature is increased. Samples were taken from the reactor then washed acid free and dried. CPE-36, 40 and 48 were also industrial products from the same raw material. CPE-53 and 60 are experimental grades produced in pilot plant reactors.

PVC sample was a commercial suspension type of 58 K-value. CPVC a low molecular weight (injection molding grade) type of 68% Cl content.

The 70% chlorine-containing material was commercial-type solid chlorinated paraffin (CP) intended for use as flame retardant.

### Sample preparation

All polymer samples were prepared by roll milling on a Schwabenthan 150U electrically heated laboratory roll-mill at 20/24 rpm (front/back).  $160\text{ }^{\circ}\text{C}$  was used for CPE,  $175\text{ }^{\circ}\text{C}$  for PVC and  $190\text{ }^{\circ}\text{C}$  for CPVC. CPE was stabilized with 1 phr calcium stearate. PVC and CPVC samples were stabilized with 1.5 phr organotin stabilizer. The different rheological behaviors made necessary the different processing

temperatures. CPVC, e.g., cannot melt at the optimal rolling temperature of CPE.

Roll-milled sheets of about 0.5–1 mm thickness were compression molded over the roll milling temperature by  $5\text{ }^{\circ}\text{C}$ . The actual thickness was used in the evaluation program. Disks were die cut, and gold electrodes were sputter coated. The thickness of gold electrodes was about 8–10 nm. The chlorinated paraffin was soaked onto borosilicate filter paper (SIGMA F7769;  $2.6\text{ }\mu\text{m}$ , relative pore volume  $87 \pm 2\%$ ). The method was described in detail in the previous paper [10].

### Instruments

The TSD measurements were carried out with the TSD part of Multirelax instrument constructed by Múanyag-ipari Kutató Intézet (Research Institute of Plastics, Budapest) described in [11, 12]. Polarizing supply was designed and assembled by the author.

Summarized technical data of the instrument:

Electrometer sensitivity: 0.1 pA to 1 mA.

Temperature range:  $-150$  to  $250\text{ }^{\circ}\text{C}$ .

Sample size: 53 mm diameter, 0.05–1 mm thickness.

Electrode size: 38 mm diameter ( $11.3\text{ cm}^2$ ).

Heat transfer: metal (brass) block.

Cooling: liquid nitrogen.

Cooling and heating rate:  $1\text{ K min}^{-1}$  (fixed).

Polarizing voltage: 60 V to 3 kV.

Actual polarizing voltage: 1200 V.

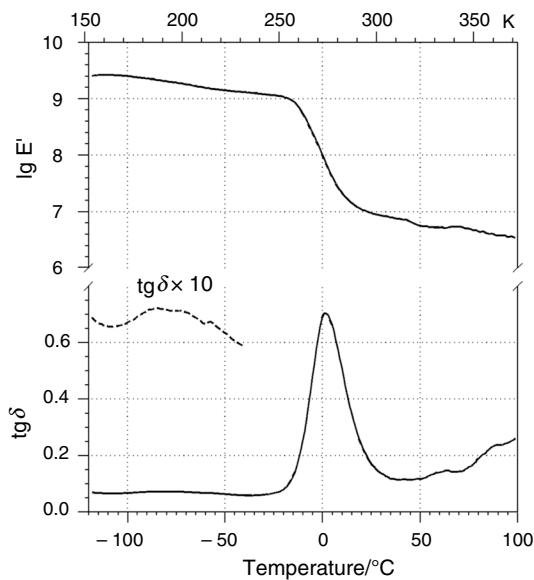
Dynamic mechanical measurement (demonstrated in Fig. 1.) was performed with a Rheometric Scientific DMTA MK-III instrument in dual cantilever mode at 1 Hz frequency and  $64\text{ }\mu\text{m}$   $p-p$  amplitude equivalent to about 0.1% deformation. Heating rate was  $2\text{ K min}^{-1}$  in the  $-120$  to  $100\text{ }^{\circ}\text{C}$  range.

### Brief description of the experimental technique and evaluation

The usual representation of a TSD measurement is a function of current against temperature. For the sake of simpler comparison normalization of the measured current is suggested, i.e., transforming the raw curves to equal electrode area and electric field. In this paper, all results are transformed to a field of  $1\text{ kVmm}^{-1}$  and to a  $30\text{ cm}^2$  electrode area as described in [4, 10].

The evaluation program was compiled by the author.

In the case of short circuit TSD during depolarization, the external field is zero, the obtained current is the algebraic sum of the currents originating from the overlapping processes.



**Fig. 1** DMA curve of CPE containing 30.6% chlorine by mass (910/9)

$$I_{d(T)} = \sum_{i=1}^n I_{d(T)_n} \quad (1)$$

The energies of activation values were determined from the half-width of the peaks as described in [11]. Individual transitions are calculated by Eq. (13) in the same paper.

The  $\Delta\epsilon$  relaxation strength represents the permittivity change during the depolarization:

$$\Delta\epsilon = \sigma / E\epsilon_0 \quad (2)$$

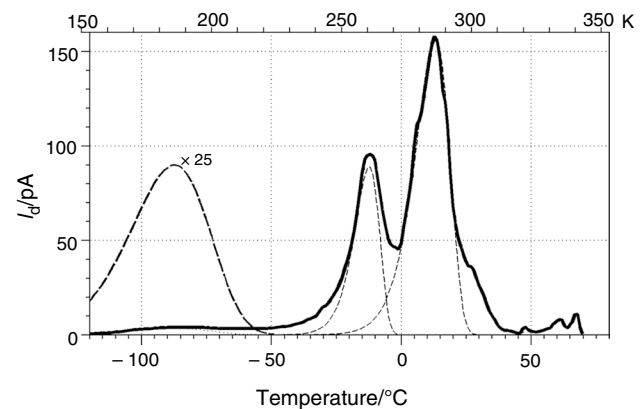
$E$  is the polarizing field,  $\sigma$  is the surface charge density, and  $\epsilon_0$  is the permittivity of vacuum:

$$\sigma = Q/A \quad (3)$$

where  $A$  is the electrode area;  $Q$  is the full charge of a transition and can be determined by integration of current by time.

## Results and discussion

Because of the stepwise chlorination of polyethylene, the CPE always consists of two structural unique units. One of them has higher, the other lower chlorine content than the average as it was demonstrated by a swelling procedure in a former paper [13]. However, dynamic mechanical method (DMA) shows a single broad transition only (Fig. 1), while the TSD reveals these phases and gives well-separated peaks as shown in Fig. 2. The high resolving power of TSD makes the analysis of the low temperature region possible.



**Fig. 2** TSD curve of CPE containing 30.6% chlorine by mass (910/9) Dashed line represents the resolved elementary transitions

**Table 1** Materials and TSD results

Cl %	Material	$\vartheta_{\max}/^{\circ}\text{C}$	$I_{\max}/\text{pA}$	$\Delta\epsilon$	$A_d/\text{kJmol}^{-1}$
7.5	910/2	-83	1	0.06	26.5
10.5	910/3	-93.5	1.8	0.147	15.5
14.8	910/4	-91.5	1.55	0.094	24
17.8	910/5	-86	1.25	0.068	28.5
21.0	910/6	-88.8	1.9	0.13	21
24.1	910/7	-83.5	1.9	0.12	24
27.0	910/8	-85.6	3.25	0.206	25
30.6	910/9*	-87	3.6	0.3	17.4
33.8	910/10	-88.3	3.3	0.21	24
36.0	CPE product	-81	3.9	0.26	25
40.0	CPE product	-83.2	4.3	0.34	20
48.0	CPE product	-72	3	0.28	20
53.0	CPE experimental	-89	2.04	0.178	15.7
56.7	PVC $K=58$	-87.8	2.7	0.32	13.8
65.0	CPE experimental	-78	1.04	0.049	37
68.0	CPVC	-104.8	2.4	0.019	31.3
70.0	Chlorinated paraffin	-105	0.11	0.0037	40

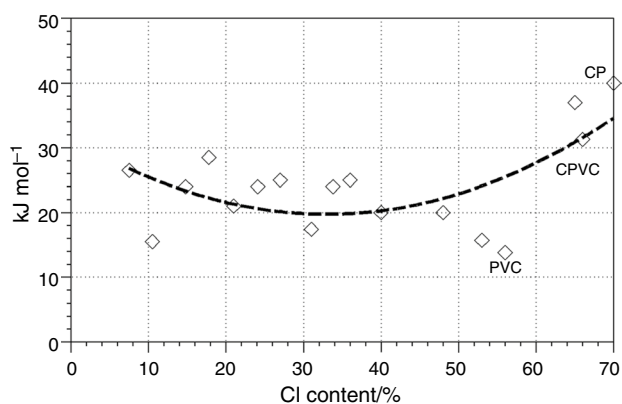
910 samples 2–10 taken from the industrial chlorination autoclave

\*sample for demonstrating DMA and TSD curves

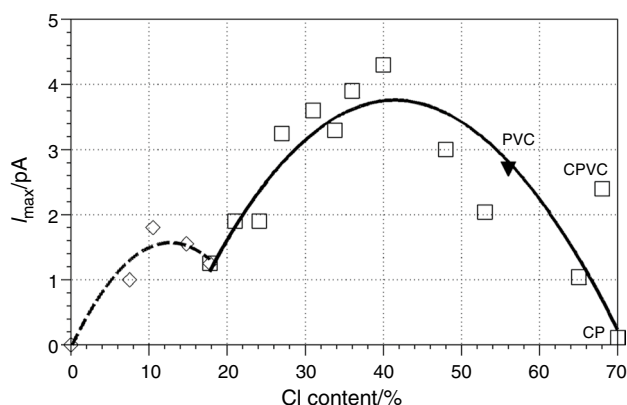
The DMA and the main transitions are not the target of this paper.

All chlorine-containing materials tested show a weak transition in the  $-120 \dots -70$   $^{\circ}\text{C}$  range. This transition is demonstrated in Fig. 2 magnified 25 times. The data of results on all tested materials are summarized in Table 1.

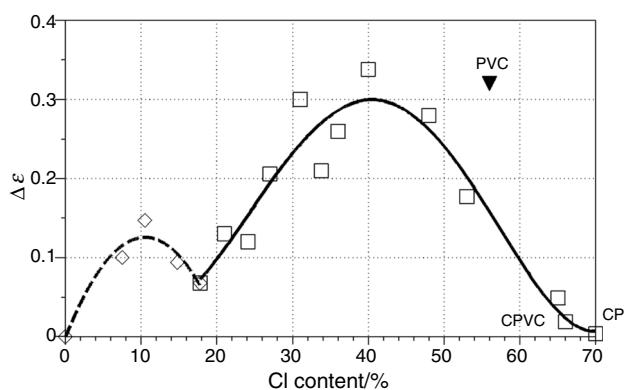
Energy of activation values is relatively low, and the scattering of the values is considerable as shown in Fig. 3. Plotting the current maxima of normalized currents as function of chlorine content in Fig. 4 shows a bimodal curve. Plotting the relaxation strength ( $\Delta\epsilon$ ) in Fig. 5, the result is similar. The first maximum occurs at about 10–12% by mass, and the



**Fig. 3** Calculated energy of activation of low-temperature peak of polymers and CP vs. chlorine content

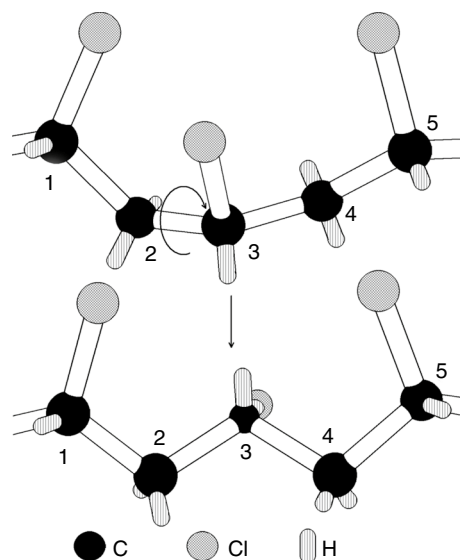


**Fig. 4** Current maxima of low-temperature peak of polymers and CP vs. chlorine content



**Fig. 5** Relaxation strength ( $\Delta\epsilon$ ) of low-temperature peak of polymers and CP vs. chlorine content

second one at about 40% by mass in both representations. This peak maximum is well below the chlorine content of PVC (56.7%).



**Fig. 6** The two extreme states of  $-\text{CH}_2-\text{CHCl}-$  parts if the position of carbon atoms 1 and 5 are fixed

It is assumed that this low-temperature transition in Cl containing polymers is caused by rotational motion of  $-\text{CH}_2-\text{CHCl}-$  triads as shown in Fig. 6. In regular PVC structure such structural units are along the backbone. However, the substitution reaction, thus the formation of these triads, is also a statistical process using any kind of chlorination. Increasing the chlorine content, the probability of these units is increasing, but the probability of defective structures is also increasing in parallel. At about 40% Cl content, the previously created regular structures are destroyed. Chlorination of PVC leads to decreasing the number of existing regular triads. Therefore, in case of CPE over 40% Cl content, the intensity of this transition decreases. It is interesting that in case of the chlorinated paraffin of 70% Cl content, this peak is still detectable, although it is near to the noise-limited sensitivity of the instrument used.

The first maximum observed at 10–12% chlorine in both relaxation strength ( $\Delta\epsilon$ ) and  $I_{\text{max}}$  can be explained by chlorination technology. As it was mentioned, the temperature in first stage of chlorination is below the melting range of polyethylene. At this temperature, the crystalline part of the polyethylene remains intact; the reaction takes place in the amorphous phase only. Because the amorphous phase of HDPE is about 30% at 10–12% Cl content, the number of regular units starts to decrease. Melting the crystalline part by increasing the temperature the full amount of polyethylene becomes able for chlorination.

TSD method showed undoubtedly the presence of the transition and proved excellent tool for observing these processes of low intensity. The results support the concept about the structure formation during chlorine substitution reaction.

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