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## Physiological effects of reduced tidal volume at constant minute ventilation and inspiratory flow rate in acute respiratory distress syndrome

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**Abstract Objective:** To assess the effect of changes in tidal volume ( $V_T$ ) with a constant inspiratory flow and minute ventilation ( $\dot{V}_E$ ) on gas exchange and oxygen transport in acute respiratory distress syndrome (ARDS).

**Design:** A crossover study of three  $V_T$  in two study groups, using patients as their own controls.

**Setting:** A medical-surgical intensive care unit in a tertiary care center.

**Patients:** Eight patients with ARDS and seven postoperative cardiac surgery patients with uncomplicated recoveries were studied during volume-controlled mechanical ventilation.

**Interventions:** During controlled mechanical ventilation, patients were first ventilated with a  $V_T$  of 9–11 ml/kg.  $V_T$  was then increased to 12–14 ml/kg (+25%) for 30 min and subsequently decreased to 6–8 ml/kg (–25%) for 30 min by adjusting the respiratory rate (RR) while the inspiratory flow rate,  $\dot{V}_E$ , and inspiratory duty cycle ( $T_L/T_{TOT}$ ) were kept constant. At the end, patients were ventilated with the baseline settings for another 30 min.

**Measurements and results:**  $V_E$ , carbon dioxide production ( $\dot{V}CO_2$ ) and

oxygen consumption ( $\dot{V}O_2$ ) were measured continuously with a gas exchange monitor, and cardiac output and arterial and mixed venous blood samples were taken at the end of each 30-min period to assess  $CO_2$  removal and oxygen transport. Alveolar minute ventilation ( $\dot{V}_A$ ) and the deadspace to tidal volume ratio ( $V_D/V_T$ ) were calculated from the Bohr equation. Despite large changes in  $V_T$ , arterial oxygenation ( $P_aO_2$ ) and oxygen transport ( $\dot{D}O_2$ ) were unchanged throughout the study. When  $V_T$  was increased, physiological  $V_D$  increased from  $448 \pm 34$  ml to  $559 \pm 46$  ml (mean  $\pm$  SE) in ARDS ( $P < 0.001$ ) and from  $281 \pm 22$  ml to  $357 \pm 35$  ml in CABG ( $P < 0.05$ ). With the small  $V_T$ ,  $V_D$  decreased to  $357 \pm 22$  ml in ARDS ( $P < 0.01$ ), and to  $234 \pm 24$  ml in CABG ( $P < 0.05$ ). In ARDS,  $V_D/V_T$  decreased from  $0.57 \pm 0.03$  to  $0.55 \pm 0.03$  ( $P < 0.05$ ) with the large  $V_T$ , and increased to  $0.60 \pm 0.03$  ( $P < 0.01$ ), when  $V_T$  was reduced. In CABG,  $V_D/V_T$  did not change significantly. ARDS patients had a higher  $P_aCO_2$  than cardiac patients ( $P < 0.001$ ), and only minor changes in  $P_aCO_2$  were observed (for ARDS and CABG respectively, baseline  $5.9 \pm 0.3$  kPa and

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$4.1 \pm 0.1$  kPa, large  $V_T$   $5.7 \pm 0.3$  kPa and  $4.1 \pm 0.2$  kPa, small  $V_T$   $6.2 \pm 0.3$  kPa and  $4.2 \pm 0.2$  kPa;  $P < 0.05$ ).

**Conclusions:** Tidal volumes can be reduced to 6–8 ml/kg in ARDS patients without compromising oxygen transport, while adequate  $\text{CO}_2$  elimination can be maintained.

**Key words** ARDS · Mechanical ventilation · Oxygen transport · Gas exchange · Respiratory deadspace · Tidal volume

## Introduction

The challenge in mechanical ventilatory support in ARDS is finding a balance between adequate gas exchange and oxygen transport, while preventing further lung damage. With conventional volume-cycled ventilation, a relatively large tidal volume ( $V_T$ ) has been used, while adjusting the respiratory rate to reach an acceptable arterial  $\text{PCO}_2$ , and  $\text{FIO}_2$  and positive end-expiratory pressure (PEEP) have been titrated to achieve appropriate arterial oxygenation [1]. This approach has been implicated in ventilator-induced lung injury because of the high peak-airway pressures often encountered [2]. In addition, overdistending the lung may reduce the perfusion of healthy alveoli and reduce cardiac output [3]. Alternative modes of ventilation, e.g., inverse ratio ventilation, pressure release ventilation and high-frequency ventilation, have recently been proposed to avoid these harmful effects [4, 5, 6]. However, the possibilities of the conventional volume controlled ventilation have not been fully explored. In an earlier study, we found that effective gas exchange may also be achieved by traditional volume controlled ventilation with simultaneously reduced  $V_T$  and flow rates [7]. The aim of this study was to assess the effect of an isolated  $V_T$  change with unaltered minute ventilation ( $\dot{V}_E$ ), inspiratory flow and ( $T_I/T_{TOT}$ ) on gas exchange and oxygen transport in the treatment of ARDS.

## Patients and methods

Eight patients with ARDS and a control group of seven patients requiring mechanical ventilation after coronary artery bypass surgery (CABG) were included in the study. All CABG patients had previously normal lungs. The patients with lung injury fulfilled the following clinical criteria for ARDS: a triggering event known to be associated with the development of ARDS, bilateral diffuse lung infiltrates in the chest X-ray,  $P_a\text{O}_2 < 8.0$  kPa on a  $\text{FIO}_2$  of at least 0.4 and PEEP higher than 5 cm  $\text{H}_2\text{O}$ , and no cardiogenic cause (confirmed by pulmonary artery catheterization) [1]. The ARDS group was studied  $5 \pm 1$  days (mean  $\pm$  SE, range: 1–8) after the diagnosis of ARDS was made and when the patients were hemodynamically stable. Hemodynamic stability was verified by normotension, normal peripheral capillary perfusion as evaluated clinically, and a pulmonary artery occlusion pressure of 8–12 mmHg. None of the patients had any signs of pulmonary

edema prior to the diagnosis of ARDS. The severity of the lung injury was assessed according to the scoring system described by Murray and associates [8]. The mean  $P_a\text{O}_2/\text{FIO}_2$  ratio was  $13.2 \pm 0.7$  kPa ( $99 \pm 5$  mmHg). Seven patients had a lung injury score equivalent to severe lung injury ( $\geq 2.5$ ), and one patient a score of 2.3 corresponding to mild-to-moderate lung injury. Three patients had a PEEP level equal to or exceeding 9 cm  $\text{H}_2\text{O}$ , and five patients had a PEEP below 9 cm  $\text{H}_2\text{O}$  (the cutoff limit for scores exceeding 2 for PEEP in the Murray scoring system). The PEEP level was selected according to the individual patient needs by the attending physician. The characteristics of the ARDS patients are presented in Table 1. The mean duration of mechanical ventilation at the time of the study was  $104 \pm 20$  hours (range: 35–192). The CABG group (6 male/1 female, ages =  $55 \pm 5$  years) was studied on the day of operation,  $5.9 \pm 0.4$  h after admission to the intensive care unit. The  $P_a\text{O}_2/\text{FIO}_2$  ratio was  $35.6 \pm 4.7$  kPa ( $267 \pm 35$  mmHg). Informed consent was obtained from the patient or, when appropriate, from the family. This study was approved by the Ethics Committee of the hospital.

All studies were conducted using the controlled mechanical ventilation mode of a Siemens Servo 900C ventilator (Siemens, Solna, Sweden) and square wave inspiratory flow. The ventilator settings are presented in Table 2. Slight hyperventilation was allowed in the CABG group to prevent an increase in the pulmonary vascular resistance in the early postoperative period (arterial  $\text{PCO}_2$   $4.1 \pm 0.1$  kPa). The baseline value of hemoglobin (Hb) was  $118 \pm 3$  g/l in ARDS and  $113 \pm 5$  g/l in CABG. No blood transfusions were given during the study. All patients were sedated with oxycodone and diazepam, and pancuronium or vecuronium was used for muscle relaxation. No spontaneous breathing efforts were observed clinically or from the airway pressure gauge or the trigger indicator of the ventilator. Gas exchange was monitored continuously, and when the minute-to-minute results were stable, data collection was started. After the baseline (baseline 1),  $V_T$  was first increased by 25% ( $1.25 V_T$ ), and reduced thereafter to 75% of the baseline  $V_T$  ( $0.75 V_T$ ). At the end, measurements were repeated with the baseline settings (baseline 2). The duration of each period was 30 min. The  $V_T$  was altered by changing the respiratory rate. Hence, in addition to the  $V_T$ , only the inspiratory time ( $T_I$ ) and the duration of the breath ( $T_{TOT}$ ) changed, whereas the inspiratory flow, inspiratory duty cycle ( $T_I/T_{TOT}$ ) and minute ventilation ( $\dot{V}_E$ ) were constant. The small variability of the measured  $\dot{V}_E$ , despite unchanged  $\dot{V}_E$  setting, reflects the combined variability of the measurement and the ventilator. Cardiac output ( $\dot{Q}$ ) was measured and blood samples were taken at the end of each period.  $\text{FIO}_2$  and PEEP were kept at the baseline levels throughout the study. Periods lasting 30 min were chosen since the study protocol was designed to assess the acute effects of a ventilatory change on gas exchange and oxygen transport. Body  $\text{CO}_2$  stores may not reach a steady state in this time, but the validity of the gas exchange measurement even in non-steady-state conditions has been shown previously [9]. The non-randomized order of changes in  $V_T$  was selected due to safety considerations. To minimize the risk of worsening pulmonary hypertension in ARDS, the higher  $V_T$  was tested first, because we believed this would result in a slightly lower starting  $P_a\text{CO}_2$  at the low  $V_T$ . Intrinsic PEEP (PEEP<sub>I</sub>) was assessed from the pressure manometer after

**Table 1** Characteristics of the ARDS patients. The lung injury score is calculated according to Murray et al. [8]

Age (years)	Sex	Days from ARDS diagnosis	Predisposing condition	Outcome	Lung injury score
34	M	6	Multiple fractures, fat embolism	Died	3.7
64	M	7	Emergency coronary bypass surgery	Survived	2.7
31	M	4	Pneumonia	Died	4.0
64	M	3	Perforated prepyloric ulcer, peritonitis	Survived	2.7
47	M	3	Flail chest, pulmonary contusion	Died	2.3
58	M	7	Acute pancreatitis	Died	2.7
36	M	1	Postoperative peritonitis	Survived	3.0
58	F	8	Pneumonia	Survived	2.7
49 ± 5		5 ± 1			3.0 ± 0.2

**Table 2** Ventilator settings (1.25  $V_T$   $V_T$  increased 25% from baseline; 0.75  $V_T$   $V_T$  decreased 25% from baseline,  $V_T$  tidal volume, RR respiratory rate, PEEP positive end-expiratory pressure,  $FIO_2$  fraction of oxygen in inspired air)

	$V_T$ (ml/kg)	RR (breaths/min)	PEEP (cm H <sub>2</sub> O)	$FIO_2$ (fraction)
<b>ARDS</b>				
Baseline <sup>a</sup>	9.3 ± 0.9	18.9 ± 1.6**	9.0 ± 1.6**	0.58 ± 0.03**
1.25 $V_T$	12.2 ± 1.4	14.8 ± 1.5**	9.0 ± 1.6**	0.58 ± 0.03**
0.75 $V_T$	7.0 ± 0.6	24.4 ± 1.6**	9.0 ± 1.6**	0.58 ± 0.03**
<b>CABG</b>				
Baseline	9.6 ± 0.2	12.1 ± 0.2	5.0 ± 0.0	0.43 ± 0.02
1.25 $V_T$	12.9 ± 0.3	8.8 ± 0.2	5.0 ± 0.0	0.43 ± 0.02
0.75 $V_T$	7.4 ± 0.3	15.6 ± 0.2	5.0 ± 0.0	0.43 ± 0.02

<sup>a</sup> Mean of the two measurements at baseline ventilator settings \*\* $P < 0.01$  (difference between patient groups)

occluding the expiratory port of the ventilator at end-expiratory using the built-in end-expiratory occlusion function of the ventilator.

$\dot{V}CO_2$ ,  $\dot{V}O_2$  and  $\dot{V}E$  were measured continuously with a gas exchange monitor (Deltatrac, Datex/Instrumentarium, Helsinki, Finland), which has been previously described in detail [10] and validated in this laboratory [11]. The relative error of the measurements under the study conditions is 5% [11–13]. The last 5 min of  $\dot{V}CO_2$  and  $\dot{V}O_2$  preceding each blood sampling were included in the data analysis. The coefficient of variation for  $\dot{V}CO_2$  and  $\dot{V}O_2$  was  $2.2 \pm 5\%$  and  $2.9 \pm 3\%$ , respectively. Cardiac output was measured in triplicate with 10 ml of room-temperature injectate (built-in cardiac output computer of the Kone 565 Patient Monitor, Kone Instruments, Helsinki, Finland) and the mean value used for calculations. Arterial and mixed venous blood samples were analyzed immediately after sampling. Blood gases were measured with a standard blood gas analyzer (IL 1302, Instrumentation Laboratories, Lexington, Mass.) and oxygen saturations with a co-oximeter (IL 282, Instrumentation Laboratories, Lexington, Mass.). Alveolar ventilation ( $\dot{V}_A$ ) was calculated as

$$\dot{V}_A = 0.115 * \dot{V}CO_2 / PaCO_2 \quad (1)$$

where  $\dot{V}_A$  is in liters per minutes, and STPD, and  $PaCO_2$ , in kilopascals. The ratio of physiologic dead space ( $V_D$ ) to  $V_T$  was calculated as  $V_D/V_T = 1 - \dot{V}_A/V_E$ . From this ratio and  $V_T$ ,  $V_D$  was obtained. This approach has been separately validated: a change in  $V_D$  can be measured with a relative error of  $8.2 \pm 4.7\%$ , when the change in  $V_D$  is 73–84 ml (9–16% of  $V_T$ ) [9]. Using this approach,  $V_A$  can also be measured in non-steady-state conditions. While the

body  $CO_2$  pool is changing, the measured  $\dot{V}CO_2$  still reflects the elimination of  $CO_2$  from the alveoli, but is not equal to the metabolic production of  $CO_2$ . The  $PaCO_2$  reflects the average or "ideal" alveolar  $CO_2$  at the time of sampling, and  $\dot{V}_A$ ,  $V_D$ , and  $V_D/V_T$  can be calculated, providing the temporal relationship between the  $PaCO_2$  sample and the measured  $\dot{V}CO_2$  is preserved [9]. Arterial and mixed venous oxygen contents ( $CaO_2$ ,  $C\bar{v}O_2$ ) were calculated from the hemoglobin values (hemoglobin oxygen saturations and partial pressures). Oxygen delivery ( $\dot{D}O_2$ ) was calculated as  $\dot{D}O_2 = \dot{Q} * CaO_2$ , and venous admixture as  $\dot{Q}_s/\dot{Q}_T = (C\bar{c}O_2 - CaO_2)/(C\bar{c}O_2 - C\bar{v}O_2)$ , where  $C\bar{c}O_2$  is the calculated oxygen content of the pulmonary end-capillary blood [14].

#### Statistical analysis

The two baseline periods were first compared by a paired  $t$ -test to confirm the stability of the patients' condition during the measurement. The mean value of data obtained at the two baseline periods was used to represent the baseline value in the subsequent analysis. Changes in the respiratory and oxygen transport variables were assessed with two-way analysis of variance for repeated measures (procedure MANOVA, SPSS/PC +) [15] using one grouping factor (study group) and one within subject factor ( $V_T$ ). When significant effects of  $V_T$  or group- $V_T$  interactions were observed, these were located post hoc by a paired  $t$ -test for comparisons between baseline vs large and small  $V_T$  within each group, and an unpaired  $t$ -test for between-group comparisons at each  $V_T$  level [15]. The relationship between  $V_T$  and  $V_D$  was assessed with regression analysis [15]. All

**Table 3** Alveolar ventilation and CO<sub>2</sub> elimination<sup>a</sup> ( $V_D$  physiological dead space,  $V_D/V_T$  physiological dead space to tidal volume ratio,  $\dot{V}_E$  minute ventilation,  $\dot{V}_A$  alveolar ventilation;  $\dot{V}CO_2$  CO<sub>2</sub> production,  $P_aCO_2$  CO<sub>2</sub> partial pressure in arterial blood)

	$V_T$ (ml)	$V_D$ (ml)	$V_D/V_T$ (fraction)	$\dot{V}_E$ (l/min)	$\dot{V}_A$ (l/min)	$\dot{V}CO_2$ (ml kg <sup>-1</sup> min <sup>-1</sup> )	$P_aCO_2$ (kPa)
<b>ARDS</b>							
Baseline	794 ± 66	448 ± 34 <sup>d</sup>	0.57 ± 0.03 <sup>e</sup>	14.3 ± 0.6 <sup>e</sup>	6.1 ± 0.4	3.5 ± 0.1 <sup>e</sup>	5.9 ± 0.3 <sup>e</sup>
1.25 $V_T$	1052 ± 107 <sup>b</sup>	559 ± 46 <sup>cd</sup>	0.55 ± 0.03 <sup>ue</sup>	14.5 ± 0.6 <sup>e</sup>	6.6 ± 0.5	3.6 ± 0.1 <sup>e</sup>	5.7 ± 0.3 <sup>d</sup>
0.75 $V_T$	602 ± 43 <sup>b</sup>	357 ± 22 <sup>bd</sup>	0.60 ± 0.03 <sup>bc</sup>	14.2 ± 0.5 <sup>e</sup>	5.7 ± 0.4	3.4 ± 0.1 <sup>be</sup>	6.2 ± 0.3 <sup>bc</sup>
<b>CABG</b>							
Baseline	782 ± 43	281 ± 22	0.36 ± 0.02	9.5 ± 0.5	6.1 ± 0.4	2.6 ± 0.1	4.1 ± 0.1
1.25 $V_T$	1056 ± 59 <sup>c</sup>	357 ± 35 <sup>a</sup>	0.34 ± 0.02	9.3 ± 0.6	6.1 ± 0.4	2.7 ± 0.1	4.1 ± 0.2
0.75 $V_T$	605 ± 44 <sup>c</sup>	234 ± 24 <sup>a</sup>	0.38 ± 0.02	9.4 ± 0.6	5.8 ± 0.4	2.6 ± 0.1 <sup>a</sup>	4.2 ± 0.2

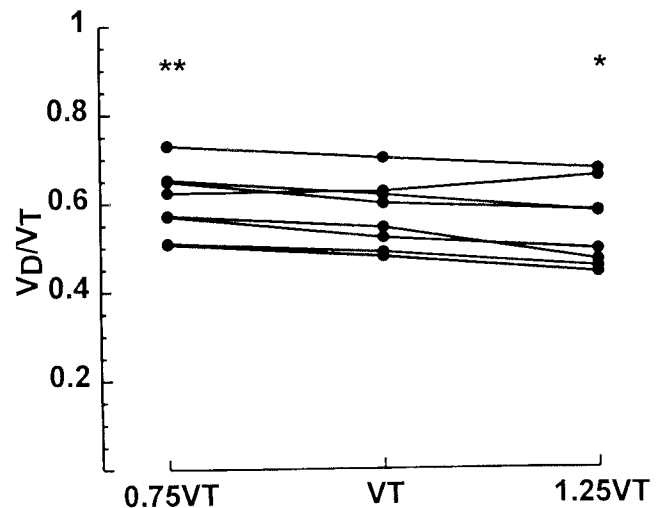
Analysis of variance: effect of  $V_T$ :  $V_D$  and  $\dot{V}_A$ ,  $P < 0.001$ ,  $V_D/V_T$  and  $\dot{V}CO_2$ ,  $P < 0.01$ , and  $P_aCO_2$ ,  $P < 0.05$ ; difference between patient groups:  $V_D/V_T$ ,  $\dot{V}_E$ ,  $\dot{V}CO_2$ ,  $P_aCO_2$ ,  $P < 0.001$ ,  $V_D$ ,  $p < 0.01$ ; post hoc t-tests: differences from baseline within groups: <sup>a</sup> $P < 0.05$ , <sup>b</sup> $P < 0.01$ , <sup>c</sup> $P < 0.001$ ; difference between diagnostic groups: <sup>d</sup> $P < 0.01$ , <sup>e</sup> $P < 0.001$

data are given as mean ± SE, and a  $P$ -value  $< 0.05$  was considered significant.

## Results

Table 3 shows the parameters of alveolar ventilation and CO<sub>2</sub> elimination. At baseline,  $\dot{V}_E$  was 51% higher in ARDS than in CABG ( $P < 0.001$ ). This was due to both a higher CO<sub>2</sub> production and  $V_D/V_T$  ( $P < 0.001$  for  $\dot{V}CO_2$  and  $V_D/V_T$ ) in the ARDS patients. Baseline  $P_aCO_2$  was also significantly higher in the ARDS patients than in the CABG group ( $P < 0.001$ ).

Table 3 also presents the alveolar ventilation variables obtained in both the ARDS and CABG patients with the different  $V_T$ s. These can be interpreted in terms of Eq. (1). In both ARDS and CABG, physiological  $V_D$  ( $V_D$  phys) increased when  $V_T$  was increased, and decreased with the small  $V_T$  ( $P < 0.001$ ). Changes in  $V_D/V_T$  ( $P < 0.01$ ) were small. Despite the large increase in  $V_T$  at 1.25  $V_T$ ,  $V_D/V_T$  decreased only marginally in ARDS ( $P < 0.05$ ). At the small  $V_T$ ,  $V_D/V_T$  increased in seven ARDS patients, and decreased in one ( $P < 0.01$ ; Fig. 1). No significant change in  $V_D/V_T$  was observed in CABG.  $V_D/V_T$  was higher in ARDS, reflecting a higher  $V_D$  ( $P < 0.01$ ).  $V_D$  correlated with  $V_T$  in both ARDS and CABG (Fig. 2). The changes in  $V_A$  were small and variable when  $V_T$  was changed, and only minor overall changes in  $P_aCO_2$  were observed (analysis of variance  $P < 0.05$ ).  $\dot{V}CO_2$  was reduced at 0.75  $V_T$  ( $P < 0.01$ ), and marginally also at the second baseline measurement in ARDS ( $3.6 \pm 0.2$  ml kg<sup>-1</sup> min<sup>-1</sup> at the first baseline vs  $3.5 \pm 0.1$  ml kg<sup>-1</sup> min<sup>-1</sup> at the second baseline:  $P < 0.05$ ), reflecting the non-steady-state conditions during the 30-min observation periods. For other

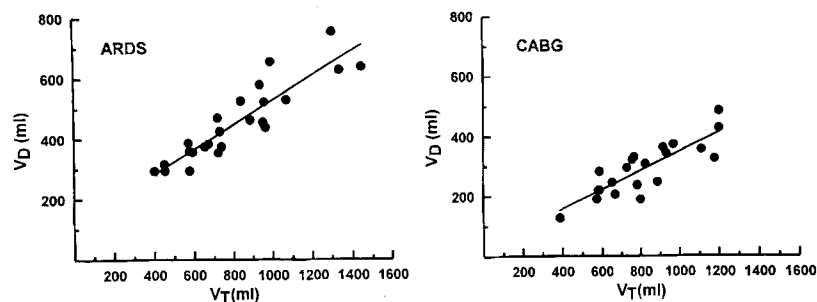


**Fig. 1** Individual  $V_D/V_T$  responses in ARDS.  $V_T$  baseline ventilator settings; 0.75  $V_T$   $V_T$  decreased by 25% from baseline settings; 1.25  $V_T$   $V_T$  increased 25% from baseline settings. \* $P < 0.05$ , \*\* $P < 0.01$ , compared with baseline

measured variables, no significant difference between the two baseline periods were observed.

Table 4 shows the oxygen transport variables during the study. Despite large changes in  $V_T$ ,  $\dot{Q}$  was unchanged throughout the study in both groups. Consequently,  $\dot{D}O_2$  did not change significantly. However, major changes were observed in some patients. The individual changes in  $\dot{D}O_2$  in ARDS are shown in Fig. 3. A trend of higher  $\dot{D}O_2$  with the smaller  $V_T$ s can be observed (Fig. 3). Despite the lower  $P_aO_2$ ,  $\dot{D}O_2$  was higher in the ARDS patients than in the CABG group due to the higher  $\dot{Q}$  ( $P < 0.01$ ). At baseline,  $CaO_2$  was  $144 \pm 4$  ml/l in ARDS and  $156 \pm 6$  ml/l in CABG (NS), and no change was observed during the study. Similarly, there was no difference in the mixed venous

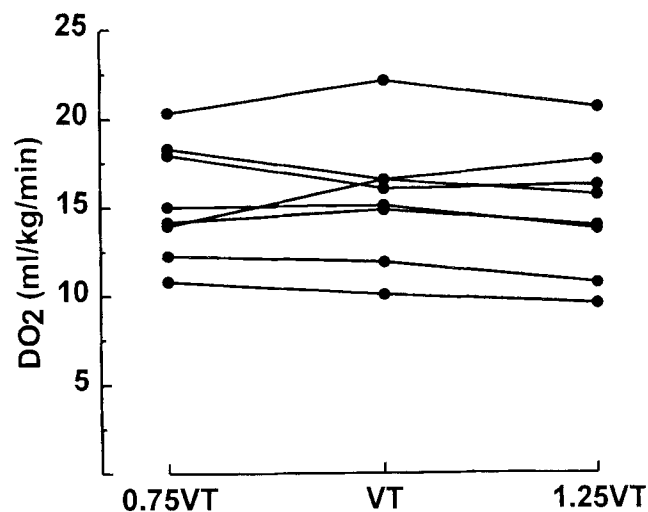
**Fig. 2** The relationship between  $V_T$  and  $V_D$ . In ARDS,  $V_D = 0.41 * V_T + 119$ ;  $r^2 = 0.82$  ( $P < 0.001$ ). In CABG,  $V_D = 0.32 * V_T + 31$ ;  $r^2 = 0.70$  ( $P < 0.001$ )



**Table 4** Oxygen transport ( $\dot{Q}$  cardiac output,  $\dot{D}O_2$  oxygen delivery,  $P_{aO_2}$ ,  $P_{vO_2}$   $O_2$  partial pressure in arterial and mixed venous blood,  $\dot{Q}_s/\dot{Q}_T$  fraction of venous admixture,  $\dot{V}O_2$  oxygen consumption)

	$\dot{Q}$ ( $l \cdot m^{-2} \cdot \min^{-1}$ )	$\dot{D}O_2$ ( $ml \cdot kg^{-1} \cdot \min^{-1}$ )	$P_{aO_2}$ (kPa)	$P_{vO_2}$ (kPa)	$\dot{Q}_s/\dot{Q}_T$ (fraction)	$\dot{V}O_2$ ( $ml \cdot kg^{-1} \cdot \min^{-1}$ )
<b>ARDS</b>						
Baseline	$4.7 \pm 0.3^b$	$15.5 \pm 1.3^b$	$8.1 \pm 0.5^c$	$5.2 \pm 0.3$	$0.48 \pm 0.02^c$	$3.8 \pm 0.2^a$
1.25 $V_T$	$4.5 \pm 0.4^b$	$14.9 \pm 1.3^a$	$8.5 \pm 0.5^b$	$5.2 \pm 0.3$	$0.46 \pm 0.03^c$	$3.7 \pm 0.2^a$
0.75 $V_T$	$4.9 \pm 0.3^b$	$15.4 \pm 1.1^b$	$7.9 \pm 0.5^c$	$5.3 \pm 0.3$	$0.51 \pm 0.03^c$	$3.8 \pm 0.2^a$
<b>CABG</b>						
Baseline	$3.0 \pm 0.3$	$10.6 \pm 0.9$	$15.1 \pm 1.2$	$4.7 \pm 0.2$	$0.18 \pm 0.03$	$3.3 \pm 0.2$
1.25 $V_T$	$3.1 \pm 0.3$	$10.8 \pm 0.9$	$14.7 \pm 1.7$	$4.7 \pm 0.2$	$0.18 \pm 0.03$	$3.2 \pm 0.1$
0.75 $V_T$	$3.1 \pm 0.3$	$11.0 \pm 0.8$	$14.4 \pm 1.0$	$4.7 \pm 0.2$	$0.19 \pm 0.03$	$3.3 \pm 0.1$

Analysis of variance: effect of  $V_T$ : not significant for any variable; difference between patient groups:  $P_{aO_2}$  and  $\dot{Q}_s/\dot{Q}_T$ ,  $P < 0.001$ ,  $\dot{Q}$ ,  $P < 0.01$ ,  $\dot{D}O_2$  and  $\dot{V}O_2$ ,  $P < 0.05$ ; post hoc t-tests: difference between diagnostic groups:  $^a P < 0.05$ ,  $^b P < 0.01$ ,  $^c P < 0.001$



**Fig. 3** Individual responses of oxygen delivery to changes in  $V_T$  in ARDS.  $V_T$  baseline ventilator settings; 0.75  $V_T$   $V_T$  decreased by 25% from baseline settings; 1.25  $V_T$   $V_T$  increased 25% from baseline settings

$O_2$  contents throughout the study ( $110 \pm 4$  ml/l in ARDS and  $109 \pm 7$  ml/l in CABG at baseline, respectively). There were no significant changes in  $P_{aO_2}$  during the experiment in either group. Arterial oxygen

saturation ( $S_aO_2$ ) tended to increase marginally in ARDS with the large  $V_T$  ( $86 \pm 1\%$ ,  $88 \pm 2\%$ , and  $86 \pm 1\%$ , for baseline, and the large and the small  $V_T$ , respectively, NS), whereas it remained unchanged at  $97 \pm 1\%$  in the CABG patients. This was associated with minor but consistent changes in arterial pH at the different  $V_T$  levels ( $P < 0.05$ ; for ARDS:  $7.384 \pm 0.016$ ,  $7.395 \pm 0.021$ , and  $7.370 \pm 0.014$ ; for CABG:  $7.469 \pm 0.019$ ,  $7.470 \pm 0.017$ , and  $7.461 \pm 0.018$ , for baseline and the large and the small  $V_T$ , respectively;  $P < 0.01$  for ARDS vs CABG, and  $P < 0.05$  for large  $V_T$  vs baseline in ARDS).

Intrinsic PEEP ( $PEEP_i$ ) was  $2.4 \pm 1.2$  cm  $H_2O$  in ARDS, and  $0.3 \pm 0.3$  cm  $H_2O$  in CABG ( $P < 0.05$ ). No changes were observed during the study in either group.

## Discussion

The main observations following large changes in  $V_T$  with a constant  $\dot{V}_E$  and inspiratory flow were a well-maintained gas exchange and oxygen transport at the low  $V_T$ , and that the  $V_T$  can be changed over a wide range without detrimental effect on arterial oxygenation.

In our earlier study, where  $V_T$  changes were accompanied by concomitant changes in  $\dot{V}_E$  and inspiratory flow,  $\dot{Q}$  and  $\dot{D}O_2$  were inversely related to  $V_T$  [7]. In contrast, in the present study,  $\dot{Q}$  and  $\dot{D}O_2$  did not change despite substantial changes in  $V_T$ . However, a trend to improved  $\dot{D}O_2$  at the low  $V_T$  was observed: five ARDS patients had the highest  $\dot{D}O_2$  at the lowest  $V_T$ , and the lowest  $\dot{D}O_2$  at the large  $V_T$ . The hemodynamic effects of mechanical ventilation are largely determined by the effect on mean airway pressure ( $P_{aw,mean}$ ) [16]. Since respiratory mechanics were not measured, we estimated the effects of a  $V_T$  change on the  $P_{aw,mean}$  by the formula presented by Marini:  $P_{aw,mean} = (R_I \dot{V} / 60 + V_T / 2C + PEEP) * T_I / T_{TOT} + PEEP * T_E / T_{TOT}$ , where  $R_I$ ,  $\dot{V}$ ,  $C$  and  $PEEP$  represent inspiratory resistance, flow, compliance and end-expiratory pressure. Assuming  $R_I$  and  $C$  values typical of ARDS (e.g.  $R_I = 4.5$  cm H<sub>2</sub>O/L/s,  $C = 25$  ml/cm H<sub>2</sub>O,  $PEEP = 10$ ,  $T_I / T_{TOT} = 0.35$ , baseline  $V_T = 800$  ml, and a frequency of 19 breaths/min), changes in  $V_T$  such as in the present study can be expected to alter  $P_{aw,mean}$  by only 6% in either direction. This probably explains the lack of significant hemodynamic alterations. In contrast, when the  $\dot{V}_E$  is altered in parallel with  $V_T$ , changes in  $P_{aw,mean}$  are much larger, and most likely explain the difference between the present findings and the quite substantial hemodynamic changes found in our previous study. Similarly, Leatherman and coworkers [17] found an increase in cardiac output, when  $V_T$  together with  $\dot{V}_E$  and  $T_I$  was decreased at high PEEP levels.

When  $V_T$  is increased, a proportional increase in  $\dot{V}_A$  may be expected. However, the change in  $\dot{V}_A$  is attenuated by the concomitant change in  $V_D$ . No significant effect on  $\dot{V}_A$  was observed in the current study, whereas  $\dot{V}_A$  followed the changes in  $V_T$  when  $\dot{V}_E$  was concomitantly changed [7]. We have previously shown a correlation between  $V_D$  and  $V_I$  in ARDS with changing  $\dot{V}_E$  and inspiratory flow.

The  $V_D/V_T$  ratio was unchanged over a wide range of  $V_T$ s [7]. A similar relationship between  $V_D$  and  $V_T$  has been shown by Cooper in mechanically ventilated anesthetized patients with normal lungs [18]. Also, Severinghaus and Stupfel, in a study on anesthetized dogs showed that  $V_{Dphys}$  correlates with  $V_T$  [19]. In their study, the relative contribution of alveolar  $V_D(V_{Dalv})$  to the physiological  $V_D$  increased with in-

creasing  $V_T$ , but  $V_D/V_T$  was affected little by  $V_T$  changes. In the present study,  $V_{Dphys}$  increased markedly with increasing  $V_T$ , but the  $V_D/V_T$  was slightly reduced in ARDS, indicating that the  $V_{Dphys}$  increased somewhat less than the  $V_T$ . Similarly, when  $V_T$  was decreased to the lowest level, the small increase in the  $V_D/V_T$  demonstrates that the  $V_{Dphys}$  decreased slightly less than the  $V_T$ . The full effect of the consequent decrease in  $\dot{V}_A$  on  $P_aCO_2$  at the small  $V_T$  was not evident in the 30-min observation period, as a steady state was not achieved in the gas exchange. At this point, the  $P_aCO_2$  was marginally higher than at baseline (6.2 at 0.75  $V_T$  vs 5.9 kPa at baseline), and no untoward hemodynamic effects were observed. However, if the metabolic  $CO_2$  production is assumed to remain unchanged from baseline, the  $P_aCO_2$  at a steady state would have reached  $6.4 \pm 0.3$  kPa, still only slightly higher than with the baseline  $V_T$ . Thus, an increase in  $P_aCO_2$ , secondary to the reduced  $V_T$ , is counteracted by the concomitant reduction in  $V_D$ .

Large  $V_T$ s (12–15 ml/kg), previously in common use, also increase the risk of barotrauma in the lung. Kolobow and coworkers demonstrated the connection of large  $V_T$ s and high transpulmonary pressures with worsening of lung injury [2]. In ARDS, normoventilation can be maintained only at alveolar pressure that could damage the lung. Several studies have suggested that in ARDS, decrease of peak airway pressure and minimizing lung overdistention should be the primary goals. This may be accomplished by decreasing  $\dot{V}_E$  and  $V_T$ , and consequently also  $\dot{V}_A$ . In retrospective studies, moderate, permissive hypercapnia has been associated with lesser lung injury and has enhanced survival in status asthmaticus [20] and ARDS [21]. According to the findings in the present study, a substantial decrease in  $V_T$  will induce only a modest increase in  $P_aCO_2$ .  $V_T$  can be decreased without impairing arterial oxygenation and  $\dot{D}O_2$ .

In conclusion, our results indicate that tidal volumes can be reduced in the treatment of severe hypoxemia without impairing oxygenation. The reduction in  $V_D$  together with  $V_T$  will minimize the effect of  $V_T$  reduction on  $\dot{V}_A$ .

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