Fig. 2—Fracture surfaces of broken tensile specimens tested after (a) dry N_2 anneal, (b) wet N_2 anneal, (c) dry H_2 anneal, and (d) wet N_2 anneal + $250^\circ C$ for 2 h treatment.

2(b) to (d). Figure 2(d) indicates a ductile, dimple-rupture type fracture similar to Fig. 2(a). The fracture behavior discussed in this section agrees well with the trend shown in Table II and Fig. 1.

In large-scale commercial heat treatment, the humidity control of the high-temperature annealing atmosphere may not always be easy. The low-temperature hydrogen-relief treatment such as used in the present work could thus serve as a safety precaution to cure undesirable hydrogen-embrittlement resulting from inadvertently introduced high humidity in the annealing atmosphere.

In summary, the high humidity present in the high temperature annealing atmosphere was found to cause

a hydrogen embrittlement in the Fe-Cr-Co ductile magnet alloy. A low-temperature, hydrogen-relief anneal was found to reduce the hydrogen content of the alloy and restore the ductility of the embrittled alloy.

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Correction to *Met. Trans. A*, 1980, vol. 11A

Iterative Solutions for One-Dimensional Diffusion with Time Varying Surface Composition and Composition-Dependent Diffusion Coefficient by M. Chow and C. R. Houska

Page 111, the 3rd equation should read:

$$n = \frac{t}{\delta t} = \left(\frac{z}{\delta z} \right)^2.$$

Page 112, 1st column, 3rd paragraph. The following sentence should be omitted:

The concentration at an interior point at a time t is given by $C(x, t) = C_S(t)C_F(x, t)$.