

- (3) aspects of modeling at the macro, meso, and micro levels ;
- (4) fiber-matrix interface properties and their integration in analytical models ;
- (5) behavior, analysis and modeling of cyclic and reversed cyclic response ;
- (6) computer modeling of material and structural response ;
- (7) manufacturing, production processes, and matrices compatible with high performance ;
- (8) rational testing and meaningful test standards ;
- (9) applications at the material and structural levels, and relationships between material properties and structural performance ;
- (10) applications in repair and rehabilitation ;
- (11) use of HPFRCC in combination with reinforcing bars and prestressing tendons ;
- (12) bond characteristics of bars and tendons with HPFRCCs ; and
- (13) research needs.

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Fig. 2 – During a discussion.

shop was sponsored by RILEM, and co-sponsored by the American Concrete Institute (ACI) and the NSF Center for Advanced Cement Based Materials (ACBM). Participation was primarily by invitation. In all 72 researchers and 13 students attended. About half the participants were from the

US and the other half from sixteen different countries, mostly from Europe. The next and third HPFRCC workshop is planned to take place in Stuttgart, Germany, in 1999.

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Errata

RILEM Draft Recommendation 'Creep and shrinkage prediction model for analysis and design of concrete structures-model B3' *Materials and Structures*, 28, (1995), 357-365.

- Eq. (20) on page 361 should read :

$$k_t = 190 \cdot 8t_0^{-0.08} f'_c{}^{-1/4} \text{ days in}^{-2}$$

(Exponent $-1/4$ correctly appeared in the proofs but was somehow lost afterwards)

- Eq. (A3) in appendix A on page 363 should read :

$$Q_f(t') = \left[0.086 (t')^{2/9} + 1.21 (t')^{4/9} \right]^{-1}$$

- The second equation in Eq. (B5) in appendix B on page 363 should read :

$$\frac{U_c}{R} = 110 \left[(w/c)(c) \right]^{-0.27} (f'_c)^{0.54}$$