



# Spectral Engineering for Optimal Signal Performance in the Microwave SQUID Multiplexer

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## Abstract

We describe a technique to optimize the dynamic performance of microwave SQUID multiplexer ( $\mu$ MUX)-based systems. These systems proved to be adequate for reading out multiple cryogenic detectors simultaneously. However, the requirement for denser detector arrays to increase the sensitivity of scientific experiments makes its design a challenge. When modifying the readout power, there is a trade-off between decreasing the signal-to-noise ratio (SNR) and boosting the nonlinearities of the active devices. The latter is characterized by the spurious free dynamic range (SFDR) parameter and manifests as an increment in the intermodulation products and harmonics power. We estimate the optimal spectral location of the SQUID signal containing the detector information for different channels. Through the technique, what we refer to as *Spectral Engineering*, it is possible to minimize the SNR degradation while maximizing the SFDR of the detector signal, thus, overcoming the trade-off.

**Keywords** Cryogenic detectors · Microwave SQUID multiplexing · Signal processing · Spectral engineering

## 1 Introduction

The high sensitivity of cryogenic detectors makes them ideal for a wide range of scientific applications including particle physics, astrophysics, and materials science. Based on the scientific topic of interest, the detectors are designed to measure energy (calorimeters) like the magnetic microcalorimeters (MMC) [1] or power (bolometers) like the recently proposed magnetic microbolometers (MMB) [2]. Cosmic microwave background (CMB) surveys like QUBIC (Q & U Bolometric

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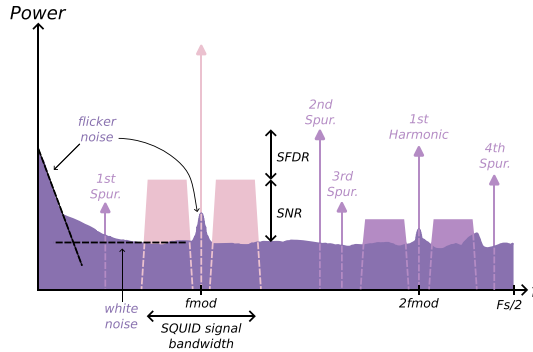
Interferometer for Cosmology) [3] utilize bolometers to measure the B mode polarization of the CMB. Experiments which seek to detect the energy of an emitted particle use calorimeters. For example, ECHo (Electron Capture in  $^{163}\text{Ho}$ ) [4] aims to establish a new upper limit of the neutrino mass in the sub-eV range through the electron capture process of  $^{163}\text{Ho}$ . A dedicated multiplexer based on superconducting quantum interference devices (SQUID) is typically designed to readout arrays of cryogenic detectors. This system is called microwave SQUID multiplexer ( $\mu\text{MUX}$ ), [5] and it is designed to multiplex as many detectors as possible in different frequency channels within a given bandwidth using a frequency division multiplexing (FDM) technique. Each channel is composed of a unique superconducting resonator coupled through a radio frequency (RF) SQUID to cryogenic detectors. Room temperature electronics (RTE) designed in a software defined radio (SDR) scheme synthesize and condition a frequency comb to monitor all the  $\mu\text{MUX}$  channels.

To meet the demand for increasingly sensitive detection systems, more densely populated detector arrays are required. This makes the readout system design more complex since multiple factors must be optimized. For example, one of the challenges to overcome is the trade-off between the signal-to-noise ratio (SNR) and spurious free dynamic range (SFDR) [6]. Keeping the same readout power per channel, the total tone comb power increases with the amount of channels, which raise the power of intermodulation products and harmonics in the active devices. Similarly, the SFDR, specifying the amplitude relation between the signal of interest and the worst spurious signal in the spectrum, is reduced. In contrast, if the readout power per channel decreases, a degradation of the SNR occurs in the RTE as well as in the  $\mu\text{MUX}$  if the readout power is below the optimal value [7]. This could diminish the sensitivity of the detection system, therefore contradicting the reason for increasing the density of the detector array.

In this article, we present a technique called *spectral engineering* to overcome this trade-off. It consists of locating the SQUID signal containing the detector information in the spectral band that optimizes SNR and SFDR of the detector signal.

## 2 Concept

As described in Sect. 1, a multi-tonal signal is synthesized to monitor all channels in the  $\mu\text{MUX}$ . Each tone drives a different channel formed by a unique resonator filter coupled to a SQUID which is at the same time coupled to a cryogenic detector. A sawtooth-shaped magnetic flux signal (FR) is synthesized to drive all the SQUIDs and linearize their responses [8]. Hence, the signal generated by each detector is translated to a phase shift of the SQUID response. Therefore, the  $\mu\text{MUX}$  imprints the detector's information to the multi-tonal signal in a process that involves two levels of modulation. The first modulation is given by the periodic variation of the magnitude and phase of each channel given by the FR. The second modulation occurs in the SQUID and as a consequence of mixing both the FR and the magnetic flux generated by the detector. The frequency comb is then reconditioned and processed in the RTE to recover first the SQUID signal and then the detector signal for each channel. In Fig. 1, a sketch of the processed SQUID signal spectrum is given.



**Fig. 1** An illustration of a typical SQUID signal spectral profile after downconverting it with the monitor tone. The SQUID signal is shown in pink and is formed by a carrier signal and its phase modulation, the detector signal. The carrier frequency is defined by the FR as  $f_{mod} = N_{\Phi_0} f_{ramp}$ . In dark violet, the white noise and flicker noise contributions are shown. In light violet, undesired signals are shown in the spectrum due to spurious, intermodulation products, harmonics, etc.

The SQUID signal carrier frequency ( $f_{mod}$ ) is defined by the FR frequency ( $f_{ramp}$ ) and amplitude in terms of number of magnetic flux quanta ( $N_{\Phi_0}$ ) as  $f_{mod} = N_{\Phi_0} f_{ramp}$  [9]. Since the ultimate goal is to recover the detector signal, the SNR and SFDR parameters are considered relative to it (see Fig. 1). Noise components such as white noise and flicker noise determine the SNR. Undesired components like spurious signals and the SQUID signal harmonics define the SFDR value. Different SNR and SFDR values can be obtained experimentally for the particular set of hardware by adjusting the  $f_{mod}$  value. It is desired that both SNR and SFDR parameters are positive and large.

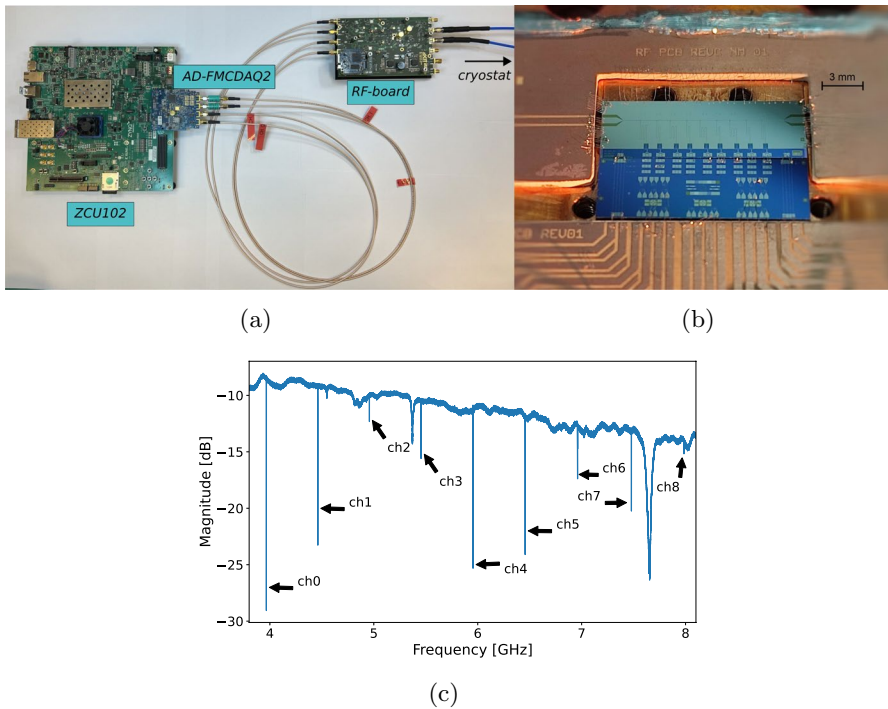
Despite each channel in the  $\mu$ MUX having a different spectrum profile, a value for  $f_{ramp}$  and  $N_{\Phi_0}$  can be found to maximize the SNR and SFDR for the worst case and at the same time set a lower limit for the rest of the channels.

### 3 Measurements

#### 3.1 Experimental Setup

In Fig. 2a, we show the used RTE. It consists of the commercial evaluation board ZCU102 build around a Multi-Processor System-on-Chip (MPSoC) and the converter board AD-FMCDQA2 that generate and process the tone comb. A custom microwave board [10] up-converts the tone comb to the  $\mu$ MUX frequency band. The  $\mu$ MUX is shown in Fig. 2b. It has nine channels between 4 and 8 GHz separated every 500 MHz. In Fig. 2c, the transmission parameter ( $S_{21}$ ) of the  $\mu$ MUX is plotted.

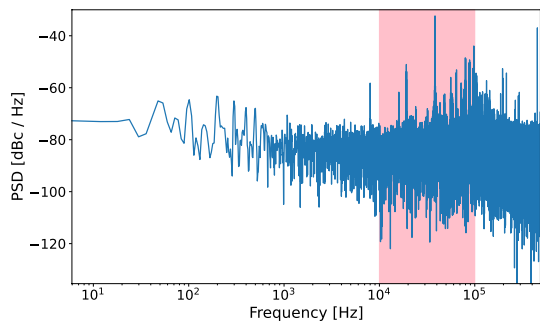
Since the current electronics allows an instantaneous readout bandwidth of 800 MHz, we measured three different channels one after the other at around 3.965 GHz (ch0), 5.954 GHz (ch4) and 6.456 GHz (ch5). A channelizer based on a Goertzel filter [13] was implemented for separating each monitor tone. In order



**Fig. 2** **a** RTE, composed of two commercial boards (ZCU102 [11], AD-FMCAQ2 [12]) and a custom RF-board [10]. **b** The  $\mu$ MUX used for the measurements. It has nine channels distributed between 4 and 8 GHz. For scientific purposes, channels 2, 3, 4, 7 and 8 have different input coils attached to the SQUIDs, meanwhile channels 0, 1, 5 and 6 do not have it. **c** The  $\mu$ MUX  $S_{21}$  parameter. Apart from the channel resonances, also a resonance between channels 2 and 3 and between channels 7 and 8 is present that correspond to the cavity resonance of the sample holder

not to lose generality in this technique, no magnetic flux signal was concatenated into the SQUID, and we assumed the noise power and spurious signals do not change when magnetic flux signal is present. Therefore, we acquired noise and nonlinearity contributions of the RTE and the  $\mu$ MUX (see Fig. 3).

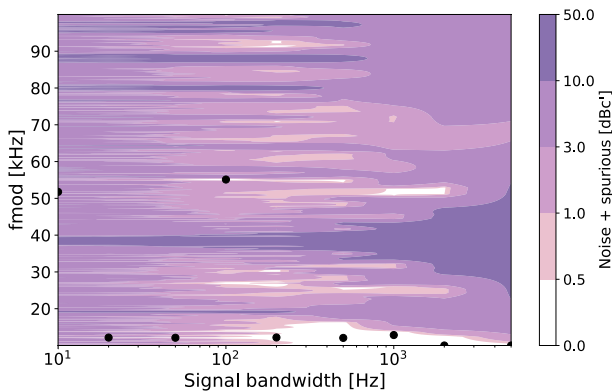
**Fig. 3** Power spectral density of the monitor signal related to ch5 after the channelizer. The power is referenced to the monitor tone power, thus, expressed in dBc units. The pink shaded area indicates the region in frequency across which the center frequency of the boxcar filter was varied



To find the optimal  $f_{mod}$  that maximizes the SNR and SFDR values of the detector signal, we emulated different conditions for the SQUID signal carrier frequency and bandwidth. We calculated the total spectrum power of the signal in Fig. 3 after filtering it with a rectangular window for the different conditions. The rectangular window filter was chosen since it is the standard [7, 8, 14–16] to recover the detector signal from the  $\mu$ MUX. Although, it is not the best window filter to attenuate the harmonics of the SQUID signal as explained in [9]. The center frequency of the boxcar filter (which should match the  $f_{mod}$  frequency) was varied between 10 and 100 kHz in steps of 5.96 Hz. Afterward, we obtained the optimal  $f_{mod}$  value which results in the lowest sum of noise power and spurious power. Another parameter that was also varied is the boxcar filter bandwidth. This parameter should match the SQUID signal bandwidth which depends on the amplitude and bandwidth of the detector signal. As mentioned in Sect. 1, there are many projects that use this readout technique for cryogenic detectors. These projects cover different detector bandwidths that can range from Hz to MHz regimes. For this work, we chose boxcar filter bandwidths between 10 and 5000 Hz.

### 3.2 Results

The results obtained are displayed in Fig. 4. It shows the integrated spectrum power for the different boxcar filter bandwidths and central frequencies. In addition, for each calculated power, only the worst case was plotted among the three measured channels, i.e., the highest power. Each spectrum power trace per detector bandwidth was normalized to the minimum power of each one ( $\text{dBc}_{\min}$ ) so the best situation occurs when the calculated spectrum power is 0 dBc' (where  $\text{dBc}' = \text{dBc} - \text{dBc}_{\min}$ ). These cases, which indicate the optimal  $f_{mod}$  value, were marked with circles in Fig. 4. Considering the overall spectral power, an enhancement of up to 50 dB can be obtained if the optimal  $f_{mod}$  value is set against the worst case. If only the noise



**Fig. 4** Spectrum power for the different boxcar filter central frequencies (or  $f_{mod}$ ) and bandwidths (or SQUID signal bandwidth). In color, the total spectrum power (noise + spurious) for the worst case among the three measured channels is shown. Therefore, the  $f_{mod}$  value that maximizes the SNR and SFDR is marked with circles

contributions are considered, setting the optimal  $f_{mod}$  value improves up to 7 dB against the worst case.

## 4 Conclusions

In this work, we present a technique to overcome the trade-off between the signal-to-noise ratio (SNR) and the spurious free dynamic range (SFDR) in the microwave SQUID multiplexer ( $\mu$ MUX)-based systems. This technique seeks to optimize both parameters by placing the SQUID signal in the spectral region that maximize the detector SNR and SFDR or what we call *Spectral Engineering*. By this technique, we demonstrated an improvement of up to 50 dB and 7 dB comparing the optimal case against the worst one considering the total spectrum power and only the noise contributions, respectively.

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**Author Contributions** JMS wrote the paper, did the measurements, and processed the data; MEGR and LPF did the measurements; NM prepared Fig. 2c. All authors reviewed the manuscript.

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## Declarations

**Conflict of interest** The authors declare no competing interests.

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