AC Hopping Conductance in Nanocomposite Films with Ferromagnetic Alloy Nanoparticles in a PbZrTiO_3 Matrix

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In this work, the temperature and frequency dependences of the real part of the admittance $[\sigma(f, T)]$ of annealed nanocomposite films containing $\text{Co}_{45}\text{Fe}_{45}\text{Zr}_{10}$ -based nanoparticles covered with native oxides and embedded in a doped PbZrTiO_3 ferroelectric matrix were studied. The nanocomposites studied were deposited by ion sputtering a complex target in a mixed Ar/O_2 atmosphere followed by a 15-min annealing process (with steps of 25 K) in air in the temperature range of $398 \text{ K} \leq T_a \leq 573 \text{ K}$. The $\sigma(f, T)$ of the annealed samples was measured in the temperature range of $77 \text{ K} < T_p < 373 \text{ K}$ at frequencies of $50 \text{ Hz} < f < 1 \text{ MHz}$. The observed $\sigma(f, T)$ dependences confirmed that the annealed samples displayed the effects of negative capacitance over the whole frequency and temperature ranges studied because of the pronounced oxidation of the nanoparticles. The $\sigma(f, T)$ dependences obtained are described using an earlier-developed AC hopping conductance model. Comparisons between experimental and simulation results allow the model parameters to be estimated, such as the activation energies of the hopping conductance and the lifetimes of the electrons in the nanoparticles.

Key words: Admittance, electronic transport, hopping conductance, nanocomposite

INTRODUCTION

Nanocomposites that include nanoparticles made of ferromagnetic metals or alloys embedded in different matrices have great potential for some industrial applications. Ceramics,¹ low-conductive metallic materials,² and even insulating liquids^{3,4} can be used as matrices to impart composites with improved mechanical,^{1,2} magnetic,^{5–7} and electrical properties.^{8,9} Particular attention has been paid to composites containing granules of soft ferromagnetic highly conductive metallic alloys about a few nanometers in size, randomly distributed in low-conductive matrices including dielectric, ferroelectric, or piezoelectric substances. It is of great interest to apply such materials particularly in

electrical engineering, e.g., in capacitors and high-ohmic resistors to protect systems from problems including high-frequency electromagnetic radiation, and in transducers of temperature and magnetic and electric fields.¹⁰

Besides, metal–dielectric nanocomposites are excellent model systems to study fundamental effects in heterogeneous media including percolation, hopping conductance, and weak localization.¹¹ In accordance with percolation theory,¹² the extreme values of some physical parameters (including the electrical and magnetic properties) in nanocomposites have been observed around the threshold concentration (x_c) of the high-conductive phase, corresponding to the onset of a current-conducting net of nanoparticles. In binary metal–dielectric composites, the x_c value is defined as the percolation threshold. When the volume ratio (x) increases and approaches x_c , the composite

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undergoes an insulator–metal transition. Below x_c the composite behaves as a dielectric (highly resistive material), whereas beyond x_c its behavior becomes metallic like, owing to the formation of a whole net of low-resistive current-conducting routes in the dielectric matrix. The x_c value is strongly dependent on the relative conductivities of the high- and low-conductive phases, x , and the concentration of chemically active impurities incorporated into the matrix and/or metallic filler during synthesis and further heat treatments. In this context, clarification of the correlation between deposition conditions, x values, the phase composition of the nanoparticles, matrices, and the integrated electric properties of the nanocomposites becomes important.

In our earlier studies on $(\text{Fe}_{45}\text{Co}_{45}\text{Zr}_{10})_x(\text{Al}_2\text{O}_3)_{(100-x)}$ nanocomposite granular films,^{8,13–16} it was shown that deposition conditions play the key role in the phase composition of the films. In particular, transmission electron microscopy, x-ray diffraction (XRD) analysis, and Mössbauer spectroscopy (MS) measurements revealed that adding oxygen to the sputtering atmosphere results in formation of CoFe-based oxide shells around the FeCoZr nanoparticles.¹⁷ Formation of such a metallic core/oxide shell structure of the nanoparticles inside the matrix induces radical modification of the electric and magnetic properties of the nanocomposite films as a whole. Also, the formation of a core/shell structure shifts x_c up to 55 at.%, compared with 44 at.% to 47 at.% for films deposited in a pure Ar gas atmosphere.

It has also been established that some granular nanocomposites exhibit the effect of negative capacitance (NC) with positively phase-shifted angles between the current and voltage applied when measuring the reactive part of the admittance.^{18–20} The observation of NC is associated with a dominant inductive-like (L) contribution in the imaginary part of the admittance, which could be utilized to produce microscale planar inductive elements in electrical engineering of integrated circuits. It has been proved that the dominant L -contribution is related to the formation of the core/shell structure of the nanoparticles,^{8,13–16,19,20} namely, it strongly increased with growth of the semiconducting CoFe-based oxide shell thickness. Technologically, the formation of the core/shell nanoparticle structure can be obtained by either annealing in air (for FeCoZr–alumina and FeCoZr–CaF₂ nanocomposites^{15,21}) or adding oxygen to the atmosphere during synthesis (for FeCoZr–PbZrTiO₃ nanocomposites^{17,19,22}).

The experimentally observed frequency dependences of admittance with NC in as-deposited and annealed FeCoZr–alumina and as-deposited FeCoZr–PbZrTiO₃ nanocomposite films can be explained by the hopping AC conductance model developed in Refs. 9, 19, and 22. This model takes into account that, before an electric field is applied, the electrons are localized in potential wells (namely,

nanoparticles with a core/shell structure embedded in a dielectric matrix). The application of a weak AC electric field causes the electrons to jump from one neutral well to another (on the order of 10^{-13} s) following the phase of the applied electric field. At first, electrons jump between two neutral potential wells (nanoparticles), forming a dipole containing two charged particles, which enhances the dielectric permeability of the material.¹⁹ Interactions between electrons trapped by neighboring metallic nanoparticles (potential wells), and the polarized dielectric matrix, lead to the breakdown of the equal probability (p) of electrons jumping forward and backward following the direction of the applied AC electric field. Consequently, the electrons jump back into the charged wells and their forward jumps to the next wells are delayed by a time τ_m . In accordance with the developed model, the frequency region in which the delay is substantial can be determined by

$$f \leq \frac{1}{2\tau_m} \approx f_{\min}. \quad (1)$$

In this case, the frequency dependence of the real part of the impedance can be written as the known Mott relation²³

$$\sigma(f) \approx \sigma_0 f^{\alpha(p)}, \quad (2)$$

where σ_0 is a coefficient and the exponent α is the frequency factor. Compared with the Mott model where $\alpha \approx 0.8$, in our model this factor determines the jump probability p and therefore depends on the change in the frequency in the range $0 < \alpha < 2$. In this case, the $\sigma(f, T)$ dependences for the composites studied in the dielectric regime should be characterized by a sigmoid-like shape,^{21,24,25} displaying three characteristic frequency regions: $\sigma_L \approx \text{const.}$ for low frequencies, $\sigma_H \approx \text{const.}$ for high frequencies, where $\sigma_H > \sigma_L$, and an intermediate frequency region described by Eq. 2. This nearly sigmoid-like behavior of $\sigma(f, T)$ allows the factor α and the probability density p to be extracted using the developed model and the characteristic parameters of the model to be estimated, namely the energies of activation for dipole formation and mean lifetime τ_m (1) of an electron in a nanoparticle.

The presence of the NC effect in as-deposited and annealed $(\text{Fe}_{45}\text{Co}_{45}\text{Zr}_{10})_x(\text{Al}_2\text{O}_3)_{(100-x)}$ films can be primarily controlled by the volume ratio and the phase composition of the oxide shells around the metallic nanoparticles;^{7–9,13–17,22} namely, the shells should have semiconducting properties and be as thick as possible. In addition, the phase composition and volume contribution of the shells depend on several factors: (1) the composition of the films with respect to the percolation threshold (progressive oxidation of metallic nanoparticles with x growth is shown in Ref. 26), (2) partial oxygen pressure in the sputtering atmosphere, and (3) annealing in air.

Detailed investigation of the structure and phase composition of FeCoZr-PbZrTiO_3 films sputtered in an oxygen-containing atmosphere^{19,22} showed more advanced oxidation, thus leading to the higher contribution from the oxide shells. Based on the earlier experimental results and modeling, such phase composition should favor a high NC effect, which could be further enhanced by annealing of the films. Therefore, the present paper is focused on the influence of annealing FeCoZr-PbZrTiO_3 films in air on the NC effect. Also the applicability of the hopping conductivity model to the description of this effect in the films is studied.

EXPERIMENTAL PROCEDURES

Nanocomposite $(\text{Fe}_{45}\text{Co}_{45}\text{Zr}_{10})_x(\text{PbZrTiO}_3)_{(100-x)}$ films were deposited by ion-beam sputtering of a complex target in a vacuum chamber. Sputtering was performed in a mixed argon-oxygen atmosphere in a chamber evacuated with a mixture of Ar/O_2 under partial pressures of $P_{\text{Ar}} = 6.7$ mPa and $P_{\text{O}_2} = 3.2$ mPa, respectively. The method to manufacture the films and the characterization of their structures are described in detail elsewhere.^{15,26–28} The compound target contained $\text{Fe}_{45}\text{Co}_{45}\text{Zr}_{10}$ alloy plates with PbZrTiO_3 stripes arranged on their surfaces. The irregular distribution of the PbZrTiO_3 stripes (with continuously increasing spaces between them) on the target surfaces allows synthesis of films with variable metal-to-dielectric ratios, x (depending on the mutual arrangement of the targets and substrates) in one technological cycle.

The films were sputtered at 373 K onto glass ceramic substrates 250 mm in length, 50 mm in width, and 0.6 mm in thickness for the electric measurements. The chemical compositions of the films were verified by microprobe x-ray analysis (EDX) with a scanning electron microscope (SEM, LEO1455VP) and a Rutherford backscattering (RBS) method with accuracy of ~ 1 at.%.^{26,29,30} The thicknesses of the films ranged from 1 μm to 2 μm as estimated by SEM on cleaved regions of the samples with accuracy of approximately 3% to 4%.

Ten nanocomposite $(\text{Fe}_{45}\text{Co}_{45}\text{Zr}_{10})_x(\text{PbZrTiO}_3)_{(100-x)}$ samples with x ranging from 39.9 at.% to 88.4 at.% were studied, as well as a sample of metallic $(\text{Fe}_{45}\text{Co}_{45}\text{Zr}_{10})$ film (with $x = 100$ at.%), which was produced under identical conditions to the nanocomposite films. The electrically tested samples were covered with four silver stripes, which act as electric probes (two current and two potential probes). Four-probe admittance measurements were performed using a digital LCR meter (HIOKI 3532 HiTester, Japan) in the frequency range from 50 Hz to 1 MHz. All measurements were carried out within the temperature range of $77\text{ K} < T_p < 373\text{ K}$, where the temperature was recorded by a thermocouple using an Agilent 34970A multimeter. During the experiments, the changes in the phase shift and the full resistance of the

studied samples were fixed to calculate the real and imaginary parts of the admittance. This procedure is described in detail elsewhere.^{31,32} The absolute values of the admittance were measured with accuracy of $\sim 5\%$, whereas the specific admittance was measured with accuracy of less than 10% because of the errors in the measured thicknesses and the distances between the potential probes in the samples. The as-deposited samples were subjected to a set of 15-min isochronous annealing within the temperature range of $373\text{ K} < T_a < 673\text{ K}$ with steps of 25 K.

RESULTS AND DISCUSSION

The PbZrTiO_3 matrix in the studied nanocomposite films was selected because of two specific features. First, PbZrTiO_3 is a less corrosion-resistant material than alumina, allowing it to make a much higher contribution to the oxidized metallic fraction in $(\text{Fe}_{45}\text{Co}_{45}\text{Zr}_{10})_x(\text{PbZrTiO}_3)_{(100-x)}$ films. This is favorable for enhancing the NC effect as well as to shift it to the room-temperature region (which is preferable for potential applications). Second, PbZrTiO_3 possesses ferroelectric and piezoelectric properties in the crystalline state, expanding the possibilities for tuning the magnetic and electric properties of nanocomposites if required for a particular application.

Before the admittance is characterized, a brief review of the phase structure of $(\text{FeCoZr})_x(\text{PbZrTiO}_3)_{(100-x)}$ films is presented based on results from XRD analysis, x-ray absorption spectroscopy (XAS), MS, Raman spectroscopy, magnetometry, and electric conductivity measurements.^{22,26,29,33} Mössbauer and Raman spectra collected at room temperature from selected $(\text{FeCoZr})_x(\text{PbZrTiO}_3)_{(100-x)}$ films fabricated at $P_{\text{O}} \leq 3.2$ mPa are shown in Fig. 1. Fitting of Mössbauer spectra in Fig. 1a shows that, in films with $x < 67$ at.%, synthesized at low oxygen partial pressures, the nanoparticles were fully oxidized and contained various types of oxide, namely $\text{Fe}(\text{Co})_3\text{O}_4$ or $\text{Fe}(\text{Co})_2\text{O}_3$ (characterized with the superparamagnetic doublet, $\delta = 0.3$ mm/s to 0.45 mm/s, $\Delta E = 0.9$ mm/s to 1.2 mm/s), and $(\text{Fe}_x\text{Co}_{1-x})_{1-\delta}\text{O}$ (characterized with the doublet, $\delta = 0.9$ mm/s to 1.1 mm/s, $\Delta E = 1.7$ mm/s to 1.8 mm/s). This means that the (FeCoZr) -based nanoparticles in a PbZrTiO_3 matrix cannot be characterized by the metal core/oxide shell structure typically observed for the FeCoZr -alumina nanocomposites that we studied previously.^{22,26,29} Taking into account the similarities of the oxide phase compositions in the nanoparticles in FeCoZr-PbZrTiO_3 and $\text{FeCoZr-Al}_2\text{O}_3$ films, identified by comprehensive analysis of the MS, XAS, and XRD data, it is believed that the nanoparticles in FeCoZr-PbZrTiO_3 films have an oxide core/oxide shell structure. In this case, the core may comprise the oxides $\text{Fe}(\text{Co})_3\text{O}_4$ and $\text{Fe}(\text{Co})_2\text{O}_3$, while the shell may consist of $(\text{Fe}_x\text{Co}_{1-x})_{1-\delta}\text{O}$. Possible contributions from a small quantity of zirconium oxide to addi-

Fig. 1. Mössbauer spectra of $(\text{FeCoZr})_x(\text{PZT})_{(100-x)}$ ($35 \text{ at.}\% \leq x \leq 77 \text{ at.}\%$) fabricated at $P_O = 2.4 \times 10^{-3} \text{ Pa}$ (a) and Raman spectra of as-sintered and annealed $(\text{FeCoZr})_{63}(\text{PZT})_{37}$ fabricated at $P_O = 3.2 \times 10^{-3} \text{ Pa}$ (b).

tionally stabilize the oxide shells cannot be excluded, as it is proved by EXAFS and reported in Ref. 34.

Mössbauer spectra of films with $x > 67 \text{ at.}\%$ (Fig. 1a) show that films contain superparamagnetic $\text{Fe}(\text{Co})_3\text{O}_4$ or $\text{Fe}(\text{Co})_2\text{O}_3$ and $(\text{Fe}_x\text{Co}_{1-x})_{1-\delta}\text{O}$ oxides (characterized with two doublets) and ferromagnetic

metallic $\alpha\text{-FeCoZr}$ nanoparticles (or their agglomerations). The latter phase is associated with the sextet which appears in the spectra for $x \geq 67 \text{ at.}\%$.

Raman spectroscopy performed on as-prepared $(\text{FeCoZr})_{63}(\text{PZT})_{37}$ film sputtered at $P_O = 3.2 \times 10^{-3} \text{ Pa}$ (Fig. 1b) reveals several peaks in the range

Fig. 2. Mössbauer spectra of $(\text{FeCoZr})_{43}(\text{PZT})_{57}$ and $(\text{FeCoZr})_{81}(\text{PZT})_{19}$ films fabricated at $P_{\text{O}} = 3.7 \times 10^{-3}$ Pa (a) and Raman spectra of as-sintered and annealed $(\text{FeCoZr})_{63}(\text{PZT})_{37}$ fabricated at $P_{\text{O}} = 5.0 \times 10^{-3}$ Pa (b).

of small wavenumbers (90 cm^{-1} to 300 cm^{-1}) with Raman shifts very similar to those reported for PbZrTiO_3 phase.²⁶ In the region of large Raman shifts (300 cm^{-1} to 700 cm^{-1}), the spectrum of the film annealed during 10 min at temperature of 600°C indicates also the presence of several peaks associated with various Fe and Co oxides in correlation with Mössbauer spectroscopy results. Short-term annealing of film results in an increase of intensity and decrease in width of observed spectral lines, evidencing some crystallization of phases.²⁶

FeCoZr-PbZrTiO_3 films synthesized at high oxygen partial pressures of $P_{\text{O}} \geq 3.7 \text{ mPa}$ contained fully oxidized superparamagnetic nanoparticles of

Fig. 3. Low-frequency conductivity, σ_L ($f = 100 \text{ Hz}$) versus metallic-phase content (x) for the nanocomposite $(\text{Fe}_{45}\text{Co}_{45}\text{Zr}_{10})_x(\text{PZT})_{(100-x)}$ films, as-deposited (1) and annealed at $T_a = 448 \text{ K}$ (2).

either $\text{Fe}(\text{Co})_3\text{O}_4$ or $\text{Fe}(\text{Co})_2\text{O}_3$ oxides over the whole range of x ($x \leq 81 \text{ at. \%}$).^{22,26} This is confirmed by corresponding Mössbauer spectra shown in Fig. 2. An increase in the concentration of isolated oxide core/oxide shell nanoparticles is observed with x . In the absence of the $(\text{Fe}_x\text{Co}_{1-x})_{1-\delta}\text{O}$ phase, which was not detected in these strongly oxidized films, the superparamagnetic state of oxide nanoparticles is stabilized at $x > x_c$, which may be caused by precipitation of the zirconium oxide formed at the nanoparticle/matrix interface.³⁴ Thus, it is believed that PbZrTiO_3 is a more friable matrix than alumina, as it does not assist in the conservation of the non-oxidized metallic cores in the nanoparticles during both the deposition and annealing procedures.

In the first step of electrical characterization of the composite samples, their percolation thresholds were determined. For this reason, preliminary measurements in the low-frequency (100 Hz) real part of the specific admittance (σ_L) versus metallic-phase content (x) at room temperature ($T_p = 303 \text{ K}$) were carried out. The preliminary measurements were carried out before (curve 1 in Fig. 3) and after (curve 2) the low-temperature annealing procedure (at 448 K), when the oxidation of the nanoparticles was negligible. In accordance with the procedure developed in Ref. 35, x_c could be determined from the intersection of curves 1 and 2. This low-temperature heat treatment increased the electrical resistance of the as-deposited composite samples below x_c , while they decreased above x_c . The increase in the resistance for $x < x_c$ was caused by structural relaxation of the dielectric matrix and the increasing distance between the nanoparticles (caused by partial agglomeration of some of them). The decrease in the electrical resistivity of the composites for $x > x_c$ was associated with structural relaxation of the nanoparticles. For this reason, the point of intersection of the $\sigma_L(x)$ curves for the as-deposited and annealed composites can be considered to be the percolation threshold.

The behavior of the $\sigma_L(x)$ dependence is shown in Fig. 3. For the as-deposited samples, three nearly linear regions in the $\sigma_L(x)$ dependence with different slopes in curve 1 could be separated. The first region with x between 39.9 at.% and ~ 52 at.% corresponds to σ_L increasing by approximately two orders of magnitude. In the second (very narrow) region with $52 \text{ at.\%} < x < 55.5 \text{ at.\%}$, where curves 1 and 2 intersect, a sharp increase in σ_L by almost four orders of magnitude was observed. At higher x values, curve 1 in Fig. 3 was saturated, possessing a nearly constant σ_L value (shelf) with x growth up to the highest concentration of metallic atoms. Based on this analysis, the metallic-phase concentration $x_c \approx 53 \pm 2 \text{ at.\%}$ can be considered as the percolation threshold at which the electrically contacting nanoparticles form the first percolating cluster. In this case, the concentration $x \approx 55.5 \text{ at.\%}$ at the beginning of the shelf could be considered as the concentration corresponding to the onset of the whole net of high-conductive (percolating) clusters that formed in the as-deposited composites. The observed x_c is very close to the magnitudes of 55 at.% to 56 at.% detected for as-deposited $(\text{Fe}_{45}\text{Co}_{45}\text{Zr}_{10})_x(\text{PbZrTiO}_3)_{(100-x)}$ films (see Fig. 3a in Ref. 19) and to $x_c \approx 54 \text{ at.\%}$ observed for $(\text{Fe}_{45}\text{Co}_{45}\text{Zr}_{10})_x(\text{Al}_2\text{O}_3)_{(100-x)}$ nanocomposites produced with closed sputtering regimes (see Fig. 3b in Ref. 19).

The complex behavior described for curve 1 in Fig. 3 (in particular, the sharp bend at $x \approx 52\%$) strongly correlates with the similar behavior of $\sigma_L(x)$ that was observed for different frequencies in the as-deposited samples, deposited with closed regimes.^{19,22} Based on the Mössbauer, Raman, and extended x-ray absorption fine structure spectroscopy measurements, the complex $\sigma_L(x)$ behavior below the percolation threshold was attributed to the competition between the formation of an insulating $(\text{Fe}_x\text{Co}_{1-x})_{1-\delta}\text{O}$ core oxide and a semiconducting $\gamma\text{-Fe}(\text{Co})_2\text{O}_3$ shell oxide with x growth.^{19,22} The output of curve 1 on the shelf at $x > x_c$ can be explained by the competition between two processes during deposition:²⁶ the progressive oxidation of the metallic nanoparticles with increasing x [resulting in $\sigma_L(x)$ decreasing] at $x < x_c$, and the tendency to form a less resistive (percolating) net from the oxidized nanoparticles [resulting in $\sigma_L(x)$ increasing because of the significant decrease in the dielectric matrix fraction in the films] at $x > x_c$.

Curve 2 in Fig. 3 shows that, after the samples were annealed at $T_a = 448 \text{ K}$, the $\sigma_L(x)$ dependence changed radically and became linear in the region of $39.9 \text{ at.\%} < x < 67 \text{ at.\%}$. In the concentration range of 52 at.% to 60 at.%, the σ_L values were reduced by almost two orders of magnitude compared with that in the as-deposited sample. When approaching the shelf with an almost constant $\sigma_L(x)$, it was assumed that the concentration was $x \approx 67 \text{ at.\%}$, which is associated with the onset of the formation of a percolation net in the annealed nanocomposites. The

shelf began to shift to a metallic phase with a higher concentration after annealing, confirming the additional oxidation of the CoFeZr nanograins. There was a small excess in σ_L at $x > 67 \text{ at.\%}$ after annealing, compared with the σ_L values in the as-deposited state, in the region where the shelf was caused by an increase in the volume fraction of the semiconducting $\gamma\text{-Fe}(\text{Co})_2\text{O}_3$ oxide during the annealing procedure. As seen in Fig. 3, the value of σ_L for a fully metallic $(\text{Fe}_{45}\text{Co}_{45}\text{Zr}_{10})$ film with $x = 100 \text{ at.\%}$ was 100 times higher than that obtained for a composite film with the maximum concentration of metallic atoms at $x = 88.4 \text{ at.\%}$. This also confirms the strong influence of the oxidation on the admittance of the composites.

The next step was to verify the adequacy of the developed AC hopping conductance model to explain the hopping nature of the NC effect in the annealed nanocomposites. To do this, the samples were annealed at higher temperatures to intensify the oxidation of the FeCoZr-based nanoparticles inside the PbZrTiO₃ matrix. In accordance with the developed model and our previous experiments, the NC effect is usually exhibited in the form of two peculiarities: a positive phase shift (θ) between the applied voltage and current, and also sigmoid-like dependences of the real part of $\sigma(f)$.

To demonstrate the adequacy of the developed model, Fig. 4 shows typical $\sigma(f)$ dependences obtained at different temperatures (T_p) for a sample with $x = 51.7 \text{ at.\%}$ annealed at $T_a = 573 \text{ K}$, when the amount of oxidation was significant. After annealing, this sample displayed a sigmoid-like $\sigma(f)$ dependence [and positive $\theta(f)$ values, as shown in the inset in Fig. 4] over the whole f range and for all of the temperatures studied.

Moreover, in the low-frequency region [$\sigma_L(f_L) \approx \text{const.}$], the value of σ_L at $f < f_L$ was strongly dependent on temperature (Fig. 4). In particular, the σ_L values in this frequency region

Fig. 4. Real part of the admittance versus frequency $\sigma(f)$ for $(\text{Fe}_{45}\text{Co}_{45}\text{Zr}_{10})_{51.7}(\text{PZT})_{48.3}$ nanocomposite films (dots) and the simulated curves (solid lines): 1—168 K, 2—198 K, 3—228 K, 4—258 K, 5—288 K. Inset experimental $\theta(f)$ dependences.

Fig. 5. Factor (α) versus frequency (f) for an annealed $(\text{Fe}_{45}\text{Co}_{45}\text{Zr}_{10})_{51.7}(\text{PZT})_{48.3}$ nanocomposite sample extracted from the experimental (dots) and simulation (solid lines) estimations: 1—168 K, 2—198 K, 3—228 K, 4—258 K, 5—288 K.

Fig. 6. Maximum values of the frequency factor ($\alpha_{\max}$) versus electron jump probability (p) for an $(\text{Fe}_{45}\text{Co}_{45}\text{Zr}_{10})_{51.7}(\text{PZT})_{48.3}$ nanocomposite sample: experimental data (dots) and simulation results (solid line).

increased with temperature, confirming the activation characteristics of the AC conductance in the studied temperature range. Moreover, the width of the f_L range with $\sigma_L \approx \text{const.}$ increased from 100 Hz to 1000 Hz with increasing temperature. In the high-frequency region, the situation was very similar: while the $\sigma_H(f_H)$ curves did not saturate, they converged to one line with very small growth of $\sigma_H(f_H)$ with increasing f at $f > f_H \approx 50$ kHz to 60 kHz.

In the intermediate frequency range of $(100 \text{ Hz to } 1000 \text{ Hz}) < f_M < f_H$, very strong $\sigma_M(f_M)$ dependences were observed, which can be described by Eq. 2. Then, as follows from the model,^{15,19} to check the validity of the developed model for the annealed samples, the probability (p) of the next electron jump after the first one needed to be calculated under the application of an AC bias voltage. It was shown in the “Introduction” that, for the simplest

Fig. 7. Temperature dependences of the low-frequency σ_L for $f = 100$ Hz (1), the high-frequency σ_H for $f = 300$ kHz (2), and the electron jump probability (p) (3) on Arrhenius scales for an annealed nanocomposite $(\text{Fe}_{45}\text{Co}_{45}\text{Zr}_{10})_{51.7}(\text{PZT})_{48.3}$ sample.

case, when the $\sigma(f)$ dependences display sigmoid-like behavior in the studied frequency range, the probability can be extracted with the simple equation

$$p = \frac{\sigma_L}{2\sigma_H}. \quad (3)$$

All of the mathematical relationships that describe the AC hopping model as well as the simulation software for AC conductance, used to estimate the $\sigma(f, p)$ and $\alpha(f, p)$ dependences, are presented in Ref. 15. The model was improved in Ref. 36 to take the unequal distances between the nanoparticles and their size distribution into account, such that the lifetime (τ_m) of an electron in a nanoparticle in Eq. 1 is not constant, having some distribution.

In Fig. 4, the solid lines represent the $\sigma(f)$ dependences, calculated using the discussed model. The values obtained experimentally for the $(\text{Fe}_{45}\text{Co}_{45}\text{Zr}_{10})_{51.7}(\text{PbZrTiO}_3)_{48.3}$ sample were in accordance with the simulations.

Figure 5 shows very good agreement between the frequency dependences of the α factor in the Mott Eq. 2, which were extracted from both the experimental data and the corresponding simulations.

Figure 5 shows that the $\alpha(f)$ dependences exhibit a distinct maximum, in correlation with the model. $\alpha_{\max}$ is shown in Fig. 6 as a function of p . The solid line in Fig. 6 represents the dependence of $\alpha_{\max}(p)$, obtained from simulations at different temperatures. The experimental data points (dots) in Fig. 6, calculated from $\sigma(f)$ for various T_p values in Fig. 4 using formula (3), also show very good agreement between the experimental and simulation results.

To estimate the activation energy of dipole formation (hopping conductance), Fig. 7 presents the temperature dependences of the low-frequency σ_L

($f = 100$ Hz), high-frequency σ_H ($f = 300$ kHz), and electron hopping probability (p), which are Arrhenius plots. The linearization of these curves with an Arrhenius scale allowed for the activation energies to be estimated for AC hopping conductance as follows: $\Delta E(\sigma_L) = 0.153$ eV, $\Delta E(p) = 0.151$ eV, and $\Delta E(\sigma_H) = 0.0013$ eV.

A comparison between the straight lines of the slopes in Fig. 7 indicates that $\Delta E(\sigma_L) \gg \Delta E(\sigma_H)$. This is in accordance with the developed model.^{15,19} The higher $\Delta E(\sigma_L)$ value can be explained as follows: When an electron jumps from the second nanoparticle (charged after the first jump) to the third one in the direction opposite to the applied AC electric field, it must overcome a potential barrier that appears from the formation of dipoles because the electron occupies the second nanoparticle. Alternatively, if the electron returns to the first nanoparticle (which is occupied by a hole), it will be attracted by its positive charge. This will lower the value of the activation energy [$\Delta E(\sigma_H)$] to nearly zero. Considering the almost zero slope of the σ_H versus $(1000/T_p)$ dependence in Fig. 7, it can be concluded that the variations in p versus $(1000/T_p)$ were caused by the great extent of the σ_L versus $(1000/T_p)$ dependence (see Eq. 3). For this reason, $\Delta E(p) \approx \Delta E(\sigma_L)$.

From the presented dependences of the real part of the admittance $\sigma(f, T)$ for $(\text{Fe}_{45}\text{Co}_{45}\text{Zr}_{10})_x(\text{PZT})_{(100-x)}$ nanocomposite films, it can be concluded that, after annealing, they (a) displayed an NC effect over the whole temperature (100 K to 300 K) and frequency (100 Hz to 1 MHz) ranges, and (b) could be well described by the developed AC hopping conductance model.^{9,15,19,22}

CONCLUSIONS

It was established that the real part of $\sigma(f)$ for annealed $(\text{Fe}_{45}\text{Co}_{45}\text{Zr}_{10})_x(\text{PbZrTiO}_3)_{(100-x)}$ films displayed sigmoid-like behavior, accompanied with positive phase shifts between the current and voltage applied over the whole frequency and temperature ranges studied. This behavior confirms that the $\sigma(f, T)$ dependences followed the known Mott relationship $\sigma(f) \sim f^\alpha$. However, in accordance with the developed AC hopping model, the exponent $0 < \alpha < 2$ is the so-called frequency factor, which determines the probability of electron jumping. It is therefore dependent on the frequency (compared with the known Mott model with $\alpha \approx 0.8$). The experimental data and simulation results based on the hopping conductivity model showed very good agreement and allowed a hopping conductance activation energy of ~ 0.15 eV to be estimated.

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CONFLICT OF INTEREST

The authors declare that they have no conflict of interest.

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