A Comprehensive Evaluation of a Gaseous Portable Emissions Measurement System with a Mobile Reference Laboratory

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Abstract In-lab and on-road emission comparisons are made between AVL's M.O.V.E GAS PEMS 493 system and the UCR mobile emissions laboratory (MEL), which served as a Federal Reference Method (FRM) for comparison and validation. These comparisons are made for three different heavy-duty engines with NO_x emission certification levels ranging from 0.27 g/kWh (0.2 g/hph) to 5.4 g/kWh (4.0 g/hph). The brake-specific emissions during the Not-To-Exceed (NTE) engine operating zone are compared between the FRM and portable emission measurement systems (PEMS) to quantify the measurement uncertainty of the new commercial PEMS. Overall, the PEMS shows good correlation to the FRM and demonstrate its ability to measure a wide variety range of emission levels. The PEMS brake-specific NO_x (bsNO_x) measurement is well-behaved with +5 to −10 % relative error over the 1.0 to 7.0-g/kWh range. Further, the relative NO_x error ranged from a +15 to −15 % over the 0.1 to 1-g/kWh range. The relative NO_x error increases sharply below 0.1 g/kWh from 15 % to more than 50 % at 0.02 g/kWh. The relative error below 0.10 g/kWh is high due to the very low NO_x emission rates that approach the detection limit of both the raw PEMS and dilute FRM measurement methods. The PEMS bsCO₂ average bias is observed to be slightly higher than the MEL reference laboratory at 2 % overall. The PEMS NMHC and CO emissions were on average −11.8 and −3.6 %

compared to the MEL for the 2006 engine, respectively. The main purpose of this study was to determine the measurement uncertainty of recently released PEMS in comparison with legacy and ultra-low emission modern heavy-duty vehicles.

Keywords PEMS · 40CFR1065 · Real world emissions

1 Introduction

The US Environmental Protection Agency (EPA) and California Air Resources Board (ARB) have implemented a series of regulations to control oxides of nitrogen (NO_x) and particulate matter (PM) emissions, from diesel engines during “in-use” conditions [1]. The purpose of these regulations is to ensure that emission standards are maintained throughout the course of the engine's useful lifetime. One of the most important US regulations with respect to controlling in-use emissions is the Not-To-Exceed (NTE) standard. The US NTE standard sets limits for gaseous and PM pollutants that are emitted during operation in a defined portion of the engine map and specifies the protocols required to make those measurements [2]. The European Union and other international agencies implemented similar in-use regulations with slightly different measurement approaches. The European Union approach considered emissions over a work-based window (WBW) [3, 4]. In either case, portable emissions measurement systems (PEMS) are critical for the implementation of these in-use regulations.

In the USA, regulators agreed that PEMS measurement uncertainty could be larger than that for laboratory measurements and thus conducted a study to evaluate the “Measurement Allowance” (MA) for PEMS [5]. The allowance accounts for PEMS measurement uncertainty and adds to the in-use standard for a Not-To-Exceed combined standard.

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EPA, ARB, and the Engine Manufacturers Association (EMA) formed a heavy-duty in-use testing measurement allowance steering committee (HDIUT-MASC) to develop these MA values [2, 5]. The University of California at Riverside's (UCR) College of Engineering—Center for Environmental Research and Technology (CE-CERT) was part of this study and used its mobile emissions laboratory (MEL) as a Federal Reference Method (FRM) to validate the developed MAs for in-use conditions for both gaseous and PM PEMS MA programs [6, 7]. The in-use validation study found PEMS measurement uncertainties were higher during in-use conditions. In particular, PEMS NO_x emissions were highly biased by as much as 0.47 g/hph, or +9 to +25 % of the measured point [7]. As a result of the MA study, a NO_x allowance of 0.60 g/kWh (0.45 g/hph) was adopted for 2007–2009 MY engines, which is around 25 % of the 2007 standard. The NO_x allowance for post 2010 MY engines was found to be 0.20 g/kWh (0.15 g/hph), which is over 60 % of the 2010 NTE standard [8, 9]. ARB has proposed an optional 90 % reduction in NO_x emissions in California where the previously adopted MA would suggest the PEMS 0.20 g/kWh NO_x uncertainty for this optional regulation is greater than 650 % [10]. The high PEMS measurement uncertainty suggests future HDVs operating at 90 % of the 2010 NO_x standard will need new PEMS tools for their in-use measurement and compliance determination.

Since the completion of the MA program, the development, evaluation, and implementation of PEMS have continued to expand. The implementation of gaseous PEMS for regulatory measurements has been studied extensively in Europe, although this work has been less focused on instrument accuracy and more focused on emissions from the WBWs, pilot implementations, and measurement of PM and particle number [3, 11, 12]. There has also been a considerable effort in the development and characterization of PEMS for the measurement of particulate matter (PM) in the USA [13–15]. Following the completion of the MA program, however, there has been less emphasis on characterizing how the accuracy of PEMS might be improving over time. During the MA program and since its conclusion, PEMS manufacturers have been continuously improving the designs of gaseous PEMS. Testing conducted by Southwest Research Institute (SwRI) near the end of the MA showed that the accuracies of gaseous PEMS improved over the course of the MA program for fixed laboratory testing [16]. Studies that have focused on in-use comparisons between FRMs and gaseous PEMS have been very limited since the conclusion of the MA program, however. With the recent implementation of more stringent on-road and non-road emission standards, the emissions levels of the new engines have dropped significantly compared to the emission levels that were evaluated during the MA program. Thus, the in-use accuracy of PEMS needs to be evaluated at current modern emission levels.

As today's engine technologies rapidly evolve, manufacturers, regulators, and scientists worldwide are looking to use PEMS to generate in-use emissions and engine performance data to aid in their research and development. AVL, an Austrian-based PEMS manufacturer, released the M.O.V.E GAS PEMS 493 in late 2011 that incorporated a number of new features to address the issues found with earlier PEMS with accuracy, repeatability, and reliability [17]. The goals of this study were to provide information on the accuracy and measurement capability of AVL's PEMS with legacy and modern HDV emission levels. This study was conducted as part of a verification testing program on this PEMS system for approval under the US heavy-duty in-use testing (HDIUT) program and to quantify the new PEMS's in-use uncertainties using UCR's MEL as the FRM. The verification program consisted of a comprehensive audit and engine testing evaluation with a FRM [18]. Additionally, UCR performed two unique in-use comparisons between the PEMS and the UCR FRM utilizing a high NO_x and a low NO_x heavy-duty on-road vehicle.

This paper presents the first in-use comparison between a PEMS and a FRM under in-use conditions with a modern heavy-duty vehicle (HDV) where emission rates were within and below the 2010 certification level of 0.3 g/kWh. Emission rates during this comparison testing reached levels 90 % below the 2010 standard which allows an analysis of in-use measurement uncertainty at California's future optional standard of 0.03 g/kWh [10]. Additionally, this research represents a comparative analysis between a recently developed state-of-the-art PEMS and a FRM.

2 Experimental

2.1 Test Engines and Vehicles

Three correlation exercises were performed as part of the PEMS audit evaluation. One utilized UCR's engine dynamometer, the second utilized UCR's in-house 2001 Freightliner heavy-duty truck, and the third utilized a 2010 compliant SCR equipped low NO_x heavy-duty on-road HDV.

A list of the HDV engines tested and their certification ratings is shown in Table 1. The range of engines tested includes brake-specific NO_x (bs NO_x) emission levels from 5.4 g/kWh representing MY 2000 HDV certifications to less than 0.3 g/kWh representing modern MY 2010 and later HDV certifications. The selected emission levels thus provide PEMS users a comprehensive evaluation of the PEMS performance over a wide range of NO_x operating conditions. The main comparisons were based on the NTE points, where a NTE point is defined when an engine enters a predefined speed and torque zone for more than 30 s

Table 1 Engine dynamometer and in-use vehicle test matrix

Test units	Location	Test Engine	Power and Torque	ECS	Certif. NO _x g/kWh (g/hph)	Number NTE points
1	Engine lab	2006 Cummins ISM 10.8 L	370 hp 1450 ft-lb	EGR	2.7 (2.0)	150
2	In-use	2000 Caterpillar C15 15.0 L	475 hp 1650 ft-lb	CRT-retrofit	5.4 (4.0)	145
3	In-use	2011 Cummins ISX 11.9 L	425 hp 1650 ft-lb	OEM DOC, DPF SCR	0.3 (0.2)	174

The 2006 Cummins engine is referred to as the 2006 CUM 10.8, the 2000 Caterpillar is denoted 2000 CAT 15, and the 2011 Cummins is denoted as the 2011 CUM 11.9

ECS emissions control system, *DOC* diesel oxidation catalyst, *DPF* diesel particulate filter, *OEM* original equipment manufacturer, *SCR* selective catalytic reduction, *EGR* exhaust gas recirculation, *CRT* continuously regenerative trap

[1, 6, 9]. The three tests generated anywhere from 145 NTE points to 174 NTE points.

this approach would not be representative of most in-use testing and, thus, were not performed in this comparison.

2.2 PEMS Description

The PEMS evaluated are the gaseous unit of AVL's Mobile On-Board Vehicle Evaluation (M.O.V.E) system. The 493 gaseous PEMS include a system controller, a post processor, and an exhaust flow meter. The AVL gaseous PEMS use heated flame ionization detection (HFID) for total hydrocarbon measurement, non-dispersive ultraviolet (NDUV) for NO and NO₂ measurements, and non-dispersive infrared (NDIR) for carbon monoxide (CO) and carbon dioxide (CO₂) measurements. The AVL PEMS design was based on accuracy and long-term measurement stability and includes some new features, such as internal damping, climate control, and a multi-stage water removal system [17]. The AVL 494 PM PEMS was previously validated in some earlier studies by the same MEL and, thus, was not included in this research [14, 15].

The PEMS were first evaluated in an engine test cell and were subjected to variations in test cell temperature, but with constant pressure and no vibration. Then the PEMS were installed on two HDVs where the PEMS were mounted outside the tractor cab and exposed to ambient conditions and on-road conditions which included vibration, barometric pressure changes with elevation, and electrical interferences possible during on-road operation. The PEMS were secured to a shock absorbing system provided by the PEMS manufacturer which was mounted to a custom frame located behind the passenger side fuel tank. The electrical power and necessary operating gases for the PEMS were provided by the UCR MEL. A PEMS weather probe was installed inside of a weather shield mounted on the rear of the cab away from any obvious heat sources. The PEMS were calibrated at the beginning and the end of the day, as per typical in-use test operating procedures. The PEMS were automatically zero checked hourly using zero air gas as recommended by the manufacturer. Measurement accuracies could be improved by hourly span calibrations, but

2.3 UCR Mobile Emissions Laboratory Description

The UCR MEL was used as the FRM for this PEMS comparison study and was the same validation laboratory used during the federal PEMS MA program, making this correlation study directly comparable to previous PEMS studies [6, 7]. The MEL consists of a number of operating systems typically found in a stationary certification laboratory. However, the MEL is a 53-ft trailer that can be hauled under typical driving conditions and used to measure the emissions directly from the vehicle towing the MEL [19, 20].

The MEL is a qualified mobile reference laboratory for performing PEMS validations. A 40 CFR Part 1065 audit for the gaseous and constant volume sampler (CVS)-related measurements was successfully completed in the MEL prior to performing the correlation testing with this PEMS study and previous MA studies [6, 21]. The UCR MEL has also previously performed cross-correlations with several certification laboratories throughout the USA. In 2006, the UCR MEL has cross-correlated with SwRI on two separate trips and ARB's heavy-duty chassis laboratory [6, 21]. In addition, the UCR MEL successfully completed a blind audit by ARB as part of another research project. The MEL was operated with hourly zero and span calibrations during comparison with AVL's 493 gaseous PEMS, thus minimizing its uncertainty and reducing instrument drift, as performed during the previous MA studies [6, 7].

2.4 Interferences, Validation, and Accuracy

The main purpose of this study was to characterize the in-use uncertainty of the latest PEMS technology for legacy and modern HDVs. Prior to conducting these tests, several steps were performed before the emission testing to characterize and quantify the PEMS measurement capabilities, including

a successful 40 CFR Part 1065 audit [18]. The audit included NDIR interference checks, NO_x measurement interference checks (NDUV and CLD), measurement linearity, etc. for both the PEMS and MEL, respectively. This combined effort resulted in over 100 experiments (interference checks, accuracy checks, and linearity verifications) on both systems. In all cases, the comparisons showed excellent agreement where interferences and accuracies were within 2 % for all measurements except exhaust flow, which had uncertainties in the range of 5 % and varied by installation and application.

3 Results

This paper focuses on the correlation results of the gaseous PEMS with the UCR MEL, which is termed the FRM in the discussion below. Brake-specific emission factors for NO_x , non-methane hydrocarbon (NMHC), CO, and CO_2 were calculated using the J1939 broadcast speed and torque values from the vehicle's electronic control module (ECM) [7]. It should be noted that the PEMS met all the 40 CFR Part 1065 requirements during the correlation testing.

3.1 NO_x Emission Results

The comparisons in this report are expressed in either absolute emission deltas, which are defined as the absolute difference between the PEMS and the FRM in units of grams per kilowatt-hour, or in relative deltas, which are defined as the relative error of the PEMS compared to the FRM in unit of percentages. The PEMS's NO_x deltas as a function of FRM emission level for the engine dynamometer and on-road comparisons are displayed in Fig. 1.

The 2000 MY Caterpillar engine had higher bsNO_x emission levels and showed higher bsNO_x deltas compared to the other two engines tested in this study. However, the validation

Fig. 1 bsNO_x NTE comparison summary shown in absolute deviation. ^aThe in-use NTE standard was based on the 2007 emission levels of 1.68–2.68 g/kWh (1.25–2.0 g/hph); thus, emissions higher than 2.68 g/kWh are not representative of the MA of 0.60 g/kWh shown and may exceed the MA on a difference basis. The relative error is more representative for emission rates above 2.68 g/kWh as presented in the next figure

of the ability of PEMS measurement to maintain a specific delta relative to the MA is heavily dependent on the emission level. Therefore, the relative error is more important to evaluate higher emission levels while absolute error is more important to evaluate lower emission levels (e.g., post 2010 MY engines). The relative error of the 2000 MY engine is approximately 5 % relative error overall, similar to the 2006 MY engine (Fig. 2).

The bsNO_x relative error for the 2000 engine and 2011 engine (above 0.10 g/kWh) tested in-use is similar overall to that for the 2006 engine tested on an engine dynamometer suggesting that the PEMS NO_x measurement is robust down to 0.10 g/kWh regardless of sources (Fig. 2). PEMS NO_x relative error is observed to be approximately +5 to –10 % from 1.0 to 7.0 g/kWh and +15 to –15 % from 0.1 to 1 g/kWh, respectively.

The PEMS NO_x relative error increased below 0.1 g/kWh as the emission level approached the zero measurement detection limit of both the PEMS and the FRM measurement methods (Fig. 2). NO_x measurements below 0.10 g/kWh are subjected to higher levels of uncertainty of 50 % at 0.03 g/kWh. Differences in NO_x emissions at such low levels could be due to several different factors. There is a fundamental difference between the NDUV and chemiluminescence methods for NO_x measurements. Chemiluminescence detection method is based on the amount of light generated via a chemiluminescence reaction of NO as it reacts in an ozone atmosphere to form NO_2 . The NDUV measurement method is based on the absorption of UV radiation from a broadband UV source to quantify the amount of NO_x in a given sample.

For NDUV, the NO and NO_2 spectroscopy signal occurs during the very large water wavelength in addition to other smaller contributing signals such as sulfur compounds. The water signal is so large in relationship to the NO and NO_2 signals that special processing is required to quantify the nitrogen compounds on top of this signal. During near-zero measurements, the large water signal makes the nitrogen species signal hard to detect and thus causes larger variability at

Fig. 2 bsNO_x NTE comparison summary shown in relative percent deviation

zero. Thus, there is not an interferent issue like CLD, but there is a signal detection response issue resulting from other species. The CLD measurement method, on the other hand, has interferences from water and CO_2 where these molecules block light transmission during the measurement process. The CLD interferences are on the order of 1–2 % for large water and CO_2 concentrations at high and low signal level; thus, the magnitude does not change at low NO concentrations. In general, radiation absorption spectroscopy of NDUV analyzers typically is less sensitive than the light generated in the chemiluminescence reaction in CLD analyzer near-zero measurement quantification.

Analyzer drift also becomes more critical for measurements at such low levels. The PEMS manufacturer-specified drift criteria of the NDUV analyzer is 2 ppm per 8 h for both NO and NO_2 , which equates to 4 ppm/8 h NO_x [17]. Based on the in-use zero drift evaluation of this study, the NDUV analyzer showed a max 1.67 ppm drift at the 90th percentile (Table 3). The lowest NO_x measurements observed by the PEMS are near the instrument drift specifications and possibly the PEMS detection limit during in-use testing. It should be noted that analyzer drift is expected to become an even more critical issue if there are further reductions in the NO_x standard from 0.2 to 0.02 g/hph. One of the major limiting factors under those conditions will be the analyzer drift specification under CFR 1065.550 which requires the drift to be within ± 4 % of the standard. This represents a 0.008-g/hph drift allowance for a 0.2-g/hph standard, but would be lowered to a 0.0008-g/hph drift allowance for a 0.02-g/hph standard. It is expected that such drift specifications could be difficult to meet not only for PEMS but also for laboratory type analyzers.

3.2 NMHC and CO Emissions Summary

The NMHC and CO emission deltas were well below their respective MAs for all three vehicles tested. The relative error was large for NMHC and CO due to the very low emission levels for the ECS-equipped diesel engines where these emissions were on average below 0.03 and 0.02 g/kWh for CO and NMHC, respectively. Thus, at these very low values, relative error is not an appropriate comparison. For the 2006 engine, which did not have an ECS, the PEMS NMHC and CO emissions were on average -11.8 and -3.6 % compared to the MEL. During the previous MA study, CO and NMHC emission levels were low for all the evaluations; thus, NMHC and CO were never investigated for the PEMS ability to make these measurements. During the MA study, it was considered that CO and NMHC would not contribute to the overall compliance issue and was, thus, not pursued given ECSs would be found on most modern engines. Thus, the results here do show a perspective on PEMS ability for CO and NMHC which is in good agreement with the FRM.

3.3 CO_2 Emissions and Exhaust Flow Summary

The bsCO_2 relative error between the PEMS and the FRM for both engine dynamometer and in-use showed the highest positive deviation (+1.9 %) and the in-use vehicles with lower bias (-2.3 % for MY 2011 engine and +1.8 % for the MY 2000 engine). The range of bsCO_2 deviations varied from +10 to -5 % for all tests (Fig. 3). The bsCO_2 deviations are attributed to uncertainties in exhaust flow measurement.

The PEMS exhaust flow relative error ranged from +10 to -6 % (+2 % overall) for all the comparison tests (Fig. 4). The FRM exhaust flow is calculated by the difference between the two CVS venturis (total flow minus dilute flow) in the CVS system. The FRM venturis are accurate to within ± 2 %, are routinely verified by propane verifications ensuring robust measurement, and have been used for comparison in the previous MA studies [6, 7, 14, 15, 21].

The FRM diluted venturi exhaust flow calculation is a very stable and reliable measurement on an integrated NTE basis and is not subject to the rapid transients that occur in the raw exhaust. The PEMS exhaust flow is measured using differential pressures sensors corrected for density using the static pressure and temperature in the exhaust line. It is difficult to accurately estimate the exhaust density because of the rapid temperature changes observed in the exhaust. Additionally, the measured dynamic pressure must be correlated with exhaust flow using a constant correction factor K as part of the Bernoulli equation that the flow measurement is based on. This K constant is a function of Reynolds number (Re) and thus impacted by uncertainty in exhaust parameters. More analysis outside the scope of this work is required to understand these differences; the magnitude of these uncertainties is in the order of ± 10 %.

3.4 Measured Absolute Concentration

NTE brake-specific emissions and concentrations for NO_x , CO, NMHC, and CO_2 are summarized in Table 2 for both the PEMS and FRM. The concentrations represent average measured values where the FRM is for diluted CVS measurements while the PEMS is for raw exhaust measurements.

Fig. 3 Percent bsCO_2 deviation between PEMS and FRM

Fig. 4 Relative error in exhaust flow measurement (scfm) between the PEMS and FRM

Therefore, the concentrations between the PEMS and the FRM are not expected to be similar; rather, they provide a magnitude of the concentrations of each species measured. The MY 2000 vehicle had the highest NO_x concentrations, the MY 2011 vehicle had the highest CO_2 concentrations, and the MY 2006 engine had the highest CO and NMHC concentrations. The THC and CO concentrations were only a few parts per million for both the MY 2000 and MY 2011 vehicles. The average NO_x concentrations were lowest for the 2011 vehicle and averaged 19 ppm for the PEMS and 5 ppm for the FRM. The PEMS correlated well with the FRM over the wide range of average emission concentrations for the three engines in this study.

4 PEMS In-use Experience

This section addresses additional issues related to the applicability of the AVL PEMS system for on-road applications. These observations are based on the PEMS installation and in-use testing for the two on-road vehicles, as discussed previously. The additional environmental conditions to be considered for in-use testing include variations in temperature, humidity, pressure, and vibration level.

4.1 Temperature, Humidity, Pressure, and Vibration Affects

A few past PEMS studies have suggested that PEMS are exposed to wider temperature extremes than typical ambient temperatures during in-use applications due to its exposure to different environmental conditions [21, 22]. This can in turn lead to measurement failures/issues. No additional noticeable drift of the PEMS analyzer or operational issues were encountered during in-use operations due to temperature, humidity, pressure, and vibration variations. The PEMS were operated in ambient temperatures ranging from 9 to 29 °C, in ambient relative humidities ranging from 20 to 90 %, and at elevations ranging from sea level to 1500 m. Although ambient variations were not extreme, the gaseous PEMS are subjected to much higher temperatures when it is installed on the vehicle due to direct sun radiation, radiation from the engine, and low-speed/stationary operation from test vehicle, with the PEMS itself heating up to 38 °C under very warm ambient conditions [6].

4.2 Analyzer Drift

Determining analyzer drift is critical for stable and repeatable emission measurements. The 40 CFR Part 1065 requirements include an analyzer drift limit that requires a PEMS test to be repeated if the analyzer drift-corrected brake-specific value exceeds ± 4 % of the uncorrected value or the applicable emission standard, whichever is greater. Brake-specific drift is a complex calculation based on spans, zeros, and work done during the given test interval which do not reflect the absolute analyzer concentration drift of the given PEMS system. Since AVL only published the absolute zero drift data over an 8-h period, Table 3 compared the PEMS and FRM zero drift data from this study against the published reference values. In-use operation subjects to greater vibration and changes in barometric pressure and temperature that may increase PEMS

Table 2 Averaged concentration levels and bsEmission level measured by FRM and PEMS

Vehicle/engine	Averaged emission concentrations					bsEmissions (g/kWh)			
	Test	CO ppm	CO_2 %	NO_x ppm	THC ppm	CO	CO_2	NO_x	NMHC
2006 CUM 10.8	PEMS	79.8	7.0	191.8	52.4	0.582	867	2.54	0.212
2006 CUM 10.8	FRM	24.4	2.0	53.7	13.6	0.660	851	2.43	0.220
2000 CAT 15	PEMS	16.6	7.5	799.0	6.4	0.086	622	6.87	0.016
2000 CAT 15	FRM	3.7	2.5	247.4	2.2	0.056	611	6.36	-0.0028
2011 CUM 11.9	PEMS	0.5	8.9	19.1	1.2	0.001	622	0.145	0.002
2011 CUM 11.9	FRM	2.1	2.7	5.1	1.3	0.026	638	0.139	-0.0006

Note the average concentrations for the FRM are based on dilute measurements and raw measurements for the PEMS. Thus, the concentrations are not meant to be compared but used to show a comparative measurement level for the overall comparison

Table 3 Statistical summary of PEMS and FRM zero drift results during the comparison

Limit ^b	Number of zeros		CO ₂ vol%		CO ppm		NO _x ppm		THC ppmC	
	PEMS	FRM	PEMS ^a 0.1/8 h	FRM 0.03/24 h	PEMS 20/8 h	FRM 2/24 h	PEMS 2/8 h	FRM 3/24 h	PEMS 1.5/8 h	FRM 1.5/24 h
Dyno. ave.	16	14	0.00	−0.001	7.8	−1.4	0.77	0.03	3.1	0.1
Dyno. stdev.			0.00	0.005	4.0	0.7	0.47	0.06	1.9	1.0
Dyno. 50th			0.00	0.000	9.8	−1.6	0.91	0.03	3.6	0.3
Dyno. 90th			0.00	0.001	10.9	−0.4	1.19	0.04	5.4	1.1
In-use ave.	49	35	0.00	0.000	10.5	−0.9	0.26	0.09	1.2	0.6
In-use stdev.			0.00	0.002	18.0	0.8	1.53	0.14	1.8	0.9
In-use 50th			0.00	0.000	3.7	−0.9	0.70	0.01	0.2	0.0
In-use 90th			0.00	0.002	47.3	0.0	1.67	0.29	4.4	1.9

^a The PEMS CO₂ zero drift was small and only recorded to two decimal points and is thus shown as zeros

^b The zero limit are pushed values from AVL 493 and CAI 600 series specifications (analyzer used in FRM)

analyzer drift compared with stationary laboratory conditions. The AVL M.O.V.E's PEMS zero drift was evaluated during 1 day of engine dynamometer testing and 4 days of in-use testing. The testing intervals ranged from 6 to 8 h per day.

The average, standard deviation, 50th percentile, and 90th percentile statistics for the 16 in-lab and 49 in-use zero deltas for the PEMS and FRM are shown in Table 3. The limit values shown were published values from product specifications. PEMS zero calibration was only performed at the beginning of each day, with subsequent zeros audits done once per hour thereafter, as part of its standard operating procedures. For the FRM, on the other hand, zero and span calibrations were done before and after each test cycle, as part of its standard operating procedures. Thus, to provide a fair comparison to the PEMS, the FRM zero results are shown as the zero deviations from the first calibration of each test day. Overall, the FRM showed significantly less zero drift compared to the PEMS due to the more frequent calibration (hourly) as well as the more accurate and stable overall sampling system.

5 Overall Discussion

The goal of this study was to provide insight into the capabilities of a PEMS representing the latest commercially available technology for making measurements at today's ultra-low emissions levels. Overall, the AVL's M.O.V.E GAS PEMS 493 system met and exceeded the verification acceptance criteria for in-use emission measurements. The results from this study showed that the latest PEMS have evolved over time and have similar accuracies to those of fixed laboratories for pre-2010 emission levels. Further, PEMS are now more versatile in-use applications compared to the fixed reference laboratories, which are much larger in size and cost.

The correlation between the PEMS and FRM depends on the emission level and the specific pollutant. The PEMS brake-specific NO_x (bsNO_x) measurement is well-behaved with +5 to −10 % relative error over the 1.0 to 7.0-g/kWh range. Further, the relative NO_x error ranged from a +15 to −15 % over the 0.1 to 1-g/kWh range. The relative NO_x error increases sharply below 0.1 g/kWh from 15 % to more than 50 % at 0.02 g/kWh. The relative error below 0.10 g/kWh is high due to the very low NO_x emission rates that approach the detection limit of both the raw PEMS and dilute FRM measurement methods. In general, the PEMS have relatively high accuracy for higher NO_x emission levels down to 0.1 g/kWh where the PEMS measured nominal NO_x concentration is between 10 and 1000 ppm. However, for the ultra-low bsNO_x emission levels below 0.1 g/kWh, the PEMS started to lose accuracy as the very low NO_x concentrations approaches its in-use analyzer drift. The PEMS ability to measure NO_x and the proposed optional NO_x emission regulations of 0.03 g/kWh (5 ppm raw and less than 1 ppm dilute) will be a challenge with the latest PEMS and may have uncertainties of ~50 % at 0.03 g/kWh as evaluated in this study.

The bsCO₂ emissions agreed to within 2 % overall, with the measurement differences being largely related to uncertainties in exhaust flow measurements. The PEMS exhaust flow measurement is subject to greater variations due to the more transient nature of the raw exhaust PEMS measurements. The PEMS NMHC and CO emissions were on average −11.8 and −3.6 % compared to the MEL for the 2006 engine, respectively. The PEMS and the FRM NMHC and CO emissions were both relatively similar and typically below 0.05 g/kWh for both pollutants for the exhaust aftertreatment-equipped engines.

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