the fatigue than in the creep specimens to account for the earlier failure.

Conclusions. 1. Prior fatigue deformation to produce a "diamond" grain configuration results in decreased fracture elongation during subsequent creep testing.

2. Specimens with the "diamond" grain configuration exhibited enhanced grain boundary sliding particularly at low creep strains as compared to annealed specimens.

3. With increasing creep strain the "diamond" configuration disappeared in the fatigued specimens and the grain configuration approached that of the annealed specimens at high strains.

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Stress-Strain Relationship During Transformation Enhanced Plasticity by J. R. C. Guimarães and R. J. DeAngelis, pp. 2379-81.

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Eqs. [18]-[21] are in error. They should have appeared as follows:

$$\frac{d\sigma}{d\epsilon_i} = \frac{d\sigma}{d\sigma^*} \times \frac{d\epsilon^*}{d\epsilon_i} \times \frac{d\sigma^*}{d\epsilon^*} \qquad \text{[no number]}$$

$$\frac{d\sigma}{d\epsilon_i} = \left(\frac{1 + \Delta - f\Delta}{1 + \Delta}\right)\left(1 - \frac{\phi_{sc}\, df/d\epsilon^*}{1 + f\phi_{sc}}\right)^{-1} \frac{d\sigma^*}{d\epsilon^*} \qquad [18]$$

$$\frac{d\sigma}{d\epsilon_i^p} \simeq \frac{1 - \dfrac{f\Delta}{1 + \Delta}}{1 - \dfrac{\phi_{sc}\, df/d\epsilon_p^*}{1 + f\phi}} \frac{d\sigma^*}{d\epsilon_p^*} \qquad [19]$$

$$\frac{d\sigma}{d\epsilon_i^p} = \frac{d\sigma^*/d\epsilon_p^*}{\left(1 - \dfrac{\phi_{sc}\, df/d\epsilon_p^*}{1 + f\phi s}\right)} \qquad [20]$$

$$R^* = \frac{\phi\, df/d\epsilon^*}{1 + f\phi_{sc}} \qquad [21]$$