



# Thermal and mechanical characterization of complex electrospun systems based on polycaprolactone and gelatin

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## Abstract

Nowadays, continuous development of soft-electronics and wearable devices opens to the development needs of stretchable and flexible materials able to interface with the human body. In this scenario, biopolymers are particularly intriguing materials given their biocompatibility and biodegradability. For the application in this specific field the material requires several properties such as biological and mechanical performance and thermal stability. In this study, membranes able to fulfill some of these requirements are described. The electrospun membranes, composed of a blend of polycaprolactone (PCL) and gelatin (GN), have been produced in various configurations. The results show how blend or coaxial systems have different effects on both the interactions between the polymers and their thermal and mechanical properties. An important result of the chosen experimental conditions is the narrow dimensional distribution of the nanofiber diameters constituting the electrospun membranes. Thermal and mechanical tests evidenced that, by properly choosing the material composition and the method of the electrospinning process, membranes capable of withstanding high strain values before the failure can be obtained. In particular, optimizing the electrospinning process and using a blend PCL/GN with a mass ratio of 80/20, it is possible to increase the thermal stability up to 310 °C and confer to the sample the ability to reach a percentage of strain up to 350%.

**Keywords** Electrospun membranes · Mechanical properties · Thermal properties · Coaxial electrospinning · Biopolymers

## Introduction

In recent years, advances in flexible and stretchable electronics have enabled the development of soft wearable and implantable devices that can reliably and unimpeded interface with the surface of the human body [1]. These devices must be able to interface perfectly with the body, minimizing contact resistances and disturbances caused by mechanical sliding during movement [2].

From the recent literature, the development of functional green polymer emerges as a relevant field of innovation [3, 4]. As regards the wearable devices, they are made of

materials that require to be strong and soft enough to wrap around the body, hence leading to a pleasant feeling of comfort [5]. This aspect requires the development of membranes with adequate dimensions and mechanical properties. Many techniques have been developed to manufacture these materials, such as sol–gel [6], chemical vapor deposition [7], and the layer-by-layer method [8]. However, the complex properties of these materials require the development of new manufacturing techniques. From this point, electrospinning has proven to be an effective approach to the preparation of functional materials [9]. Many new electrospinning techniques have been developed for the design of new materials [10, 11]. Moreover, the electrospinning process allows obtaining nanofiber membranes suitable for being used as scaffolds [12], as drug delivery systems [13] and with the possibility to obtain nanocomposite nanofibers [14–16]. However, wearable and implantable devices often require good biocompatibility [17].

In particular, thermoplastic biopolymers used for these applications can be mainly of two types: natural (e.g., gelatin (GN), collagen, hyaluronic acid) characterized in general by biocompatibility and biodegradability, or synthetic

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(e.g., polycaprolactone (PCL), polylactic acid) characterized by better mechanical properties [18, 19]. However, their combination can be particularly effective: on the one hand in fact natural polymers can guarantee relevant biocompatibility and, on the other hand, the synthetics can enhance the mechanical properties of the material [20]. Biopolymers are now greatly applied for several types of applications including the biomedical field [21].

In this study, the electrospinning process is used to produce GN and PCL membranes in blend and in coaxial systems, to understand how the configuration of the process acts on the thermal, mechanical properties and morphological features of the obtained membranes.

Even if several papers deal with the usability of electrospun membranes based on PCL and GN for biomedical applications (mainly as scaffold) [22–26], rarely thermal and mechanical characterization of these types of membranes have been simultaneously analyzed using different process configurations with the same chemical composition of the blend. Zhang et al. [26] already noticed that GN and PCL electrospun blend (50:50 mass/mass) can have a higher strain at break, up to 138%. On the other hand, Yao et al. [25] proved that PCL/GN blend electrospun membranes in different mass ratio (1:4 to 4:1) have strongly different mechanical properties, with the higher elongation at break reported at 4:1 mass ratio (PCL/GN), which is around 90%, significantly lower than the results reported in our work (349%). This result is most likely due to the fact that SEM images of membranes presented by Yao et al. show fibers with a very wide diameter distribution that could strongly affect the mechanical properties [27].

In particular, in the present paper PCL-GN-based electrospun membranes are produced in blend and in coaxial systems. Firstly, the morphology of the membranes is presented, then the mechanical properties are discussed in the light of the thermal investigation of the different membranes.

## Materials and methods

### Materials

Poly( $\epsilon$ -caprolactone) used for the membrane preparation was provided by Perstorp (Sweden), CAS N° 24980-41-4. It is a linear polyester characterized by a high molecular weight (about 80,000 Da) and was provided in the form of pellets (granules with an approximate diameter of 3 mm). GN from Porcine skin type A used for the membrane preparation was provided by Sigma-Aldrich (CAS N°9000-70-8). Hexafluoro-isopropanol (HFIP) used for the polymeric solution has been purchased by Apollo Scientific Limited.

### Preparation of polymeric solutions for electrospinning

The solutions were prepared by dissolving the polymers in HFIP. The mass percentage of 5% of the polymers in HFIP has been chosen for the formulations containing both components (PCL and GN). A percentage by mass of 6% of PCL has been chosen for the membranes composed of PCL alone. The percentage allows good spinnability and processability of the solutions that have been kept under stirring at 40 °C for 24 h just after the preparation to obtain complete dissolution of the components. In blend systems, PCL-GN (Blend 80:20), and PCL-GN (Blend 60:40) samples, the ratios 80/20 and 60/40 refer to the mass ratio percentage of the two components.

The polymeric solutions have been fed at a flow rate of 1 mL h<sup>-1</sup> to the injector of the electrospinning equipment (EC-CLI by IME Technologies, Spaarpot 147, 5667 kV, Geldrop, Netherlands, injector diameter of 0.8 mm) and have been spun thanks to the electric field in a controlled climate room at 25 °C and 35% relative humidity.

In coaxial electrospinning, GN and PCL are spun in parallel using a coaxial injector that allows obtaining bilayer nanofibers. For the blend membrane, GN and PCL are solved in the same solution and spun using monoaxial electrospinning. The process parameters have been optimized for obtaining membranes with no evident defects. The optimized parameters are shown in Table 1.

All the membranes have been kept in vacuum for 24 h after the production to remove any solvent residuals.

### Morphological analysis

The morphological analysis has been performed using scanning electron microscopy (SEM) by which information about the size and the distribution of fibers has been obtained. The electrospun membranes have been metalized using an Agar Automatic Sputter Coater before SEM analysis. A thin layer of Au is deposited on the membrane surface to improve the quality of the morphological acquisitions. The analysis to obtain the fiber size distribution has been done using ImageJ software, whereas the data to obtain the pore diameter distribution using MATLAB software following the procedure is reported by Havlíček et al. [28] Distribution curves are normalized so that the area under the histograms is equal to 1.

### Thermal analysis

Thermogravimetric analysis (TGA) has been performed using Mettler Toledo TC-10 thermobalance in air

**Table 1** Electrospinning process parameters

#	Materials	Concentration/g g <sup>-1</sup>	Injector–collector distance/cm	Positive and negative electrodes voltages/kV
PCL	PCL	6	25	17/–2
PCL-GN (blend 80:20)	Blend 80% PCL and 20% GN (in mass)	5	22.5	13/0
PCL-GN (blend 60:40)	Blend 60% PCL and 40% GN (in mass)	5	22.5	18/0
PCL-GN (coaxial core–shell)	Core: PCL Shell: GN	5 5	24	22/0
GN-PCL (coaxial core–shell)	Core: GN Shell: PCL	5 5	24.5	20/0
GN	GN	5	24.5	14/0

atmosphere (50 mL min<sup>-1</sup>) with 10 °C min<sup>-1</sup> heating rate from 30 to 700 °C.

Differential scanning calorimetry (DSC) has been performed using Mettler Toledo DSC 822e in N<sub>2</sub> atmosphere (50 mL min<sup>-1</sup>) from –50 to 250 °C with 10 °C heating rate.

### Structural analysis

X-ray diffraction (XRD) measurements have been taken using a Bruker D8 Advance diffractometer at 35 kV and 40 mA.

### Mechanical characterization

Mechanical characterization has been performed using Dual Column Tabletop Testing Systems (INSTRON, series 5967-INSTRON, Norwood, MA, USA) in tensile tests. For each membrane, five samples have been prepared of 1 cm (width) per 5 cm (length) per 0.1 mm (thickness) in ambient conditions. The tensile tests have been performed lifting at 10 mm min<sup>-1</sup> the beam and acquiring data about force and distance covered. Thus, the data are converted in stress–strain curves.

## Results and discussion

### Morphological analysis

SEM images have been acquired for all the membranes to obtain a wide range of information about the morphology. They are reported in Fig. 1.

The morphological parameters of the membranes are reported in Table 2.

Figure 1 shows a monomodal narrow fiber distribution, as evidenced in Fig. 2, for all the membranes with no evident defects, with the formation of a non-oriented mat. The thinnest nanofibers are produced for the PCL (≈ 490 nm), but, however, nano-sizes are obtained also for the other systems (up to 890 nm). Moreover, the fiber dimension also affects the pore size, as already reported in the literature. Generally, an increase in the fiber dimensions determines an increase of the pore dimensions [29].

### Thermogravimetric analysis

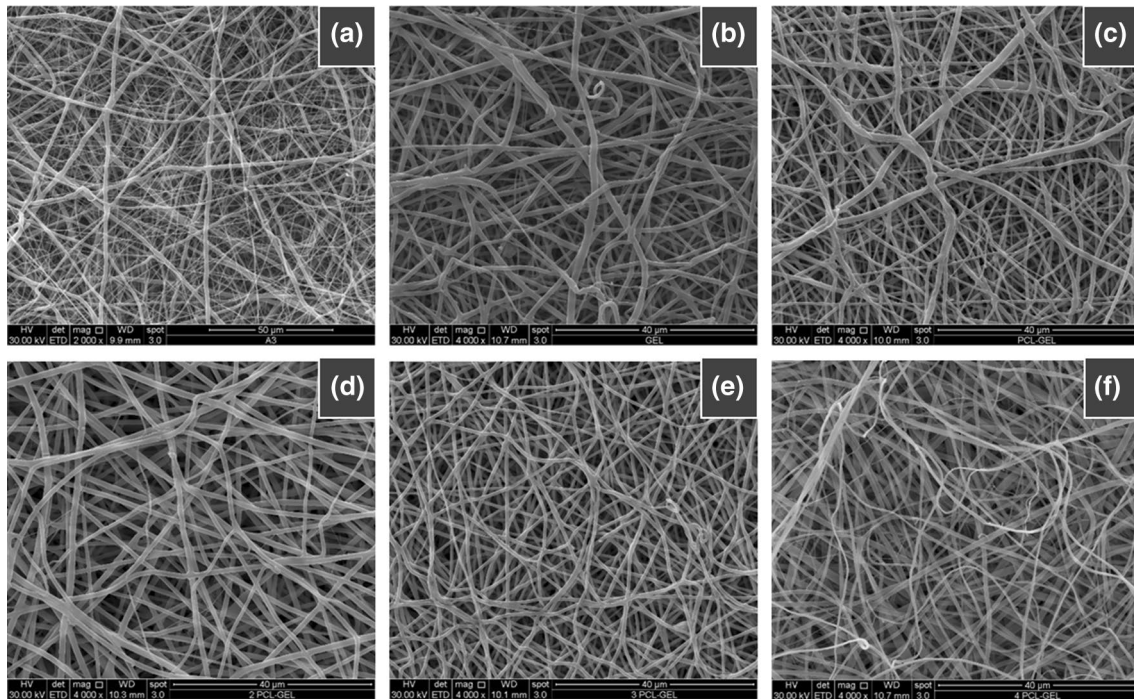
TGA analysis is reported in Fig. 3.

The derivative TGA of electrospun GN and PCL are reported in Fig. 4.

PCL and GN are characterized by different thermal curves. On the one hand, PCL shows two steps of degradation. The first begins around 320 °C and has its maximum rate of mass loss in DTG graph around 400 °C, and is due to the rupture of the ester chains, leading to the formation of H<sub>2</sub>O, CO<sub>2</sub> and 5-hexenoic acid. Then, around 450 °C, the second degradation peak leads to depolymerization, producing ε-caprolactone [30].

On the other hand, GN mass loss can be divided in three different steps: The first one (up to 100 °C) corresponds to the loss of water, probably due to the water absorption because of the high hydrophilicity of GN. The second one (from 200 to 400 °C) is caused by protein degradation, whereas the third one by the rupture and decomposition of the GN network [31].

As reported in Fig. 4, the steps of degradation of GN and PCL are still well visible also for the blend and the coaxial systems. In particular, for the coaxial systems, a visible acceleration especially in the first degradation step



**Fig. 1** SEM images of membranes: **a** PCL; **b** GN; **c** PCL-GN (blend 80:20); **d** PCL-GN (blend 60:40); **e** PCL-GN (coaxial core-shell); **f** GN-PCL (coaxial core-shell)

**Table 2** Fiber and pore diameter

		PCL	GN	PCL-GN blend (80:20)	PCL-GN blend (60:40)	PCL-GN (coax- ial core-shell)	GN-PCL (coaxial core- shell)
Fiber diameter	Mean/ $\mu\text{m}$	0.49	0.79	0.52	0.89	0.65	0.78
Pore diameter	Mean/ $\mu\text{m}$	1.25	2.47	1.52	2.67	1.62	2.31

is observed. This behavior is most likely due to the occurrence that in the coaxial configuration, the GN component is characterized by weaker interactions with PCL component; hence, its behavior tends to be more similar to GN alone.

### Differential scanning calorimetry

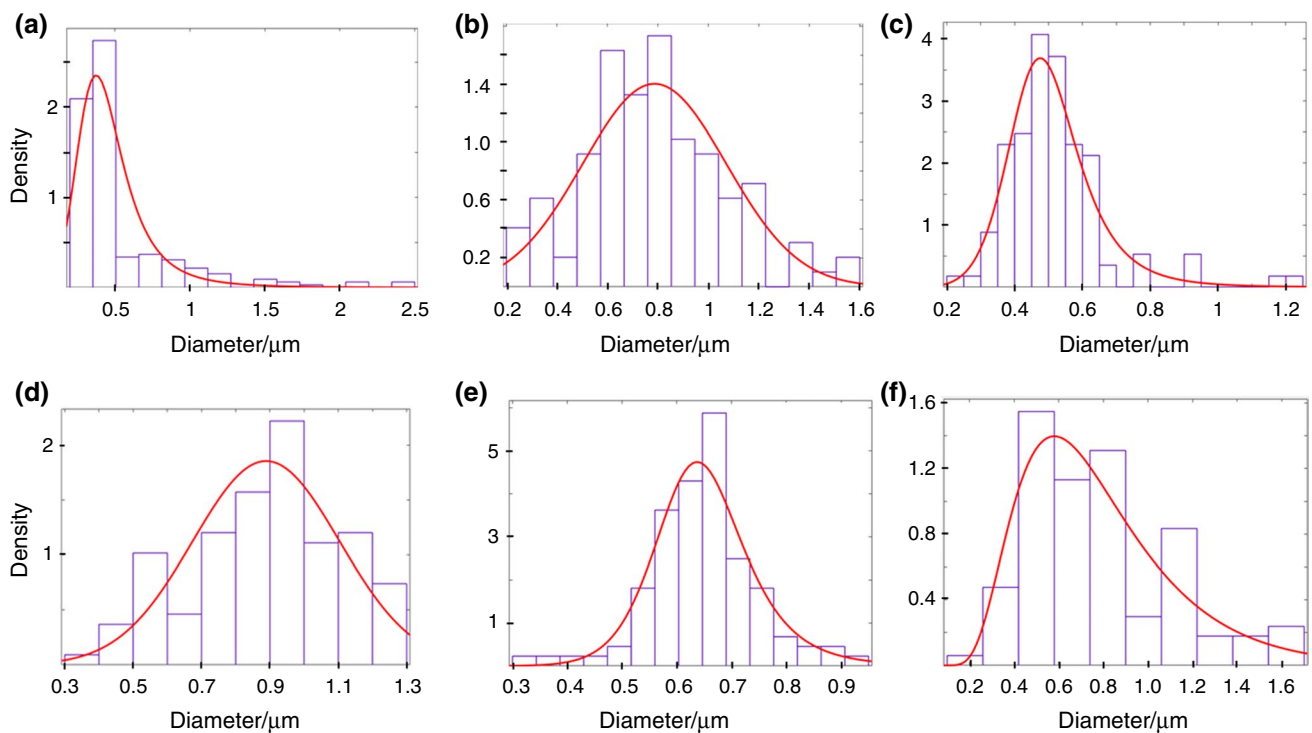
DSC curves are reported in Fig. 5.

DSC graph of the PCL alone shows the melting point at 59.3 °C, whereas the graph of GN manifests a very wide endothermic peak most likely due to water evaporation during the thermal scanning. This hypothesis is confirmed by the profile of the TGA and DTG curves shown in Figs. 3–4. The peak related to water evaporation is present also for the coaxial and blend systems, whereas it is absent for the PCL alone, confirming that water absorption is due to the high GN hydrophilicity, suggesting, as expected, that the more is the GN quantity, more wide and relevant is the peak

(between 50 and 100 °C) after the main melting point of PCL.

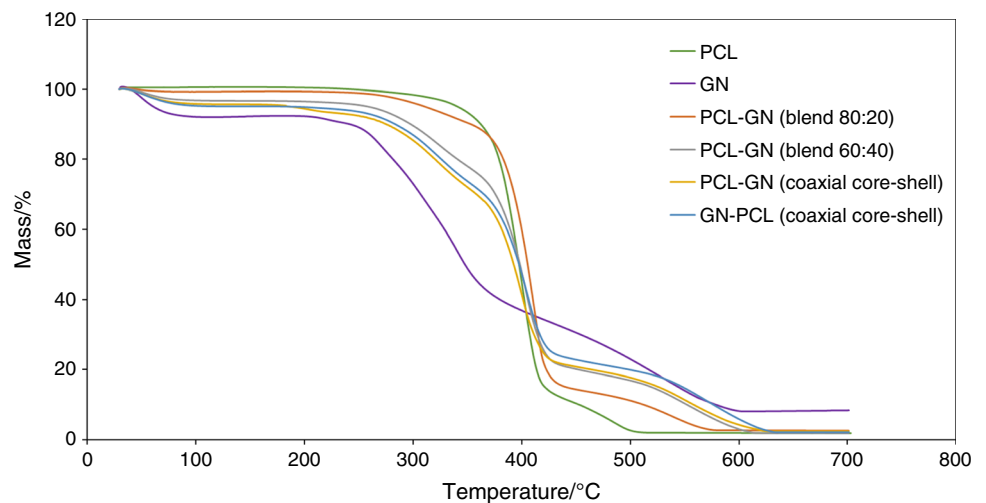
The melting peak of the PCL is affected by the presence of GN; its results strongly depend on the configuration process of electrospinning. In fact, the different results are observed for coaxial and blend systems. On the one hand, the PCL melting peak is slightly anticipated from 59.3 °C for the pure PCL to 58 °C for both the coaxial systems, whereas the blend systems show higher anticipation of the melting point according to the GN amount. For the system PCL-Blend (80:20), the melting point is detected at 57.0 °C, whereas for PCL-Blend (60:40) at 54.0 °C. The anticipation of the melting point suggests the formation of smaller crystallites that requires lower temperature energy to melt [32].

The DSC results are confirmed by XRD analysis, displayed in Fig. 6. PCL typical peaks at 21.5° and 23.8° (slightly shifted) are evident in the three diffractometric profiles. They are generated by the 110 and 200 reflections of the orthorhombic PCL crystalline structure [33].



**Fig. 2** Fiber diameter distribution of: **a** PCL; **b** GN; **c** PCL-GN (blend 80:20); **d** PCL-GN (blend 60:40); **e** PCL-GN (coaxial core-shell); **f** GN-PCL (coaxial core-shell)

**Fig. 3** Thermogravimetric analysis



As expected, by increasing GN percentage an increase of the amorphous phase is observed. Furthermore, smaller crystallites size is well-evident by the profile of the diffractometric peaks corresponding to the samples obtained by the blends.

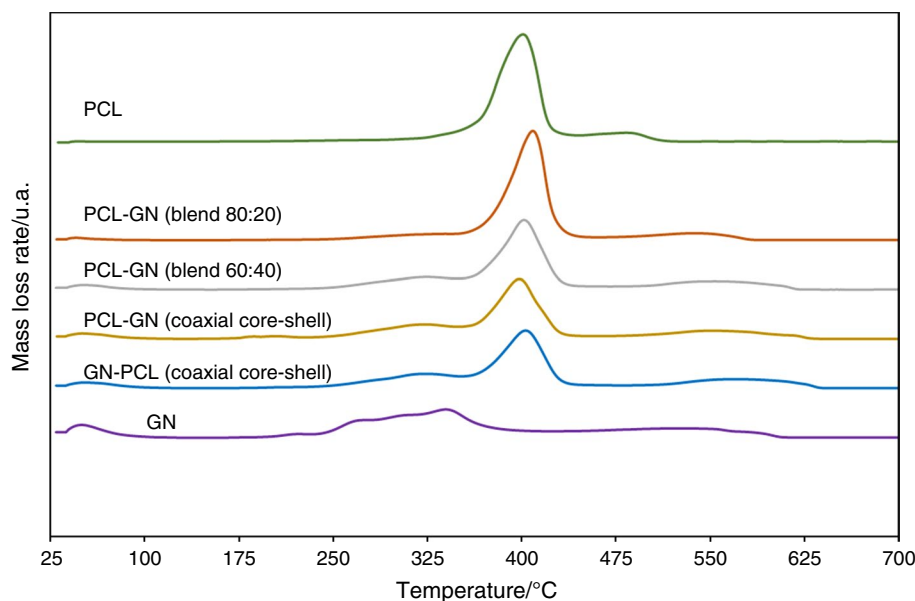
The half-height widening of the 110 and 200 reflections, which is diagnostic of smaller and defective crystals in the membranes from the blends with respect to that from pure PCL, is perfectly in line with the calorimetric results which

highlight a decrease in the melting temperature of the membranes from blends compared to that obtained from the pure polycaprolactone.

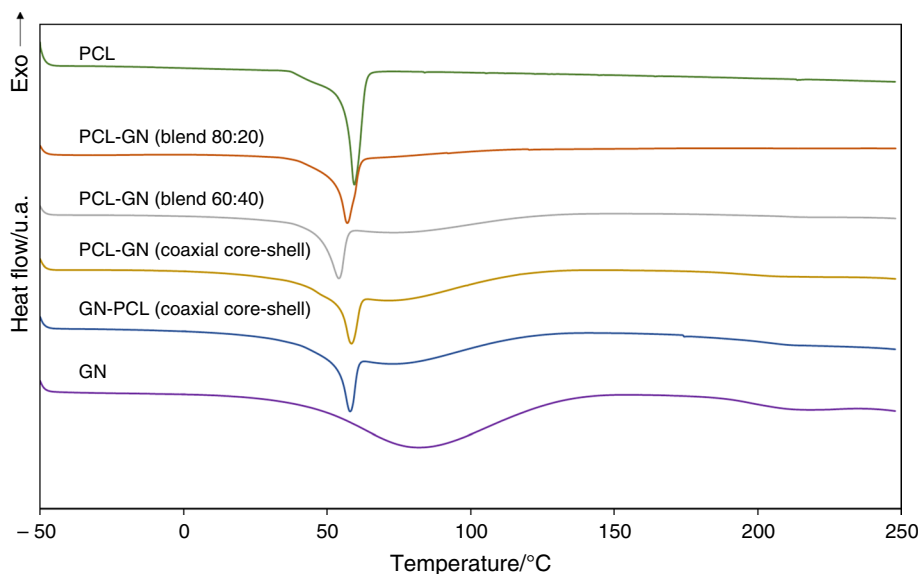
### Mechanical characterization

The mechanical properties of the membranes have been studied in tensile mode to understand how the composition of the polymeric system and the process configuration affects the

**Fig. 4** Derivative TGA of PCL and GN



**Fig. 5** DSC of the membranes



tensile properties of the membranes. The stress–strain curves are shown in Fig. 7.

The main parameters obtained for the different obtained membranes are displayed in Table 3.

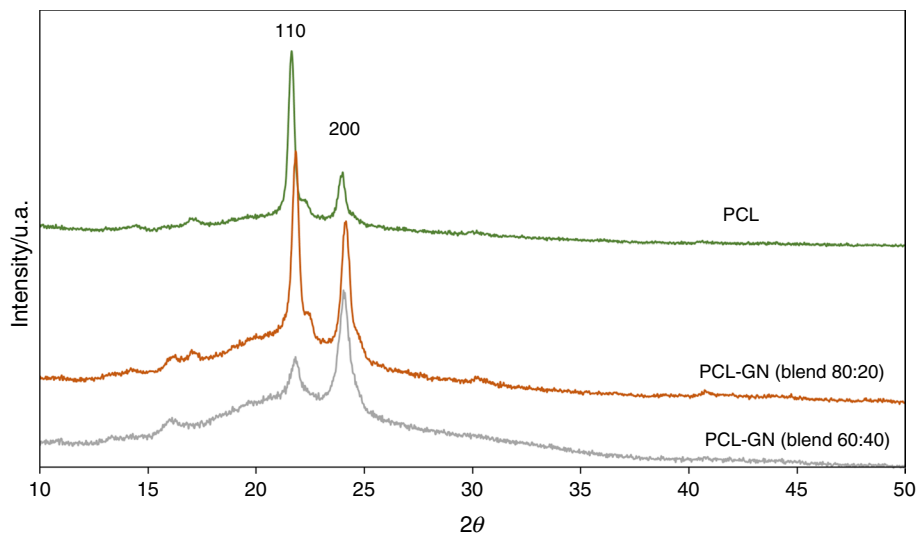
The mechanical behavior of the PCL and GN is strongly different. GN is more elastic and, as expected, shows a lower elongation at break than all other compositions. The coaxial systems that are formed by bilayer nanofibers show elastic modulus values between the GN and PCL (111.3 MPa and 17.7 MPa) and therefore higher than the pure PCL.

Concerning the strain at break, with this type of morphological configuration, a very strong reduction is detected with respect to the membranes of PCL alone. For the membrane PCL-GN blends, very good results in the tensile

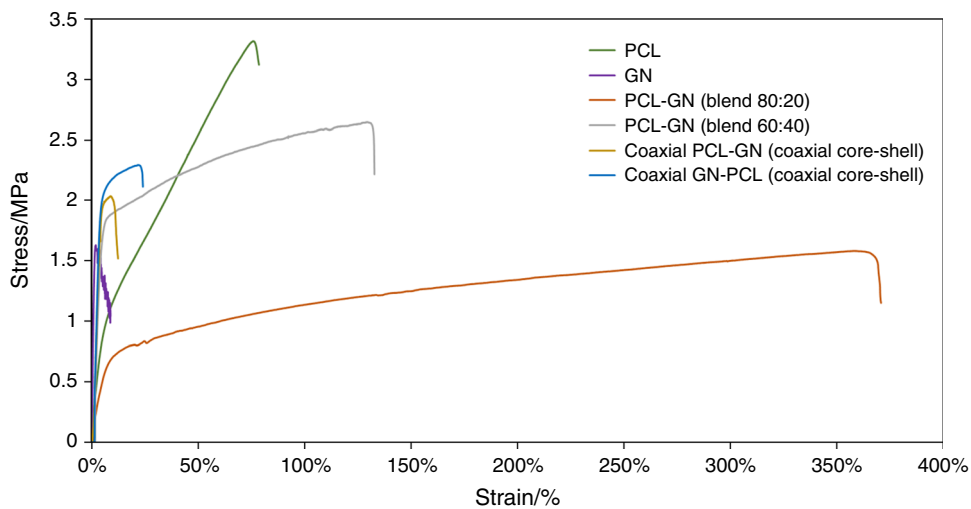
properties are detected, the presence of GN is able to enhance the elastic modulus together with the elongation at break with respect to the pure PCL. This behavior is most likely due to an intimate interaction between GN and PCL. This favorable occurrence seems confirmed in Fig. 5 by the anticipation of the melting point of PCL in the blend.

GN determines the formation of smaller crystallites allowing a better compatibility between GN and PCL in the amorphous phase. This good compatibility confers to PCL chains a better mobility which allows high values of strain. PCL-GN (Blend 80:20) system shows strain at break around 350% with an increase of about 270% with respect to the strain at break of the pure PCL. PCL-GN (Blend 60:40) shows a strain at break around the 110% (still higher than

**Fig. 6** XRD spectra of PCL, PCL-(blend 80:20) and PCL (blend 60:40) samples



**Fig. 7** Stress–strain curves



**Table 3** Mechanical properties membranes

		PCL	GN	PCL-GN blend (80:20)	PCL-GN blend (60:40)	PCL-GN (coaxial core-shell)	GN-PCL (coaxial core-shell)
Young modulus /MPa	Mean	17.7	111.3	21.3	54.5	47.35	63.3
	Standard deviation	2.00	22.7	6.59	8.92	5.08	15.4
Strain at yield/mm mm <sup>-1</sup>	Mean	3.88	2.34	4.27	2.72	3.71	3.78
	Standard deviation	0.577	0.733	0.262	0.151	0.353	0.843
Stress at break /MPa	Mean	3.16	1.97	1.99	2.14	1.84	2.3
	Standard deviation	0.71	0.368	0.272	0.41	0.508	0.32
Strain at break /mm mm <sup>-1</sup>	Mean	78.8	3.15	349.3	112.8	10.95	22.2
	Standard deviation	15.7	0.980	22.8	15.1	1.76	3.78

pure PCL), because even if the crystallites of PCL are even smaller, the GN amount starts to be very high and causes a diminution of the strain at break of the material.

## Conclusions

Electrospun membranes of PCL and GN have been produced, and their characteristics have been compared to PCL-GN blend and coaxial systems. The morphology investigations have revealed no evident defects and an average diameter between 480 and 890 nm for all the membranes. TGA investigation has evidenced that the membranes obtained from the blends manifest a slightly better thermostability with respect to the membranes obtained by coaxial configuration. The DSC results suggest better compatibility between PCL and GN in the membranes from blends than those prepared by coaxial configuration. In this last case, the interaction between the two components is less intimate because the GN and PCL form bilayer nanofibers. Hence, a minor surface area, only that at the interphase between the fiber layers, is involved in the interaction between the two polymers. This also affects the mechanical properties. The most relevant difference is detected in the elongation at break. For the membranes from the blends an increase up to 110% and 350% (depending on the composition) with respect to the membranes of pure PCL is observed. These results, together with data already discussed in the literature on these systems, open up new application scenarios because allowing margins of tolerance to the strain, before the failure, is very high.

## Declarations

**Conflict of interest** The authors have no conflicts of interest to declare that are relevant to the content of this article.

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