

Effect of Heat Treatment on Microstructure and Mechanical Properties of ZM6 Alloy Prepared by Solid Recycling Process

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(Submitted July 28, 2008; in revised form October 9, 2008)

ZM6 magnesium alloy was prepared by solid recycling process. Effect of heat treatment on microstructure and mechanical properties of the alloy was investigated. Cold pressing was employed to prepare extrusion billets of ZM6 chips, then the billets were hot extruded at 773 K with an extrusion ratio of 25:1. During hot extrusion, the grains refined and the particles were broken. The peak-aging materials showed fine plate-shaped β' precipitates. The ultimate tensile strength and elongation to failure of as-extruded rods was 232.2 MPa and 23%, respectively. After T5 and T6 heat-treatment, obvious improvement of the tensile strength was obtained because of dispersive particles or fine precipitates. The morphology of the fracture surfaces was examined by employing scanning electron microscope.

Keywords Hot extrusion, Mechanical properties, Microstructure, ZM6 alloy

ratio is 25:1. Effect of heat treatment on microstructure and mechanical properties of ZM6 magnesium alloys prepared by solid recycling process is discussed.

1. Introduction

Magnesium is one of the lightest metals and an abundant element that constitutes about 2.3% of earth's crust. There are many distinguished properties such as high specific strength, specific stiffness, and good electromagnetic shielding characteristics (Ref 1) of magnesium alloys for use in automobile; aerospace and 3C industries. It is easily recyclable and considered as green and environmental protection material in the 21st century (Ref 2). On the other hand, because of resource depletion in the future, recycling of materials draws more and more attention in order to ensure the sustainable development of society. In general, metallic scraps always can be remelted to be cast into ingot for subsequent processing. However, this liquid state recycling may not be efficient for magnesium alloys because of the needs of special protective environment and extra caution. Hot extrusion is an advanced technique for recycling magnesium machined chips because it is not expensive, and extruded materials show excellent mechanical properties (Ref 3, 4).

Many studies showed that magnesium alloys such as AZ31 (Ref 5), ZK60 (Ref 6), and AZ91 (Ref 7) prepared by solid recycling process exhibited high tensile strength and high elongation to failure. In this article, cold-pressing was employed to prepare extrusion billets of ZM6 magnesium alloy chips. Hot extrusion was carried out at 773 K. Extrusion

2. Experimental Procedures

The chemical composition of the ZM6 alloy is Mg-3.0wt.%Nd-0.4wt.%Zn-0.4wt.%Zr. The alloy chips were prepared by machining an as-received ingot in a lathe. The appearance of machined chips is shown in Fig. 1. The size of a chip was 4–5 mm in length, 1.5–2 mm in width, and 0.5 mm in thickness. The machined chips were filled into a cylindrical container with a diameter of 40 mm and cold pressed by slowly increasing pressure up to 300 MPa for 30 s at room temperature into billets. Then the billets were hot extruded into rods. The extrusion temperature was 773 K with a speed of about 0.15 mm/s. The diameter of as-extruded rod was 8 mm with extrusion ratio of 25:1. Some of extruded specimens were solution treated at 803 K for 2.5 h in an electric resistance furnace under the mixed atmosphere of SO₂ and SF₆ with the ratio of 100:1, quenched into hot water at ~333 K (extruded-T4), and then subsequently aged at 473 K (extruded-T6). A few of the extruded specimens were directly aged at 473 K for 16 h (extruded-T5).

Tensile experiments were performed at room temperature at a strain rate of $5 \times 10^{-3} \text{ s}^{-1}$ on WDW-10 electron universal strength testing machine. The samples were machined into tensile specimens of 5-mm gauge diameter and 25-mm gauge length. The tensile axis was parallel to the extrusion direction. The ultimate tensile stress, 0.2% offset yield stress, and elongation to failure were recorded. Each datum was the average of results from more than three samples. Specimens were etched in 4% nitric acid liquor for microstructure observation. Microstructures were examined by using OLYMPUS-GX71-6230A optical microscope (OM) and transmission electron microscope (TEM, Philips CM20 and JEM-2010) operating at 200 kV.

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A FEI-SIRION scanning electron microscope (SEM) was employed for the observation of the fracture surfaces of the specimens.

3. Results and Discussion

3.1 Effect of Aging Time

The extruded specimens from the consolidated chips were solution treated at 803 K for 2.5 h, and then aged at temperature of 473 K for various periods of time. The variation in tensile strength with aging time plotted as the aging curve is given in Fig. 2. It takes about 16 h to reach peak aging. The peak-aged specimen presents an ultimate strength of 294.5 MPa with an elongation to failure of 13.5%. After 16 h aging, the alloy suffers an obvious overaging with the decrease in tensile strength from 294.5 to 252.1 MPa.

Figure 3 shows the evolution of the aging microstructure on the plane perpendicular to the extrusion direction. As the aging process reaches the time of 16 h, a large amount of the second phase particles precipitate homogeneously from the α -Mg matrix. The average grain size was 25.3 μm . The solution and aging treatment results in a more homogeneous distribution of

the microprecipitates throughout the entire volume of the ZM6 alloy. The particles of the specimen aged for 96 h are much bigger than that of the specimens aged for 16 h. Figure 4 presents transmission electron micrographs recorded from an alloy sample aged at 473 K for 8 h, with the incident electron beam approximately parallel to $[0001]_{\alpha}$. Many shaft-like precipitates were formed and distributed in the matrix, as shown in Fig. 4(a). In the corresponding selected area electron diffraction (SAED) pattern (Fig. 4b), there was a hexagonal



Fig. 1 Machined chips of the alloy

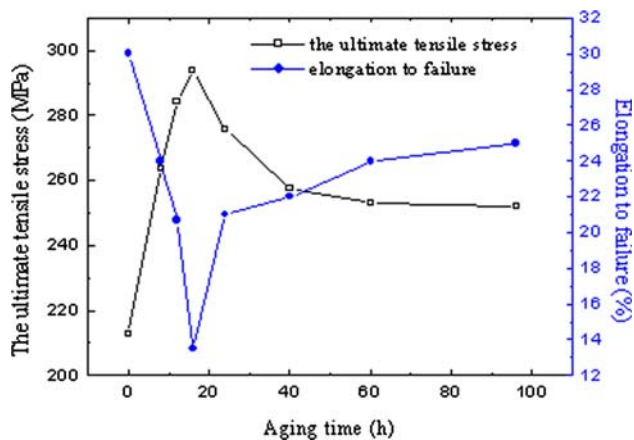


Fig. 2 The variation with aging time of the tensile properties

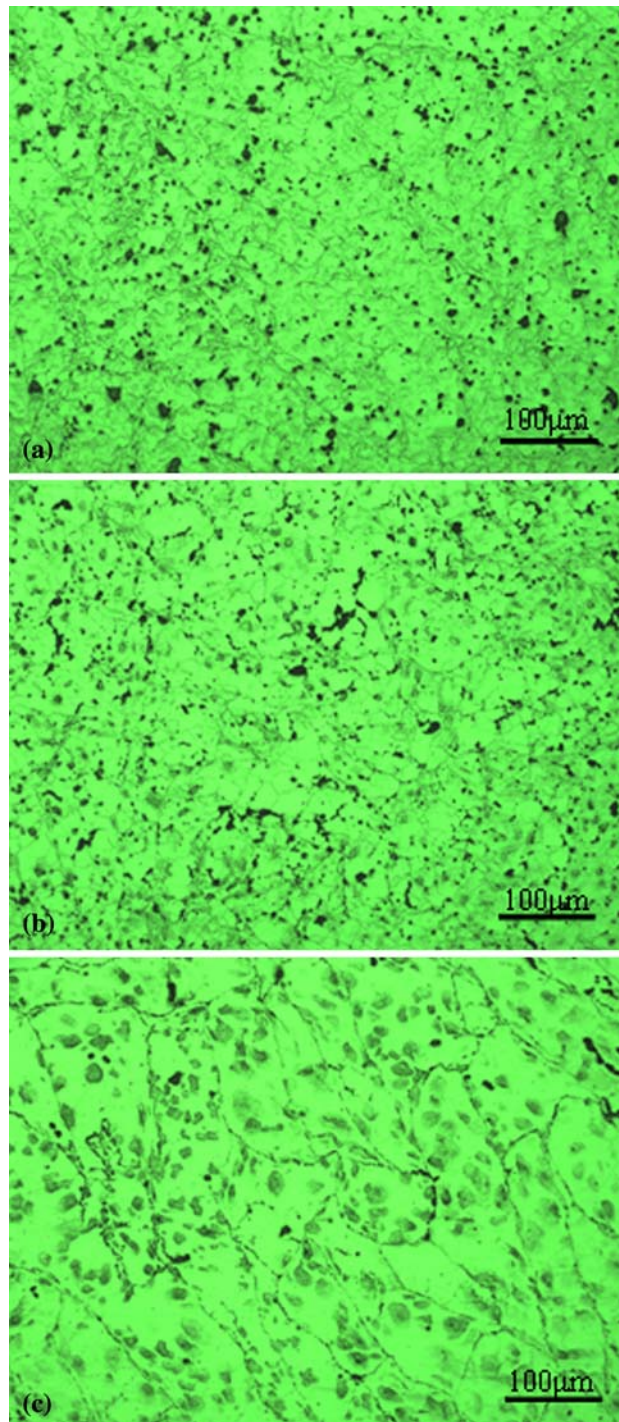


Fig. 3 Optical microstructures of the rods aged at 473 K for various aging time. (a) 12 h; (b) 16 h; (c) 96 h

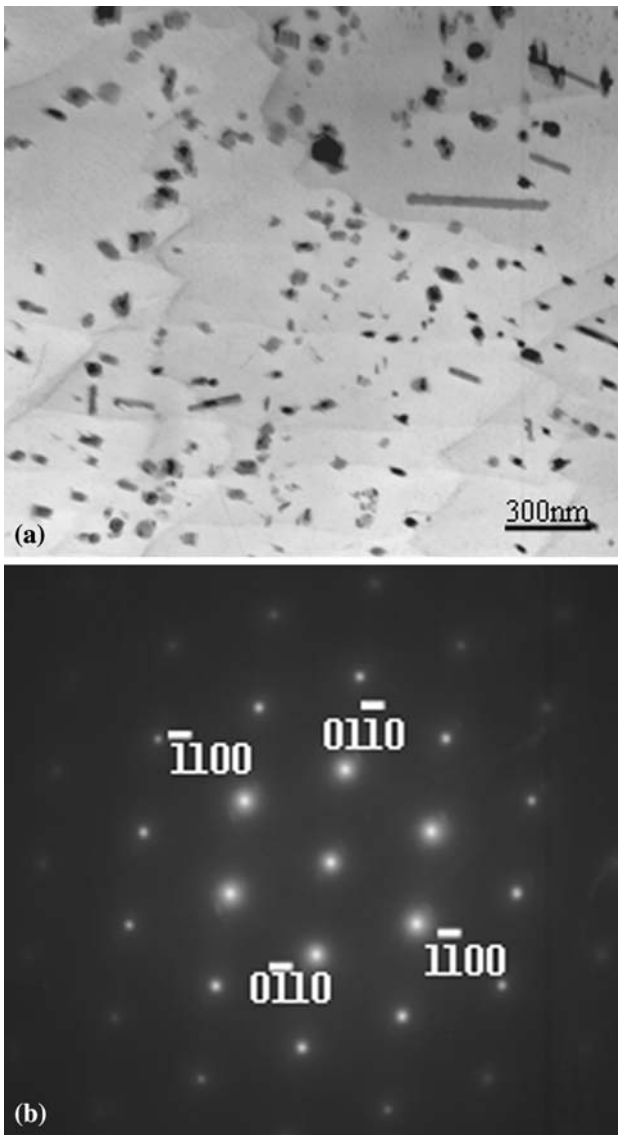


Fig. 4 Transmission electron micrographs recorded from an alloy sample aged at 473 K for 8 h. (a) Bright-field images; (b) SAED patterns taken along $[0001]_z$

$D0_{19}$ structure in the alloys, namely β'' (Ref 8). At the peak and over-aged stages, plate-shaped precipitates were observed. Figure 5(a) and (b) shows bright field images recorded from the alloy samples aged at 473 K for 16 and 96 h, respectively. From the aging time of 16-96 h, the plate-shaped precipitates grew from typical ~ 200 nm in length, with a thickness of <10 to ~ 400 nm in length, with a thickness of ~ 10 nm. The SAED pattern corresponding to Fig. 5(a) was face-centered cubic structure, namely β' . The plate-shaped β' precipitates make the strength to be the maximum (Ref 9).

3.2 Microstructure in Different Conditions

Figure 6(a)-(c) shows the microstructures of the alloy in the as-extruded, extruded-T4, and extruded-T5, respectively. The extruded specimens exhibited partial dynamic recrystallization and the grains refined greatly. It can be seen from Fig. 6(a) that some coarse brittle intermetallic phases were broken into small particles and moved from grain boundaries to grain interiors

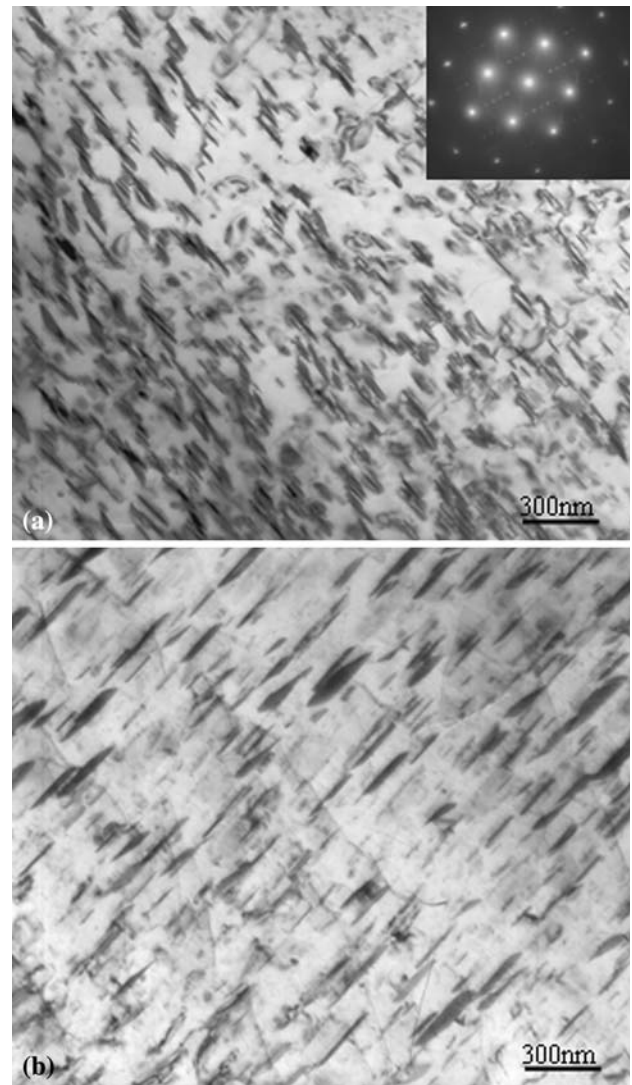


Fig. 5 Bright field images recorded from the samples aged at 473 K for (a) 16 h and (b) 96 h

during the hot extrusion process (Ref 10). The solution heat treatment of the alloy at 803 K for 2.5 h reduced the Nd-rich second phases at grain boundaries and left only some discrete, rounded precipitates, as shown in Fig. 6(b). This kind of discontinuous particle morphology can improve the ductility of the alloy by reducing the nucleation, growth, and coalescence of cracks and cavities at grain boundaries (Ref 11). In the extruded-T5 condition, the average grain size was $12.3 \mu\text{m}$. The grain refinement and less grain growth tendency may be attributed to the Mg_{12}Nd particles which pin the grain boundaries and impede grain growth during extruding and subsequent heat treatment (Ref 12).

3.3 Mechanical Properties of the Alloy

Figure 7 presents the mechanical properties at room temperature of the alloy in different conditions. The as-extruded rods have the UTS of 232.2 MPa, the TYS of 118.8 MPa, and the elongation of 23%. After solution treatment (extruded-T4), the UTS and the TYS have a little decline, but the elongation increases from 23 to 30%. Compared with those of the

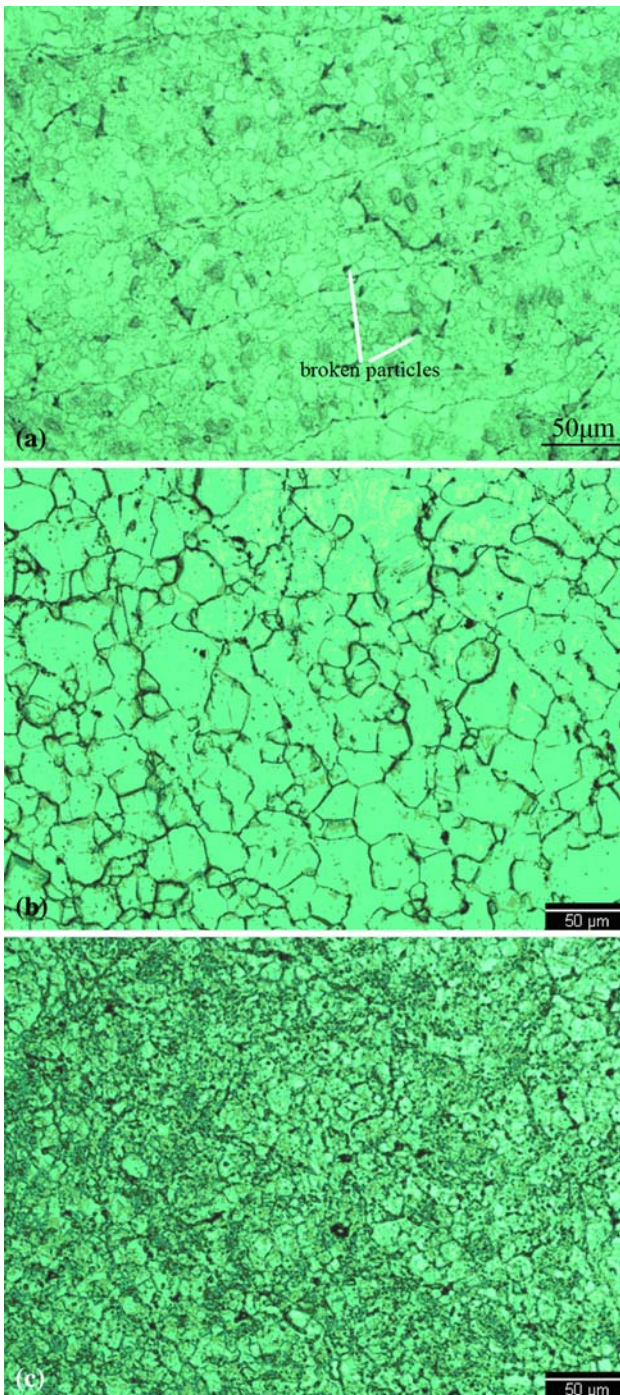


Fig. 6 Microstructures of the samples in different conditions. (a) As-extruded; (b) extruded-T4; (c) extruded-T5

as-extruded rods, both the UTS, and the TYS of the extruded-T5 rods increase while the elongation decreases due to the precipitation hardening. Large improvements of the UTS and the TYS are obtained from extruded-T4 condition to extruded-T6 condition, but the elongation is greatly reduced. The extruded-T6 rods have the highest UTS of 294.5 MPa and the highest TYS of 142.9 MPa.

During the hot-extrusion process, $Mg_{12}Nd$ intermetallics were destroyed and broken into small particles, responsible for a substantial strengthening. Furthermore, hot extrusion may

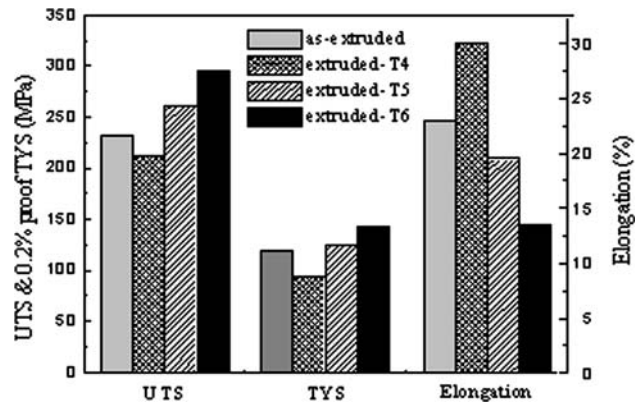


Fig. 7 Mechanical properties at room temperature of the alloy in different conditions

promote the formation of finer microstructure. According to the well-known Hall-Petch relation, the increase in yield stress depends on the grain size as follows (Ref 13):

$$\Delta\sigma_{0.2} = Kd^{-1/2}$$

where $\Delta\sigma_{0.2}$ is the increase in yield stress due to grain refinement, K is a constant, and d is the grain size. In the extruded-T4 condition, many of the particles were resolved into the matrix, which contribute to the tensile strength decreasing and the elongation increasing. In the extruded-T5 condition, the other potential sources of strengthening are the $Mg_{12}Nd$ particles, which are observed to exist as relatively small particles. After solution heat treatment and aging treatment, the second phase particles precipitate from the matrix and retard the dislocation movement and grain boundaries migration, producing strengthening effects (Ref 14). In addition, due to the uncoordinated deformation with the matrix, the precipitates may act as crack sources and in turn decrease the elongation to fracture of tensile samples.

3.4 Fracture Behavior

Figure 8(a) and (b) shows SEM images of the tensile fracture surfaces of the alloys in the as-extruded and extruded-T6 conditions. It can be seen from Fig. 8(a) that the failure surfaces are composed of some deep and small dimples. The diameter of dimples is about 8-15 μm . Moreover, apparently tearing ridges are observed in the fracture surface of the as-extruded alloys. Cleavage planes, some dimples and tear ridges are observed in the failure surfaces of the extruded-T6. The cleavage planes means that the direction of the cracks frequently changes during propagation and the crack extension resistance increases. Many small particles are seen in the dimples. The particles are Nd-containing intermetallics by EDS analysis as shown in Fig. 9. Due to the fragile characteristic of Nd-containing compounds, the particles were broken during the tensile test (or during extrusion) and become a cracking source.

4. Conclusions

- (1) Solid recycling process were carried out on the ZM6 alloy. The solid recycling process consisted of cold

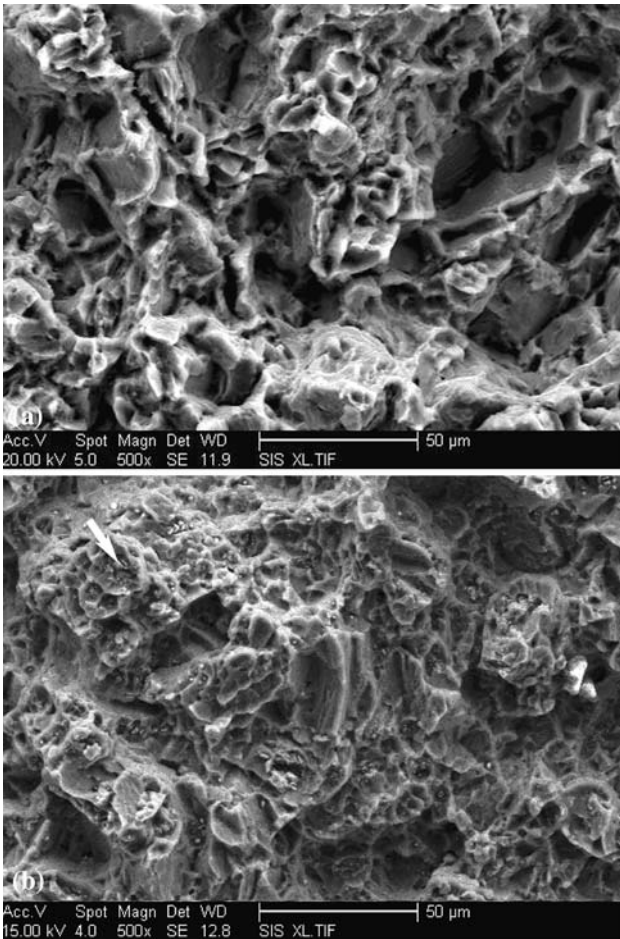


Fig. 8 SEM images of the tensile fracture surfaces. (a) As-extruded; (b) extruded-T6

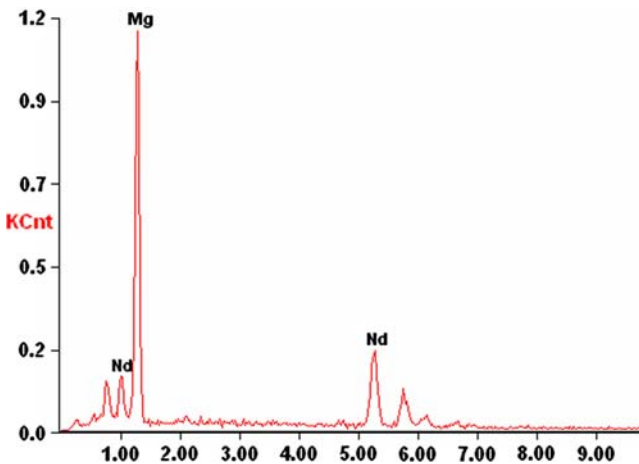


Fig. 9 EDS analysis of arrow site in Fig. 8

pressing of extrusion billets of ZM6 chips and hot extrusion of the billets at 773 K with an extrusion ratio of 25:1.

- (2) Grains of the as-extruded specimens were refined because of the occurrence of partial recrystallization. A large amount of the second phase particles were observed in the extruded-T5 and extruded-T6 alloys.
- (3) The ultimate tensile strength and elongation of the as-extruded rods was 232.2 MPa and 23%, respectively. After T5 and T6 heat treatment, obvious improvement of the tensile strength was obtained.
- (4) SEM observations of the fracture surfaces revealed that the fracture mode of the alloy in the as-extruded and extruded-T6 conditions is a mix mechanism with brittle fracture and gliding fracture.

Acknowledgment

The authors gratefully acknowledge the financial support by the Chinese National Science Foundation (No. 50674038E0410).

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