CORRECTION

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Correction to: Effects of random laminate misalignment on macroscopic and microscopic elastic/viscoplastic behaviors of ultrafine plate–fin structures

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Correction to: Continuum Mech. Thermodyn.
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In the original publication of the article, the below errors have occurred.
These errors have been corrected in original article.

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No.	Location in original publication	Incorrect	Correct
1	Page 5, Line 2	The substitution of Eqs. (7)–(9) ...	The substitution of Eqs. (7)–(9) ...
2	Page 5, Line 2		
3	Page 5, Line 6	The substitution of Eqs. (7)–(9) in Eq. (6) leads to ... Then, according to the homogenization theory of nonlinear time-dependent materials ...	The substitution of Eqs. (7)–(9) into Eq. (6) leads to ... Then, according to the homogenization theory of nonlinear time-dependent materials ...
4	Page 5, Eq. (17)	$\int_{V_\alpha} \dot{\sigma}_{ij} v_{i,j} dV - \int_{\hat{\Gamma}_\alpha} \dot{\sigma}_{ijn_j} v_i d\Gamma = 0$	$\int_{V_\alpha} \dot{\sigma}_{ij} v_{i,j} dV - \int_{\hat{\Gamma}_\alpha} \dot{\sigma}_{ijn_j} v_i d\Gamma = 0$
5	Page 6, Eq. (19)	$\mathbf{K}_\alpha = \int_{V_\alpha} \mathbf{B}^\top \mathbf{C} \mathbf{B} dV$	$\mathbf{K}_\alpha = \int_{V_\alpha} \mathbf{B}^\top \mathbf{C} \mathbf{B} dV$
6	Page 6, Eq. (19)	$\mathbf{F}_\alpha^{kl} = - \int_{V_\alpha} \mathbf{B}^\top \mathbf{C}^{kl} dV$	$\mathbf{F}_\alpha^{kl} = - \int_{V_\alpha} \mathbf{B}^\top \mathbf{C}^{kl} dV$
7	Page 6, Eq. (19)	$\mathbf{G}_\alpha = \int_{V_\alpha} \mathbf{B}^\top \mathbf{C} \beta dV$	$\mathbf{G}_\alpha = \int_{V_\alpha} \mathbf{B}^\top \mathbf{C} \beta dV$

No.	Location in original publication	Incorrect	Correct
8	Page 6, Eq. (19)	$S_{\alpha}^{(f)} = \int_{\tilde{V}_{\alpha}} \dot{\sigma} n d\Gamma$	$S_{\alpha}^{(f)} = \int_{\tilde{V}_{\alpha}} \dot{\sigma} n d\Gamma$
9	Page 6, Eq. (21)	$\tilde{\mathbf{K}}_{\alpha}^{(f)*\#(f)} = \dot{E}_k \tilde{\mathbf{F}}_{\alpha}^{kl(f)} + \tilde{\mathbf{G}}_{\alpha}^{(f)} + \mathbf{S}_{\alpha}^{(f)}$	$\tilde{\mathbf{K}}_{\alpha}^{(f)*\#(f)} = \dot{E}_k \tilde{\mathbf{F}}_{\alpha}^{kl(f)} + \tilde{\mathbf{G}}_{\alpha}^{(f)} + \mathbf{S}_{\alpha}^{(f)}$
10	Page 6, Eq. (22)	$\tilde{\mathbf{K}}_{\alpha}^{(f)} = \mathbf{K}_{\alpha}^{(f)} - \mathbf{K}_{\alpha}^{(f\Omega)} \left(\mathbf{K}_{\alpha}^{(\Omega)} \right)^{-1} \mathbf{K}_{\alpha}^{(\Omega f)}$	$\tilde{\mathbf{K}}_{\alpha}^{(f)} = \mathbf{K}_{\alpha}^{(f)} - \mathbf{K}_{\alpha}^{(f\Omega)} \left(\mathbf{K}_{\alpha}^{(\Omega)} \right)^{-1} \mathbf{K}_{\alpha}^{(\Omega f)}$
11	Page 6, Eq. (23)	$\tilde{\mathbf{F}}_{\alpha}^{kl(f)} = \mathbf{F}_{\alpha}^{kl(f)} - \mathbf{K}_{\alpha}^{(f\Omega)} \left(\mathbf{K}_{\alpha}^{(\Omega)} \right)^{-1} \mathbf{F}_{\alpha}^{kl(\Omega)}$	$\tilde{\mathbf{F}}_{\alpha}^{kl(f)} = \mathbf{F}_{\alpha}^{kl(f)} - \mathbf{K}_{\alpha}^{(f\Omega)} \left(\mathbf{K}_{\alpha}^{(\Omega)} \right)^{-1} \mathbf{F}_{\alpha}^{kl(\Omega)}$
12	Page 6, Eq. (24)	$\tilde{\mathbf{G}}_{\alpha}^{(f)} = \mathbf{G}_{\alpha}^{(f)} - \mathbf{K}_{\alpha}^{(f\Omega)} \left(\mathbf{K}_{\alpha}^{(\Omega)} \right)^{-1} \mathbf{G}_{\alpha}^{(\Omega)}$	$\tilde{\mathbf{G}}_{\alpha}^{(f)} = \mathbf{G}_{\alpha}^{(f)} - \mathbf{K}_{\alpha}^{(f\Omega)} \left(\mathbf{K}_{\alpha}^{(\Omega)} \right)^{-1} \mathbf{G}_{\alpha}^{(\Omega)}$
13	Page 6, Eq. (25)	$\tilde{\mathbf{K}}^{(f)*\#(f)} = \dot{E}_k \tilde{\mathbf{F}}^{kl(f)} + \tilde{\mathbf{G}}^{(f)}$	$\tilde{\mathbf{K}}^{(f)*\#(f)} = \dot{E}_k \tilde{\mathbf{F}}^{kl(f)} + \tilde{\mathbf{G}}^{(f)}$
14	Page 6, Line 18–19	where $\mathbf{u}^{\#(f)}$ represents the nodal vector of $\dot{u}_i^{\#}$ for the boundary nodes of all V_{α} , $\tilde{\mathbf{K}}^{(f)}$ is the matrix comprising $\tilde{\mathbf{K}}_{\alpha}^{(f)}$, and $\tilde{\mathbf{F}}^{kl(f)}$ and $\tilde{\mathbf{G}}^{(f)}$ are respectively the vectors comprising $\tilde{\mathbf{F}}_{\alpha}^{kl(f)}$ and $\tilde{\mathbf{G}}_{\alpha}^{(f)}$	where $\mathbf{u}^{\#(f)}$ represents the nodal vector of $\dot{u}_i^{\#}$ for the boundary nodes of all V_{α} , $\tilde{\mathbf{K}}^{(f)}$ is the matrix comprising $\tilde{\mathbf{K}}_{\alpha}^{(f)}$, and $\tilde{\mathbf{F}}^{kl(f)}$ and $\tilde{\mathbf{G}}^{(f)}$ are respectively the vectors comprising $\tilde{\mathbf{F}}_{\alpha}^{kl(f)}$ and $\tilde{\mathbf{G}}_{\alpha}^{(f)}$
15	Page 6, Line 19–20	It is noted that $\mathbf{S}_{\alpha}^{(f)}$ into Eq. (21) has vanished ...	It is noted that $\mathbf{S}_{\alpha}^{(f)}$ in Eq. (21) has vanished ...
16	Page 7, Eq. (26)	$\tilde{\mathbf{K}}^{(f)} \chi^{kl(f)} = \tilde{\mathbf{F}}^{kl(f)}$	$\tilde{\mathbf{K}}^{(f)} \chi^{kl(f)} = \tilde{\mathbf{F}}^{kl(f)}$
17	Page 7, Eq. (27)	$\tilde{\mathbf{K}}^{(f)} \varphi^{(f)} = \tilde{\mathbf{G}}^{(f)}$	$\tilde{\mathbf{K}}^{(f)} \varphi^{(f)} = \tilde{\mathbf{G}}^{(f)}$
18	Page 7, Line 5	where $\chi^{kl(f)}$ and $\varphi^{(f)}$ respectively denote the boundary node components of χ^{kl} and φ for all V_{α}	where $\chi^{kl(f)}$ and $\varphi^{(f)}$ respectively denote the boundary node components of χ^{kl} and φ for all V_{α}
19	Page 7, Eq. (28)	$\chi_{\alpha}^{kl(\Omega)} = \left(\mathbf{K}_{\alpha}^{(\Omega)} \right)^{-1} \left(\mathbf{F}_{\alpha}^{kl(\Omega)} - \mathbf{K}_{\alpha}^{(\Omega f)} \chi_{\alpha}^{kl(f)} \right)$	$\chi_{\alpha}^{kl(\Omega)} = \left(\mathbf{K}_{\alpha}^{(\Omega)} \right)^{-1} \left(\mathbf{F}_{\alpha}^{kl(\Omega)} - \mathbf{K}_{\alpha}^{(\Omega f)} \chi_{\alpha}^{kl(f)} \right)$
20	Page 7, Footnote	¹ The stochastic homogenization method [37, 37, 39] evaluates variabilities of ...	¹ The stochastic homogenization method [37–39] evaluates variabilities of ...
21	Page 8, Eq. (31)	$d_{\alpha} = \frac{L}{64} I_{\alpha}$ ($\alpha = 1, 2, \dots, N$)	$d_{\alpha} = \frac{L}{64} I_{\alpha}$ (31)
22	Page 9, Line 32	This can be attributable to the fact that in these loading conditions, the macroscopic loads are ...	This can be attributable to the fact that, in these loading conditions, the macroscopic loads are ...
23	Page 13, Table 2	Maximum microscopic equivalent stress $\bar{\sigma}^{\max}$ (MPa)	Maximum microscopic equivalent stress $\bar{\sigma}^{\max}$ (MPa)

No.	Location in original publication	Incorrect	Correct
24	Page 13–14, Sect. 5.2	<p>As a microscopic quantity of interest, microscopic equivalent viscoplastic strain $\bar{\epsilon}_{vp}$ was considered because it generally has a strong relation with the strength properties such as fatigue life of metallic materials. The distribution of $\bar{\epsilon}_{vp}$ in Y at 0.4% macroscopic strain was calculated in each trial of the MC simulation, and the maximum value $\bar{\epsilon}_{vp}^{\max}$ was selected from the distribution. Histograms of $\bar{\epsilon}_{vp}^{\max}$ are shown in Fig. 12a–e for the two tensile cases and three shear cases. The marked variability of $\bar{\epsilon}_{vp}^{\max}$ is seen. Differences between maximum and minimum values of $\bar{\epsilon}_{vp}^{\max}$ (i.e., the maximum differences of $\bar{\epsilon}_{vp}^{\max}$) are summarized in Fig. 13 for all loading conditions. This figure also shows the maximum differences for the macroscopic elastic moduli (C_1, C_2, G_{12}, G_{23}, and G_{31}) and the maximum microscopic equivalent stress $\bar{\sigma}^{\max}$ in the elastic analysis, which were respectively calculated from Figs. 6 and 7. It is seen from Fig. 13 that the variability of $\bar{\epsilon}_{vp}^{\max}$ due to the laminate misalignment becomes considerably large compared with the variabilities of the elastic moduli and $\bar{\sigma}^{\max}$ except for y_2–y_3 shear, ranging from 17% (y_1–y_2 shear) to 37% (y_3–y_1 shear). It is noted that the differences in N and M between the elastic and elastic-viscoplastic MC simulations can affect the results of analysis. To confirm this, the elastic MC simulation with $N = 5$ and $M = 3000$ was additionally conducted, revealing that the results obtained gave almost the same tendency as in Fig. 13</p>	<p>As a microscopic quantity of interest, microscopic equivalent viscoplastic strain $\bar{\epsilon}_{vp}$ was considered because it generally has a strong relation with the strength properties such as fatigue life of metallic materials. The distribution of $\bar{\epsilon}_{vp}$ in Y at 0.4% macroscopic strain was calculated in each trial of the MC simulation, and the maximum value $\bar{\epsilon}_{vp}^{\max}$ was selected from the distribution. Histograms of $\bar{\epsilon}_{vp}^{\max}$ are shown in Fig. 12a–e for the two tensile cases and three shear cases. The marked variability of $\bar{\epsilon}_{vp}^{\max}$ is seen. Differences between maximum and minimum values of $\bar{\epsilon}_{vp}^{\max}$ (i.e., the maximum differences of $\bar{\epsilon}_{vp}^{\max}$) are summarized in Fig. 13 for all loading conditions. This figure also shows the maximum differences for the macroscopic elastic moduli (C_1, C_2, G_{12}, G_{23}, and G_{31}) and the maximum microscopic equivalent stress $\bar{\sigma}^{\max}$ in the elastic analysis, which were respectively calculated from Figs. 6 and 7. It is seen from Fig. 13 that the variability of $\bar{\epsilon}_{vp}^{\max}$ due to the laminate misalignment becomes considerably large compared with the variabilities of the elastic moduli and $\bar{\sigma}^{\max}$ except for y_2–y_3 shear, ranging from 17% (y_1–y_2 shear) to 37% (y_3–y_1 shear). It is noted that the differences in N and M between the elastic and elastic-viscoplastic MC simulations can affect the results of analysis. To confirm this, the elastic MC simulation with $N = 5$ and $M = 3000$ was additionally conducted, revealing that the results obtained gave almost the same tendency as in Fig. 13</p>

No.	Location in original publication	Incorrect	Correct
25	Page 15, Caption of Fig. 12	<p>As in Sect. 4.2, the distributions of $\bar{\epsilon}_{vp}$ and the locations of $\bar{\epsilon}_{vp}^{\max}$ in Y for y_2 tension at $E_{22} = 0.4\%$ are depicted in Fig. 14a, b for the cases with the maximum and minimum $\bar{\epsilon}_{vp}^{\max}$, respectively. It is seen that $\bar{\epsilon}_{vp}^{\max}$ concentrates on the fin parts irrespective of the laminate misalignment, although it has slightly different distributions in the left and right fin parts depending on the misalignment. It is also seen from Fig. 14b that the minimum $\bar{\epsilon}_{vp}^{\max}$ takes place in the almost aligned case, similar to the case of the minimum $\bar{\sigma}^{\max}$ shown in Fig. 8b. The location of the minimum $\bar{\epsilon}_{vp}^{\max}$ depicted in Fig. 14b is the same as that of $\bar{\sigma}^{\max}$ illustrated in Fig. 9 (i.e., in the connecting region of the fin and blazing parts) while the maximum is observed in the left fin part in Fig. 14a. Examination of locations of $\bar{\epsilon}_{vp}^{\max}$ in all trials reveals that $\bar{\epsilon}_{vp}^{\max}$ occurred at one of the eight points indicated by red circles in Fig. 15. This means that $\bar{\epsilon}_{vp}^{\max}$ does not necessarily occur at the locations of $\bar{\sigma}^{\max}$ owing to the progress of the viscoplastic deformation of plate-fin structures, and that one has to pay attention to the strain concentration also in fin parts for y_2 tension. In contrast, locations of $\bar{\epsilon}_{vp}^{\max}$ for the other loading conditions indicated by blue and green circles in Fig. 15 are limited to the same four points as those of $\bar{\sigma}^{\max}$ in Fig. 9</p> <p>Fig. 12 Histograms of maximum microscopic equivalent viscoplastic strain $\bar{\epsilon}_{vp}^{\max}$ in ultrafine plate-fin structures ...</p>	<p>As in Sect. 4.2, the distributions of $\bar{\epsilon}_{vp}$ and the locations of $\bar{\epsilon}_{vp}^{\max}$ in Y for y_2 tension at $E_{22} = 0.4\%$ are depicted in Fig. 14a, b for the cases with the maximum and minimum $\bar{\epsilon}_{vp}^{\max}$, respectively. It is seen that $\bar{\epsilon}_{vp}^{\max}$ concentrates on the fin parts irrespective of the laminate misalignment, although it has slightly different distributions in the left and right fin parts depending on the misalignment. It is also seen from Fig. 14b that the minimum $\bar{\epsilon}_{vp}^{\max}$ takes place in the almost aligned case, similar to the case of the minimum $\bar{\sigma}^{\max}$ shown in Fig. 8b. The location of the minimum $\bar{\epsilon}_{vp}^{\max}$ depicted in Fig. 14b is the same as that of $\bar{\sigma}^{\max}$ illustrated in Fig. 9 (i.e., in the connecting region of the fin and blazing parts) while the maximum is observed in the left fin part in Fig. 14a. Examination of locations of $\bar{\epsilon}_{vp}^{\max}$ in all trials reveals that $\bar{\epsilon}_{vp}^{\max}$ occurred at one of the eight points indicated by red circles in Fig. 15. This means that $\bar{\epsilon}_{vp}^{\max}$ does not necessarily occur at the locations of $\bar{\sigma}^{\max}$ owing to the progress of the viscoplastic deformation of plate-fin structures, and that one has to pay attention to the strain concentration also in fin parts for y_2 tension. In contrast, locations of $\bar{\epsilon}_{vp}^{\max}$ for the other loading conditions indicated by blue and green circles in Fig. 15 are limited to the same four points as those of $\bar{\sigma}^{\max}$ in Fig. 9</p> <p>Fig. 12 Histograms of maximum microscopic equivalent viscoplastic strain $\bar{\epsilon}_{vp}^{\max}$ in ultrafine plate-fin structures ...</p>
26	Page 16, Caption of Fig. 13	<p>Fig. 13 Maximum differences resulting from random laminate misalignment: macroscopic elastic moduli (green), maximum microscopic equivalent stress $\bar{\sigma}^{\max}$ obtained from elastic analysis (blue), and maximum microscopic equivalent viscoplastic strain $\bar{\epsilon}_{vp}^{\max}$ (red), respectively calculated ...</p>	<p>Fig. 13 Maximum differences resulting from random laminate misalignment: macroscopic elastic moduli (green), maximum microscopic equivalent stress $\bar{\sigma}^{\max}$ obtained from elastic analysis (blue), and maximum microscopic equivalent viscoplastic strain $\bar{\epsilon}_{vp}^{\max}$ (red), respectively calculated ...</p>
27	Page 16, Caption of Fig. 14	<p>Fig. 14 Distributions of $\bar{\epsilon}_{vp}$ under y_2 tension with a maximum $\bar{\epsilon}_{vp}^{\max}$, b minimum $\bar{\epsilon}_{vp}^{\max}$ (elastic-viscoplastic ...</p>	<p>Fig. 14 Distributions of $\bar{\epsilon}_{vp}$ under y_2 tension with a maximum $\bar{\epsilon}_{vp}^{\max}$, b minimum $\bar{\epsilon}_{vp}^{\max}$ (elastic-viscoplastic ...</p>
28	Page 17, Caption of Fig. 15	<p>Fig. 15 Locations of maximum $\bar{\epsilon}_{vp}^{\max}$ in V_a (elastic-viscoplastic analysis)</p>	<p>Fig. 15 Locations of maximum $\bar{\epsilon}_{vp}^{\max}$ in V_a (elastic-viscoplastic analysis)</p>

No.	Location in original publication	Incorrect	Correct
29	Page 17, Caption of Fig. 16	<p>Fig. 16 Maximum deviations of randomly mis-aligned cases from the regularly aligned case; macroscopic elastic moduli (green), maximum microscopic equivalent stress $\bar{\sigma}^{\max}$ obtained from elastic analysis (blue), and maximum microscopic equivalent viscoplastic strain $\bar{\epsilon}_{vp}^{\max}$ (red), calculated from ...</p>	<p>Fig. 16 Maximum deviations of randomly mis-aligned cases from the regularly aligned case; macroscopic elastic moduli (green), maximum microscopic equivalent stress $\bar{\sigma}^{\max}$ obtained from elastic analysis (blue), and maximum microscopic equivalent viscoplastic strain $\bar{\epsilon}_{vp}^{\max}$ (red), calculated from ...</p>
30	Page 17, Caption of Fig. 17	<p>Fig. 17 Distribution of $\bar{\epsilon}_{vp}$ and locations of $\bar{\epsilon}_{vp}^{\max}$ under y_2 tension in the regularly aligned case (elastic-viscoplastic ...</p>	<p>Fig. 17 Distribution of $\bar{\epsilon}_{vp}$ and locations of $\bar{\epsilon}_{vp}^{\max}$ under y_2 tension in the regularly aligned case (elastic-viscoplastic ...</p>

No.	Location in original publication	Incorrect	Correct
31	Page 17–18, Sect. 5.3	<p>The elastic-viscoplastic analysis of the ultrafine plate–fin structure without laminate misalignment was conducted for all loading conditions, providing the macroscopic stress–strain relationships already shown in Fig. 11 and $\bar{\epsilon}_{vp}^{max}$ listed in Table 3. Little effect of the presence or absence of laminate misalignment on the stress–strain relationships was seen, as already mentioned in Sect. 5.1. In contrast, a comparison of $\bar{\epsilon}_{vp}^{max}$ in Table 3 and Fig. 12 reveals that random laminate misalignment can bring about large $\bar{\epsilon}_{vp}^{max}$; even the minimum values of $\bar{\epsilon}_{vp}^{max}$ in Fig. 12a–e are higher than $\bar{\epsilon}_{vp}^{max}$ in Table 3. The maximum deviations of $\bar{\epsilon}_{vp}^{max}$ in Fig. 12 from those in Table 3 are summarized in Fig. 16. In addition, the maximum deviations for the elastic moduli and $\bar{\sigma}^{max}$ calculated from Figs. 6 and 7 and Table 2 are shown in the figure. This figure shows that $\bar{\epsilon}_{vp}^{max}$ can be much higher than those in the regularly aligned case except for y_2–y_3 shear, and the maximum deviation for y_1 tension reaches 50%. These results indicate that analysis based on the regularly aligned case can appreciably underestimate microscopic viscoplastic strain occurring in ultrafine plate–fin structures, resulting in dangerous estimation. This suggests that random laminate misalignment needs to be considered especially in the situation that (visco)plastic strain becomes an important factor for the strength/life prediction of ultrafine plate–fin structures, such as in fatigue life problems</p> <p>The distribution of $\bar{\epsilon}_{vp}$ for y_2 tension in the regularly aligned case is shown in Fig. 17. The figure shows that $\bar{\epsilon}_{vp}^{max}$ simultaneously occurs at the four points in the connecting regions of the fin and brazing parts, which agree with the locations of $\bar{\sigma}^{max}$ shown in Fig. 9. Looking back at Fig. 15, however, $\bar{\epsilon}_{vp}^{max}$ in the randomly misaligned cases occurred at eight points; i.e., the four points of $\bar{\sigma}^{max}$ and the other four points in the fin parts. This implies that the random laminate misalignment affected the locations of $\bar{\epsilon}_{vp}^{max}$ for y_2 tension. In contrast, the locations of $\bar{\epsilon}_{vp}^{max}$ for the other loading conditions were the same four points as in Fig. 15, meaning that they were not affected by the laminate misalignment</p>	<p>The elastic-viscoplastic analysis of the ultrafine plate–fin structure without laminate misalignment was conducted for all loading conditions, providing the macroscopic stress–strain relationships already shown in Fig. 11 and $\bar{\epsilon}_{vp}^{max}$ listed in Table 3. Little effect of the presence or absence of laminate misalignment on the stress–strain relationships was seen, as already mentioned in Sect. 5.1. In contrast, a comparison of $\bar{\epsilon}_{vp}^{max}$ in Table 3 and Fig. 12 reveals that random laminate misalignment can bring about large $\bar{\epsilon}_{vp}^{max}$; even the minimum values of $\bar{\epsilon}_{vp}^{max}$ in Fig. 12a–e are higher than $\bar{\epsilon}_{vp}^{max}$ in Table 3. 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In contrast, the locations of $\bar{\epsilon}_{vp}^{max}$ for the other loading conditions were the same four points as in Fig. 15, meaning that they were not affected by the laminate misalignment</p>

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32	Page 19, Caption of Fig. 18	Fig. 18 Relationships between normalized standard errors of maximum microscopic equivalent stress <i>Overline</i> $\sigma^{\max}$ and number of ...	Fig. 18 Relationships between normalized standard errors of maximum microscopic equivalent stress $\bar{\sigma}^{\max}$ and number of ...
33	Page 19, Caption of Fig. 19	Fig. 19 Relationships between normalized standard errors of maximum microscopic equivalent viscoplastic strain $\bar{\epsilon}_{vp}^{\max}$ and number of ...	Fig. 19 Relationships between normalized standard errors of maximum microscopic equivalent viscoplastic strain $\bar{\epsilon}_{vp}^{\max}$ and number of ...
34	Page 19, Line 12	the SEs of the maximum microscopic equivalent viscoplastic strain $\bar{\epsilon}_{vp}^{\max}$ calculated at ...	the SEs of the maximum microscopic equivalent viscoplastic strain $\bar{\epsilon}_{vp}^{\max}$ calculated at ...
35	Page 20, Ref. 27	27. Ohno, N., Matsuda, T., Wu, X.: A homogenization theory for elastic-viscoplastic composites with point-symmetry of internal distributions. Int. J. Solids Struct. 38 , 2867–2878 (2001)	27. Ohno, N., Matsuda, T., Wu, X.: A homogenization theory for elastic-viscoplastic composites with point-symmetry of internal distributions. Int. J. Solids Struct. 38 , 2867–2878 (2001)

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