ORIGINAL RESEARCH



Are all ventilators for NIV performing the same? A bench analysis

Sara Martínez-Castro¹ · Francisco Javier Belda Nacher² · Jaume Puig Bernabeu^{2,3} · Marina B Soro Domingo⁵ · Carlos Delgado Navarro³ · Héctor Ortega Pons⁴

Received: 14 October 2022 / Accepted: 15 April 2023 / Published online: 31 July 2023 © The Author(s) 2023

Abstract

Global pandemic due to COVID-19 has increased the interest for ventilators ´ use worldwide. New devices have been developed and older ones have undergone a renewed interest, but we lack robust evidence about performance of each ventilator to match appropriate device to a given patient and care environment. The aim of this bench study was to investigate the performance of six devices for noninvasive ventilation, and to compare them in terms of volume delivered, trigger response, pressurization capacity and synchronization in volume assisted controlled and pressure support ventilation. All ventilators were tested under thirty-six experimental conditions by using the lung model ASL5000® (IngMar Medical, Pittsburgh, PA). Two leak levels, two muscle inspiratory efforts and three mechanical patterns were combined for simulation. Trigger function was assessed by measurement of trigger-delay time. Pressurization capacity was evaluated as area under the pressure-time curve over the first 500 ms after inspiratory effort onset. Synchronization was evaluated by the asynchrony index and by incidence and type of asynchronies in each condition. All ventilators showed a good performance, even if pressurization capacity was worse than expected. Leak level did not affect their function. Differences were found during low muscle effort and obstructive pattern. In general, Philips Trilogy Evo/EV300 and Hamilton C3 showed the best results. NIV devices successfully compensate air leaks but still underperform with low muscle effort and obstructive lungs. Clinicians´ must have a clear understanding of the goals of NIV both for devices´ choice and set main parameters to achieve therapy success.

Keywords Bench study \cdot Breathing mechanics \cdot Computer simulation \cdot Noninvasive ventilation \cdot Respiratory mechanics \cdot Ventilator performance

Abbreviat	ions	Crs	compliance of the respiratory system
ACV	assist-control ventilation	DT	double trigger
AI	asynchrony index	Е	effort
ASL500®	Active Servo Lung 5000	Н	high leak level
AT	auto-triggering	ICU	intensive care unit
Bpm	breaths per minute	IE	ineffective effort
BTPS	body temperature pressure saturated	I/E	inspiration/expiration
🖂 Jaume Pi	ig Bernabeu	¹ Anest	thesia and Critical Care Department, Hospital Cl

⁴ Anesthesia and Critical Care Department, Hospital Clínico Universitario de Valencia (HCUV), Valencia, Spain

- ² Universidad de Valencia (UV), Valencia, Spain
- ³ Anesthesia and Critical Care Department, Consorcio Hospital General Universitario de Valencia (CHGUV), Valencia, Spain
- ⁴ Instituto de Investigación Sanitaria de Valencia (INCLIVA), Valencia, Spain
- ⁵ Anesthesia Department, Hospital IMED Valencia (ES), IMED, Valencia, Spain

Francisco Javier Belda Nacher fjbelda@uv.es

jaume.puig@uv.es

Sara Martínez-Castro

saradacuris@hotmail.com;

anestesia.saramartinezcastro@gmail.com

Marina B Soro Domingo soromarina@gmail.com

Carlos Delgado Navarro cardelna@gmail.com

Héctor Ortega Pons hortegapons@gmail.com

Le	low effort
Lpm	liters per minute
М	moderate leak level
Ne	normal effort
NIV	non-invasive ventilation
0	obstructive mechanical pattern
P _{0.1}	airway occlusion pressure in the first 100 ms
Paw	airway pressure
PEEP	positive end-expiratory pressure
Pmus	muscle pressure
PSV	pressure support ventilation
PTP500	pressure-time product in the first 500 ms
R	restrictive mechanical pattern
Raw	airway resistance
RR	respiratory rate
RT	reverse or double trigger
S	standard mechanical pattern
S	seconds
TDT	trigger delay time
VT	tidal volume

1 Introduction

The leading role that advanced hemodynamic or neurological monitoring has taken in recent years should not overshadow the ubiquitous ventilators. Pandemic due to COVID-19 has enhanced the role of these devices in critical care units, around other hospital areas and for home care. By following a recent review and as a result of the daily work with patients we could establish the main goals of ventilation as (1) do not harm, (2) ensure adequate gas exchange and (3) promote patient comfort [1]. These are the objectives that any ventilator should have, so clinicians in charge must know how ventilators work, which setting options they give and if their informative screens offer the whole truth. But few studies systematically analyze devices' performance, so actually decisions can be solely based on theoretical principles.

Thille et al. in 2009 [2] stated that maybe we had reached the ceiling of technological development in terms of ventilators development. But while new devices continue to reach the market, bench studies that provide information about performance characteristics must be developed. The results of these works can support clinicians' decisions in terms of indications and adjustments based on patient mechanical characteristics, influence the choice in equipment acquisition and encourage manufacturers to implement improvements in ventilators and their settings. The following study tries to give light to some of the above-mentioned statements.

2 Objective

The objective of the present work was to describe the performance of six ventilators during non-invasive ventilation (NIV) in Emergency or Respiratory therapy and Intensive Care Unit (ICU) scenario. The ventilators were assessed under two ventilatory modes: volume assist-control ventilation (ACV) and pressure support ventilation (PSV). Using a lung simulator, thirty-six experimental conditions were created, by the combination of three respiratory mechanical patterns and two leak levels under low and normal muscle effort. With these experimental conditions, the following variables were evaluated: (1) Tidal Volume delivered (V_T) in ml, (2) Trigger-delay time (TDT) in ms, and (3) Pressurization capacity as pressure-time product in the first 500 ms (PTP500). Even if safety tends to predominate over comfort objectives, ventilation must ensure both of them. As synchronization directly correlates to the comfortable patientventilator interaction, our study also analyzed (4) Incidence and type of asynchronies developed.

3 Material and methods

3.1 Devices

Six devices suitable for NIV and available in European hospitals were studied: Savina 300 (Dräger, Germany), Elisa 500 (Löwenstein Medical, Germany), Hamilton C3 (Hamilton Medical, Switzerland), Servo Air (Maquet, Sweden), Mindray 300 (Mindray Biomedical, China) and Philips Trilogy Evo/EV300 (Philips, United States of America). They were used with the appropriate limbs and connectors according to each manufacturer guidelines and calibrated before each laboratory session.

3.2 Lung model

For the experiment we used the lung model Active Servo Lung 5000® (ASL5000®- IngMar Medical, Pittsburgh, PA; *software version* SW3.6). It consists of a computer- operated piston that simulates spontaneous breathing by displacing a predetermined volume; piston displacement is controlled following the equation of motion of the Respiratory System and allows adjusting the values of airway resistance (Raw) and compliance of the respiratory system (Crs), mimicking different mechanical conditions and inspiratory muscle efforts. [3, 4] To simulate different leak levels, Simulator Bypass and Leak Valve Module of ASL5000[©], was also used. This simulator has been used and validated in many previous works [5–14]. Before each session, calibration of pressure, flow and volume was performed against standards using a custom pressure water column, a differential pressure flowmeter (Validyne MP45, ± 2.5 cm H₂O, Northridge, CA) and a calibration syringe (Hans Rudolph KS, USA).

3.3 Simulated breathing test

3.3.1 Respiratory system conditions

For analysis, three mechanical patterns of the respiratory system were defined: standard (S) [Crs = 50 ml/cm H₂O, Raw = 5 cm H₂O*s/l], obstructive (O) [Crs = 50, Raw = 20] and restrictive (R) [Crs = 20, Raw = 5]. [15–17].

3.3.2 Spontaneous ventilation

Choosing a scheme similar to previous analysis [2, 7–10, 16, 18–26], standard settings were adjusted as spontaneous respiratory rate (RR) 12 breaths per minute (bpm); two levels of inspiratory muscle effort were defined by airway occlusion pressure (P_{0.1}): low (Le) P_{0.1}=-0.9 cm H₂O, and normal (Ne) P_{0.1}=-3.5 cm H₂O [27–29]. Patient effort model selected was sinusoidal, with inspiratory rise time 15%, inspiratory hold time 0%, inspiratory release time 18.3% and no expiratory activity.

3.3.3 Ventilatory modes and settings

Ventilators were set in ACV with V_T 500 ml, and in PSV with two levels of pressure (Paw): 10 (PSV10) and 20 (PSV20) cm H₂O. Ventilator respiratory rate was 10 bpm (I/E 1:2 in ACV), PEEP 5 cm H₂O with minimal flow triggering (maximum sensitivity) of 0.5-1 lpm without developing auto- triggering (AT). If AT was detected, increase in flow triggering was adjusted up to 2 lpm to avoid them [30]. Higher flow triggering would increase the TDT resulting in a decrease in PTP500; this may worsen patient work of breathing and respiratory drive promoting patient-ventilator asynchronies. Other settings remained by default, including bias flow (set by manufacturer). Two leak levels were also simulated by using the Simulator Bypass and Leak Valve Module of ASL5000[©]: 6 lpm (moderate, M) and 10 lpm (high, H) measured at 10 cm H₂O [31]. In PSV, the fastest value for pressurization rate (shorter rise time) was set, expiratory trigger at 25% peak flow and other settings by default.

With both ventilatory modes (ACV and PSV) combining mechanical pattern, inspiratory muscle effort and leak level, thirty-six experimental conditions were obtained (see Table 1). In all of them a minimum time of one minute was left for stabilization of the system (until clear sequence of cycles with similar morphology appeared); then consecutive respiratory cycles corresponding to one minute (minimum

Table 1 Experimental conditions in the bench test

Effort	Leak	Pattern	Ventilatory mode			
			ACV	PSV10	PSV20	
Low	Moderate	S	1	13	25	
		0	2	14	26	
		R	3	15	27	
	High	S	4	16	28	
		0	5	17	29	
		R	6	18	30	
Normal	Moderate	S	7	19	31	
		0	8	20	32	
		R	9	21	33	
	High	S	10	22	34	
		0	11	23	35	
		R	12	24	36	

ACV assist-control ventilation, PSV pressure support ventilation, S standard mechanical pattern, O obstructive mechanical pattern, R restrictive mechanical pattern



Fig. 1 Graphic representation of PTP500 [2]. PTP500: pressure-time product in the first 500 ms. *s* seconds

of 10 cycles) were recorded for subsequent analysis. The curves and data values of muscle pressure (Pmus), airway pressure (Paw) and flow were recorded and exported to an Excel spreadsheet. With those curves delivered volume, trigger response, pressurization capacity and asynchronies (incidence and type) were evaluated; sampling frequency of the curves was 512 Hz.

3.3.4 Measurements

Delivered V_T was measured in ml for all synchronous respiratory cycles in ACV; when synchronization was not

achieved in any cycle, V_T was measured in auto-triggering (AT) cycles in which V_T is theoretically equivalent to the V_T delivered in a controlled cycle. Trigger response was evaluated as the delay in triggering response (TDT) in ms, measured from the initial drop in muscular pressure to the onset of inspiratory flow above default bias flow. Pressurization capacity was evaluated through PTP500, in % of ideal Pressure–time product (see Fig. 1) measured as the area under the airway pressure from the initial drop to 500 ms. Synchronization was evaluated by Asynchrony Index (AI) and types of asynchronies (time and flow asynchronies):

(A) Asynchrony Index (AI): is the simplest method to evaluate synchronization. It is calculated as the number of asynchronous events divided by the total number of respiratory cycles (sum of triggered and non-triggered cycles), expressed as a percentage. It takes into account: ineffective efforts (IE), auto-triggering (AT), reverse triggering (RT) and double trigger (DT). An AI \geq 10% is considered clinically relevant. [3–7].

(B) Qualitative analysis of the asynchronies developed during the experiment: carried out by inspection and visual detection of the flow curves, Paw and Pmus of the recorded cycles. The asynchronies developed in all conditions were mainly time asynchronies (IE, AC and RT). [8].

3.3.5 Protocol sequence

Before initiating any ventilator experiment, we assessed $P_{0.1}$ by recording an occlusion maneuver in the inspiratory port

of the lung model (see Supplementary Material: Occlusion maneuver, Table 1 and Figs. 1–4 in Supplementary material). After stabilization of the ventilator-lung system, ten to twelve breathing cycles were recorded at each condition and stored for off-line analysis.

3.3.6 Statistical analysis

Each parameter value was represented as mean and standard deviation (SD) of ten breaths (whenever it was possible). Standard deviation showed very small differences (range 1-2%) as expected during bench test conditions; but SD was not representative when high incidence of asynchronies appeared. We used Kruskal-Wallis rank sum test to detect statistical significant differences among groups. Once differences among pairs of ventilators were found, we used Wilcoxon rank sum exact test to find out which groups were statistically different. A P value < 0.05 was considered statistically significant. Asynchrony analysis was performed by visual inspection of respiratory cycle graphs for each experimental condition; the evaluation was carried out individually by two researchers on the same traces agreeing on type and magnitude of asynchronies. Values taken for reference were based on the safety standards in design and manufacture of ventilators for home use (ISO 80601-2-72:2015 Medical *electrical equipment*) [9] assuming a negligible variability intra-condition that was not considered clinically relevant [3, 6, 10].

Table 2Mean tidal volumein BTPS delivered by eachventilator in all conditionsduring ACV, and percentageof deviation from the pre-set500 ml

ACV	Condition	Dräger Savina 300		Hamilton C3		Philips Trilogy Evo/ EV300		
		$Mean \pm SD$	%D	$Mean \pm SD$	% D	$Mean \pm SD$	% D	
Low effort								
Moderate Leak	1 S	531 ± 3	6	530 ± 1	6	483 ± 5	-3	
	2 O	529 ± 2	6	528 ± 1	6	482 ± 6	-4	
	3 R	558 ± 4	12	531 ± 2	6	480 ± 3	-4	
Low effort								
High Leak	4 S	528 ± 6	6	539 ± 10	8	487 ± 7	-3	
	5 O	516 ± 3	3	528 ± 1	6	475 <u>+</u> 7	-5	
	6 R	526 ± 2	5	530 ± 1	6	486 ± 5	-3	
Normal effort								
Moderate Leak	7 S	641 ± 2	28	577 ± 6	15	554 ± 0	11	
	8 O	516 ± 3	3	528 ± 1	6	515 ± 1	3	
	9 R	529 ± 2	6	527 ± 7	5	503 ± 9	1	
Normal effort								
High Leak	10 S	647 ± 3	29	566 ± 6	13	607 ± 1	21	
	11 O	523 ± 6	5	520 ± 5	4	479 ± 1	-4	
	12 R	527 ± 4	5	532 ± 4	6	500 ± 6	0	
Mean \pm SD		548 ± 46	$10\pm9\%$	536 ± 17	$7\pm3\%$	504 ± 39	$1\pm 8\%$	

Condition nomenclature in Table 1. BTPS Body Temperature Pressure Saturated, SD standard deviation

4 Results

4.1 Volume delivered

 V_T was measured in all conditions, but the clinical purposes of this study made it essential to highlight the V_T in ACV to assess the accuracy in volume delivered in controlled ventilation conditions (assuming variations up to 10%). Obviously, VT in PSV conditions would vary according to support pressure set for each patient requirements. Table 2 recorded V_T in ml and deviation from the 500 ml set (in %). Elisa 500 was not represented because it does not include ACV mode; V_T recorded for Servo Air and Mindray 300 were also excluded because they do offer ACV only for invasive ventilation and do not have leak compensation if ACV is used during NIV.

Dräger Savina 300, Hamilton C3 and Philips Trilogy Evo/ EV300 delivered the prescribed tidal volume in the expected range (settings \pm 10%) for almost all conditions regardless air leak or inspiratory effort. All ventilators tended to deliver higher tidal volumes during normal effort in standard lungs (Fig. 2).

4.1.1 General performance

It is remarkable that ACV mode for NIV was only available in three out of the six ventilators analyzed. All of them showed a good performance by assuring volume delivered regardless changing conditions. During standard mechanical pattern, normal inspiratory muscle effort increased V_T for the three ventilators (from 11 to 29%).



Fig. 2 Mean tidal volume delivered in all conditions for the ventilators analyzed in ACV. Differences with low and normal effort

4.2 Trigger delay time (TDT)

TDT was measured in all conditions for the six ventilators analyzed (see complete values in Table 2 in Supplementary Material). It is interesting to evaluate TDT during PSV (Table 3) and pay special attention in obstructive mechanical pattern, as TDT is directly related to comfort during NIV, especially at home, and numerous users of home-care ventilators are patients with obstructive pathology. Values higher than 200 ms have been described as clinical limit related to dyspnea [26, 32]. Table 3 also includes trigger sensitivity adjustment for each ventilator, as it directly influences TDT results. Figure 3 shows TDT in ms for conditions of low and normal effort in PSV; Fig. 4 shows TDT in ms for conditions with obstructive mechanical pattern in PSV.

4.2.1 General performance

There were great differences regarding TDT for the analyzed ventilators. Leak level did not affect TDT significantly. Changes in PSV from 10 to 20 cm H_2O slightly worsened TDT (from 0 to 60 ms, variation around 15%) that could explain in part the pressurization worsening (see next section). In contrast, low effort almost doubled TDT values for most of the ventilators (except for Philips Trilogy Evo/ EV300).

Elisa 500 and Philips Trilogy Evo/EV300 showed the best results regardless PSV level, mechanical pattern, leak level and inspiratory effort followed by Hamilton C3 and Dräger Savina 300. Focusing on obstructive mechanical pattern, most common in clinical practice, Elisa 500 and Philips Trilogy Evo/EV300 showed again the best results with TDT < 100 ms in almost all conditions (similar range as ICU ventilators). As TDT is closely related to trigger sensitivity, we tried to improve ventilators' performance for those with worse TDT results (namely Servo Air and Mindray 300) by precise trigger adjustment. In fact, Mindray 300 trigger sensitivity by default was 2 lpm but we set it at 0.5 lpm (Table 3). Even though, they both showed significantly higher TDT results.

4.3 Pressurization capacity, analyzed as PTP500

PTP500 was measured in PSV conditions for the six ventilators analyzed (Table 4). Pressure values were taken from the beginning of any detected inspiratory effort and up to 0.5 s. At 20 breaths per minute (and I:E 1:2), a time-span of 0.5 s from the beginning of inspiratory effort is 50% of the inspiratory time. We considered that during this time the pressure delivered to the patient should be at least 50% of the ideal pressurization, based on previous publications [32, 33] and our clinical experience, so good pressurization capacity for NIV devices should show PTP500 values over 50%.

Table 3	Trigger delay time	$(\text{mean} \pm \text{SD})$ recorded from ea	ch ventilator during PSV	10 and 20 cm H ₂ O
---------	--------------------	------------------------------------------------	--------------------------	-------------------------------

			Dräger Savina 300 Trigger sensitivity	Hamilton C3	Mindray 300	Elisa 500	Servo Air	Philips Trilogy Evo
Conditions			1 lpm	1 lpm	0.5 lpm	0.5 lpm	1.6 lpm	1 lpm
			Mean \pm SD					
PSV 10	Moderate leak	S	152 ± 14	97±10	203 ± 17	3±3	203 ± 19	74±4
Low effort		0	203 ± 12	225 ± 8	512 ± 49	120 ± 12	401 ± 23	126 ± 7
		R	108 ± 11	115 ± 14	231 ± 14	57 ± 5	241 ± 22	86±5
	High leak	S	146 ± 22	110 ± 7	216 ± 9	56 ± 5	224 ± 17	76 ± 4
		0	226 ± 20	201 ± 15	543 ± 39	123 ± 13	417 ± 36	126 ± 10
		R	132 ± 24	108 ± 12	245 ± 18	56 ± 13	255 ± 10	87 <u>+</u> 7
PSV 10	Moderate leak	S	68 ± 12	54 ± 4	88 ± 4	44 ± 3	92 ± 10	60 ± 6
Normal effort		0	104 ± 6	93 ± 9	148 ± 19	65 ± 4	126 ± 6	95 ± 6
		R	65 ± 5	65 ± 2	78 ± 12	39 ± 3	92 ± 6	61 ± 5
	High leak	S	70 ± 11	62 ± 7	89 ± 8	33 ± 7	95 ± 7	64 ± 5
		0	103 ± 10	94 ± 4	145 ± 6	66 ± 4	119 <u>+</u> 9	88 ± 4
		R	68 ± 7	63 ± 3	104 ± 10	52 ± 22	86 <u>+</u> 7	61 ± 8
PSV 20	Moderate leak	S	144 ± 17	98 ± 8	185 ± 9	212 ± 47	245 ± 17	85 ± 7
Low effort		0	253 ± 15	215 ± 15	583±66	148 ± 18	462 ± 34	181 ± 16
		R	132 ± 13	136 ± 26	219 ± 23	62 ± 3	261 ± 10	86 ± 11
	High leak	S	143 ± 41	104 ± 6	200 ± 20	59 ± 4	236 ± 35	68 ± 13
		0	239 ± 13	223 ± 17	584 ± 50	150 ± 16	486 <u>±</u> 38	184 ± 15
		R	179±37	114±19	222 ± 11	62 ± 4	266 ± 8	103 ± 9
PSV20	Moderate leak	S	62 ± 7	59 ± 4	69 ± 6	43 <u>±</u> 1	80 <u>±</u> 16	61 ± 4
Normal Effort		0	110 ± 5	101 ± 5	151 ± 10	69 <u>±</u> 6	146±6	110 ± 7
		R	68 ± 6	64 ± 5	98 ± 10	42 ± 5	94 <u>+</u> 6	74±7
	High leak	S	67 <u>±</u> 8	54 ± 4	75 ± 8	43 ± 5	99 <u>±</u> 6	67 ± 5
		0	117±4	103 ± 7	137 ± 10	69 ± 5	145 ± 5	115 ± 8
		R	70 ± 7	64 ± 6	96 ± 9	46 ± 5	91 ± 10	74 ± 8

Mechanical pattern: S (standard), O (obstructive) and R (restrictive)



Fig. 3 Mean trigger delay time (TDT) (mean and SD) while changes in muscle inspiratory effort and pressure support (values are averaged of the three mechanical patterns and moderate and high leak conditions). *PSV* pressure support ventilation, *E* effort



Fig. 4 Mean trigger delay time (TDT) under obstructive mechanical pattern while changes in muscle inspiratory effort and pressure support (values are averaged of moderate and high leak conditions). *PSV* pressure support ventilation, *E* effort

				Dräger Savina300	Hamilton C3	Mindray 300	Elisa 500	Servo Air	Philips Trilogy Evo
PSV10	Low effort	Moderate leak	S	49 ± 4	69±1	32 ± 3	71 ± 0	34±3	66±1
			0	47±3	48 ± 1	-7 ± 1	66 ± 2	6 ± 4	64 ± 1
			R	62 ± 4	70 ± 3	33±4	77 ± 1	29 ± 1	69 ± 1
		High Leak	S	47±6	69 ± 1	32 ± 3	70 ± 1	30 ± 3	67 ± 0
			0	41±4	47 ± 1	-9 ± 1	64 ± 4	3 ± 3	64 ± 1
			R	57±6	70 ± 2	30 ± 5	78 ± 3	29 ± 2	69 ± 0
	Normal Effort	Moderate leak	S	50 ± 3	56 ± 0	37 <u>±</u> 1	61 ± 1	48 ± 1	55 ± 0
			0	65 ± 1	71 ± 1	41 ± 1	74 ± 1	52 ± 1	66 ± 0
			R	66 ± 1	76 ± 0	51±1	74 ± 1	59 ± 1	63 ± 1
		High Leak	S	48 ± 5	56 ± 2	37 ± 2	62 ± 0	47 ± 1	55 ± 1
			0	67±3	72 ± 1	41 <u>+</u> 1	74 ± 1	51 ± 1	66 ± 1
			R	64±3	77 ± 1	45 ± 4	72 ± 4	57 ± 1	63 ± 0
PSV20	Low effort	Moderate leak	S	44 ± 4	42 ± 1	32 ± 2	68 ± 9	25 ± 3	59 ± 1
			0	38 ± 3	47 ± 3	-4 ± 0	60 ± 4	-1 ± 0	49±1
			R	56 ± 4	48 ± 4	31±5	80 ± 1	25 ± 1	62 ± 1
		High Leak	S	43±8	42 ± 1	27 ± 4	68 ± 1	24 ± 2	60 ± 1
			0	41±3	46 ± 3	-4 ± 0	61 ± 3	-2 ± 1	48 ± 1
			R	45±8	52 ± 4	29 ± 3	80 ± 1	24 ± 2	62 ± 1
	Normal Effort	Moderate leak	S	49 ± 1	31 ± 0	29 ± 1	54 ± 0	42 ± 1	54 ± 0
			0	66 ± 1	71 ± 1	46 ± 1	75 ± 1	53 ± 1	61 ± 0
			R	65 ± 1	49 ± 1	46 ± 2	74 ± 1	55 ± 1	61 ± 0
		High Leak	S	47 ± 2	32 ± 1	29 ± 0	53 ± 1	39 ± 1	54 ± 0
			0	65 ± 1	70 ± 0	46 ± 2	76 ± 1	51 ± 1	62 ± 0
			R	64 ± 2	49 <u>±</u> 1	45 ± 1	74 ± 1	53 ± 1	61 ± 0

Table 4 Percentage of Ideal PTP500 (mean percentage ± standard deviation) recorded for each ventilator during PSV10 and PSV20

Values were measured only in synchronic cycles



Fig. 5 PTP500 (mean and SD in %) in PSV10 and 20 for mean values of mechanical pattern and leak level, comparing low and normal inspiratory effort



4.4 General performance

Leak level did not significantly affect PTP500 regardless mechanical pattern; changes in PSV from 10 to 20 cm H_2O slightly decreased PTP500 (from 2 to 26%) as represented in Fig. 5. Low effort also decreased PTP500 especially for Mindray300 and Servo Air. Dräger Savina 300, Hamilton C3, Elisa 500 and Philips Trilogy Evo/EV300 obtained mean PTP500 > 50% in almost all conditions. Mean values did not change for Elisa 500, which showed the most homogeneous values in all conditions followed by Philips Trilogy Evo/EV300. Mindray 300 and Servo Air comparatively developed the worst pressurization capacity in all conditions.

As recorded in Table 4 and represented in Fig. 6, the worst pressurization capacity was developed under obstructive mechanical pattern and low effort in Mindray 300 and Servo Air. These worrying results, as obstructive patients are frequent users of home care therapies, may be explained by the interdependence of PTP500 and TDT. Negative values of PTP500 (Mindray 300) indicate that trigger delay time is longer than 500 ms. This way the area under Paw curve in the first 500 ms become negative (see Fig. 7). If TDT was lower, Paw rise would occur sooner and PTP500 results would improve.

In order to elucidate why such differences in PTP500 results were obtained, influence of trigger delay (TDT)



Fig.7 Mindray 300 during PSV 10 with obstructive pattern, low effort and moderate leak. Time delay from drop in Paw until rising in flow (in purple) and Paw (in blue) is longer than 500 ms and makes

the area under airway pressure in the first 500 ms to become negative (striped area). Ideal PTP500 is represented by the shaded area



Fig. 8 Influence of TDT in pressurization capacity (PTP500) comparing low and normal effort; dots represent average values of different conditions (PSV, mechanical pattern and leak level)

Mode	Condition	s	Asynchrony Index (%) for the analyzed ventilators							
			Mechanical pattern: S	Mechanical pattern: Standard/Obstructive/Restrictive						
	Effort	Leak	Dräger Savina 300	Elisa 500	Hamilton C3	Servo Air	Mindray 300	Philips Trilogy Evo		
ACV	Low	Moderate	0/0/38		0/0/0			0/0/0		
		High	0/0/0		0/0/17			0/0/0		
	Normal	Moderate	0/0/0		18/0/0			0/0/0		
		High	0/0/0		0/0/0			0/0/0		
PSV10	Low	Moderate	0/0/0	0/0/17	0/0/0	0/0/17	0/0/0	0/0/0		
		High	0/0/0	0/0/0	0/0/0	0/0/0	0/0/0	0/0/0		
	Normal	Moderate	0/0/0	8/0/0	0/0/25	17/0/0	0/0/0	0/0/0		
		High	0/0/0	41/0/58	0/0/33	0/0/0	0/0/0	0/0/0		
PSV20	Low	Moderate	0/8/0	69/0/68	0/0/0	0/0/0	0/25/0	0/0/0		
		High	0/0/0	23/0/65	0/0/0	0/8/0	0/33/0	0/0/0		
	Normal	Moderate	0/0/0	81/0/80	0/0/0	0/0/8	8/0/0	0/0/0		
		High	0/0/0	23/0/62	0/0/8	0/0/0	0/0/0	0/0/0		

Table 5 Asynchrony index (%) for the analyzed ventilators in all conditions

over PTP500 in our bench test was analyzed; Fig. 8 shows the correlation between PTP500 and TDT. As seen, the relationship depends on the effort level: a clear relationship can be seen for low effort conditions. However, this correlation disappears for values obtained under conditions of normal effort. Inverse relationship of TDT-PTP500 may explain the worse results for Mindray 300 producing negative PTP500 values while obstructive pattern under low effort (see Fig. 6).

Table 6	Types and incidence of asynchronies develop	ed by	each	ven-
tilator ir	n all conditions analyzed			

Ventilator	Asynchronies	Incidence in con- ditions	Total incidence (%)
Savina 300	Double trigger	ACV: 3	3
	Ineffective effort	PSV: 26	3
Hamilton C3	Double trigger	ACV: 6	3
	Auto-triggering	ACV: 6, 7	6
		PSV: 21, 24, 36	8
Mindray 300	Ineffective effort	PSV: 26, 29	8
Elisa 500	Auto-triggering	PSV: 15,18,19,24 ,25,27,28,30,31 ,33,36	46
Servo Air	Ineffective effort	PSV: 29	4
Philips Trilogy Evo			0

Condition nomenclature in Table 1

4.5 Asynchrony index

Synchronization assessment of each ventilator is of paramount importance at clinical level for patient's comfort and because asynchronies can determine the failure of mechanical ventilation with potential deleterious consequences. In general, few asynchronies developed during this analysis (Table 5). Overall incidence was 12% (21asynchronies out of 180 conditions); 13% during PSV conditions (18 out of 144 conditions) and 8% during ACV (3 out of 36 conditions). The most frequent ones were Auto-Triggering (AT) and Double-Trigger (DT) (described in Table 6). Remarkably Philips Trilogy Evo/EV300 did not develop any timeasynchrony under the analyzed conditions. Elisa 500 showed asynchronies (AT) in pressure support at almost any condition (Figs. 9 and 10), increasing in PSV20 regardless changes in leak level and muscle effort (Table 6). Savina 300 showed only two asynchronies: DT in ACV and Ineffective Effort (IE) in PSV20. Hamilton C3 developed few AT and DT with restrictive mechanical pattern (Fig. 11).

It is important to describe the asynchronies developed by the analyzed ventilators as they play an important role during NIV: primarily because asynchronies directly affect comfort and tolerance of mechanical ventilation [1], and secondly as they are essential for protective mechanical ventilation as has been recently highlighted. [34].

AT and DT were the most frequently developed asynchronies, which are directly related to patient comfort because they are un-demanded pressure cycles. AT developed even with normal effort and pressure support levels used in clinical practice. In contrast, few ineffective efforts developed, which also affect comfort due to the lack of support.



Fig. 9 Paw in yellow, Volume in white, Flow in red and Pressure muscular in green: ELISA 500 in condition 24 (PSV 10, Normal effort, high leak). As shown, there is no inspiratory effort prior to the

first airway pressure increase (AT); in contrast, the second cycle starts with the inspiratory effort



Fig. 10 A 12 cycles of Elisa 500 in condition 31 recorded with AT and double trigger, **B** several IE with Mindray 300 in condition 26. Many inspiratory efforts (in green) are not followed by airway pressure (in yellow) or flow (in red) increase. Condition nomenclature in Table 1



Fig. 11 AT developed by Hamilton C3 during PSV10 in conditions 21 and 24 (restrictive pattern, normal effort and moderate and high leak, respectively). AT appeared even after modifying trigger settings (Trigger sensitivity 1 lpm)

Cursor (10.000 0.00

66.600 66.800 67

Time (s

All these asynchronies are highly dependent on trigger sensitivity, already mentioned as it was adjusted during the experiments to avoid AT. In our performance analysis, whenever we detected AT in any condition, we modified trigger sensitivity up to 1.6 lpm (for Servo Air) to cope with them. In many cases, asynchronies mentioned developed in identical conditions for many devices, so they must be linked to performance characteristics of the equipment itself. Ventilators' intrinsic behavior that favors asynchronies could be related to the magnitude of bias flow (set by each manufacturer). Flow sensitivity should be adjusted around 1/2 of bias flow magnitude; this way high bias flow will require a higher flow sensitivity which may prolong TDT, decrease PTP500 and favor asynchronies.

5 Discussion

As different ventilators have been recently marketed, it is important to know how they perform in order to choose the device which best fits each patient needs. This study explored general performance of six ventilators using the ASL5000[©] lung simulator, validated in previous analysis [8, 9, 35, 36]. They were tested during NIV against different combinations of mechanical pattern, ventilatory mode, leak level and inspiratory effort, with similar methodology as our previous work [32]. Measured results included volume delivered, time response to trigger, pressurization capacity and synchronization. As far as we know, our publication is one of the few analyzing VT in ACV during NIV [37, 38]. Despite doubts about leak compensation from portable ventilators discussed in previous publications [23, 36, 39, 40], the analyzed devices successfully compensated changeable air leaks. Variable efforts in NIV have not been as addressed in recent literature, but we also found a good compensation for effort variations with our devices. The availability of ACV mode for NIV in only three devices and the interdependence between PTP500 and TDT values with low effort were new findings.

Main results:

- 1- ACV mode for NIV was available in three out of six ventilators analyzed: Savina 300, Hamilton C3 and Philips Trilogy Evo/EV300. All of them obtained V_T within the security range in all conditions, so they could be reliable devices for home use under ACV even with variable leaks or inspiratory efforts.
- 2- Trigger delay (TDT) remained into an acceptable range < 200 ms for many conditions in spite of PSV level and leak magnitude changes, as already seen in previous series [28]. In contrast, TDT worsened significantly with low muscle effort, even doubling TDT values except for Philips Trilogy Evo/EV300. Servo Air and Mindray 300

 Table 7
 Values for obstructive mechanical pattern under high leak and moderate effort (condition 35), linked to Fig. 12

Obstructive mechanical pattern under high leak and moderate effort PSV20	TDT (in ms)	PTP500 (in %)	
Dräger Savina 300	103	67	
Hamilton C3	94	72	
Mindray 300	145	41	
Elisa 500	66	74	
Servo Air	119	51	
Philips Trilogy Evo/EV300	88	62	

TDT trigger delay time, % PTP500 percent of ideal pressure time product in the first 500 ms



Fig. 12 Graphic representation of TDT and PTP500 measured for the six ventilators analyzed in the obstructive most frequent home-care condition

obtained the highest TDT values even after trigger sensitivity adjustment.

- 3- Results of pressurization were worse than expected for NIV. PTP500 remained unaffected regardless leak level. Increased pressure support and lower effort slightly decreased PTP500 results for Mindray 300 and Servo Air under obstructive lungs and low effort. Elisa 500 and Philips Trilogy Evo/EV300 achieved similar PTP500 values for all conditions and showed good performance above 50% in all conditions with normal effort.
- 4- The effect of TDT over PTP500 was isolated and we found that under low effort, PTP500 presented interdependence with TDT (lower pressurization with higher TDT values). That is why Mindray 300 showed inability for airway pressurization in the first 500 ms even if, after that time interval, pressurization was correct.
- 5- In general, Asynchrony Index was low. AT and DT were the most frequently developed asynchronies. To avoid them, trigger sensitivity was adjusted but in some cases AT did not disappear. That could be explained by performance characteristics of the equipments (ventilators'

intrinsic behavior). Philips Trilogy Evo/EV300 did not show any asynchrony with trigger sensitivity of 1 lpm.

All ventilators demonstrated great capability to counteract the effect of higher leaks, as performance did not worsen in those conditions. This fact points out the great technological improvements done in the last years, as previous assessments achieved heterogeneous results [36, 41]. In contrast, differences observed with changes in muscle inspiratory effort must be taken into account for ventilator choice (for example, patients with neuromuscular weakness must be carefully assessed after initiating ventilatory therapy to avoid hypoventilation and discomfort [42, 43]). Pressurization capacity was highly dependent on TDT values, so both must be checked and analyzed together (Table 7). Elisa 500 showed the best results of trigger response and pressurization capacity (Fig. 12).

5.1 Clinical implications

The perfect device for NIV does not exist because we must take into account characteristics of paramount importance and the variable clinical situation of each patient. A good approach on the ideal device for NIV is the ventilator that combines security (safe V_T and high PTP500) and comfort (low TDT and synchronization); it should compensate variable leaks and adapt to different inspiratory efforts regardless level of support without developing asynchronies. Even if we did not find the perfect device, some are close to the best performance and almost all worked within acceptable values.

Whenever ACV in NIV is needed, Savina 300, Hamilton C3 and Philips Trilogy Evo/EV300 are good options. During PSV, some differences could make a difference on device selection. For patients with low muscle effort, Philips Trilogy Evo/EV300 developed a fast response without asynchronies, and in case of normal effort both Trilogy Evo/EV300 and Elisa 500 presented similar performance and could be interchangeable. Worse options for patients which need a fast response are Servo Air and Mindray 300, as they presented longer TDT even after trigger sensitivity adjustment. For patients whose main concern is airway pressurization, Elisa 500 achieved the best performance even in adverse conditions; in contrast, Mindray 300 is the last option because of the worst PTP500 linked to TDT influence. As tolerance during home care is matter of great importance, good options seem both Philips Trilogy Evo/EV300 and Savina300, because of their lower rates of asynchronies combined with faster TDT responses, specially the first one. Also, they both have ACV mode so neuromuscular patients can benefit from these options, as whenever they need controlled ventilation at home, worse adaptation leads to lower survival rates and poor prognosis [42].

5.2 Limitations

Our findings should be interpreted in the context of several limitations. Firstly, this was a laboratory analysis, thus clinical studies with patients could show different results due to variable conditions associated to patients' heterogeneous characteristics and dynamic changes. Secondly, we chose thirty-six conditions that only reproduced few clinical scenarios even if more complex conditions could be taken into consideration. Performance in ACV mode was analyzed even if it does not have a spread clinical use. We decided to consider it because some ventilators offer this mode and it has its indication in, for instance, patients with neuromuscular pathology. Thirdly, many ventilator settings, as trigger sensitivity, can be adjusted in different ways during the clinical practice. In contrast, we are limited in the context of using a lung model. Also, by using ASL5000[©] the spontaneous inspiratory profile is not modified by pressurization during the inspiratory phase. Errors in the measurements during the experiment may have occurred but being systematic they would affect all the devices in a similar way. At last, we evaluated the ventilators based in four parameters that we considered to be representative of their performance, and that have been already used in previous publications [9, 17, 44, 45]. Other combinations and setting would generate different results.

6 Conclusions

As a result of the bench test developed, we found a relevant variation in the performance among devices. In PSV conditions, Philips Trilogy Evo/EV300, Hamilton C3 and Elisa 500 seemed the most reliable devices, as they showed the best performance in terms of trigger response and pressurization capacity. When patient comfort was of main concern, only Philips Trilogy Evo/EV300 did not develop any time-asynchrony and must be the preferable choice; Dräger Savina 300 and Servo Air also seem good options. In contrast, Elisa 500 showed poor synchronization. In case ACV is necessary, only three well founded options remain available: Dräger Savina 300, Hamilton C3 and Philips Trilogy Evo/EV300.

Supplementary Information The online version contains supplementary material available at https://doi.org/10.1007/s10877-023-01019-z.

Acknowledgements Alberto Centeno, facilitator of the experimental model; Department of Pneumology of Hospital Clínico Universitario de Valencia, for their valuable experience with ventilators'use; Informatics Service of INCLIVA, by their help whenever computer issues did not let us advance with the experiment.

Author contributions All the authors performed the laboratory analysis. SMC, JBN, JPB and CDN analyzed and recorded the results obtained. JBN, MSD and SMC interpreted the main data. HOP performed the statistical analysis. JBN and SMC were major contributors in writing the manuscript. All authors read and approved the final manuscript.

Funding Open Access funding provided thanks to the CRUE-CSIC agreement with Springer Nature. The authors have not disclosed any funding.

Data availability All data generated or analyzed during this study are included in this published article (and its supplementary information files). Data are however available from the corresponding author upon reasonable request in saradacuris@hotmail.com or anestesia.saramartinezcastro@gmail.com.

Declarations

Competing interests The authors have not disclosed any competing interests.

Ethical approval Not applicable.

Consent for publication Not applicable

Open Access This article is licensed under a Creative Commons Attribution 4.0 International License, which permits use, sharing, adaptation, distribution and reproduction in any medium or format, as long as you give appropriate credit to the original author(s) and the source, provide a link to the Creative Commons licence, and indicate if changes were made. The images or other third party material in this article are included in the article's Creative Commons licence, unless indicated otherwise in a credit line to the material. If material is not included in the article's Creative Commons licence and your intended use is not permitted by statutory regulation or exceeds the permitted use, you will need to obtain permission directly from the copyright holder. To view a copy of this licence, visit http://creativecommons.org/licenses/by/4.0/.

References

- 1. Cammarota G, Simonte R, De Robertis E. Comfort during noninvasive ventilation. Front Med. 2022;9:1–9.
- Thille AW, Lyazidi A, Richard JCM, Galia F, Brochard L. A bench study of intensive-care-unit ventilators: new versus old and turbine-based versus compressed gas-based ventilators. Intensive Care Med. 2009;35(8):1368–76.
- 3. Olivieri C, Costa R, Conti G, Navalesi P. Bench studies evaluating devices for non-invasive ventilation: critical analysis and future perspectives. Intensive Care Med. 2012;38:160–7.
- https://www.ingmarmed.com/product/asl-5000-lung-solutionfor-simman/. User manual ASL5000. IngMar Medical. 2016. p. 292.
- Dexter A, McNinch N, Kaznoch D, Volsko TA. Validating lung models using the ASL 5000 breathing simulator. Simul Healthc. 2018;13(2):117–23.
- Ferreira JC, Chipman DW, Hill NSKR. Bilevel vs ICU ventilators providing noninvasive ventilation: effect of system leaks: a COPD lung model comparison. Chest. 2009;136(2):448–56.
- Garnier M, Quesnel C, Fulgencio JP, Degrain M, Carteaux G, Bonnet F, et al. Multifaceted bench comparative evaluation of latest intensive care unit ventilators. Br J Anaesth. 2015;115(1):89–98. https://doi.org/10.1093/bja/aev028.

- 8. Marjanovic NS, De Simone A, Jegou G, L'Her E. A new global and comprehensive model for ICU ventilator performances evaluation. Ann Intensive Care. 2017;7(1):1–13.
- 9. L'Her E, Roy A, Marjanovic N. Bench-test comparison of 26 emergency and transport ventilators. Crit Care. 2014;18(5):1–14.
- 10. Zhu K, Rabec C, Gonzalez-bermejo J, Hardy S, Aouf S, Escourrou P, et al. Combined effects of leaks, respiratory system properties and upper airway patency on the performance of home ventilators: a bench study. BMC Pulm Med. 2017;17(1):1–9.
- Stell IANM, Paul G, Lee KC, Ponte J, Moxham J. Noninvasive ventilator triggering in chronic obstructive pulmonary disease. A test lung comparison. Am J Respir Crit Care Med. 2001;164:2092–7.
- 12. Costa R, Navalesi P, Spinazzola G, Rossi M, Cavaliere F, Antonelli M, Proietti RCG. Comparative evaluation of different helmets on patient-ventilator interaction during non-invasive ventilation. Intensive Care Med. 2008;34:1102–8.
- 13. Ferreira JC, Chipman DWKR. Trigger performance of mid-level ICU mechanical ventilators during assisted ventilation: a bench study. Intensive Care Med. 2008;34:1669–75.
- Borel JC, Sabil A, Janssens JP, Couteau M, Boulon L, Levy PPJ. Intentional leaks in industrial masks have a significant impact on efficacy of bilevel non-invasive ventilation: a bench test study. Chest. 2009;135(3):669–77.
- 15. Adams AB, Bliss PLHJ. Effects of respiratory impedance on the performance of bi-level pressure ventilators. Respir Care. 2000;45:390–400.
- Mehta S, Mccool FD, Hill NS. Leak compensation in positive pressure ventilators: a lung model study. Eur Resp. 2001;17:259–67.
- Robert D, Zanetta G, Guérin C. Evaluation of ventilators used during transport of ICU patients—a bench study. Intensive Care Med. 2002;28:443–51.
- Battisti A, Tassaux D, Janssens JP, Michotte JB, Jaber SJP. Performance characteristics of 10 home mechanical ventilators in pressure—support mode. A comparative bench study. Chest. 2005;127(5):1784–92. https://doi.org/10.1378/chest.127.5.1784.
- Vignaux L, Tassaux D, Carteaux G, Roeseler J, Piquilloud L, Brochard LJP. Performance of noninvasive ventilation algorithms on ICU ventilators during pressure support: a clinical study. Intensive Care Med. 2010;36(12):2053–9.
- Carlucci A, Jaber S, Maggiore S, Fougère S, Harf A. Bench testing of pressure support ventilation with three different generations of ventilators. Intensive Care Med. 2002;28(8):1049–50.
- Chipman DW, Caramez MP, Miyoshi E, Kratohvil JP, Kacmarek RM. Performance comparison of 15 transport ventilators. Respir Care. 2007;52(6):740–51.
- 22. Khirani S, Louis B, Leroux K, Delord V, Fauroux B, Trousseau A, et al. Harms of unintentional leaks during volume targeted pressure support ventilation. Respir Med. 2013;107:1021–9.
- Ueno Y, Nakanishi N, Oto J, Imanaka H, Nishimura M. A Bench study of the effects of leak on ventilator performance during noninvasive ventilation. Respir Care. 2011;56(11):1758–64.
- Camus P. Evaluating noninvasive ventilation using a monitoring system coupled to a ventilator: a bench-to-bedside study. Eur Respir J. 2009;34(4):902–13.
- 25. Oscroft NSSI. A bench test to confirm the core features of volume-assured non-invasive ventilation. Respirology. 2010;15:361-4.
- Fresnel E, Muir J-F, Letellier C. Performances of domiciliary ventilators compared by using a parametric procedure. EPJ Nonlinear Biomed Phys. 2016. https://doi.org/10.1140/epjnbp/ s40366-016-0033-9.
- 27. Aslanian P, Atrous SEL, Isabey D, Valente E, Corsi D, Harf A, et al. Effects of flow triggering on breathing effort

during partial ventilatory support. Am J Respir Crit Care Med. 1998;157:135–43.

- Delgado C, Romero JE, Puig J, Izquierdo A, Ferrando C, Belda FJ, et al. Performance of the new turbine mid-level critical care ventilators. Respir Care. 2016;62(1):34–41.
- Ríos-Castro F, González-Seguel F, Molina J. Impulso, esfuerzo y trabajo respiratorio: revisión de definiciones y herramientas no invasivas de ventiladores de cuidados intensivos durante tiempos de pandemia. Medwave. 2022;22(3):1–13.
- Racca F, Squadrone V, Ranieri VM. Patient-ventilator interaction during the triggering phase. Respir Care Clin N Am. 2005;11(2):225–45.
- Battisti A, Tassaux D, Janssens JP, Michotte JB, Jaber SJP. Performance characteristics of 10 home mechanical ventilators in pressure—support mode. A comparative Bench Study. Chest. 2005;127(5):1784–92.
- 32. Martínez S, Belda J, Delgado C, Puig J. A bench evaluation of eight home-care ventilators. Respir Care. 2021;66(10):1531–41.
- 33. Jaber S, Tassaux D, Sebbane M, Pouzeratte Y, Battisti A, Capdevila X, et al. Performance characteristics of five new anesthesia ventilators and four intensive care ventilators in pressuresupport mode: a comparative bench study. Anesthesiology. 2006;105(5):944–52.
- Goligher EC, Jonkman AH, Dianti J, Vaporidi K, Beitler JR, Patel BK, et al. Clinical strategies for implementing lung and diaphragm-protective ventilation: avoiding insufficient and excessive effort. Intensive Care Med. 2020;46(12):2314–26. https://doi. org/10.1007/s00134-020-06288-9.
- Schettino GP, Tucci MRSR, Valente Barbas CS, PAM CRC. Mask mechanics and leak dynamics during non-invasive pressure support ventilation: a bench study. Intensive Care Med. 2001;27:1887–91.
- Oto J, Chenelle CT, Marchese AD, Kacmarek RM, Faarc RRT. A comparison of leak compensation in acute care ventilators during noninvasive and invasive ventilation: a lung model study. Respir Care. 2013;58(12):2027–37.

- Kelly J, Jaye J, Pickersgill R, Chatwin M, Morrell MSA. Randomized trial of ' intelligent ' autotitrating ventilation versus standard pressure support non-invasive ventilation: impact on adherence and physiological outcomes. Respirology. 2014;19:596–603.
- Chen Y, Cheng K, Zhou X. Performance characteristics of seven bilevel mechanical ventilators in pressure-support mode with different cycling criteria: a comparative bench study. Med Sci Monit. 2015;21:310–7.
- Mehta S, Hill NS. Noninvasive ventilation. State of the art. Am J Respir Crit Care Med. 2001;163:540–77.
- Mehta S, McCool FDHN. Leak compensation in positive pressure ventilators: a lung model study. Eur Respir J. 2001;17:259–67.
- Piquilloud L, Vignaux L. Varying leaks: A challenge for modern ventilators? Respir Care. 2013;58(12):2194–5.
- Sancho J, Servera E, Bañuls P, Marín J. Prolonging survival in amyotrophic lateral sclerosis: efficacy of noninvasive ventilation and uncuffed tracheostomy tubes. Am J Phys Med Rehabil. 2010;89(5):407–11.
- Morelot-Panzini C, Bruneteau G, Gonzalez-Bermejo J. NIV in amyotrophic lateral sclerosis: the 'when' and 'how' of the matter. Respirology. 2019;24(6):521–30.
- Carteaux Guillaume, Lyazid Aissam, Cordoba-Izquierdo Ana, Vignaux Laurence, Jolliet Philippe, Thille Arnaud W, Richard Jean-Christophe M, LB,. Patient-ventilator asynchrony during noninvasive ventilation: a bench and clinical study. Chest. 2012;142(2):367–76.
- 45. Chiumello D, Pelosi P, Croci M, Bigatello LM, Gattinoni L. The effects of pressurization rate on breathing pattern, work of breathing, gas exchange and patient comfort in pressure support ventilation. Eur Respir J. 2001;18:107–14.

Publisher's Note Springer Nature remains neutral with regard to jurisdictional claims in published maps and institutional affiliations.