## AMWS Seeks New Scientists

Nominees are being sought for the 19th edition of American Men \& Women of Science (AMWS), a biographical directory of prominent living U.S. and Canadian scientists. The individuals must not have been previously listed and must have distinguished themselves in the fields of natural science, agriculture, medicine, engineering, mathematics, and computer science.

The deadline for submissions is September 1, 1993. Nominees' names, with their general scientific discipline and full address, should be sent to Tanya Hurst, American Men \& Women of Science, R.R. Bowker, 121 Chanlon Road, New Providence, New Jersey 07974.

## Letters to the Editor

To the Editor:
In the March issue, there was an invitation to address the issue of the difference between the words "aluminum" and "aluminium" [Forum Features, page 72-ed.J.
When I was a student in England during the 1950s, we were told about an organization called the international Union of Pure and Applied Chemistry, to which the United States and most major countries belonged. This organization called a meeting sometime in the 1930 s
to resoive differences between countries with regard to the names of the chemical elements. It was apparently agreed that it should be niobium, not columbium, and tungsten, not wolfram. It was also agreed that, wherever possible, metals should have names ending in "ium." Hence aluminium, not aluminum.

Is my memory at fault or does anyone else have any knowledge of this?

## J.A. Smith

Metallurgical Consultant
[No one at the editorial office is familiar with this convention, but we too would enjoy learning more about it. Readers?ed.]

To the Editor:
I thoroughly enjoyed the article in the April issue titled "The Value of Professional Registration-Part II" by Morris E. Nicholson [pages 10-11-ed]. I believe that an official accreditation system is essential to ensure that metallurgists remain conversant in the fundamentals and that we do not lose touch with the basics.

I found an error in the solution to the PE exam on page 70. The first equation for the terminal velocity of a spherical particle should be:

$$
V_{\mathrm{t}}=\sqrt{\frac{4 \mathrm{D}\left(\rho_{\mathrm{p}}-\rho_{\text {fiviic }}\right) \mathrm{g}}{3 f_{\text {ptuid }}}}
$$

Since your final equation for the terminal velocity is correct, the original mistake was obviously a typographical error.

## Ernest Mast <br> CCR Minéraux Noranda

[It is, indeed, a typo that appears in the article and the study guide as well. It will be corrected in a future edition-ed.]

## Corrections

In addition to the error referenced by Ernest Mast's letter to the editor, the following corrections to recent issues must, with our apologies, be noted.

## MARCH

In the article "The Processing and Properties of a Nylon 6/Clay Hybrid" (page 71 in Forum Features), the last sentence of the next-to-last paragraph of the article should read "NCH is now open to practical use."

## JUNE

In the article"The Principles and Properties of Thermostat Metals" by Prasad Khadkikar (pages 39-42), Table I is referenced, but it was inadvertently omitted from the article. It now appears on this page. Also, in Equation 4, the term (1+ $m^{2}$ ) should be $(1+m)^{2}$.

| Composition | TM1 | TM2 | TM3 | TM4 | TM5 | TM6 | TM8 | TM9 | TM10 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| High Expansive (wt.\%) |  |  |  |  |  |  |  |  |  |
| Nickel | 22 | 10 | 25 | 25 | 25 | 22 | 10 | 22 | 22 |
| Chromium | 3 | - | 8.5 | 8.5 | 8.5 | 3 | - | 3 | 3 |
| Manganese | - | 72 | - | - | - | - | 72 | - | - |
| Copper | $\overline{75}$ | 18 | - | - | - | $\overline{75}$ | 18 | $\overline{7}$ | $\overline{75}$ |
| Iron | 75 | - | 66.5 | 66.5 | 66.5 | 75 | - | 75 | 75 |
| Intermediate (wt.\%) |  |  |  |  |  |  |  |  |  |
| Nickel | - | - | - | - | - | - | - | 100 | 100 |
| Manganese | - | - | - | - | - | - | - | - | - |
| Low Expansive (wt.\%) |  |  |  |  |  |  |  |  |  |
| Nickel | 36 | 36 | 42 | 45 | 50 | 40 | 36 | 36 | 36 |
| Iron | 64 | 64 | 58 | 55 | 50 | 60 | 64 | 64 | 64 |
| Cobalt | - | - | - | - | - | - | - | - | - |
| Component Thickness Ratio (\%) |  |  |  |  |  |  |  |  |  |
| High Expansive | 50 | 53 | 50 | 50 | 50 | 50 | 80 | 27 | 34 |
| Intermediate | - | - | - | - | - | - | - | 46 | 32 |
| Low Expansive | 50 | 47 | 50 | 50 | 50 | 50 | 20 | 27 | 34 |
| Properties |  |  |  |  |  |  |  |  |  |
| Max. Sensitivity Temp. Range ( ${ }^{\circ} \mathrm{C}$ ) | -18-149 | -18-204 | 93-316 | 121-371 | 149-454 | 38-288 | -18-204 | -18-149 | -18-149 |
| Max. Recommended Temp. ( ${ }^{\circ} \mathrm{C}$ ) | 538 | 260 | 538 | 538 | 538 | 538 | 260 | 482 | 482 |
| Flexivity ( $\times 10^{-6}$ ) |  |  |  |  |  |  |  |  |  |
| $10-93{ }^{\circ} \mathrm{C}$ | 27.0* | 38.7* | $18.7{ }^{\dagger}$ | $15.1^{\dagger}$ | $11.3{ }^{\dagger}$ | 23.2* | $28.6{ }^{\text { }}$ | $20.2{ }^{\dagger}$ | $22.3{ }^{+}$ |
| $38-149^{\circ} \mathrm{C}$ | 26.3 * | 38.0 * | $19.1{ }^{\dagger}$ | $15.5{ }^{\dagger}$ | $11.5{ }^{\dagger}$ | 23.2* | $28.6{ }^{\ddagger}$ | $18.9{ }^{\dagger}$ | $22.9{ }^{\dagger}$ |
| Heat Treatment ( ${ }^{\circ} \mathrm{C}$ ) | 371 | 260 | 371 | 371 | 371 | 371 | 260 | 371 | 371 |
| Electrical Resistivity at $25^{\circ} \mathrm{C}(\mu \Omega \cdot \mathrm{m})$ | $0.790{ }^{5}$ | 1.12* | $0.732^{8}$ | $0.665{ }^{8}$ | $0.582^{*}$ | $0.73{ }^{8}$ | 1.41* | $0.166^{*}$ | $0.208{ }^{\circ}$ |
| Modulus of Elasticity (GPa) | 172 | 138 | 172 | 172 | 176 | 172 | 134 | 179 | 179 |
| Specific Heat [J/(kg $\cdot \mathrm{K}$ )] | 500 | 500 | 500 | 500 | 500 | 500 | 500 | 500 | 500 |
| Density ( $\mathrm{g} / \mathrm{cm}^{3}$ ) | 8.03 | 7.75 | 8.03 | 8.03 | 8.03 | 8.03 | 7.47 | 8.58 | 8.3 |
| * $\pm 5 \% \quad \dagger \pm 6 \% \quad \ddagger \pm 8 \% \quad \S \pm 4 \%$ | $\bigcirc \pm 5.5 \%$. |  |  |  |  |  |  |  |  |

