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Stature estimation by semi-automatic measurements of 3D CT images of the femur

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Abstract

Stature estimation is one of the most basic and important methods of personal identification. The long bones of the limbs provide the most accurate stature estimation, with the femur being one of the most useful. In all the previously reported methods of stature estimation using computed tomography (CT) images of the femur, laborious manual measurement was necessary. A semi-automatic bone measuring method can simplify this process, so we firstly reported a stature estimation process using semi-automatic bone measurement software equipped with artificial intelligence. Multiple measurements of femurs of adult Japanese cadavers were performed using automatic three-dimensional reconstructed CT images of femurs. After manually setting four points on the femur, an automatic measurement was acquired. The relationships between stature and five femoral measurements, with acceptable intraobserver and interobserver errors, were analyzed with single regression analysis using the standard error of the estimate (SEE) and the coefficient of determination (R^2). The maximum length of the femur (MLF) provided the lowest SEE and the highest R^2 ; the SEE and R^2 in all cadavers, males and females, respectively, were 3.913 cm (R^2 =0.842), 3.664 cm (R^2 =0.705), and 3.456 cm (R^2 =0.686) for MLF on the right femur, and 3.837 cm (R^2 =0.848), 3.667 cm (R^2 =0.705), and 3.384 cm (R^2 =0.699) for MLF on the left femur. These results were non-inferior to those of previous reports regarding stature estimation using the MLF. Stature estimation with this simple and time-saving method would be useful in forensic medical practice.

Keywords Stature estimation · Femur · Computed tomography · Artificial intelligence · Semi-automatic measurement

Introduction

Stature estimation is one of the most important and basic methods for individual identification as well as for sex and age estimation [1-10]. Recent forensic anthropology reports have described sex, weight, and age estimation

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using computed tomographic (CT) images of bones [11–22]. Regarding stature estimation, the long bones of the limbs provide the most accurate stature estimation over a wide age range in studies conducted on different races. Among them, the femur is reported as one of the most useful for stature estimation [4, 10, 23–30].

Conventionally, the femur is measured using an osteometric board, which is placed on a horizontal plane [31–35]. In recent reports, the femur was measured using X-ray photography [36–38]. Some reports have provided stature estimation using CT images of the femur [39–44], and researchers in these studies manually measured the femur on CT images for estimation. However, manual measurement requires a certain level of technical proficiency and can be affected by the performance of the measurer. Thus, using a simpler measurement method than the manual method may provide benefits such as reduction of time and effort required for measurement and prevention of unintentional measurement errors. Herein, we created three-dimensional (3D) reconstructed images from postmortem CT images and measured the femur using a semi-automatic measurement software, with the aim of providing new stature estimation formulae based on these semi-automatic measurements.

Materials and methods

This study included 300 cadavers of known sex and age over 18 that underwent whole-body postmortem CT imaging and subsequent forensic autopsy at the forensic medicine departments at Chiba University and the University of Tokyo in Japan between October 2016 and October 2020. Cadavers with severe decomposition, burn injuries, congenital malformations, postoperative changes, missing parts, femoral fractures, severe deformation of the vertebral bodies, and severe trauma to the head, neck, trunk, or lower limbs were excluded because such conditions have possible effects on the condition of the femur or stature. We included the cadavers of 150 males (10–20 years, n = 1; 21–30 years, n = 21; 31-40 years, n = 19; 41-50 years, n = 37; 51-60 years, n = 38; 61–70 years, n = 20; 71–80 years, n = 12; 81–90 years, n = 2) and 150 females (10–20 years, n = 13; 21-30 years, n = 12; 31-40 years, n = 28; 41-50 years, n = 24; 51-60 years, n = 21; 61-70 years, n = 18; 71–80 years, n = 20; 81–90 years, n = 14). Cadaver stature was measured in the supine position before autopsy using a measuring tape or a ruler. The adjusted stature (AS) was calculated by subtracting 2.0 cm from the measured stature to obtain an estimate of the living stature according to previous studies [45-48].

At Chiba University, postmortem CT was performed using a 64-row detector CT system (Supria Grande; Fujifilm Healthcare Corporation, Tokyo, Japan), and the scanning protocol was as follows: tube voltage, 120 kV; tube current, 250 mA; scan time, 0.75 s; collimation, 0.625 mm. The slice thickness, reconstruction interval, and field of view during image reconstruction were 1.0, 0.725, and 500 mm, respectively. At the University of Tokyo, postmortem CT was performed using a 16-row detector CT system (ECLOS; Fujifilm Healthcare Corporation), and the scanning protocol was as follows: tube voltage, 120 kV; tube current, 200 mA; scan time, 1 s; collimation, 1.25 mm. The slice thickness, reconstruction interval, and field of view during image reconstruction were 1.25, 1.25, and 500 mm, respectively.

Image data were processed on a workstation (Synapse Vincent; Fujifilm Medical), and a semi-automatic application was used to measure the femur. Just after launching, this application automatically recognizes the femur and displays it as a reconstructed 3D image. If it contains other structures, such as calcified blood vessels or cartilage, manual adjustments are necessary. After confirmation that the reconstruction is appropriate, the bone surface information is automatically extracted with a single click. By manually marking the four points—the center of the femoral head, intercondylar notch (ICN), medial epicondyle, and lateral epicondyle—on the model (Fig. 1), 41 measurements are automatically calculated and displayed (Table 1). The time required from manual marking to displaying the results was approximately 40 s. Using the results of each cadaver, the average values of the right and left femurs were also calculated (Fig. 2).

First, to select measurements with acceptable intraobserver and interobserver errors, 20 cadavers were randomly selected. To evaluate the intraobserver error, a single researcher measured the femurs twice with an interval of \geq 1 day for each cadaver. To evaluate the interobserver error, another researcher measured the femurs, and the result was then compared with the first result from the first researcher. The intraobserver and interobserver errors were assessed with the technical error of measurement (TEM), relative technical error of measurement (rTEM), and coefficient of reliability (R) [49, 50]. The acceptance range for rTEM was set at < 1.5% for intraobserver error and < 2.0% for interobserver error [51].

Second, the sexual differences in age, AS, and acceptable measurement were evaluated. If these values followed a normal distribution, Student's t-test was used. If the values did not follow a normal distribution, the Wilcoxon rank sum test was used instead [52, 53]. The absolute *z* values of skewness and kurtosis were used to assess normal distribution [54].

Lastly, the relationship between AS and each measurement for all 300 cadavers was assessed using single regression analysis with the statistical values of the coefficient of determination (R^2) and the standard error of the estimate (SEE). In this analysis, all manual markings were performed by a single researcher. A residual plot was created with the predicted stature calculated with the obtained regression equation, and the difference between the predicted stature and AS and the existence of heteroscedasticity was examined [55].

Statistical significance was set at P < 0.05 to reject the null hypothesis that there was no significant difference in statistical values between males and females and that the regression coefficient was 0. Statistical analysis was performed using Excel 2010 (Microsoft Corporation, Redmond, WA, USA).

Results

The 41 measurements were classified into groups 1 and 2 based on the results of intraobserver and interobserver errors (Table 2), and the TEM, rTEM, and R values for each measurement of both the right and left femurs are shown

Fig. 1 Four points where manual marking are necessary (each picture shows one point in the horizontal, coronal, and sagittal planes and the threedimensional reconstruction of the computed tomography images). a Center of the femoral head: the central point of the femoral head. **b** Intercondylar notch: posterior 1/4 point on the midline of the recess located between the medial and lateral condyles on the bottom surface of the lower end of the femur. c Medial epicondyle: the most medial point of the medial condyle. **d** Lateral epicondyle: the most lateral point of the lateral condyle



Fig. 2 Five measurements with acceptable intraobserver and interobserver errors. **a** Maximum length of the femur (MLF). **b** Lateral anterior–posterior length (LAP). **c** Crosssection medial–lateral width (C-ML). **d** C-lateral anterior– posterior length (C-LAP). **e** C-medial anterior–posterior length (C-MAP)



Table 1 Definition of measurements

| Measurement | Abbreviation | Definition |
|---|--------------|---|
| Maximum length of the femur | MLF | Distance between the plane tangent to the lowest points of the medial and lateral condyles of the femur (referred to as plane α) and the plane parallel to plane α that is tangent to the upper end of the femur |
| Valuation angle | VA | Angle formed by the MA and the line segment connecting the center of the femoral diaphysis and the ICN when the femur is observed from the ventral side |
| Lordosis angle | LA | Angle formed by the MA and the line segment connecting the center of femoral diaphysis and the ICN when the femur is observed from the lateral side |
| Lateral anterior-posterior length | LAP | Distance between the two lines when lines parallel to the SEA are drawn to pass through the anterior and posterior ends of the lateral epicondyle when the femur is observed from the bottom side |
| Medial anterior-posterior length | MAP | Distance between the two lines when lines parallel to the SEA are drawn to pass through the anterior and posterior ends of the medial epicondyle when the femur is observed from the bottom side |
| Partial lateral anterior-posterior length | P-LAP | Distance between the two lines when lines parallel to the SEA is drawn to pass through the rearmost end of the lateral condyle and the posterior end of the intercondylar fossa when the femur is observed from the bottom side |
| Partial medial anterior-posterior length | P-MAP | Distance between the two lines when lines parallel to the SEA is drawn to pass through the rearmost end of the medial condyle and the posterior end of the intercondylar fossa when the femur is observed from the bottom side |
| Lateral distal resection amount | LRA | Distance between two lines when straight lines parallel to SEA are drawn through the lower end of the lateral condyle and the ICN when observed facing the plane created by SEA and MA (referred to as plane β) |
| Medial distal resection amount | MRA | Distance between two lines when straight lines parallel to SEA are drawn through the lower end of the medial condyle and the ICN when observed facing plane β |
| Cross-section partial lateral anterior-posterior length | C-P-LAP | Distance on CS A' (which is a cross section that is orthogonal to plane β and approximates a horizontal section at a height that passes through the ICN) between the SEA and the straight line parallel to the SEA drawn so as to pass through the posterior end of the lateral condyle |
| Cross-section partial medial anterior-posterior length | C-P-MAP | Distance on CS A' between the SEA and the straight line parallel to the SEA drawn so as to pass through the posterior end of the medial condyle |
| Posterior condyle axis angle | PCA-angle | Angle formed by the SEA and a straight line passing through the posterior ends of the medial and lateral condyles when the femur is observed from the bottom |
| Cross-section lateral-middle length | C-LML | Distance between the two lines when straight lines perpendicular to the SEA are drawn so as to pass through the lateral end of CS A' and the ICN |
| Cross-section medial-middle length | C-MML | Distance between the two lines when straight lines perpendicular to the SEA are drawn so as to pass through the medial end of CS A' and the ICN |
| Cross-section medial-lateral width | C-ML | Distance between the two lines when straight lines perpendicular to the SEA are drawn so as to pass through the medial end of CS A' and the lateral end of CS A' |
| Lateral distal anterior angle | LDA-angle | Angle formed on CS A' by the straight line orthogonal to the SEA and line passing through points A and B, which are the intersections of a straight line parallel to the SEA through ICN and the SEA with the outermost side of CS A' |

Table 1 (continued)

| Measurement | Abbreviation | Definition |
|---|--------------|---|
| Medial distal anterior angle | MDA-angle | Angle formed on CS A' by the straight line orthogonal to the SEA and the line passing through points C and D, which are the intersections of a straight line parallel to the SEA through the ICN and the SEA with the innermost side of CS A' |
| Medial distal radius of the curvature | MDAC | Radiation of the curvature of point C on CS A' |
| Joint line angle | JL-angle | Angle formed by the line parallel to the SEA passing through the ICN and the straight line passing through the lower end of the lateral condyle and that of the medial condyle when the femur is observed from the ventral side |
| Medial superior-inferior length | MSI | Length from the top to the bottom of CS B', which is a cross section formed on the medial condyle that is perpendicular to CS A' and passes through the lateral and medial posterior ends of CS A' |
| Lateral superior-inferior length | LSI | Length from top to bottom of CS C', which is a cross section formed on the lateral condyle so as to be perpendicular to CS A' and passes through the lateral and medial posterior ends of CS A' |
| Medial condyle width | MCW | Length from the medial end to the lateral end of CS B' |
| Lateral condyle width | LCW | Length from the medial end to the lateral end of CS C' |
| Medial condyle to middle width | MCMW | Distance between two lines when the lines perpendicular to CS A' are drawn so as to pass through the ICN and the medial end of CS B' when observed so as to face CS B' |
| Lateral condyle to middle width | LCMW | Distance between two lines when lines perpendicular to CS A' are drawn so as to pass through the ICN and the lateral end of CS C' when observed so as to face CS C' |
| Middle-lateral outer angle | MLO-angle | Angle between the straight line that passes through the lateral end of CS C' at the height of CS A' and the lateral end of CS C' at the height of the lateral epicondyle and the straight line perpendicular to CS A' when observed so as to face CS C' |
| Front protrusion length | FPL | Distance between two lines when two straight lines parallel to the MA are drawn so as to pass through the point perpendicu- lar to CS D', which is formed with a cross section that is paral- lel to SEA and perpendicular to CS A', which passes through the anterior end of the intercondylar fossa surface of CS A', from the ICN and the upper end of CS D |
| Coronal-section outer angle | CSO-angle | Angle formed by the straight line parallel to the MA and the straight-line EF, where point E is the lateral end of CS D' and point F is the point where the curvature of the outer edge of CS D' changes from convex to concave |
| Radiation of the curvature of the lateral anterior excision contour | RLAC | Radius of curvature at the midpoint between point F and the upper end of CS D' |
| Lateral anterior excision contour width | LAEC | Distance between two lines when straight lines parallel to the MA are drawn on CS D' so as to pass through point E and the ICN |
| Medial anterior excision contour width | MAEC | Distance between two lines when straight lines parallel to the MA are drawn on CS D' so as to pass through the medial end of CS D' and the ICN |
| Anterior excision middle-lateral length | AEML | Length of the line segment perpendicular to CS D' from the front end of the lateral condyle |
| Anterior excision middle-medial length | AEMM | Length of the line segment perpendicular to CS D' from the front end of the medial condyle |
| Patella coronal-section length | PCS | Length of the line segment connecting the point perpendicular to CS D' from the point at the rear end of the margin connect- ing the front end of the medial condyle and that of the lateral condyle |

Table 1 (continued)

| Magazina | Abbrowietien | Definition |
|---|--------------|---|
| Measurement | Abbreviation | Delinition |
| Radiation of curvature of the lateral distal condyle | RLDC | Radius of curvature at the point where the straight line connect- ing the center of the femoral head and the lateral epicondyle intersects the base of the lateral epicondyle when the femur is observed from the lateral side |
| Radiation of curvature of the lateral posterior condyle | RLPC | Radius of curvature at the midpoint of side GH, where point G, which is orthogonal to CS A', is the intersection of the edge of the shadow of the lateral condyle projected so as to be perpen- dicular to plane γ (which is the plane in contact with the lateral epicondyle and orthogonal to CS A') and CS A'; point H is the intersection of a straight line from point G that is orthogonal to CS A' and the upper edge of the shadow |
| Radiation of curvature of the medial distal condyle | RMDC | Radius of curvature at the point where the straight line connect- ing the center of the femoral head and the medial epicondyle intersects the base of the medial epicondyle when the femur is observed from the medial side |
| Radiation of curvature of the medial posterior condyle | RMPC | Radius of curvature at the midpoint of side IJ, where point I, which is orthogonal to CS A', is the intersection of the edge of the shadow of the lateral condyle projected so as to be perpen- dicular to plane δ (which is the plane in contact with the lateral epicondyle and orthogonal to CS A') and CS A'; point J is the upper edge of the shadow |
| Epicondyle axis angle | CEA-angle | Angle formed by a straight line connecting the lateral and medial epicondyles and a straight line passing through the posterior ends of the medial and lateral epicondyles |
| C-lateral anterior-posterior length | C-LAP | Distance between two lines when lines parallel to the SEA are drawn on the anterior and posterior ends of the lateral condyle on CS A' |
| C-medial anterior-posterior length | C-MAP | Distance between two lines when lines parallel to SEA are drawn on the anterior and posterior ends of the medial condyle on CS A' |

ICN intercondylar notch, which is located at the posterior 1/4 point on the midline of the recess between the medial and lateral condyles on the bottom surface of the lower end of the femur, *MA* mechanical axis, which is the axis passing through the center of the femoral head and ICN [29], *SEA* surgical epicondyle axis, which is the axis passing through the medial epicondyle process groove and the lateral epicondyle process [29, 70, 71]

in Table 3. Group 1 included measurements with rTEM values < 1.5% for intraobserver error and < 2.0% for interobserver error on both the right and left sides. Group 2 included the other measurements whose rTEM values for intraobserver or interobserver errors were larger than the acceptable range. Group 1 comprised five measurements: maximum length of the femur (MLF), lateral anterior–posterior length (LAP), cross-section medial–lateral width (C-ML), C-lateral anterior–posterior length (C-LAP), and C-medial anterior–posterior length (C-MAP), for which *R* values were > 0.9. Group 2 was classified into groups 2–1 and 2–2 according to measurement type. Group 2–1 included measurements for angles and curvature radii, and group 2–2 included measurements for length.

The descriptive statistics for age, AS, and five group 1 measurements are presented in Table 4. Age, AS, MLF, LAP, C-LAP and C-MAP followed a normal distribution, while only C-ML did not follow a normal distribution. There was no significant difference in mean age between the sexes (P=0.482).

The mean values of AS and of each measurement were significantly greater in men than in women (C-ML, P<0.01; AS, MLF, LAP, C-LAP, and C-MAP, P<0.001).

Table 5 describes the result of the single linear regression analysis for estimating AS using five group 1 measurements for all cadavers, regardless of sex. Tables 6 and 7 show the results for males and females, respectively. Significant positive correlations were observed between the AS and each measurement. MLF had the strongest correlation and the lowest SEE for all cadavers, while LAP had the second strongest correlation and lowest SEE. Figures 3, 4, and 5 show the residual plots for the five measurements.

Discussion

In this study, we obtained stature estimation formulae based on a 3D model reconstructed from CT images using semiautomatic measurement software. This is the first report that

| Grou | р | Measurements |
|------|-----|--|
| 1 | | MLF, LAP, C-ML, C-LAP, C-MAP |
| 2 | 2–1 | VA, LA, PCA-angle, LDA-angle, MDA- angle, JL-angle, MLO-angle, CSO-angle, CEA-angle, MDAC, RLAC, RLDC, RLPC, RMDC, RMPC |
| | 2–2 | LRA, MRA, C-P-LAP, C-P-MAP, C-LML, C-MML, P-LAP, P-MAP, MSI, LSI, MCW, LCW, MCMW, LCMW, FPL, LAEC, MAEC, AEML, AEMM, PCS, MAP |

Group 1: measurements with rTEM values <1.5% intraobserver error and <2.0% interobserver error; group 2: measurements with rTEM values \geq 1.5% intraobserver error or \geq 2.0% interobserver error; group 2–1: measurements for angles and radius of curvature; group 2–2: measurements for length.

MLF maximum length of the femur, *LAP* lateral anterior–posterior length, *C-ML* cross-section medial–lateral width, *C-LAP* C-lateral anterior–posterior length, *C-MAP* C-medial anterior–posterior length, *MLF* maximum length of the femur, *AEML* anterior excision middlelateral length, *AEMM* anterior excision middle-medial length, *PCS* patella coronal-section length, *MAEC* medial anterior excision contour width, *RLAC* radiation of the curvature of the lateral anterior excision contour, *LAEC* lateral anterior excision contour width, *RLPC* radiation of curvature of the lateral posterior condyle, *RMPC* radiation of curvature of the medial posterior condyle, *CEA* epicondyle axis angle, *LAP* lateral anterior–posterior length, *C-ML* cross-section medial–lateral width, *C-LAP* C-lateral anterior–posterior length, *C-MAP* C-medial anterior–posterior length.

obtained stature estimation formulae from measurements in 3D CT-reconstructed images using semi-automatic measurement software. In the present study, artificial intelligence (AI) was used for recognition of the femur, extraction of bone surface information, and semi-automatic measurement. AI has been applied in multiple fields of medical research. In the field of diagnostic imaging, it has been shown to reduce not only time for analysis but also interreader variability or false-positive markings [56–59]. Furthermore, AI has been shown to improve adenoma detection rates and reduce examination time in colonoscopy [60], thus reducing waiting time for outpatients [61] and the time interval between CT angiography at a primary stroke center to door-in at a comprehensive stroke center [62]. In the present study, the advantages of using a semi-automatic measurement software were the following: it is a simple measurement method; the time required for measurement is short (approximately 1 min); multiple measurements can be obtained with a single method.

Previously, some stature estimation methods with a single linear regression analysis from MLF measured using radiographic images were reported (Table 8). In two previous reports that presented intraobserver and interobserver errors [40, 44], the rTEM values for intraobserver errors were 0.108–0.277 and those for interobserver errors were 0.192–0.289. In this report, the rTEM values for intraobserver errors were 0.034–0.035 and those for interobserver errors were 0.018–0.019, which were lower than in these two reports. It is possible that these errors were reduced using semi-automatic measurement software.

Compared with previous reports [37, 40, 42, 44] of Japanese cadavers, the results of R^2 and SEE in this study were either better or at least not inferior; therefore, the stature estimation formulae determined in this study could be useful in forensic medical practice. Compared with previous reports providing stature estimations using CT images of Japanese femurs [40, 42, 44], the present study observed the lowest SEE in males, whereas the SEE in females was the second lowest after Chiba et al. [44], and the difference was < 0.2 cm. In their report, MLF was manually measured by reproducing the conventional anthropological measurement method using a CT arbitrary cross-section reconstruction image. Although it may be highly applicable to conventional bone measurements, their measurement method is complicated and time consuming, taking approximately 140 s for measuring MLF, and approximately 440 s for measuring the 5 measurements needed for single side written in the research [44]. In contrast, the semi-automatic measurement method examined in this study is much simpler and faster. It took approximately 40 s from manual marking to displaying 41 measurements, and approximately 280 s from launching this application to displaying all the results. This time period includes measurements of both sides of the femur and includes the time required for 3D model reconstruction. Since the semi-automatic measurement method reduced the measurement error and shortened the measurement time, it is expected that if a fully automatic measuring method is developed, it will be possible to measure with smaller errors and shorter measurement time than the results of this study currently show.

Hasegawa et al. [37] showed lower SEE values in females than those observed in this study (difference, > 0.3 cm), and their report showed the best results in terms of SEE in Japanese subjects, as shown in Table 8 [37, 40, 42, 44]. However, the SEE in males was slightly higher than that observed in males in this study. In addition, the difference in SEE between males and females was 0.74 and 0.83, which was greater than difference in this study (0.003 and 0.072). Hasegawa et al. [37] provided stature estimation formulae using an X-ray photograph of a living human. The difference between this report and theirs might be because their patients were alive, the radiation imaging device was different, and the number of female samples was higher than that of the male samples in their study.

Comparison of the present study with those of Zhang et al. [63] and Lee et al. [39] is complicated because the subjects are different, but our results were superior to those of Zhang et al. [63] and slightly inferior to those of Lee Table 3 TEM, rTEM, and R values for each measurement of both the right and 1 left femurs (n = 20)

| TEM (mm) rTEM (%) R TEM (mm) rTEM (%) R Right MLF 0.14332 0.03506 0.99997 0.00662 0.01000 0.99999 Right VA 0.15572 3.19926 0.98174 0.38923 7.63945 0.89849 Left VA 0.15083 3.13741 0.98725 0.241135 4.90799 0.077020 Right LA 0.3024 10.89524 0.93475 0.56613 23.78686 0.77883 Left LA 0.29917 10.78074 0.92963 0.667704 26.27887 0.77118 Right LA 0.20173 0.41746 0.99475 0.37550 0.968901 Lc3232 2.08738 0.86675 Left LAP 0.17103 0.27458 0.99775 0.54658 0.87376 0.58969 0.98901 L2012 2.03052 0.98897 Left MAP 0.5059 9.00008 0.97716 1.22913 2.03052 0.05887 0.21673 Left P.MAP 2.03252 0.76741 2.02727 9.9775 0.05897 | | Intraobserver error | | | Interobserver error | | |
|--|-----------------|---------------------|-----------|---------|---------------------|-----------|----------|
| Right MLF 0.14832 0.03506 0.99997 0.07746 0.01831 0.99999 Right VA 0.15572 3.19926 0.98174 0.38923 7.63945 0.89849 Left VA 0.15083 3.13741 0.98725 0.24135 4.90799 0.97020 Right LA 0.31024 10.89524 0.93475 0.56613 23.78686 0.77883 Left LA 0.2917 10.78074 0.92963 0.60704 26.27887 0.77151 Right LAP 0.17103 0.27458 0.99775 0.54658 0.87352 0.997751 Left LAP 0.17103 0.27458 0.99775 0.54658 0.87352 0.98775 Right MAP 0.70054 1.14443 0.9619 1.22913 2.03052 0.88977 Right PAAP 0.91228 3.84562 0.76038 2.20777 9.97975 0.08897 Right PAAP 1.95371 6.67366 0.45896 5.32863 21.07217 -0.45641 Left PAAP 2.09249 7.14159 <th></th> <th>TEM (mm)</th> <th>rTEM (%)</th> <th>R</th> <th>TEM (mm)</th> <th>rTEM (%)</th> <th>R</th> | | TEM (mm) | rTEM (%) | R | TEM (mm) | rTEM (%) | R |
| Left MLF 0.14318 0.03374 0.99997 0.08062 0.01900 0.99999 Right VA 0.15572 3.19926 0.98174 0.38923 7.63945 0.99999 Right LA 0.31024 10.89524 0.93475 0.26113 24.07980 0.97020 Right LA 0.29917 10.78074 0.92963 0.60704 26.27887 0.77118 Right LAP 0.26173 0.41746 0.99475 0.37550 0.59669 0.98901 Left LAP 0.17103 0.27458 0.99775 0.54658 0.87352 0.97751 Right MAP 0.70054 1.14443 0.96109 1.26323 2.08738 0.86675 Left MAP 0.91228 3.84562 0.76938 2.20777 9.97975 0.88897 Right PLAP 0.91228 3.84562 0.76938 2.20777 9.97975 0.88897 Left PLAP 0.91228 3.84562 0.76938 2.20777 9.97975 0.88897 Right PLAP 0.91228 3.84562 0.76938 2.20777 9.97977 0.078897 Right PLAP 0.91228 3.84562 0.76938 2.20777 9.97977 0.508897 Right PLAP 0.91228 3.84562 0.76938 2.20777 9.97977 0.508897 Right PLAP 0.91228 1.94651 0.98780 0.24495 3.25514 0.96701 Left PMAP 1.95371 6.67366 0.45896 5.32863 21.107217 -0.45641 Left PMAP 2.09249 7.14159 0.47266 5.63392 22.1807 -0.51700 Right RA 0.17832 1.241738 0.97740 0.15572 2.17416 0.988023 Right MRA 0.18841 1.77498 0.97750 0.20797 1.97828 0.96717 Left CP-LAP 0.98729 5.29168 0.77641 2.29042 13.51676 0.19975 Left CP-LAP 0.98729 5.34785 0.73812 2.03384 12.60310 0.09859 Right CP-MAP 2.01041 7.85700 0.38403 5.61095 26.22588 -0.55940 Left CP-MAP 2.01041 7.85700 0.38403 5.61095 26.22588 -0.55940 Left CP-MAP 2.01041 7.85700 0.38403 5.61095 26.22588 -0.55940 Left CA-MLP 2.20528 8.53518 0.49377 5.79055 2.661711 -0.51468 Right CP-MAP 2.01041 7.85700 0.38403 5.61095 2.62258 -0.55940 Right CP-MAP 2.01041 7.85700 0.38403 5.61095 2.62258 -0.55940 Right C-ML 0.8265 2.31696 0.93975 1.45301 4.29536 0.79284 Right C-ML 0.8265 2.31696 0.93975 1.45301 4.24953 0.59239 0.99375 Left C-ML 0.8265 3.31096 0.93975 1.45301 4.24953 0.52390 0.99375 Left C-ML 0.82866 1.14514 0.97573 0.40988 0.56833 0.99940 Left C-ML 0.82866 1.36712 0.78414 4.90677 3.404988 0.56833 0.99940 Left C-ML 0.82866 1.36712 0.78414 4.90673 3.90621 0.26475 Right MDA-angle 2.23561 3.392389 0.79549 4.46789 2.90873 0.3788 Right MDA-angle 2.23561 3.2 | Right MLF | 0.14832 | 0.03506 | 0.99997 | 0.07746 | 0.01831 | 0.99999 |
| Right VA 0.15572 3.19926 0.98174 0.38923 7.63945 0.89849 Left VA 0.15083 3.13741 0.98725 0.24135 4.90799 0.977080 Right LA 0.20121 10.78074 0.99475 0.56613 23.78686 0.77883 Left LA 0.29171 10.78074 0.99475 0.37550 0.59669 0.98901 Left LAP 0.70154 1.14443 0.96109 1.26323 2.08738 0.86675 Left MAP 0.91228 3.84562 0.76381 2.20777 9.97975 0.08897 Right PAAP 0.91228 3.84562 0.76210 1.99744 9.02898 0.21163 Right PAAP 1.93571 6.67366 0.45896 5.32863 2.10777 -0.51700 Right IRA 0.14822 1.94651 0.98780 0.24495 3.2514 0.96701 Left PAA 0.17321 2.41738 0.97740 0.15722 2.17416 0.98029 Right CAA 0.17321 2.41738 | Left MLF | 0.14318 | 0.03374 | 0.99997 | 0.08062 | 0.01900 | 0.99999 |
| Left VA 0.15083 3.13741 0.98725 0.24135 4.90799 0.97020 Right LA 0.31024 10.89524 0.93475 0.56613 23.78686 0.77883 Left LA 0.29917 10.78074 0.92963 0.60704 26.27887 0.77118 Right LAP 0.26173 0.41746 0.99475 0.37550 0.59669 0.98901 Left LAP 0.17103 0.27458 0.99775 0.54658 0.87352 0.97751 Right PLAP 0.91228 3.84562 0.76938 2.20777 9.97975 0.08897 Left PLAP 0.96099 4.09629 0.76210 1.99744 9.02898 0.21163 Right PAAP 1.95371 6.67366 0.47866 5.63326 21.07217 -0.51700 Right RA 0.14832 1.94651 0.98780 0.24495 3.25514 0.96011 Left PAAP 2.09249 7.14159 0.47266 5.63326 21.07217 -0.51608 Right RA 0.17832 2.41738 </td <td>Right VA</td> <td>0.15572</td> <td>3.19926</td> <td>0.98174</td> <td>0.38923</td> <td>7.63945</td> <td>0.89849</td> | Right VA | 0.15572 | 3.19926 | 0.98174 | 0.38923 | 7.63945 | 0.89849 |
| Right LA 0.31024 10.89524 0.93475 0.56613 23.78686 0.77883 Left LA 0.2917 10.78074 0.92963 0.60704 26.27887 0.77118 Right LAP 0.2173 0.41746 0.99975 0.54658 0.87352 0.97751 Right PLAP 0.17103 0.27458 0.99775 0.54658 0.87352 0.97751 Right PLAP 0.91094 1.14443 0.96109 1.26323 2.08738 0.86675 Left PLAP 0.96099 4.09629 0.76210 1.99744 9.02898 0.21163 Right PLAP 0.96099 4.09629 0.76210 1.99744 9.02898 0.21163 Right RA 0.14821 1.94651 0.98780 0.24495 3.25514 0.66717 Left LA 0.17321 2.41738 0.97740 0.15572 2.17416 0.98029 Right RA 0.18841 1.77498 0.97750 0.23348 2.42851 0.96747 Left HRA 0.22694 2.13086 | Left VA | 0.15083 | 3.13741 | 0.98725 | 0.24135 | 4.90799 | 0.97020 |
| Leit LA 0.29917 10.78074 0.92963 0.60704 26.27887 0.77118 Right LAP 0.2173 0.41746 0.99475 0.37550 0.59669 0.98901 Left LAP 0.17103 0.27458 0.99775 0.54658 0.87352 0.97751 Right MAP 0.70054 1.14443 0.96109 1.26323 2.03052 0.89877 Right PLAP 0.91228 3.84562 0.76938 2.20777 9.97975 0.08897 Left P.AP 0.96099 4.09629 0.76210 1.99744 9.02898 0.21163 Right P.AP 1.95371 6.67366 0.45896 5.32863 21.0717 -0.45641 Left P.MAP 1.95371 6.67366 0.97850 0.22495 3.25514 0.96217 Left LRA 0.17321 2.41738 0.97750 0.25348 2.4281 0.96217 Left LRA 0.17545 5.34785 0.77641 2.20424 1.351676 0.99872 Left C-P.LAP 0.97554 5.34785< | Right LA | 0.31024 | 10.89524 | 0.93475 | 0.56613 | 23.78686 | 0.77883 |
| Right LAP 0.26173 0.41746 0.99475 0.37550 0.59669 0.99801 Left LAP 0.17103 0.27458 0.99775 0.54658 0.87352 0.97751 Right MAP 0.50159 0.90008 0.97916 1.22913 2.00352 0.89897 Right P-LAP 0.91228 3.84562 0.76938 2.20777 9.97975 0.08897 Left P-LAP 0.96099 4.09629 0.76210 1.99744 9.02898 0.21163 Right P-MAP 1.95371 6.67366 0.45896 5.32863 21.07217 -0.45700 Right RA 0.14832 1.94651 0.98780 0.24495 3.25514 0.96701 Left PAMAP 2.09249 7.14159 0.97746 0.51572 2.17416 0.98023 Right RA 0.14832 1.94651 0.98780 0.24495 3.25514 0.96711 Left PAMAP 0.98729 5.29168 0.77641 2.20942 1.351676 0.19975 Left C-PLAP 0.98725 5. | Left LA | 0.29917 | 10.78074 | 0.92963 | 0.60704 | 26.27887 | 0.77118 |
| Left LAP 0.17103 0.27458 0.99775 0.54658 0.87352 0.97751 Right MAP 0.70054 1.14443 0.96109 1.26323 2.08738 0.86675 Left MAP 0.55159 0.90008 0.97916 1.22913 2.03052 0.89877 Right PLAP 0.91228 3.84562 0.76938 2.2077 9.97975 0.08887 Right P-MAP 1.95371 6.67366 0.45896 5.32863 21.07217 -0.45641 Left P-MAP 2.09249 7.14159 0.47266 5.63392 22.18077 -0.51700 Right RA 0.1482 1.94651 0.98780 0.24495 3.25514 0.96217 Left LRA 0.1721 2.41738 0.97750 0.20377 1.97828 0.97478 Right RA 0.18841 1.77498 0.97150 0.20344 12.06310 0.09859 Right C-P-LAP 0.97545 5.34785 0.73812 2.03384 12.06310 0.09859 Right C-P-MAP 2.01041 7 | Right LAP | 0.26173 | 0.41746 | 0.99475 | 0.37550 | 0.59669 | 0.98901 |
| Right MAP 0.70054 1.14443 0.96109 1.26323 2.08738 0.86675 Left MAP 0.55159 0.90008 0.97916 1.22913 2.03052 0.89877 Right P-LAP 0.91228 3.84562 0.76938 2.20777 9.97975 0.08897 Right P-MAP 1.95371 6.67366 0.45896 5.32863 21.07217 -0.45641 Left P-MAP 2.09249 7.14159 0.47266 5.63392 22.18077 -0.51700 Right LRA 0.14332 1.94651 0.98780 0.24495 3.25514 0.96217 Left HRA 0.17321 2.41738 0.97740 0.15572 2.17416 0.98023 Right CP-LAP 0.98729 5.29168 0.77641 2.20424 13.51676 0.19975 Left CP-LAP 0.97545 5.34785 0.73812 2.03384 12.06310 0.09859 Left C-P-MAP 2.01041 7.85700 0.38403 5.61952 2.61711 -0.51468 Right CA-angle 2.31571 | Left LAP | 0.17103 | 0.27458 | 0.99775 | 0.54658 | 0.87352 | 0.97751 |
| Left MAP 0.55159 0.90008 0.97916 1.22913 2.03052 0.89877 Right P-LAP 0.91228 3.84562 0.76938 2.20777 9.97975 0.08897 Left P-LAP 0.96099 4.09629 0.76210 1.99744 9.02898 0.21163 Right P-MAP 1.95371 6.67366 0.45896 5.32863 21.07217 -0.45641 Left P-MAP 2.09249 7.14159 0.47266 5.63392 22.18077 -0.51700 Right RA 0.14832 1.94651 0.98780 0.24495 3.25514 0.96701 Left LRA 0.17321 2.41738 0.97740 0.15572 2.17416 0.98023 Right CP-LAP 0.98729 5.29168 0.77641 2.20421 13.51676 0.19975 Left CP-LAP 0.98729 5.29168 0.77641 2.20422 13.51676 0.19975 Left C-P-LAP 0.97545 5.34785 0.73812 2.03384 12.06310 0.088597 Left C-A-angle 2.51501 | Right MAP | 0.70054 | 1.14443 | 0.96109 | 1.26323 | 2.08738 | 0.86675 |
| Right P-LAP 0.91228 3.84562 0.76938 2.20777 9.97975 0.08897 Left P-LAP 0.96099 4.09629 0.76210 1.99744 9.02898 0.21163 Right P-MAP 1.95371 6.67366 0.45896 5.32863 21.07217 -0.45641 Left P-MAP 2.09249 7.14159 0.47266 5.63392 22.18077 -0.51700 Left RA 0.14332 1.94651 0.98780 0.24495 3.25514 0.96701 Left LRA 0.17321 2.41738 0.97740 0.15572 2.17416 0.98023 Right RA 0.18841 1.77498 0.97952 0.23384 1.206310 0.90859 Left C-HAP 0.97545 5.34785 0.73812 2.03384 12.06310 0.90859 Right C-P-MAP 2.01041 7.85700 0.38403 5.61095 2.61711 -0.51468 Left C-P-MAP 2.0528 8.53518 0.49375 1.45301 4.29370 -0.28593 Left C-LML 0.79152 | Left MAP | 0.55159 | 0.90008 | 0.97916 | 1.22913 | 2.03052 | 0.89877 |
| Left P-LAP 0.96099 4.09629 0.76210 1.97744 9.02898 0.21163 Right P-MAP 1.95371 6.67366 0.45896 5.32863 21.07217 -0.45641 Left P-MAP 2.09249 7.14159 0.47266 5.63392 22.18077 -0.51700 Right LRA 0.14832 1.94651 0.98780 0.24495 3.25514 0.96023 Right CA 0.17211 2.41738 0.97740 0.15572 2.17416 0.98023 Right CP-LAP 0.98729 5.29168 0.77641 2.20421 13.51676 0.19975 Left CP-MAP 2.01041 7.85700 0.34033 5.61095 2.661711 -0.51468 Right CP-MAP 2.01041 7.85700 0.34403 5.61095 2.661711 -0.51468 Right CA-angle 2.51501 31.90618 0.49377 5.79055 2.661711 -0.51468 Right C-ML 0.79152 2.31743 0.99241 0.90375 1.45301 4.29536 0.79284 Right C-M | Right P-LAP | 0.91228 | 3.84562 | 0.76938 | 2.20777 | 9.97975 | 0.08897 |
| Right P-MAP 1.95371 6.67366 0.45896 5.32863 21.07217 -0.45641 Left P-MAP 2.09249 7.14159 0.47266 5.63392 22.18077 -0.51700 Right LRA 0.14322 1.94651 0.98780 0.24495 3.25514 0.96701 Left LRA 0.17321 2.41738 0.97740 0.15572 2.17416 0.98023 Right MRA 0.18841 1.77498 0.97952 0.23348 2.42851 0.96217 Left MRA 0.22694 2.13086 0.97150 0.20797 1.97828 0.97478 Right C-P-LAP 0.97545 5.34785 0.73812 2.03384 12.06310 0.09859 Left C-P-MAP 2.00228 8.5318 0.43976 5.05962 112.74920 -0.28593 Left C-MAP 2.05272 28.03717 0.10174 5.40562 114.2340 -0.48830 Right C-LML 0.79152 2.31743 0.92812 0.98944 2.90373 0.88707 Left C-MML 0.84020 2.40922 0.07673 1.60008 4.47543 0.69924 | Left P-LAP | 0.96099 | 4.09629 | 0.76210 | 1.99744 | 9.02898 | 0.21163 |
| Left P-MAP 2.09249 7.14159 0.47266 5.63392 22.18077 -0.51700 Right LRA 0.14832 1.94651 0.98780 0.24495 3.25514 0.96701 Left LRA 0.17321 2.41738 0.97740 0.15572 2.17416 0.98023 Right MRA 0.18841 1.77498 0.97952 0.25348 2.42851 0.96217 Left MRA 0.2694 2.13086 0.97150 0.20797 1.97828 0.97478 Right C-P-LAP 0.97545 5.34785 0.73812 2.03384 12.06310 0.09859 Right C-P-MAP 2.01041 7.85700 0.38403 5.61095 26.22858 -0.55040 Left C-P-MAP 2.0528 8.53518 0.49377 5.70055 26.61711 -0.51468 Right PCA-angle 2.3572 28.03717 0.10174 5.40562 112.74920 -0.28593 Left C-LML 0.79152 2.31743 0.429875 7.01748 0.69924 Left C-LML 0.80265 2.31696 </td <td>Right P-MAP</td> <td>1.95371</td> <td>6.67366</td> <td>0.45896</td> <td>5.32863</td> <td>21.07217</td> <td>-0.45641</td> | Right P-MAP | 1.95371 | 6.67366 | 0.45896 | 5.32863 | 21.07217 | -0.45641 |
| Right LRA 0.14832 1.94651 0.98780 0.24495 3.25514 0.96701 Left LRA 0.17321 2.41738 0.97740 0.15572 2.17416 0.98023 Right MRA 0.18841 1.77498 0.97952 0.25348 2.42851 0.96217 Left MRA 0.26694 2.13086 0.97150 0.20797 1.97828 0.97478 Right CP-LAP 0.98729 5.29168 0.77641 2.29042 13.51676 0.19975 Left C-P-LAP 0.97545 5.34785 0.73812 2.03384 12.06310 0.09859 Right CA-angle 2.51501 31.90618 0.49377 5.79055 26.61711 -0.51468 Right CA-angle 2.35372 28.03717 0.10174 5.40562 114.2340 -0.48830 Right C-MIL 0.79152 2.31743 0.49814 2.90373 0.48830 Right C-MIL 0.79152 2.31696 0.93975 1.45301 4.29536 0.79244 Right C-ML 0.82826 1.314514< | Left P-MAP | 2.09249 | 7.14159 | 0.47266 | 5.63392 | 22.18077 | -0.51700 |
| Left LRA 0.17321 2.41738 0.97740 0.15572 2.17416 0.98023 Right MRA 0.18841 1.77498 0.97952 0.25348 2.42851 0.96217 Left MRA 0.22694 2.13086 0.97150 0.20797 1.97828 0.97478 Right C-P-LAP 0.98729 5.29168 0.77641 2.29042 13.1676 0.09859 Right C-P-LAP 0.97545 5.34785 0.73812 2.03384 12.06310 0.09859 Right C-P-MAP 2.01041 7.85700 0.38403 5.61095 2.661711 -0.51468 Right CA-angle 2.51501 31.90618 0.45966 5.05962 112.74920 -0.28593 Left C-MAP 2.20528 8.3518 0.92812 0.98944 2.90373 0.88707 Left C-ML 0.79152 2.31743 0.92812 0.98944 2.90373 0.88707 Left C-ML 0.804202 2.40992 0.90767 1.60008 4.47543 0.69924 Left C-ML 0.82886 | Right LRA | 0.14832 | 1.94651 | 0.98780 | 0.24495 | 3.25514 | 0.96701 |
| Right MRA 0.18841 1.77498 0.97952 0.25348 2.42851 0.96217 Left MRA 0.22694 2.13086 0.97150 0.20797 1.97828 0.97478 Right C.P-LAP 0.97545 5.34785 0.73812 2.03384 12.06310 0.09859 Right C.P-MAP 2.01041 7.85700 0.38403 5.61095 26.22858 -0.55040 Left C.P-MAP 2.01501 31.90618 0.49367 5.79055 26.61711 -0.51468 Right PCA-angle 2.35372 28.03717 0.10174 5.40562 114.22340 -0.48830 Left C-LML 0.79152 2.31743 0.92812 0.98944 2.90373 0.88707 Left C-LML 0.80265 2.31696 0.93975 1.45301 4.29536 0.79284 Right C-ML 0.8265 13.4608 0.80431 2.49875 7.01748 0.46790 Right C-ML 0.82886 1.14514 0.97573 0.40988 0.52359 0.99540 Right C-ML 0.5174 | Left LRA | 0.17321 | 2.41738 | 0.97740 | 0.15572 | 2.17416 | 0.98023 |
| Left MRA 0.22694 2.13086 0.97150 0.20797 1.97828 0.97478 Right C-P-LAP 0.98729 5.29168 0.77641 2.29042 13.51676 0.19975 Left C-P-LAP 0.97545 5.34785 0.73812 2.03384 12.06310 0.09859 Right C-P-MAP 2.01041 7.85700 0.38403 5.61095 26.22858 -0.55040 Left C-P-MAP 2.0528 8.53518 0.49377 5.79055 26.61711 -0.28593 Left PCA-angle 2.35372 28.03717 0.10174 5.40562 114.22340 -0.48830 Right C-LML 0.80265 2.31696 0.93975 1.45301 4.29536 0.79284 Right C-ML 0.8265 2.31696 0.93975 1.45301 4.29536 0.79284 Right C-ML 0.8265 2.31696 0.93975 1.45301 4.29536 0.79284 Right C-ML 0.82686 1.14514 0.97573 0.40988 0.56833 0.99540 Right C-ML 0.517 | Right MRA | 0.18841 | 1.77498 | 0.97952 | 0.25348 | 2.42851 | 0.96217 |
| Right C-P-LAP 0.98729 5.29168 0.77641 2.29042 13.51676 0.19975 Left C-P-LAP 0.97545 5.34785 0.73812 2.03384 12.06310 0.09859 Right C-P-MAP 2.01041 7.85700 0.38403 5.61095 26.22858 -0.55040 Left C-P-MAP 2.20528 8.53518 0.49377 5.79055 26.61711 -0.51468 Right CA-angle 2.51501 31.90618 0.45966 5.05962 112.74920 -0.28593 Left C-LML 0.79152 2.31743 0.92812 0.98944 2.90373 0.88707 Left C-LML 0.80265 2.31696 0.93975 1.45301 4.29536 0.79284 Right C-ML 0.84202 2.40922 0.90767 1.60008 4.47543 0.69924 Left C-ML 0.51745 0.71815 0.99089 0.37683 0.52359 0.99540 Right LDA-angle 2.13395 12.09209 0.81491 5.74861 41.77768 0.16193 Right MDA-angle | Left MRA | 0.22694 | 2.13086 | 0.97150 | 0.20797 | 1.97828 | 0.97478 |
| Left C-P-LAP 0.97545 5.34785 0.73812 2.03384 12.06310 0.09859 Right C-P-MAP 2.01041 7.85700 0.38403 5.61095 26.22858 -0.55040 Left C-P-MAP 2.20528 8.53518 0.49377 5.79055 26.61711 -0.51468 Right PCA-angle 2.51501 31.90618 0.45966 5.05962 112.74920 -0.28593 Left PCA-angle 2.35372 28.03717 0.10174 5.40562 114.22340 -0.48830 Right C-LML 0.79152 2.31743 0.92812 0.98944 2.90373 0.88707 Left C-LML 0.80265 2.31696 0.93975 1.45301 4.29536 0.79284 Right C-LML 0.80265 2.31696 0.93975 1.45301 4.29536 0.79284 Right C-LML 0.80265 2.31696 0.93975 1.45301 4.29536 0.79284 Right C-LML 0.82868 1.14514 0.97573 0.40988 0.56833 0.99405 Left C-ML 0.82886 1.14514 0.97573 0.40988 0.56833 0.99405 Left C-ML 0.51745 0.71815 0.99089 0.37683 0.52359 0.99540 Right LDA-angle 2.33065 13.67012 0.78414 4.90607 34.90621 0.26475 Left LDA-angle 2.13395 12.09209 0.81491 5.74861 41.77768 0.16193 Right MDA-angle 2.28561 13.92389 0.79549 4.06789 29.08234 0.33301 Left MDA-angle 2.28561 13.92389 0.79549 4.06789 29.08234 0.33301 Left MDA-angle 2.23523 13.09257 0.76538 5.22705 35.32981 0.10575 Right MDA 217.05863 202.73064 0.27902 48.28600 73.31891 0.01449 Left MDAC 11.21474 17.03851 0.84829 17.25977 27.19572 0.46401 Right JL-angle 0.20125 4.66928 0.99325 0.24850 5.92714 0.99014 Left JL-angle 0.20125 4.66928 0.99324 0.51210 2.00884 0.98147 Left LSI 0.38633 1.48745 0.98837 0.37081 1.43198 0.98978 Right MSI 1.06243 4.03389 0.83388 2.08273 8.26233 0.55417 Left MSI 0.62510 2.38702 0.93223 2.16038 8.67362 0.53598 Right MCW 1.27112 4.73196 0.75036 2.45260 9.67782 0.44488 Left MCW 0.88204 3.28936 0.86778 | Right C-P-LAP | 0.98729 | 5.29168 | 0.77641 | 2.29042 | 13.51676 | 0.19975 |
| Right C-PMAP2.010417.857000.384035.6109526.22858-0.55040Left C-P-MAP2.205288.535180.493775.7905526.61711-0.51468Right PCA-angle2.5150131.906180.459665.05962112.74920-0.28593Left PCA-angle2.3537228.037170.101745.40562114.22340-0.48830Right C-LML0.791522.317430.928120.989442.903730.88707Left C-LML0.802652.316960.939751.453014.295360.79284Right C-MIL0.842022.409220.907671.600084.475430.69924Left C-MIL0.828861.145140.975730.409880.568330.99405Left C-ML0.517450.718150.990890.376830.523590.99540Right DA-angle2.3806513.670120.784144.9060734.906210.26475Left MDA-angle2.2352313.092570.765385.2270535.329810.10575Right MDAC217.05863202.730640.2790248.2860073.318910.01449Left MDAC11.2147417.038510.8482917.2597727.195720.46401Right MDAC217.05863202.730640.2790248.2860073.318910.01449Left MDAC11.2147417.038510.8482917.2597727.195720.46401Right MDA1.062434.033890.833882.082738.262330.55417 <td>Left C-P-LAP</td> <td>0.97545</td> <td>5.34785</td> <td>0.73812</td> <td>2.03384</td> <td>12.06310</td> <td>0.09859</td> | Left C-P-LAP | 0.97545 | 5.34785 | 0.73812 | 2.03384 | 12.06310 | 0.09859 |
| Left C-P-MAP2.205288.535180.493775.7905526.61711-0.51468Right PCA-angle2.5150131.906180.459665.05962112.74920-0.28593Left PCA-angle2.3537228.037170.101745.40562114.22340-0.48830Right C-LML0.791522.317430.928120.989442.903730.88707Left C-LML0.802652.316960.939751.453014.295360.79284Right C-ML0.842022.409220.907671.600084.475430.69924Left C-ML0.828861.145140.975730.409880.568330.99405Left C-ML0.517450.718150.990890.376830.523590.99540Right CDA-angle2.3806513.670120.784144.9060734.906210.26475Left MDA-angle2.1339512.092090.814915.7486141.777680.16193Right MDA-angle2.2352313.092570.755385.2270535.329810.10575Right MDAC11.2147417.038510.8482917.2597727.195720.46401Right JL-angle0.201254.669280.993250.248505.927140.99014Left MSI0.625102.387020.932232.160388.673620.53598Right MSI1.062434.033890.833882.082738.262330.55417Left MSI0.278391.096660.993840.512102.008840.98147Lef | Right C-P-MAP | 2.01041 | 7.85700 | 0.38403 | 5.61095 | 26.22858 | -0.55040 |
| Right PCA-angle2.5150131.906180.459665.05962112.74920-0.28593Right PCA-angle2.3537228.037170.101745.40562114.22340-0.48830Right C-LML0.791522.317430.928120.989442.903730.88707Left C-LML0.802652.316960.939751.453014.295360.79284Right C-ML0.842022.409220.907671.600084.475430.69924Left C-ML0.828861.145140.975730.409880.568330.99405Left C-ML0.517450.718150.990890.376830.523590.99540Right LDA-angle2.3806513.670120.784144.9060734.906210.26475Left LDA-angle2.1339512.092090.814915.7486141.777680.16193Right MDA-angle2.2856113.923890.795494.0678929.082340.33301Left MDA-angle2.2352313.092570.765385.2270535.329810.10575Right MDA11.2147417.038510.8482917.2597727.195720.46401Right JL-angle0.201254.669280.993250.248505.927140.99014Left MDAC11.2147417.038510.83882.082738.262330.55417Left MSI0.625102.387020.932232.160388.673620.53598Right MSI1.062434.033890.832882.082738.262330.55417 <td< td=""><td>Left C-P-MAP</td><td>2.20528</td><td>8.53518</td><td>0.49377</td><td>5.79055</td><td>26.61711</td><td>-0.51468</td></td<> | Left C-P-MAP | 2.20528 | 8.53518 | 0.49377 | 5.79055 | 26.61711 | -0.51468 |
| Left PCA-angle2.3537228.037170.101745.40562114.22340-0.48830Right C-LML0.791522.317430.928120.989442.903730.88707Left C-LML0.802652.316960.939751.453014.295360.79284Right C-MML0.842022.409220.907671.600084.475430.69924Left C-MML1.182693.480800.804312.498757.017480.46790Right C-ML0.517450.718150.990890.376830.523590.99540Right LDA-angle2.3806513.670120.784144.9060734.906210.26475Left LDA-angle2.1339512.092090.814915.7486141.777680.16193Right MDA-angle2.2856113.923890.795494.0678929.082340.33301Left MDA-angle2.2352313.092570.765385.2270535.329810.10575Right MDAC217.05863202.730640.2790248.2860073.318910.01449Left MDAC11.2147417.038510.8482917.2597727.195720.46401Right MSI1.062434.033890.833882.082738.262330.55417Left MSI0.625102.387020.932232.160388.673620.53598Right MCW1.271124.731960.750362.452609.677820.44488Left LSI0.386331.487450.988370.370811.431980.98978Right M | Right PCA-angle | 2.51501 | 31,90618 | 0.45966 | 5.05962 | 112.74920 | -0.28593 |
| Right C-LML0.791522.317430.928120.989442.903730.88707Left C-LML0.802652.316960.939751.453014.295360.79284Right C-MML0.842022.409220.907671.600084.475430.69924Left C-MML1.182693.480800.804312.498757.017480.46790Right C-ML0.517450.718150.990890.376830.523590.99540Right LDA-angle2.3806513.670120.784144.9060734.906210.26475Left C-ML0.517450.718150.990890.376830.523590.99540Right MDA-angle2.1339512.092090.814915.7486141.777680.16193Right MDA-angle2.2856113.923890.795494.0678929.082340.33301Left MDA-angle2.2352313.092570.765385.2270535.329810.10575Right MDAC11.2147417.038510.8482917.2597727.195720.46401Right JL-angle0.201254.669280.993250.248505.927140.99014Left JL-angle0.207974.144820.989770.352497.316890.96952Right MSI1.062434.033890.833882.082738.262330.55417Left MSI0.625102.387020.932232.160388.673620.53598Right MCW1.271124.731960.750362.452609.677820.44488Left MCW <td>Left PCA-angle</td> <td>2.35372</td> <td>28.03717</td> <td>0.10174</td> <td>5.40562</td> <td>114.22340</td> <td>-0.48830</td> | Left PCA-angle | 2.35372 | 28.03717 | 0.10174 | 5.40562 | 114.22340 | -0.48830 |
| Left C-LML0.802652.316960.939751.453014.295360.79284Right C-MML0.842022.409220.907671.600084.475430.69924Left C-MML1.182693.480800.804312.498757.017480.46790Right C-ML0.828861.145140.975730.409880.568330.99405Left C-ML0.517450.718150.990890.376830.523590.99540Right LDA-angle2.3806513.670120.784144.9060734.906210.26475Left LDA-angle2.1339512.092090.814915.7486141.777680.16193Right MDA-angle2.2856113.923890.795494.0678929.082340.33301Left MDA-angle2.2352313.092570.765385.2270535.329810.10575Right MDAC11.2147417.038510.8482917.2597727.195720.46401Right JL-angle0.201254.669280.993250.248505.927140.99014Left MDAC11.2147417.038510.8482917.2597727.195720.46401Right MSI1.062434.033890.833882.082738.262330.55417Left MSI0.625102.387020.932232.160388.673620.53598Right MCW1.271124.731960.750362.452609.677820.44488Left LSI0.386331.487450.988370.370811.431980.98978Right MCW< | Right C-LML | 0.79152 | 2.31743 | 0.92812 | 0.98944 | 2.90373 | 0.88707 |
| Right C-MML0.842022.409220.907671.600084.475430.69924Left C-MML1.182693.480800.804312.498757.017480.46790Right C-ML0.828861.145140.975730.409880.568330.99405Left C-ML0.517450.718150.990890.376830.523590.99540Right LDA-angle2.3806513.670120.784144.9060734.906210.26475Left LDA-angle2.1339512.092090.814915.7486141.777680.16193Right MDA-angle2.2856113.923890.795494.0678929.082340.33301Left MDA-angle2.2352313.092570.765385.2270535.329810.10575Right MDAC217.05863202.730640.2790248.2860073.318910.01449Left MDAC11.2147417.038510.8482917.2597727.195720.46401Right JL-angle0.201254.669280.993250.248505.927140.99014Left MDAC11.2147417.038510.833882.082738.262330.55417Left MSI0.625102.387020.932232.160388.673620.53598Right MSI1.062434.033890.833882.082738.262330.55417Left LSI0.386331.487450.988370.370811.431980.98978Right MCW1.271124.731960.750362.452609.677820.44488Left LCW <td>Left C-LML</td> <td>0.80265</td> <td>2.31696</td> <td>0.93975</td> <td>1.45301</td> <td>4.29536</td> <td>0.79284</td> | Left C-LML | 0.80265 | 2.31696 | 0.93975 | 1.45301 | 4.29536 | 0.79284 |
| InteriorInteriorInteriorInteriorInteriorLeft C-MML1.182693.480800.804312.498757.017480.46790Right C-ML0.517450.718150.990890.376830.523590.99405Left C-ML0.517450.718150.990890.376830.523590.99540Right LDA-angle2.1339512.092090.814915.7486141.777680.16193Right MDA-angle2.2856113.923890.795494.0678929.082340.33301Left MDA-angle2.2352313.092570.765385.2270535.329810.10575Right MDAC217.05863202.730640.2790248.2860073.318910.01449Left MDAC11.2147417.038510.8482917.2597727.195720.46401Right JL-angle0.207974.144820.989770.352497.316890.96952Right MSI1.062434.033890.833882.082738.262330.55417Left LSI0.386331.487450.988370.370811.431980.98978Right MCW1.271124.731960.750362.452609.677820.44488Left MCW0.882043.289360.867782.258328.885770.61669Right MCW1.024452.812110.899130.822342.257480.93518Left LCW0.310241.323130.991750.545212.337180.97519Right MCMW1.024452.812110. | Right C-MML | 0.84202 | 2.40922 | 0.90767 | 1.60008 | 4.47543 | 0.69924 |
| Right C-ML0.828861.145140.975730.409880.568330.99405Right C-ML0.517450.718150.990890.376830.523590.99540Right LDA-angle2.3806513.670120.784144.9060734.906210.26475Left LDA-angle2.1339512.092090.814915.7486141.777680.16193Right MDA-angle2.2856113.923890.795494.0678929.082340.33301Left MDA-angle2.2352313.092570.765385.2270535.329810.10575Right MDAC217.05863202.730640.2790248.2860073.318910.01449Left MDAC11.2147417.038510.8482917.2597727.195720.46401Right JL-angle0.201254.669280.993250.248505.927140.99014Left MSI0.625102.387020.932232.160388.673620.53598Right LSI0.378331.487450.988370.370811.431980.98978Right MCW1.271124.731960.750362.452609.677820.44488Left MCW0.882043.289360.867782.258328.885770.61669Right LCW0.310241.323130.991750.545212.337180.97684Left LCW0.310241.323130.991750.545212.337180.97519Right MCMW1.024452.812110.899130.822342.257480.93518 | Left C-MML | 1.18269 | 3.48080 | 0.80431 | 2.49875 | 7.01748 | 0.46790 |
| Left C-ML0.517450.718150.990890.376830.523590.99540Right LDA-angle2.3806513.670120.784144.9060734.906210.26475Left LDA-angle2.1339512.092090.814915.7486141.777680.16193Right MDA-angle2.2856113.923890.795494.0678929.082340.33301Left MDA-angle2.2352313.092570.765385.2270535.329810.10575Right MDAC217.05863202.730640.2790248.2860073.318910.01449Left MDAC11.2147417.038510.8482917.2597727.195720.46401Right JL-angle0.201254.669280.993250.248505.927140.99014Left JL-angle0.207974.144820.989770.352497.316890.96952Right MSI1.062434.033890.833882.082738.262330.55417Left MSI0.625102.387020.932232.160388.673620.53598Right MCW1.271124.731960.750362.452609.677820.44488Left LSI0.386331.487450.988370.370811.431980.98978Right MCW0.275231.190300.992340.499752.167880.97684Left LCW0.310241.323130.991750.545212.337180.97519Right MCMW1.024452.812110.899130.822342.257480.93518Left MCMW | Right C-ML | 0.82886 | 1.14514 | 0.97573 | 0.40988 | 0.56833 | 0.99405 |
| Right LDA-angle2.3806513.670120.784144.9060734.906210.26475Right LDA-angle2.1339512.092090.814915.7486141.777680.16193Right MDA-angle2.2856113.923890.795494.0678929.082340.3301Left MDA-angle2.2352313.092570.765385.2270535.329810.10575Right MDAC217.05863202.730640.2790248.2860073.318910.01449Left MDAC11.2147417.038510.8482917.2597727.195720.46401Right JL-angle0.201254.669280.993250.248505.927140.99014Left JL-angle0.207974.144820.989770.352497.316890.96952Right MSI1.062434.033890.833882.082738.262330.55417Left MSI0.625102.387020.932232.160388.673620.53598Right MCW1.271124.731960.750362.452609.677820.44488Left MCW0.882043.289360.867782.258328.885770.61669Right LCW0.310241.323130.991750.545212.337180.97519Right MCM1.024452.812110.899130.822342.257480.93518Left LCW0.310241.323130.902671.646284.494050.74669 | Left C-ML | 0.51745 | 0.71815 | 0.99089 | 0.37683 | 0.52359 | 0.99540 |
| Left LDA-angle2.1339512.092090.814915.7486141.777680.16193Right MDA-angle2.2856113.923890.795494.0678929.082340.33301Left MDA-angle2.2352313.092570.765385.2270535.329810.10575Right MDAC217.05863202.730640.2790248.2860073.318910.01449Left MDAC11.2147417.038510.8482917.2597727.195720.46401Right JL-angle0.201254.669280.993250.248505.927140.99014Left JL-angle0.207974.144820.989770.352497.316890.96952Right MSI1.062434.033890.833882.082738.262330.55417Left MSI0.625102.387020.932232.160388.673620.53598Right LSI0.278391.096660.993840.512102.008840.98147Left LSI0.386331.487450.988370.370811.431980.98978Right MCW1.271124.731960.750362.452609.677820.44488Left MCW0.882043.289360.867782.258328.885770.61669Right LCW0.310241.323130.991750.545212.337180.97684Left LCW0.310241.323130.991750.545212.337180.97519Right MCMW1.024452.812110.899130.822342.257480.93518Left MCMW0.878 | Right LDA-angle | 2.38065 | 13.67012 | 0.78414 | 4.90607 | 34.90621 | 0.26475 |
| Right MDA-angle2.2856113.923890.795494.0678929.082340.33301Left MDA-angle2.2352313.092570.765385.2270535.329810.10575Right MDAC217.05863202.730640.2790248.2860073.318910.01449Left MDAC11.2147417.038510.8482917.2597727.195720.46401Right JL-angle0.201254.669280.993250.248505.927140.99014Left JL-angle0.207974.144820.989770.352497.316890.96952Right MSI1.062434.033890.833882.082738.262330.55417Left MSI0.625102.387020.932232.160388.673620.53598Right LSI0.278391.096660.993840.512102.008840.98147Left LSI0.386331.487450.988370.370811.431980.98978Right MCW1.271124.731960.750362.452609.677820.44488Left MCW0.882043.289360.867782.258328.885770.61669Right LCW0.310241.323130.991750.545212.337180.97619Right MCMU1.024452.812110.899130.822342.257480.93518Left MCMW0.878782.448360.902671.646284.494050.74669 | Left LDA-angle | 2.13395 | 12.09209 | 0.81491 | 5.74861 | 41.77768 | 0.16193 |
| Left MDA-angle2.2352313.092570.765385.2270535.329810.10575Right MDAC217.05863202.730640.2790248.2860073.318910.01449Left MDAC11.2147417.038510.8482917.2597727.195720.46401Right JL-angle0.201254.669280.993250.248505.927140.99014Left JL-angle0.207974.144820.989770.352497.316890.96952Right MSI1.062434.033890.833882.082738.262330.55417Left MSI0.625102.387020.932232.160388.673620.53598Right LSI0.278391.096660.993840.512102.008840.98147Left LSI0.386331.487450.988370.370811.431980.98978Right MCW1.271124.731960.750362.452609.677820.44488Left MCW0.882043.289360.867782.258328.885770.61669Right LCW0.310241.323130.991750.545212.337180.97519Right MCMW1.024452.812110.899130.822342.257480.93518Left MCMW0.878782.448360.902671.646284.494050.74669 | Right MDA-angle | 2 28561 | 13 92389 | 0 79549 | 4 06789 | 29 08234 | 0.33301 |
| Right MDAC217.05863202.730640.2790248.2860073.318910.01449Left MDAC11.2147417.038510.8482917.2597727.195720.46401Right JL-angle0.201254.669280.993250.248505.927140.99014Left JL-angle0.207974.144820.989770.352497.316890.96952Right MSI1.062434.033890.833882.082738.262330.55417Left MSI0.625102.387020.932232.160388.673620.53598Right LSI0.278391.096660.993840.512102.008840.98147Left LSI0.386331.487450.988370.370811.431980.98978Right MCW1.271124.731960.750362.452609.677820.44488Left MCW0.882043.289360.867782.258328.885770.61669Right LCW0.310241.323130.991750.545212.337180.97519Right MCMW1.024452.812110.899130.822342.257480.93518Left MCMW0.878782.448360.902671.646284.494050.74669 | Left MDA-angle | 2.23523 | 13.09257 | 0.76538 | 5.22705 | 35.32981 | 0.10575 |
| Left MDAC11.2147417.038510.8482917.2597727.195720.46401Right JL-angle0.201254.669280.993250.248505.927140.99014Left JL-angle0.207974.144820.989770.352497.316890.96952Right MSI1.062434.033890.833882.082738.262330.55417Left MSI0.625102.387020.932232.160388.673620.53598Right LSI0.278391.096660.993840.512102.008840.98147Left LSI0.386331.487450.988370.370811.431980.98978Right MCW1.271124.731960.750362.452609.677820.44488Left MCW0.882043.289360.867782.258328.885770.61669Right LCW0.310241.323130.991750.545212.337180.97684Left LCW0.310241.323130.991750.545212.337180.97519Right MCMW1.024452.812110.899130.822342.257480.93518Left MCMW0.878782.448360.902671.646284.494050.74669 | Right MDAC | 217.05863 | 202.73064 | 0.27902 | 48.28600 | 73.31891 | 0.01449 |
| Right JL-angle0.201254.669280.993250.248505.927140.99014Left JL-angle0.207974.144820.989770.352497.316890.96952Right MSI1.062434.033890.833882.082738.262330.55417Left MSI0.625102.387020.932232.160388.673620.53598Right LSI0.278391.096660.993840.512102.008840.98147Left LSI0.386331.487450.988370.370811.431980.98978Right MCW1.271124.731960.750362.452609.677820.44488Left MCW0.882043.289360.867782.258328.885770.61669Right LCW0.310241.323130.991750.545212.337180.97684Left LCW0.310241.323130.991750.545212.337180.97519Right MCMW1.024452.812110.899130.822342.257480.93518Left MCMW0.878782.448360.902671.646284.494050.74669 | Left MDAC | 11.21474 | 17.03851 | 0.84829 | 17.25977 | 27.19572 | 0.46401 |
| Left JL-angle0.207974.144820.989770.352497.316890.96952Right MSI1.062434.033890.833882.082738.262330.55417Left MSI0.625102.387020.932232.160388.673620.53598Right LSI0.278391.096660.993840.512102.008840.98147Left LSI0.386331.487450.988370.370811.431980.98978Right MCW1.271124.731960.750362.452609.677820.44488Left MCW0.882043.289360.867782.258328.885770.61669Right LCW0.275231.190300.992340.499752.167880.97684Left LCW0.310241.323130.991750.545212.337180.97519Right MCMW1.024452.812110.899130.822342.257480.93518Left MCMW0.878782.448360.902671.646284.494050.74669 | Right IL-angle | 0.20125 | 4,66928 | 0.99325 | 0.24850 | 5.92714 | 0.99014 |
| Right MSI1.062434.033890.833882.082738.262330.55417Left MSI0.625102.387020.932232.160388.673620.53598Right LSI0.278391.096660.993840.512102.008840.98147Left LSI0.386331.487450.988370.370811.431980.98978Right MCW1.271124.731960.750362.452609.677820.44488Left MCW0.882043.289360.867782.258328.885770.61669Right LCW0.275231.190300.992340.499752.167880.97684Left LCW0.310241.323130.991750.545212.337180.97519Right MCMW1.024452.812110.899130.822342.257480.93518Left MCMW0.878782.448360.902671.646284.494050.74669 | Left II -angle | 0.20797 | 4.14482 | 0.98977 | 0.35249 | 7.31689 | 0.96952 |
| Left MSI0.625102.387020.932232.160388.673620.53598Right LSI0.278391.096660.993840.512102.008840.98147Left LSI0.386331.487450.988370.370811.431980.98978Right MCW1.271124.731960.750362.452609.677820.44488Left MCW0.882043.289360.867782.258328.885770.61669Right LCW0.275231.190300.992340.499752.167880.97684Left LCW0.310241.323130.991750.545212.337180.97519Right MCMW1.024452.812110.899130.822342.257480.93518Left MCMW0.878782.448360.902671.646284.494050.74669 | Right MSI | 1.06243 | 4.03389 | 0.83388 | 2.08273 | 8.26233 | 0.55417 |
| Right LSI0.278391.096660.993840.512102.008840.98147Left LSI0.386331.487450.988370.370811.431980.98978Right MCW1.271124.731960.750362.452609.677820.44488Left MCW0.882043.289360.867782.258328.885770.61669Right LCW0.275231.190300.992340.499752.167880.97684Left LCW0.310241.323130.991750.545212.337180.97519Right MCMW1.024452.812110.899130.822342.257480.93518Left MCMW0.878782.448360.902671.646284.494050.74669 | Left MSI | 0.62510 | 2.38702 | 0.93223 | 2.16038 | 8.67362 | 0.53598 |
| Left LSI0.386331.487450.988370.370811.431980.98978Right MCW1.271124.731960.750362.452609.677820.44488Left MCW0.882043.289360.867782.258328.885770.61669Right LCW0.275231.190300.992340.499752.167880.97684Left LCW0.310241.323130.991750.545212.337180.97519Right MCMW1.024452.812110.899130.822342.257480.93518Left MCMW0.878782.448360.902671.646284.494050.74669 | Right LSI | 0.27839 | 1.09666 | 0.99384 | 0.51210 | 2.00884 | 0.98147 |
| Right MCW1.271124.731960.750362.452609.677820.44488Left MCW0.882043.289360.867782.258328.885770.61669Right LCW0.275231.190300.992340.499752.167880.97684Left LCW0.310241.323130.991750.545212.337180.97519Right MCMW1.024452.812110.899130.822342.257480.93518Left MCMW0.878782.448360.902671.646284.494050.74669 | Left LSI | 0.38633 | 1 48745 | 0.98837 | 0.37081 | 1 43198 | 0.98978 |
| Left MCW0.882043.289360.867782.258328.885770.61669Right LCW0.275231.190300.992340.499752.167880.97684Left LCW0.310241.323130.991750.545212.337180.97519Right MCMW1.024452.812110.899130.822342.257480.93518Left MCMW0.878782.448360.902671.646284.494050.74669 | Right MCW | 1.27112 | 4,73196 | 0.75036 | 2,45260 | 9.67782 | 0.44488 |
| Right LCW 0.31024 1.32313 0.99175 0.449975 2.16788 0.97684 Left LCW 0.31024 1.32313 0.99175 0.54521 2.33718 0.97519 Right MCMW 1.02445 2.81211 0.89913 0.82234 2.25748 0.93518 Left MCMW 0.87878 2.44836 0.90267 1.64628 4.49405 0.74669 | Left MCW | 0 88204 | 3 28936 | 0.86778 | 2.45200 | 8 88577 | 0.61660 |
| Left LCW 0.31024 1.32313 0.99175 0.54521 2.33718 0.97519 Right MCMW 1.02445 2.81211 0.89913 0.82234 2.25748 0.93518 Left MCMW 0.87878 2.44836 0.90267 1.64628 4.49405 0.74669 | Right LCW | 0.00204 | 1 19030 | 0.99734 | 0 49975 | 2 16788 | 0.97684 |
| Right MCMW1.024452.812110.899130.822342.257480.93518Left MCMW0.878782.448360.902671.646284.494050.74669 | Left LCW | 0.27525 | 1 32313 | 0 99175 | 0.4521 | 2.10700 | 0.97510 |
| Left MCMW 0.87878 2.44836 0.90267 1.64628 4.49405 0.74669 | Right MCMW | 1 02445 | 2.81211 | 0.89913 | 0.87234 | 2.33710 | 0.93518 |
| Lett 10-11 0.07070 2.77050 0.70207 1.07020 7.7705 0.74009 | Left MCMW | 0.87878 | 2.01211 | 0.00010 | 1 64628 | 4 49405 | 0.74660 |
| Right LCMW 0.98362 2.84529 0.88269 1.42241 4.19621 0.79991 | Right LCMW | 0.98362 | 2.84529 | 0.88269 | 1.42241 | 4.19621 | 0.79991 |

Table 3 (continued)

| | Intraobserver error | | | Interobserver error | | | |
|-----------------|---------------------|-------------|----------|---------------------|-------------|----------|--|
| | | | | | D | | |
| | TEM (mm) | r1EM (%) | R | IEM (mm) | r1EM (%) | <i>K</i> | |
| Left LCMW | 1.00735 | 2.85833 | 0.90238 | 2.16991 | 6.39525 | 0.59094 | |
| Right MLO-angle | 0.78962 | 3.44737 | 0.99635 | 26.35689 | 143.08842 | -0.72276 | |
| Left MLO-angle | 1.05345 | 4.85515 | 0.99383 | 26.45265 | 149.36559 | -0.72506 | |
| Right FPL | 1.63110 | 18.80235 | 0.58494 | 2.33276 | 24.43316 | 0.39590 | |
| Left FPL | 0.98881 | 10.58969 | 0.89538 | 1.72699 | 17.73092 | 0.76812 | |
| Right CSO-angle | 2.09165 | 16.92958 | 0.78946 | 1.73458 | 14.6780 | 0.86539 | |
| Left CSO-angle | 3.02977 | 22.55131 | 0.47633 | 4.29302 | 30.80745 | 0.38151 | |
| Right RLAC | 1993.09811 | 133.54248 | 0.018494 | 2084.36477 | 169.53636 | -0.17639 | |
| Left RLAC | 6665.89030 | 261.041493 | -0.01652 | 7335.77418 | 270.10845 | -0.09082 | |
| Right LAEC | 0.58758 | 1.97191 | 0.94179 | 0.83830 | 2.80533 | 0.89137 | |
| Left LAEC | 0.84720 | 2.75894 | 0.86310 | 1.10182 | 3.67456 | 0.79487 | |
| Right MAEC | 1.33154 | 4.95089 | 0.85018 | 1.73465 | 6.69102 | 0.76575 | |
| Left MAEC | 1.11018 | 4.15098 | 0.78477 | 1.82941 | 7.02472 | 0.56696 | |
| Right AEML | 2.03568 | 12.33373 | 0.67508 | 3.34066 | 23.30421 | 0.27640 | |
| Left AEML | 1.93035 | 11.07328 | 0.54821 | 3.75955 | 25.41527 | 0.11808 | |
| Right AEMM | 1.11086 | 11.38172 | 0.84995 | 1.40214 | 15.29053 | 0.76770 | |
| Left AEMM | 1.23420 | 11.35158 | 0.72772 | 1.74900 | 17.74733 | 0.60414 | |
| Right PCS | 0.93635 | 12.43905 | 0.90597 | 5.38E+3 | 7 632.45553 | -0.02564 | |
| Left PCS | 5.38E+3 | 7 632.45553 | -0.02564 | 5.38E+3 | 7 210.87690 | 0.63944 | |
| Right RLDC | 1.00983 | 3.33194 | 0.89579 | 2.17595 | 7.48971 | 0.56117 | |
| Left RLDC | 2.31663 | 7.59362 | 0.57532 | 2.03918 | 6.99127 | 0.50181 | |
| Right RLPC | 0.42574 | 2.21881 | 0.97252 | 0.71028 | 3.73439 | 0.93883 | |
| Left RLPC | 0.46368 | 2.43722 | 0.94439 | 0.95289 | 4.98765 | 0.76205 | |
| Right RMDC | 0.87350 | 2.44403 | 0.94240 | 3.55356 | 10.64815 | 0.18188 | |
| Left RMDC | 1.81859 | 4.94281 | 0.87463 | 4.86654 | 14.28920 | 0.08782 | |
| Right RMPC | 0.33317 | 1.87172 | 0.95407 | 0.51137 | 2.89646 | 0.90400 | |
| Left RMPC | 0.38406 | 2.18401 | 0.92483 | 0.50818 | 2.90681 | 0.89752 | |
| Right CEA-angle | 1.70147 | 23.45238 | 0.76024 | 4.82237 | 106.63062 | -0.16380 | |
| Left CEA-angle | 2.46232 | 31.85402 | 0.58446 | 5.92326 | 139.37081 | -0.16024 | |
| Right C-LAP | 0.46098 | 0.97304 | 0.98342 | 0.55790 | 1.17335 | 0.97425 | |
| Left C-LAP | 0.41201 | 0.88819 | 0.98150 | 0.74967 | 1.60048 | 0.93765 | |
| Right C-MAP | 0.39686 | 0.76926 | 0.98435 | 0.96203 | 1.88707 | 0.90044 | |
| Left C-MAP | 0.46530 | 0.90139 | 0.98600 | 0.84897 | 1.66440 | 0.95143 | |

TEM technical error of measurement, *rTEM* relative technical error of measurement, *R* coefficient of reliability, *MLF* maximum length of the femur, *AEML* anterior excision middle-lateral length, *AEMM* anterior excision middle-medial length, *PCS* patella coronal-section length, *MAEC* medial anterior excision contour width, *RLAC* radiation of the curvature of the lateral anterior excision contour, *LAEC* lateral anterior excision contour width, *RLPC* radiation of curvature of the lateral posterior condyle, *RMPC* radiation of curvature of the medial posterior condyle, *CEA* epicondyle axis angle, *LAP* lateral anterior–posterior length, *C-ML* cross-section medial–lateral width, *C-LAP* C-lateral anterior–posterior length, *C-MAP* C-medial anterior–posterior length.

et al. [39]. Zhang et al. [63] studied a smaller number of cadavers than this study; therefore, the difference might be due to the sample size. Meanwhile, Lee et al. [39] had more cadavers with age of 41–60 years (65.8% for men and 45.1% for women) than our report (50.0% for men and 30.0% for women). They might have obtained better results of stature estimation formulae than this study, whose age groups of cadavers were scattered because their stature estimation

formulae were adapted to the age groups that comprised most of their cadavers. The difference in age composition ratio, CT equipment, or image reconstruction software may have affected the results.

Many reports have shown that MLF is useful for stature estimation, consistent with our finding that stature estimation with MLF showed the best performance. However, it is impossible to measure MLF if only part of the femur

| | All cadavers (n | =300) | Male $(n = 150)$ | | Female $(n=15)$ | 0) | F value | P value |
|-------------|-----------------|-------------------|------------------|-------------------|-----------------|-------------------|---------|---------|
| | Range | Mean ± SD | Range | Mean \pm SD | Range | Mean \pm SD | | |
| Age (years) | 18-88 | 50.35 ± 17.84 | 19–84 | 49.62 ± 15.15 | 18-88 | 51.07 ± 20.21 | 0.4967 | 0.482 |
| AS (cm) | 141–184 | 162.2 ± 9.84 | 152–184 | 169.6 ± 6.73 | 141–177 | 154.8 ± 6.15 | 398.5 | < 0.001 |
| MLF (cm) | | | | | | | | |
| Right | 36.14 - 50.95 | 42.69 ± 2.920 | 39.07-50.95 | 44.71 ± 2.118 | 36.14-48.65 | 40.66 ± 2.092 | 27.72 | < 0.001 |
| Left | 35.83-51.27 | 42.79 ± 2.960 | 38.95-51.27 | 44.86 ± 2.106 | 35.83-48.95 | 40.71 ± 2.116 | 28.98 | < 0.001 |
| Average | 36.06-51.11 | 42.74 ± 2.937 | 39.01-51.11 | 44.79 ± 2.108 | 36.06-48.80 | 40.69 ± 2.099 | 28.47 | < 0.001 |
| LAP (cm) | | | | | | | | |
| Right | 5.16-7.47 | 6.30 ± 0.470 | 5.86-7.47 | 6.638 ± 0.353 | 5.16-6.89 | 5.962 ± 0.298 | 32.12 | < 0.001 |
| Left | 5.26-7.46 | 6.289 ± 0.463 | 5.84-7.46 | 6.627 ± 0.338 | 5.26-6.78 | 5.951 ± 0.292 | 34.30 | < 0.001 |
| Average | 5.235-7.43 | 6.295 ± 0.464 | 5.88-7.43 | 6.633 ± 0.342 | 5.24-6.84 | 5.957 ± 0.292 | 33.98 | < 0.001 |
| C-ML (cm) | | | | | | | | |
| Right | 5.92-8.66 | 7.278 ± 0.628 | 6.97-8.66 | 7.808 ± 0.366 | 5.92-7.72 | 6.748 ± 0.303 | - | < 0.01 |
| Left | 5.95-8.71 | 7.243 ± 0.629 | 6.81-8.71 | 7.776 ± 0.365 | 5.95-7.59 | 6.710 ± 0.297 | - | < 0.01 |
| Average | 5.94-8.58 | 7.261 ± 0.629 | 6.90-8.58 | 7.792 ± 0.361 | 5.94-7.62 | 6.729 ± 0.292 | - | < 0.01 |
| C-LAP (cm) | | | | | | | | |
| Right | 3.47-5.84 | 4.686 ± 0.426 | 4.25-5.84 | 4.941 ± 0.357 | 3.47-5.09 | 4.431 ± 0.325 | 16.75 | < 0.001 |
| Left | 3.75-5.72 | 4.667 ± 0.398 | 4.00-5.72 | 4.889 ± 0.351 | 3.75-5.14 | 4.446 ± 0.308 | 13.51 | < 0.001 |
| Average | 3.63-5.68 | 4.677 ± 0.401 | 4.23-5.68 | 4.915 ± 0.343 | 3.63-5.10 | 4.438 ± 0.301 | 16.42 | < 0.001 |
| C-MAP (cm) | | | | | | | | |
| Right | 4.33-6.27 | 5.258 ± 0.371 | 4.58-6.27 | 5.483 ± 0.307 | 4.33-5.76 | 5.033 ± 0.283 | 17.43 | < 0.001 |
| Left | 4.27-6.41 | 5.240 ± 0.377 | 4.69-6.41 | 5.484 ± 0.302 | 4.27-5.71 | 4.997 ± 0.272 | 21.56 | < 0.001 |
| Average | 4.30-6.34 | 5.249 ± 0.367 | 4.71-6.34 | 5.435 ± 0.296 | 4.30-5.74 | 5.019 ± 0.270 | 20.56 | < 0.001 |

| Table 4 | Descriptive statistics | for age, AS, ar | nd group 1 | measurements |
|---------|------------------------|-----------------|------------|--------------|
|---------|------------------------|-----------------|------------|--------------|

Wilcoxon rank sum test was used to estimate the *P* value in the C-ML values, and Student's *t*-test was used to estimate the P value in the other measurements. *AS* adjusted stature, which was calculated by subtracting 2.0 cm from the measured stature; *SD* standard deviation; *AZS* absolute *Z* value of skewness; *AZK* absolute *Z* value of kurtosis; MLF, maximum length of the femur; *LAP* lateral anterior–posterior length; *C-ML* cross-section medial–lateral width; C-*LAP* C-lateral anterior–posterior length; *C-MAP* C-medial anterior–posterior length.

Table 5Simple linearregression analyses for statureestimation for all samplesregardless of sex

| | Side | Regulation formula (cm) | SEE (cm) | R^2 | P value |
|------------|---------|-------------------------|----------|-------|---------|
| MLF (cm) | Right | y = 3.091x + 32.230 | 3.913 | 0.842 | < 0.001 |
| | Left | y = 3.060 x + 33.261 | 3.837 | 0.848 | < 0.001 |
| | Average | y = 3.083 x + 32.442 | 3.850 | 0.847 | < 0.001 |
| LAP (cm) | Right | y = 17.582 x + 53.413 | 5.340 | 0.706 | < 0.001 |
| | Left | y = 17.813 x + 52.159 | 5.340 | 0.702 | < 0.001 |
| | Average | y = 17.896 x + 51.533 | 5.287 | 0.712 | < 0.001 |
| C-ML (cm) | Right | y = 12.358 x + 74.240 | 6.047 | 0.623 | < 0.001 |
| | Left | y = 12.380 x + 74.518 | 6.019 | 0.627 | < 0.001 |
| | Average | y = 12.488 x + 73.514 | 5.985 | 0.631 | < 0.001 |
| C-LAP (cm) | Right | y = 15.768 x + 90.296 | 7.199 | 0.466 | < 0.001 |
| | Left | y = 15.786 x + 90.507 | 7.583 | 0.408 | < 0.001 |
| | Average | y = 16.685 x + 86.153 | 7.226 | 0.462 | < 0.001 |
| C-MAP (cm) | Right | y = 20.192 x + 58.015 | 6.384 | 0.580 | < 0.001 |
| | Left | y = 19.710 x + 60.897 | 6.461 | 0.570 | < 0.001 |
| | Average | y = 20.656 x + 55.757 | 6.267 | 0.595 | < 0.001 |

SEE standard error of the estimate, *MLF* maximum length of the femur, *LAP* lateral anterior–posterior length, *C-ML* cross-section medial–lateral width, *C-LAP* C-lateral anterior–posterior length, *C-MAP* C-medial anterior–posterior length.

Table 6Simple linearregression analyses for statureestimation in males

 Table 7
 Simple linear

 regression analyses for stature
 estimation in females

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|---|----|
|---|----|

| | Side | Regulation formula (cm) | SEE (cm) | R^2 | P value |
|------------|---------|-------------------------|----------|-------|---------|
| MLF (cm) | Right | y = 2.667x + 52.355 | 3.664 | 0.705 | < 0.001 |
| | Left | y = 2.682x + 51.321 | 3.667 | 0.705 | < 0.001 |
| | Average | y = 2.686x + 51.298 | 3.646 | 0.708 | < 0.001 |
| LAP (cm) | Right | y = 13.391x + 82.717 | 4.807 | 0.493 | < 0.001 |
| | Left | y = 13.688x + 80.906 | 4.897 | 0.474 | < 0.001 |
| | Average | y = 13.860x + 79.686 | 4.797 | 0.495 | < 0.001 |
| C-ML (cm) | Right | y = 10.467x + 89.882 | 5.547 | 0.325 | < 0.001 |
| | Left | y = 10.266x + 91.779 | 5.608 | 0.310 | < 0.001 |
| | Average | y = 10.609x + 88.945 | 5.547 | 0.325 | < 0.001 |
| C-LAP (cm) | Right | y = 9.921x + 122.590 | 5.739 | 0.277 | < 0.001 |
| | Left | y = 9.348x + 125.910 | 5.891 | 0.238 | < 0.001 |
| | Average | y = 10.305x + 120.960 | 5.747 | 0.275 | < 0.001 |
| C-MAP (cm) | Right | y = 14.347x + 92.950 | 5.106 | 0.428 | < 0.001 |
| | Left | y = 12.911x + 100.810 | 5.504 | 0.335 | < 0.001 |
| | Average | y = 14.418x + 92.554 | 5.220 | 0.402 | < 0.001 |

SEE standard error of the estimate, *MLF* maximum length of the femur, *LAP* lateral anterior–posterior length, *C-ML* cross-section medial–lateral width, *C-LAP* C-lateral anterior–posterior length, *C-MAP* C-medial anterior–posterior length.

| | Side | Regulation formula (cm) | SEE (cm) | R^2 | P value |
|------------|---------|-------------------------|----------|-------|---------|
| MLF (cm) | Right | y = 2.434 x + 57.802 | 3.456 | 0.686 | < 0.001 |
| | Left | y = 2.428 x + 57.895 | 3.384 | 0.699 | < 0.001 |
| | Average | y = 2.442 x + 57.409 | 3.403 | 0.696 | < 0.001 |
| LAP (cm) | Right | y = 12.007 x + 85.171 | 5.012 | 0.340 | < 0.001 |
| | Left | y = 12.044 x + 85.083 | 5.060 | 0.327 | < 0.001 |
| | Average | y = 12.319 x + 83.375 | 5.005 | 0.341 | < 0.001 |
| C-ML (cm) | Right | y = 4.877 x + 123.850 | 5.986 | 0.058 | 0.003 |
| | Left | y = 5.440 x + 120.260 | 5.951 | 0.069 | 0.001 |
| | Average | y = 5.424 x + 120.260 | 5.959 | 0.067 | 0.001 |
| C-LAP (cm) | Right | y = 6.287 x + 128.900 | 5.817 | 0.110 | < 0.001 |
| | Left | y = 5.662 x + 131.590 | 5.914 | 0.081 | < 0.001 |
| | Average | y = 6.647 x + 127.260 | 5.833 | 0.106 | < 0.001 |
| C-MAP (cm) | Right | y = 10.698 x + 102.920 | 5.367 | 0.243 | < 0.001 |
| | Left | y = 10.626 x + 103.670 | 5.441 | 0.222 | < 0.001 |
| | Average | y = 11.317 x + 100.000 | 5.354 | 0.247 | < 0.001 |
| | - | | | | |

SEE standard error of the estimate, *MLF* maximum length of the femur, *LAP* lateral anterior–posterior length, *C-ML* cross-section medial–lateral width, *C-LAP* C-lateral anterior–posterior length, *C-MAP* C-medial anterior–posterior length.

remains. In this study, stature estimation using LAP showed the second lowest SEE. This suggests that LAP would be useful for stature estimation if the MLF cannot be measured, for example, if only the lower part of the femur remains. Although some reports provided stature estimation formulae using measurements of the lower part of the femur [29, 44, 64, 65], no report has suggested that LAP is useful for stature estimation. The high values of SEE for LAP and the three measurements, C-ML, C-LAP, and C-MAP, were not negligible. However, of all the studies that performed stature estimation using the measurements of the lateral side of the femur, only Chiba et al. [44] calculated SEE. They reported that the SEEs calculated from femoral epicondylar breadth (linear distance between projection points of the most medial and lateral epicondyles projected vertically to the horizontal) was 5.620–6.300. Compared to their study, SEEs calculated from LAP showed better results, and SEEs calculated from other measurements were not inferior. Since there are few



Fig. 3 Residual distribution for all samples regardless of sex with the five measurements. **a1**: Right MLF (maximum length of the femur): **a2**: left MLF, a3: average MLF; **b1**: right LAP (lateral anterior–posterior length): **b2**: left LAP, **b3**: average LAP; **c1**: right C-ML (cross-section medial–lateral width): **c2**: left C-ML, **c3**: average C-ML; **d1**:

right C-LAP (C-lateral anterior–posterior length): **d2**: left C-LAP, **d3**: average C-LAP; **e1**: right C-MAP (C-medial anterior–posterior length), **e2**: Left C-MAP, **e3**: average C-MAP. AS, adjusted stature, PS, predicted stature calculated with the obtained regression equation

comparison targets, further research on stature estimation using the measurements of the distal part of the femur is desirable in future studies.

Among the 41 measurements that were semi-automatically measured in the present study, group 2 measurements had large intraobserver and interobserver errors outside the permissible range. Descriptive statistics for the measurements corresponding to group 2 are shown in Online Resource 1. There are several possible reasons for the higher measurement errors in group 2 measurements. Group 2–1 measurements were based on information from the edge of the reconstructed 3D CT model. Therefore, the slight difference in construction due to the manual removal of calcified blood vessels and cartilage might have resulted in a large

160

170

PS (cm)

180

a3

190

b3





Fig. 4 Residual distribution for male samples with the five measurements. a1: right MLF (maximum length of the femur): a2: left MLF, a3: average MLF; b1: right LAP (lateral anterior-posterior length): b2: left LAP, b3: average LAP; c1: right C-ML (cross-section medial-lateral width): c2: left C-ML, c3: Average C-ML; d1:

right C-LAP (C-lateral anterior–posterior length): **d2**: left C-LAP, d3: average C-LAP; **e1**: right C-MAP (C-medial anterior–posterior length): **e2**: left C-MAP, e3: average C-MAP. AS, adjusted stature, PS: predicted stature calculated with the obtained regression equation

error. Group 2–2 measurements, except MAP, had smaller values than those of group 1, as shown in Table 4 and Online Resource 1. Therefore, the error caused by manual operation might have had a significant influence on these measurements. MAP had similar values to those of group 1 measurements, but it also had higher measurement errors. Unlike C-ML, C-LAP, and C-MAP, MAP is measured without

creating a cross section at the lower part of the femur. The deformation of the knee joint, including the distal end of the femur, might have occurred in most of the cadavers in this study because primary knee osteoarthritis often occurs in people over 50 years old [66, 67]. This change may have made it difficult for the AI software to have identified them. In some cadavers, the software used in this study mistakenly

Fig. 5 Residual distribution for female samples with the five measurements. a1: right MLF (maximum length of the femur): a2: left MLF, a3: average MLF; b1: right LAP (lateral anterior-posterior length): b2: left LAP, b3: average LAP; c1: right C-ML (cross-section medial-lateral width): c2: left C-ML, c3: average C-ML; d1:

recognized the knee cartilage and patella as part of the femur when it identified the femur, and the structure other than the femur had to be manually removed. This manual operation might have caused higher measurement errors. In addition, MAP had a larger measurement error than LAP, which was also measured without creating a cross section. This may be because osteoarthritis occurs more frequently on the medial side than on the lateral side [64].

right C-LAP (C-lateral anterior–posterior length): d2: left C-LAP, d3: average C-LAP; e1: right C-MAP (C-medial anterior–posterior length): e2: left C-MAP, e3: average C-MAP. AS, adjusted stature; PS, predicted stature calculated with the obtained regression equation

The residual plots indicated that the two measurements, MLF and LAP, were good models for calculating regression equations. The other three measurements were difficult to adopt for the regression equations, because of the large outliers and a small range of predicted values, especially in the residual plots using single-sex. This may be attributed to the small range of the three measurements.

| Author S | | | | | | , | | | |
|------------------------|---------|---------------------|-------|---|----------------------------|--------------|----------|--------------|--------------|
| | ubject | Equipment | Side | Sex Stature estimation formula | Correlation coefficient | R^2 | SEE (cm) | Intra-OE (%) | Inter-OE (%) |
| Present study J | apanese | Computed tomography | Right | Male $(n = 150)$ $y = 2.667x + 52.355$ | | 0.7053 | 3.664 | 0.035 | 0.018 |
| | | | | Female $(n = 150)$ $y = 2.682 x + 51.321$ | | 0.7049 | 3.667 | | |
| | | | Left | Male $(n = 150) y = 2.434 x + 57.802$ | | 0.686 | 3.456 | 0.034 | 0.019 |
| | | | | Female $(n = 150) y = 2.428 x + 57.895$ | ı | 0.6989 | 3.384 | | |
| Chiba et al. [44] J | apanese | Computed tomography | Right | Male $(n = 116) y = 2.670 x + 50.987$ | | 0.654 | 3.847 | 0.108 | 0.205 |
| | | | | Female $(n = 108) y = 2.702 x + 46.624$ | | 0.768 | 3.29 | | |
| | | | Left | Male $(n = 116) y = 2.748 x + 47.259$ | ı | 0.653 | 3.85 | 0.247 | 0.289 |
| | | | | Female $(n = 108) y = 2.646 x + 48.733$ | ı | 0.76 | 3.34 | | |
| Hasegawa et al. [37] J | apanese | X-ray photography | Right | Male $(n=92)$ $y=2.42 x+63.32$ | 0.895 | 0.8010* | 3.77 | | ı |
| | | | | Female $(n = 342) y = 2.31 x + 62.05$ | 0.809 | 0.6545* | 3.03 | | |
| | | | Left | Male $(n=92)y=2.49x+60.30$ | 0.903 | 0.8154^{*} | 3.83 | ı | ı |
| | | | | Female $(n = 342) y = 2.28 x + 63.37$ | 0.813 | 0.6610^{*} | 3.00 | | |
| Hishmat et al. [40] J | apanese | Computed tomography | Right | Male $(n = 150) y = 2.61 x + 52.17$ | 0.73 | 0.5329* | 4.83 | 0.149 | 0.192 |
| | | | | Female $(n = 109) y = 2.86 x + 38.48$ | 0.83 | 0.6889* | 4.29 | | |
| | | | Left | Male $(n = 150) y = 2.47 x + 58.04$ | 0.72 | 0.5184 | 4.72 | 0.277 | 0.201 |
| | | | | Female $(n = 109) y = 2.87 x + 37.42$ | 0.81 | 0.6561* | 4.49 | | |
| Nishio [42] J | apanese | Computed tomography | Right | Male $(n = 215) y = 3.20 x + 27.81$ | 0.8967 | 0.8041^{*} | 4.32 | | |
| | | | | Female $(n = 120) y = 3.36 x + 20.22$ | 0.8784 | 0.7716^{*} | 4.12 | | |
| | | | Left | Male $(n = 215)y = 3.11x + 31.13$ | 0.8841 | 0.7816^{*} | 4.60 | | |
| | | | | Female $(n = 120) y = 3.15 x + 29.00$ | 0.8591 | 0.7381^{*} | 4.39 | | |
| Zhang et al. [63] I | Danish | Computed tomography | Right | Male $(n = 41) y = 2.23 x + 70.70$ | | 0.52 | 4.4 | | |
| | | | | Female $(n = 37) y = 2.13 x + 69.26$ | | 0.75 | 3.5 | | |
| | | | Left | Male $(n = 41) y = 2.19 x + 72.17$ | | 0.51 | 4.4 | ı | ı |
| | | | | Female $(n = 37) y = 2.07 x + 72.03$ | ı | 0.74 | 3.6 | | |
| Lee et al. [39] k | Corean | Computed tomography | Right | Male $(n = 155) y = 2.593 x + 54.081$ | 0.85 | 0.722* | 3.305 | | |
| | | | | Female $(n = 153) y = 2.82 x + 41.926$ | 0.89 | 0.792* | 3.417 | | |
| | | | Left | Male $(n = 155) y = 2.610 x + 54.081$ | 0.859 | 0.737* | 3.214 | ı | ı |
| | | | | Female $(n = 153) y = 2.842 x + 40.776$ | 0.886 | 0.785* | 3.468 | | |

374

SEE standard error of the estimate, intra-OE and Inter-OE r-TEMs of intraobserver and interobserver errors, respectively.

This study has several limitations. The measurements useful in other reports, such as the femoral diaphysis length, physiological length, or bicondylar length [13, 29, 65, 68, 69], were not measured because the semi-automatic measurement application was not configured to measure them. Furthermore, the application was developed by Fujifilm, including measurements selection. The femurs measured in this study were collected only from cadavers with soft tissue, so further studies examining the difference between digital and analog measurements are warranted. Femur deformation due to aging was not considered. In this research, the stature of the cadavers was recalculated in AS, and the estimation formulae were assessed, but since the actual stature was measured only once, intra- and inter-observer errors were not evaluated for the stature. Age-stratified analysis was not performed because of the insufficient sample size in this study. In addition, this study was performed using images captured with two types of CT equipment. Further studies comparing and examining images acquired with different CT devices are warranted.

Conclusion

This study provided the first stature estimation formulae based on a 3D CT model of modern Japanese femurs using a simple and rapid semi-automatic measurement software. For stature estimation with this method, MLF was the best, and LAP was the second-best measurement using 41 total measurements. These formulae can be useful in forensic investigations.

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Author contribution All authors contributed to the conception and design of the study. Material preparation, data collection, and analysis were performed by Kei Kira and Fumiko Chiba. The first draft of the manuscript was written by Kei Kira, and all authors commented on the previous versions of the manuscript. All authors read and approved the final manuscript.

Data availability The datasets generated and analyzed during the current study are available from the corresponding author on reasonable request.

Code availability Code sharing not applicable to this article as no codes were generated or analyzed during the current study.

Declarations

Ethics approval The experimental protocol was approved by the Ethical Review Board of Chiba University (2987) and the University of Tokyo (10835–1).

Consent to participate This study provided sufficient protection of the privacy of the patients and their families as per the Japanese Protection Guideline of Personal Information on Research Publication in Legal

Medicine, and the requirements of informed consent from the next of kin was waived by the Ethical Review Board.

Consent for publication This study provided sufficient protection of the privacy of the patients and their families as per the Japanese Protection Guideline of Personal Information on Research Publication in Legal Medicine, and the requirements of informed consent from the next of kin was waived by the Ethical Review Board.

Conflict of interest The authors declare no competing interests.

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