# THE MARTIAN MEAN MOMENT-OF-INERTIA AND THE SIZE OF THE MARS' CORE 

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#### Abstract

The mean moment-of-inertia ratio, $I / M R^{2}$, of Mars cannot be derived from its precessional constant because the exact value of the Martian axial precession is unknown presently. Using the known geodetic parameters of Mars as the constrained condition, we constructed nine Martian internal structure models (see Table II). We can then estimate the nonhydrostatic components of the principal moment-of-inertia for these models. The interplanetary comparison suggests that the reasonable range of the mean moment-of-inertia ratio, $I / M R^{2}$, of Mars is $0.350 \sim 0.360$, and the range of the corresponding radius of Mars' core is $1520 \sim 1850 \mathrm{~km}$. The two parameterically simple models recommended in this paper (see Table IV) can be used for reference in the future theoretical researches.


## 1. Introduction

As the Soviet spacecraft mission to Phobos (1988/07) and the US Mars Observer mission (1992/09/25) were achieved in succession, there has been renewed interest recently in researches on the dynamics of Martian rotation. Lately, there are a series of papers dealing with the problems of the mean moment-of-inertia ratio, I/MR ${ }^{2}$, of Mars (Bills, 1989, 1990; Kaula et al., 1989; Kaula and Asimow, 1991), the constructions of the Martian internal structure models (Bills, 1990; Zharkov et al., 1991; Severova, 1992), and the theory of the Mars' pole motion (Hilton, 1990, 1991), etc.

The mean moment-of-inertia ratio, $I / M R^{2}$, is one of the important parameters of a planet. When we study the problems on the dynamics of Martian rotation, it is necessary to adopt the correct value of $I / M R^{2}$.

The major objective of the paper is to construct a set of internal structure models of Mars by comparing Mars with the Earth, the Moon, and the terrestrial planets, then to discuss the likely range of the size of Mars' core, and to check whether the adopted value of $I / M R^{2}$ for Mars is reasonable.

## 2. Two-Layer Model of Density Distribution

The density in the Mars' interior is assumed to have the form (cf. Zhang and Shen, 1988)

$$
\rho(x)= \begin{cases}\rho_{0}\left(1-c_{0} x^{2}\right), & 0 \leqslant x \leqslant x_{c}  \tag{1}\\ \rho_{m}, & x_{c} \leqslant x \leqslant 1\end{cases}
$$

where $\rho_{0}$ and $c_{0}$ are two positive constants; $\rho_{0}$ is the central density of Mars, $\rho_{m}$
the density of the mantle and considered as a parameter in the following discussions; $x=r / R$ is the relative radius, and $x_{c}=r_{c} / R$ is the relative radius of the core.

In this case, it is easy to see that the mean density and mean moment-of-inertia ratio $/ / M R^{2}$ have the following expression, respectively

$$
\left.\begin{array}{l}
\bar{\rho}=3 \int_{0}^{x_{c}} \rho_{0}\left(1-c_{0} x^{2}\right) x^{2} \mathrm{~d} x+3 \int_{x_{c}}^{1} \rho_{m} x^{2} \mathrm{~d} x  \tag{2}\\
\frac{I}{M R^{2}}=\frac{2}{\bar{\rho}}\left[\int_{0}^{x_{c}} \rho_{0}\left(1-c_{0} x^{2}\right) x^{4} \mathrm{~d} x+\int_{x_{c}}^{1} \rho_{m} x^{4} \mathrm{~d} x\right] .
\end{array}\right\}
$$

Let us assume that the density of the core-mantle bound is $\rho_{C M B}$. Obviously $\rho_{C M B} \geqslant \rho_{m}$ hold true. Introducing the quantity $\Delta \rho=\rho_{C M B}-\rho_{m} \geqslant 0$, we derive easily from Equation (2)

$$
\begin{equation*}
\frac{I}{M R^{2}}=\frac{2}{5} \frac{1}{\bar{\rho}}\left[\frac{5}{7} x_{c}^{2}\left(\bar{\rho}-\rho_{m}\right)+\frac{2}{7} x_{c}^{5} \Delta \rho\right]+\frac{2}{5} \frac{\rho_{m}}{\bar{\rho}} \tag{3}
\end{equation*}
$$

or

$$
\begin{equation*}
\frac{I}{M R^{2}}=\frac{2}{35} \frac{1}{\bar{\rho}} x_{c}^{5}\left[2\left(\rho_{0}-\rho_{m}\right)+5 \Delta \rho\right]+\frac{2}{5} \frac{\rho_{m}}{\bar{\rho}} \tag{4}
\end{equation*}
$$

Equations (3) and (4) can be used for estimating the range of the value of $I / M R^{2}$ for Mars. In the calculations, the mean density $\tilde{\rho}$ is taken as $3.933497 \mathrm{~g} \mathrm{~cm}^{-3}$, and the accepted value of $\Delta \rho$ is equal to $4.5 \mathrm{~g} \mathrm{~cm}^{-3}$.

Figure 1 illustrates the dependence of $I / M R^{2}$ on $x_{c}$ (Figure 1a) and on $\rho_{0}$ (Figure 1b) respectively for a set of the parameters $\rho_{m}\left(3.20 \sim 3.50 \mathrm{~g} \mathrm{~cm}^{-3}\right)$. We took $x_{c}=$ 0.5 in the calculation of the variation of $I / M R^{2}$ with $\rho_{0}$. The curves in Figure 1 are labeled according to the corresponding value of $\rho_{m}$.

It is concluded from Figure 1 that the influence of the variations of $x_{c}$ on $I / M R^{2}$ is obvious (when $\rho_{m}$ is given), and the influence of the variations of $\rho_{0}$ on $I / M R^{2}$ is slight (when $\rho_{m}$ and $x_{c}$ are given). When $x_{c}$ is given, it is necessary to adjust simultaneously the values of $\rho_{0}$ and $\rho_{m}$ in order that the value of $I / M R^{2}$ may be changed between 0.345 and 0.365 .

## 3. Estimation of the Physical Parameters of Mars

Let us assume that the Martian interior (core and mantle) is in the hydrostatic equilibrium state, and the bulk modulus $K(r)$ and the pressure $p(r)$ satisfy the following linear relation

$$
\begin{equation*}
K(r)=K_{0}+b p(r) \tag{5}
\end{equation*}
$$



Fig. 1. Dependence of the $/ / M R^{2}$ value on $r_{c} / R$ (a) and on $\rho_{0}$ (b).
where both $K_{0}$ and $b$ are two positive constants. We refer to those of the Earth's and lunar models (cf. Zhang, 1992) and adopt $K_{0}$ and $b$ values for Mars. The values of $K_{0}, b$, and $\sigma$ (Poisson's ratio) used in construction of the Martian models are listed in Table I.

Using the results of simplified two-layer model in the preceding section and the known geodetic parameters of Mars, we constructed nine Martian internal structure models (see Table II) by solving the Emden equation (e.g. Shen and Zhang, 1988; Zhang, 1992). In these models the thickness of the Martian crust is taken as 180 km .

The nine Martian models may be divided into two groups. The first group

TABLE I
Values, $K_{0}, b$, and $\sigma$, used in construction of Martian models

| Zone | $K_{0}\left(10^{3} \mathrm{kbar}\right)$ | $b$ | $\sigma$ |
| :--- | :--- | :--- | :--- |
| Core | 2.0 | 4.0 | 0.34 |
| Mantle | 2.3 | 3.25 | 0.30 |

consists of five models, MARS 93-01~93-05, in which the central density is taken as $7.76 \mathrm{~g} \mathrm{~cm}^{-3}$. When $x_{c}$ is taken from 0.55 to 0.46 and the mean mantle density, $\bar{\rho}_{m}$, increases from $3.25 \mathrm{~g} \mathrm{~cm}^{-3}$ to $3.64 \mathrm{~g} \mathrm{~cm}^{-3}$, the value of $I / M R^{2}$ increases from 0.346 to 0.365 , and the relative mass, $M_{c} / M$, of the core decreases from 0.321 to 0.182 . The second group comprises MARS 93-05~93-09, in which the relative radius, $x_{c}$, of the core is about equal to 0.45 . When the central density, $\rho_{0}$, increases from $7.76 \mathrm{~g} \mathrm{~cm}^{-3}$ to $11.00 \mathrm{~g} \mathrm{~cm}^{-3}$ and $\bar{\rho}_{m}$ is taken from $3.64 \mathrm{~g} \mathrm{~cm}^{-3}$ to $3.43 \mathrm{~g} \mathrm{~cm}^{-3}$, the value of $I / M R^{2}$ decreases from 0.365 to 0.345 , and $M_{c} / M$ increases from 0.182 to 0.229 .

Figure 2 illustrates the relation between the relative mass, $M_{c} / M$, of the core and the relative radius, $r_{c} / R$, of the core for the Martian models. In Figure 2 the symbol " $\oplus$ " represents the corresponding values of the Earth's model PREM.

In short, with the reduction of the value of $I / M R^{2}$, the mean mantle density, $\overline{\rho_{m}}$, certainly decreases (cf. Zharkov et al., 1991).

If $A<B<C$ denote three principal moment-of-inertia of Mars, and $\delta A, \delta B$, $\delta C$ are, respectively, the minimum, intermediate, and maximum nonhydrostatic components of the moment-of-inertia, the observed value of $J_{2}$, one of the Stokes coefficients of degree two, can be divided into two parts, namely,

$$
\begin{equation*}
J_{2}=J_{2}^{(0)}+\delta J_{2} \tag{6}
\end{equation*}
$$

where $J_{2}^{(0)}=1 / M R^{2}\left[C-\frac{1}{2}(A+B)\right]$ is the hydrostatic value of $J_{2}$, and $\delta J_{2}$ is the non-hydrostatic component. Hence (cf. Zharkov et al., 1991),

$$
\begin{align*}
& \delta J_{2}=\frac{1}{M R^{2}}\left[\delta C-\frac{1}{2}(\delta A+\delta B)\right]  \tag{7}\\
& J_{22}=\frac{1}{4 M R^{2}}(\delta B-\delta A) \tag{8}
\end{align*}
$$

where $J_{22}$ is another of the Stokes coefficients of degree two.
Following Bills (1989), we introduce the quantity

$$
\begin{equation*}
\delta f=\frac{\delta B-\delta A}{\delta C-\delta A} \tag{9}
\end{equation*}
$$

and may derive the expression,
TABLE II

| Zone | Parameter | Model |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 93-01 | 93-02 | 93-03 | 93-04 | 93-05 | 93-06 | 93-07 | 93-08 | 93-09 |
| Core | $\rho_{0}\left(\mathrm{~g} \mathrm{~cm}^{-3}\right)$ | 7.760 | 7.760 | 7.760 | 7.760 | 7.760 | 8.900 | 9.710 | 10.370 | 11.00 |
|  | $p_{0}$ (kbar) | 470.00 | 465.00 | 450.00 | 445.00 | 410.00 | 460.00 | 500.00 | 542.00 | 580.00 |
|  | $r_{c}(\mathrm{~km})$ | 1875.93 | 1855.08 | 1750.87 | 1730.02 | 1563.27 | 1542.43 | 1521.59 | 1521.59 | 1500.74 |
|  | $\rho\left(r_{c}\right)\left(\mathrm{g} \mathrm{cm}^{-3}\right)$ | 7.242 | 7.005 | 7.197 | 6.760 | 6.987 | 7.871 | 8.491 | 8.876 | 9.971 |
|  | $M_{c} / M$ | 0.321 | 0.304 | 0.260 | 0.242 | 0.182 | 0.198 | 0.206 | 0.218 | 0.229 |
| Mantle | $\rho\left(r_{c}\right)\left(\mathrm{g} \mathrm{cm}^{-3}\right)$ | 3.368 | 3.425 | 3.549 | 3.617 | 3.792 | 3.689 | 3.639 | 3.585 | 3.537 |
|  | $\rho\left(r_{m}\right)\left(\mathrm{g} \mathrm{cm}^{-3}\right)$ | 3.172 | 3.222 | 3.325 | 3.385 | 3.526 | 3.426 | 3.374 | 3.324 | 3.274 |
|  | $\overline{\rho_{m}}\left(\mathrm{~g} \mathrm{~cm}^{-3}\right)$ | 3.254 | 3.307 | 3.418 | 3.482 | 3.636 | 3.550 | 3.515 | 3.461 | 3.426 |
| Shell | $\rho_{\text {S2 }}\left(\mathrm{g} \mathrm{cm}^{-3}\right)$ | 3.150 | 3.200 | 3.320 | 3.381 | 3.400 | 3.400 | 3.350 | 3.300 | 3.150 |
|  | $\rho_{S 1}\left(\mathrm{~g} \mathrm{~cm}^{-3}\right)$ | 2.850 | 2.950 | 2.906 | 2.955 | 2.900 | 2.900 | 2.900 | 2.900 | 2.850 |
| Total | $I / M R^{2}$ | 0.34653 | 0.34996 | 0.35501 | 0.35909 | 0.36549 | 0.35904 | 0.35489 | 0.35102 | 0.34528 |
|  | $\bar{\rho}\left(\mathrm{g} \mathrm{cm}^{-3}\right)$ | 3.93342 | 3.93347 | 3.93346 | 3.93348 | 3.93346 | 3.93345 | 3.93348 | 3.93344 | 3.93350 |



Fig. 2. Relation between the relative mass $M_{c} / M$ and the relative radius $r_{c} / R$ of the core for the Martian models.

$$
\begin{equation*}
\delta f=\frac{4 J_{22}}{\delta J_{2}+2 J_{22}}, \tag{10}
\end{equation*}
$$

from Equations (7) ~ (9).
In the nine Martian models we choose five models - $93-01,93-03,93-05,93-07$, and $93-09$, and the profile of the flattening, $e(r)$, in the Mars' interior for these models can be obtained from solving numerically the Clairaut equation (cf. Zhang, 1993). Then the values of $J_{2}^{(0)}$ and $\delta f$ can be determined. In the calculations, the accepted values of $J_{2}$ and $J_{22}$ are equal to $1960.45 \times 10^{-6}$ and $63.098 \times 10^{-6}$, respectively (Balmino et al., 1982). The results obtained are listed in Table III.
At present, the values of $\delta f$ are well known for the Moon (0.361), the Earth ( 0.579 ), and Venus ( 0.490 ) (Bills, 1989). If the nonhydrostatic components of the second degree gravity field of Mars stand the range between those of the Earth and Venus, it seems that the reasonable range of the Martian mean moment-ofinertia ratio, $I / M R^{2}$, is $0.345 \sim 0.350$.

## 4. Discussions and Suggestions

(1) The data in Table II obviously show that the central density, $\rho_{0}$, and central pressure, $p_{0}$, for the model MARS $93-09$ are too high, whereas the mean mantle density, $\overline{\rho_{m}}$, for the model MARS $93-01$ is too low. This deviates from the knowl-

TABLE III
Inferred properties of the Martian models

| Quantity | Martian model |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | $93-01$ | $93-03$ | $93-05$ | $93-07$ | $93-09$ |
| $J_{2}\left(10^{-6}\right)$ | 1600.52 | 1708.19 | 1816.84 | 1687.81 | 1578.06 |
| $\delta I_{2}\left(10^{-6}\right)$ | 359.83 | 252.26 | 143.61 | 272.64 | 382.39 |
| $\delta f$ | 0.519 | 0.667 | 0.935 | 0.633 | 0.496 |
| $I / M R^{2}$ | 0.3465 | 0.3550 | 0.3655 | 0.3549 | 0.3453 |
| $e$ | $1 / 213.75$ | $1 / 207.21$ | $1 / 199.33$ | $1 / 207.24$ | $1 / 214.53$ |
| $e(C M B)$ | $1 / 274.27$ | $1 / 267.90$ | $1 / 258.48$ | $1 / 302.18$ | $1 / 339.00$ |

edge of the chemical composition in Mars' interior. Therefore, if the value of $I / M R^{2}$ equals 0.345 , this seems inconsistent with some known facts.
(2) If we adopt $I / M R^{2} \simeq 0.355$, the central density, central pressure, radius of the core, and the mean mantle density for two relevant models (namely, 93-03 and 93-07) are all reasonable. We consider that the two parameterically simple

TABLE IV
Two parametric models of Mars

| Region | Radius (km) | $\begin{aligned} & \rho(x) \\ & \left(\mathrm{g} \mathrm{~cm}^{-3}\right) \end{aligned}$ | $\begin{aligned} & K(x) \\ & \text { (kbar) } \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| MARS 93-03 Core | 0.0-1750.9 | $\begin{gathered} 7.7600 \\ -2.1103^{*} x^{\wedge} 2 \end{gathered}$ | $\begin{aligned} & 3799.21 \\ & +\quad 32.26^{*} x \\ & -4191.71^{*} x^{\wedge} 2 \\ & +847.99^{*} x^{\wedge} 3 \end{aligned}$ |
| Mantle | 1750.9-3209.9 | $\begin{gathered} 3.7928 \\ -0.4622^{*} x \\ -0.0355^{*} x^{\wedge} 3 \end{gathered}$ | $\begin{gathered} 3597.87 \\ -1340.80 * x \\ +\quad 32.72 * x^{\wedge} 2 \end{gathered}$ |
| Shell | $\begin{aligned} & 3209.9-3329.9 \\ & 3329.9-3389.9 \end{aligned}$ | $\begin{aligned} & 3.320 \\ & 2.906 \end{aligned}$ | $\begin{array}{r} 1150 \\ 550 \end{array}$ |
| MARS 93-07 Core | 0.0-1521.6 | $\begin{gathered} 9.7100 \\ -6.0526^{*} \times 2 \end{gathered}$ | $\begin{gathered} 3999.06 \\ +\quad 44.24^{*} x \\ -6245.71^{*} x^{\wedge} 2 \\ +1542.80^{*} x^{\wedge} 3 \end{gathered}$ |
| Mantle | 1521.6-3209.9 | $\begin{gathered} 3.8592 \\ -0.4848^{*} x \\ -0.0303^{*} x^{\wedge} 3 \end{gathered}$ | $\begin{gathered} 3868.99 \\ -2518.58 x^{*} x \\ +1720.53 * x^{\wedge} 2 \\ -792.12 x^{\wedge} 3 \end{gathered}$ |
| Shell | $\begin{aligned} & 3209.9-3329.9 \\ & 3329.9-3389.9 \end{aligned}$ | $\begin{aligned} & 3.350 \\ & 2.900 \end{aligned}$ | $\begin{array}{r} 1150 \\ 550 \end{array}$ |

models (see Table IV) can be used for reference in the future theoretical researches.
(3) The results obtained in this paper indicate that the reasonable range of the Martian mean moment-of-inertia ratio, $I / M R^{2}$, is $0.350 \sim 0.360$, meantime, the range of the radius of Mars' core is $1520 \sim 1850 \mathrm{~km}$.
(4) It is necessary for us to be engaged in ground-based astrometric observations of the Martian satellites with the $C C D$ detector. This will certainly allow detection of the exact value of the Martian axial precession (cf. Sinclair, 1989) and will directly derive the mean moment-of-inertia ratio, $/ / M R^{2}$, of Mars. In addition, it seems that the new periodic space exploration will have to include the programme for detection of the size of Mars' core and its character. This will allow improvement of the internal structure models of Mars and will help us to check the adopted value of $I / M R^{2}$ of Mars.

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