CORRIGENDA

SCATTERED RADIATION IN THE OZONE ABSORPTION BANDS AT SELECTED LEVELS OF A TERRESTRIAL, RAYLEIGH ATMOSPHERE

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A computer programming error, discovered after the publication of the monograph, has resulted in incorrect values of I_c^*/Q and I_r^*/Q of the Upward Radiation being listed in Tables 1 through 16. The error arose because the factor $3/16\mu$ in Eq. (26) (see text of monograph) was programmed as $3\mu/16$. Since the factor is associated with only one of the terms on the right-hand side of the equation, the values of I_c^*/Q and I_r^*/Q of the Upward Radiation listed in the tables need to be multiplied by a factor somewhat less than $1/\mu^2$. The values I_c^*/Q and I_r^*/Q of the Upward Radiation are correct at all pressure levels for the nadir direction ($\theta = 0^\circ$) since $\mu = 1$ for this direction of observation.

The appended tables were computed to provide a method for determining the correct values of the reflected component of the upward radiation. In order to keep the size of the errata tables to a minimum without requiring the user to do any more computation than before, values of I_c^*/I_g and I_r^*/I_g are tabulated instead of I_c^*/Q and I_r^*/Q as was done originally. It will be seen

from Eqs. (26) and (30) that the ratios now tabulated are independent of θ_0 . The procedure for using the appended tables is as follows:

1. The value of Q for a given λ and a desired R must first be determined from Eq. (31), using the values of $S^b(\tau_1)$ given in Table B of the monograph.
2. The Q thus obtained, when multiplied by the appropriate value of I_g/Q (also obtained from Table B), then gives I_g for a given θ_0 .
3. Next, the value of I_g from the step above should be multiplied by the values of I_c^*/I_g and I_r^*/I_g given in the appended tables to get I_c^* and I_r^* .
4. The values of I_c^* and I_r^* can then be applied in the manner described in Sec.C.1. (p. 9) in the monograph.

Acknowledgement. We are indebted to our colleague, Dr. Carl L. Mateer, for bringing the discrepancy in the tables to our attention and for his assistance in resolving the problem.

Parameters for computing the reflected component of the Upward Radiation

press. level (mb)	θ	$\lambda = 2875.0 \text{ \AA}$		$\lambda = 2925.0 \text{ \AA}$		$\lambda = 2975.0 \text{ \AA}$		$\lambda = 3025.0 \text{ \AA}$	
		I_e^*/I_0	I_r^*/I_0	I_e^*/I_0	I_r^*/I_0	I_e^*/I_0	I_r^*/I_0	I_e^*/I_0	I_r^*/I_0
0	0	8.590-09	8.590-09	4.747-05	4.747-05	2.752-03	2.752-03	2.892-02	2.892-02
	15	4.605	4.648	3.438	3.465	2.296	2.310	2.621	2.632
	30	5.692-10	5.970-10	1.163	1.206	1.251	1.286	1.883	1.920
	40	4.570-11	5.294-11	3.040-06	3.301-06	5.887-04	6.235-04	1.251	1.301
	50	3.091-12	6.027-12	3.721-07	4.670-07	1.751	1.976	6.473-03	6.971-03
	60	1.309	4.038	3.300-08	7.701-08	2.494-05	3.469-05	2.155	2.511
	70	7.365-13	3.642	1.423	5.409	3.050-06	8.337-06	3.278-04	5.024-04
	75	5.705	3.645	1.159	5.290	2.152	7.166	1.123	2.383
	80	4.699	3.827	1.028	5.503	1.907	7.143	6.888-05	1.807
	85	4.547	4.457	1.060	6.356	2.009	8.135	6.782	1.909
0.18	0	8.672-09	8.672-09	4.770-05	4.770-05	2.759-03	2.759-03	2.896-02	2.896-02
	15	4.651	4.694	3.455	3.482	2.302	2.316	2.624	2.636
	30	5.754-10	6.035-10	1.170	1.213	1.255	1.290	1.886	1.923
	40	4.620-11	5.349-11	3.059-06	3.321-06	5.907-04	6.256-04	1.253	1.303
	50	3.075-12	5.984-12	3.744-07	4.693-07	1.758	1.983	6.487-03	6.985-03
	60	1.279	3.944	3.276-08	7.624-08	2.502-05	3.475-05	2.160	2.516
	70	7.068-13	3.493	1.386	5.264	3.014-06	8.218-06	3.280-04	5.018-04
	75	5.399	3.447	1.117	5.095	2.103	6.995	1.115	2.360
	80	4.350	3.540	9.751-09	5.217	1.840	6.887	6.750-05	1.768
	85	4.019	3.936	9.720	5.825	1.891	7.652	6.520	1.834
1.40	0	1.026-08	1.026-08	5.190-05	5.190-05	2.887-03	2.887-03	2.965-02	2.965-02
	15	5.532-09	5.584-09	3.770	3.799	2.413	2.428	2.688	2.700
	30	6.978-10	7.317-10	1.289	1.337	1.322	1.359	1.937	1.975
	40	5.694-11	6.567-11	3.411-06	3.701-06	6.265-04	6.634-04	1.292	1.343
	50	3.464-12	6.644-12	4.224-07	5.262-07	1.883	2.122	6.722-03	7.235-03
	60	1.304	4.008	3.443-08	7.849-08	2.702-05	3.714-05	2.258	2.624
	70	6.682-13	3.287	1.309	4.936	2.988-06	8.005-06	3.432-04	5.181-04
	75	4.848	3.078	1.008	4.567	1.963	6.467	1.120	2.325
	80	3.612	2.919	8.278-09	4.395	1.620	6.015	6.281-05	1.629
	85	2.904	2.822	7.318	4.350	1.511	6.068	5.547	1.549
6.40	0	4.651-08	4.651-08	1.106-04	1.106-04	4.330-03	4.330-03	3.637-02	3.637-02
	15	2.646	2.670	8.252-05	8.316-05	3.671	3.694	3.322	3.336
	30	3.987-09	4.177-09	3.085	3.198	2.110	2.168	2.453	2.500
	40	3.958-10	4.503-10	9.116-06	9.869-06	1.062	1.123	1.686	1.751
	50	2.055-11	3.615-11	1.321	1.609	3.514-04	3.940-04	9.219-03	9.904-03
	60	5.246-12	1.575	9.760-08	1.991-07	5.773-05	7.647-05	3.366	3.882
	70	2.242	1.064	2.535	9.113-08	5.395-06	1.306	5.736-04	8.231-04
	75	1.491	9.049-12	1.741	7.479	2.876	8.907-06	1.764	3.342
	80	1.034	7.895	1.253	6.279	2.025	7.100	7.816-05	1.907
	85	8.803-13	8.012	9.728-09	5.441	1.535	5.835	5.398	1.437

(mb)	θ	$\lambda = 2875.0 \text{ \AA}$		$\lambda = 2925.0 \text{ \AA}$		$\lambda = 2975.0 \text{ \AA}$		$\lambda = 3025.0 \text{ \AA}$	
18.4	0	2.519-06	2.519-06	8.152-04	8.152-04	1.261-02	1.261-02	6.234-02	6.234-02
	15	1.649	1.664	6.523	6.573	1.110	1.117	5.803	5.827
	30	3.982-07	4.166-07	3.090	3.201	7.244-03	7.439-03	4.567	4.652
	40	6.952-08	7.772-08	1.226	1.322	4.273	4.511	3.401	3.528
	50	5.273-09	7.639-09	2.812-05	3.324-05	1.833	2.038	2.122	2.272
	60	6.812-10	1.869	2.990-06	4.855-06	4.566-04	5.743-04	9.726-03	1.107
	70	2.878	1.218	4.543-07	1.409	5.303-05	1.005	2.454	3.265-03
	75	1.985	1.039	3.046	1.124	2.109	5.438-05	8.785-04	1.405
	80	1.424	9.029-10	2.246	9.454-07	1.351	4.055	3.206	6.637-04
	85	1.125	8.211	1.766	8.153	1.035	3.349	1.966	4.599
32.8	0	5.850-05	5.850-05	3.943-03	3.943-03	2.939-02	2.939-02	9.565-02	9.565-02
	15	4.277	4.316	3.335	3.360	2.665	2.681	9.037	9.075
	30	1.498	1.566	1.904	1.970	1.922	1.972	7.483	7.618
	40	4.128-06	4.573-06	9.540-04	1.026	1.285	1.354	5.938	6.151
	50	5.640-07	7.376-07	3.178	3.693-04	6.771-03	7.481-03	4.115	4.389
	60	5.137-08	1.159	5.596-05	7.997-05	2.378	2.903	2.259	2.544
	70	1.537	5.672-08	6.616-06	1.638	4.259-04	6.785-04	7.955-03	1.011
	75	1.050	4.659	3.536	1.094	1.514	3.112	3.554	5.109-03
	80	7.602-09	3.957	2.439	8.575-06	7.316-05	1.850	1.323	2.310
	85	5.963	3.478	1.866	7.123	5.017	1.384	6.179-04	1.268
56.0	0	1.096-03	1.096-03	1.721-02	1.721-02	6.504-02	6.504-02	1.435-01	1.435-01
	15	8.878-04	8.958-04	1.532	1.543	6.063	6.097	1.375	1.380
	30	4.397	4.588	1.041	1.076	4.802	4.923	1.194	1.215
	40	1.860	2.045	6.486-03	6.946-03	3.613	3.797	1.007	1.040
	50	4.878-05	6.059-05	3.075	3.524	2.308	2.531	7.698-02	8.171-02
	60	7.192-06	1.252	9.470-04	1.259	1.125	1.340	5.011	5.578
	70	1.356	4.006-06	1.722	3.256-04	3.479-03	4.966-03	2.438	2.986
	75	8.456-07	2.969	7.614-05	1.814	1.569	2.627	1.418	1.889
	80	5.849	2.342	4.404	1.221	7.020-04	1.416	6.967-03	1.051
	85	4.563	2.003	3.026	9.102-05	3.977	8.989-04	3.184	5.548-03
132	0	2.031-02	2.031-02	7.651-02	7.651-02	1.481-01	1.481-01	2.222-01	2.222-01
	15	1.821	1.837	7.175	7.223	1.421	1.428	2.163	2.170
	30	1.269	1.319	5.804	5.978	1.239	1.266	1.977	2.005
	40	8.197-03	8.895-03	4.493	4.768	1.051	1.097	1.776	1.825
	50	4.184	4.949	3.026	3.385	8.158-02	8.805-02	1.506	1.580
	60	1.549	2.201	1.653	2.042	5.517	6.323	1.167	1.268
	70	4.492-04	8.760-04	6.867-03	1.022	3.033	3.882	7.839-02	9.085-02
	75	2.525	5.763	4.089	6.863-03	2.051	2.846	5.970	7.271
	80	1.570	4.059	2.405	4.542	1.307	1.986	4.284	5.552
	85	1.116	3.123	1.494	3.101	7.862-03	1.310	2.801	3.909
370	0	1.030-01	1.030-01	1.891-01	1.891-01	2.585-01	2.585-01	3.149-01	3.149-01
	15	9.751-02	9.808-02	1.828	1.836	2.527	2.535	3.101	3.106
	30	8.145	8.359	1.636	1.667	2.345	2.376	2.947	2.969
	40	6.553	6.908	1.432	1.486	2.145	2.198	2.773	2.812
	50	4.685	5.184	1.165	1.246	1.869	1.952	2.525	2.587
	60	2.818	3.428	8.500-02	9.585-02	1.512	1.629	2.184	2.276
	70	1.411	2.054	5.329	6.633	1.092	1.246	1.739	1.869
	75	1.005	1.626	4.053	5.407	8.867-02	1.056	1.491	1.643
	80	7.689-03	1.347	3.154	4.497	7.165	8.956-02	1.258	1.429
	85	6.237	1.151	2.569	3.843	5.937	7.735	1.069	1.255

Parameters for computing the reflected component of the Upward Radiation

press. level (mb)	θ	$\lambda = 3075.0 \text{ \AA}$		$\lambda = 3125.0 \text{ \AA}$		$\lambda = 3175.0 \text{ \AA}$		$\lambda = 3225.0 \text{ \AA}$	
		I_o^*/I_g	I_r^*/I_g	I_o^*/I_g	I_r^*/I_g	I_o^*/I_g	I_r^*/I_g	I_o^*/I_g	I_r^*/I_g
0	0	9.257-02	9.257-02	1.779-01	1.779-01	2.351-01	2.351-01	2.779-01	2.779-01
	15	8.738	8.764	1.719	1.722	2.293	2.296	2.727	2.729
	30	7.204	7.300	1.531	1.544	2.111	2.124	2.560	2.571
	40	5.679	5.828	1.329	1.351	1.908	1.930	2.370	2.390
	50	3.877	4.068	1.061	1.093	1.626	1.661	2.100	2.132
	60	2.051	2.246	7.310-02	7.728-02	1.251	1.301	1.724	1.773
	70	6.458-03	7.886-03	3.732	4.175	7.852-02	8.482-02	1.221	1.291
	75	2.557	3.589	2.122	2.520	5.326	5.980	9.217-02	1.002
	80	8.916-04	1.620	9.087-03	1.217	2.920	3.520	5.997	6.851-02
	85	5.879	1.251	3.427	5.641-03	1.118	1.563	2.814	3.550
0.18	0	9.265-02	9.265-02	1.780-01	1.780-01	2.351-01	2.351-01	2.780-01	2.780-01
	15	8.745	8.771	1.719	1.723	2.294	2.297	2.727	2.730
	30	7.210	7.306	1.532	1.545	2.112	2.124	2.561	2.571
	40	5.684	5.834	1.330	1.352	1.909	1.931	2.371	2.391
	50	3.881	4.072	1.061	1.094	1.627	1.662	2.100	2.132
	60	2.054	2.249	7.316-02	7.734-02	1.252	1.302	1.725	1.774
	70	6.468-03	7.894-03	3.736	4.178	7.858-02	8.487-02	1.222	1.292
	75	2.558	3.586	2.124	2.522	5.331	5.984	9.222-02	1.003
	80	8.858-04	1.606	9.085-03	1.215	2.921	3.520	6.000	6.853-02
	85	5.739	1.220	3.390	5.576-03	1.113	1.555	2.810	3.545
1.40	0	9.381-02	9.381-02	1.792-01	1.792-01	2.361-01	2.361-01	2.787-01	2.787-01
	15	8.858	8.885	1.731	1.734	2.303	2.306	2.735	2.737
	30	7.314	7.411	1.543	1.556	2.122	2.134	2.568	2.579
	40	5.777	5.928	1.341	1.363	1.919	1.941	2.379	2.399
	50	3.956	4.149	1.072	1.105	1.637	1.672	2.109	2.141
	60	2.104	2.301	7.408-02	7.828-02	1.262	1.311	1.734	1.782
	70	6.673-03	8.117-03	3.800	4.245	7.942-02	8.572-02	1.230	1.300
	75	2.637	3.665	2.167	2.566	5.400	6.054	9.302-02	1.011
	80	8.810-04	1.575	9.249-03	1.230	2.965	3.562	6.064	6.914-02
	85	5.183	1.094	3.270	5.333-03	1.109	1.539	2.827	3.552
6.40	0	1.044-01	1.044-01	1.891-01	1.891-01	2.439-01	2.439-01	2.844-01	2.844-01
	15	9.898-02	9.927-02	1.830	1.834	2.382	2.385	2.792	2.795
	30	8.278	8.385	1.642	1.656	2.202	2.215	2.629	2.639
	40	6.642	6.814	1.438	1.462	2.002	2.024	2.442	2.462
	50	4.670	4.892	1.165	1.200	1.721	1.756	2.175	2.207
	60	2.598	2.833	8.238-02	8.690-02	1.345	1.396	1.804	1.853
	70	8.956-03	1.075	4.417	4.910	8.694-02	9.356-02	1.301	1.373
	75	3.734	5.022-03	2.617	3.069	6.058	6.756	9.989-02	1.082
	80	1.203	2.017	1.172	1.520	3.458	4.107	6.684	7.573-02
	85	5.417-04	1.095	3.811-03	5.970-03	1.317	1.778	3.237	4.006

(mb)	θ	$\lambda = 3075.0 \text{ \AA}$		$\lambda = 3125.0 \text{ \AA}$		$\lambda = 3175.0 \text{ \AA}$		$\lambda = 3225.0 \text{ \AA}$	
18.4	0	1.384-01	1.384-01	2.178-01	2.178-01	2.654-01	2.654-01	2.996-01	2.996-01
	15	1.325	1.329	2.119	2.122	2.600	2.603	2.948	2.950
	30	1.146	1.160	1.933	1.949	2.428	2.441	2.792	2.802
	40	9.592-02	9.828-02	1.729	1.756	2.235	2.258	2.614	2.634
	50	7.227	7.553	1.450	1.491	1.961	1.999	2.358	2.390
	60	4.535	4.916	1.089	1.145	1.589	1.645	1.999	2.049
	70	1.974	2.317	6.582-02	7.246-02	1.103	1.180	1.507	1.582
	75	9.983-03	1.273	4.357	5.015	8.227-02	9.079-02	1.206	1.297
	80	3.811	5.670-03	2.326	2.894	5.284	6.148	8.695-02	9.731-02
	85	1.460	2.645	8.669-03	1.248	2.447	3.143	4.927	5.926
32.8	0	1.735-01	1.735-01	2.442-01	2.442-01	2.845-01	2.845-01	3.130-01	3.130-01
	15	1.674	1.679	2.385	2.389	2.793	2.797	3.084	3.087
	30	1.487	1.505	2.206	2.223	2.631	2.644	2.937	2.947
	40	1.287	1.317	2.007	2.036	2.446	2.470	2.768	2.786
	50	1.024	1.068	1.731	1.776	2.184	2.223	2.523	2.554
	60	7.077-02	7.626-02	1.364	1.429	1.822	1.881	2.178	2.228
	70	3.713	4.284	9.074-02	9.902-02	1.340	1.425	1.701	1.779
	75	2.213	2.723	6.564	7.442	1.054	1.153	1.407	1.503
	80	1.046	1.434	4.069	4.907	7.453-02	8.521-02	1.078	1.193
	85	3.909-03	6.321-03	1.853	2.488	4.149	5.124	6.971-02	8.188-02
56.0	0	2.154-01	2.154-01	2.733-01	2.733-01	3.051-01	3.051-01	3.277-01	3.277-01
	15	2.094	2.100	2.680	2.684	3.004	3.007	3.234	3.236
	30	1.909	1.930	2.512	2.529	2.853	2.865	3.096	3.105
	40	1.706	1.743	2.324	2.354	2.680	2.703	2.938	2.955
	50	1.431	1.487	2.059	2.107	2.433	2.471	2.707	2.736
	60	1.083	1.158	1.701	1.772	2.089	2.148	2.380	2.427
	70	6.784-02	7.686-02	1.239	1.338	1.624	1.714	1.926	2.002
	75	4.745	5.653	9.757-02	1.087	1.346	1.454	1.646	1.743
	80	2.882	3.704	7.003	8.194-02	1.043	1.169	1.335	1.457
	85	1.407	2.026	4.186	5.289	7.065-02	8.405-02	9.842-02	1.127
132	0	2.761-01	2.761-01	3.151-01	3.151-01	3.366-01	3.366-01	3.521-01	3.521-01
	15	2.708	2.713	3.105	3.109	3.325	3.327	3.484	3.485
	30	2.540	2.563	2.960	2.974	3.194	3.203	3.363	3.369
	40	2.353	2.393	2.795	2.821	3.043	3.060	3.223	3.234
	50	2.093	2.155	2.558	2.601	2.824	2.853	3.018	3.037
	60	1.745	1.836	2.231	2.297	2.513	2.560	2.722	2.754
	70	1.311	1.435	1.795	1.894	2.086	2.162	2.304	2.361
	75	1.074	1.214	1.541	1.661	1.828	1.925	2.044	2.121
	80	8.391-02	9.907-02	1.276	1.418	1.552	1.675	1.762	1.866
	85	6.066	7.577	1.001	1.161	1.266	1.416	1.471	1.608
370	0	3.511-01	3.511-01	3.757-01	3.757-01	3.892-01	3.892-01	3.990-01	3.990-01
	15	3.471	3.474	3.725	3.726	3.863	3.863	3.963	3.963
	30	3.344	3.356	3.618	3.622	3.768	3.768	3.877	3.874
	40	3.197	3.219	3.494	3.502	3.657	3.657	3.774	3.770
	50	2.982	3.019	3.309	3.323	3.489	3.491	3.618	3.612
	60	2.676	2.734	3.038	3.062	3.238	3.244	3.382	3.376
	70	2.251	2.337	2.644	2.686	2.862	2.878	3.019	3.018
	75	1.995	2.101	2.393	2.450	2.614	2.642	2.774	2.781
	80	1.732	1.862	2.121	2.199	2.336	2.382	2.490	2.512
	85	1.503	1.656	1.869	1.974	2.069	2.143	2.208	2.259

Parameters for computing the reflected component of the Upward Radiation

press. level (mb)	θ	$\lambda = 3300.0 \text{ \AA}$		$\lambda = 3400.0 \text{ \AA}$		$\lambda = 3600.0 \text{ \AA}$		$\lambda = 4950.0 \text{ \AA}$	
		I_o^*/I_g	I_r^*/I_g	I_o^*/I_g	I_r^*/I_g	I_o^*/I_g	I_r^*/I_g	I_o^*/I_g	I_r^*/I_g
0	0	3.395-01	3.395-01	3.585-01	3.585-01	3.871-01	3.871-01	4.615-01	4.615-01
	15	3.354	3.356	3.548	3.549	3.839	3.840	4.602	4.602
	30	3.224	3.230	3.429	3.433	3.737	3.740	4.560	4.560
	40	3.073	3.085	3.289	3.298	3.617	3.622	4.507	4.508
	50	2.852	2.872	3.081	3.097	3.433	3.443	4.423	4.424
	60	2.534	2.568	2.776	2.805	3.154	3.174	4.279	4.282
	70	2.079	2.141	2.329	2.382	2.723	2.761	4.008	4.013
	75	1.791	1.874	2.037	2.111	2.425	2.481	3.766	3.774
	80	1.463	1.573	1.702	1.807	2.068	2.156	3.362	3.377
	85	1.075	1.215	1.320	1.464	1.680	1.820	2.606	2.642
0.18	0	3.395-01	3.395-01	3.585-01	3.585-01	3.871-01	3.871-01	4.615-01	4.615-01
	15	3.355	3.356	3.548	3.549	3.840	3.840	4.602	4.602
	30	3.225	3.230	3.429	3.433	3.738	3.740	4.560	4.560
	40	3.074	3.085	3.289	3.298	3.617	3.622	4.508	4.508
	50	2.853	2.873	3.082	3.098	3.433	3.444	4.423	4.424
	60	2.534	2.569	2.777	2.805	3.155	3.174	4.280	4.282
	70	2.080	2.141	2.329	2.382	2.723	2.761	4.009	4.013
	75	1.792	1.874	2.038	2.112	2.425	2.482	3.766	3.774
	80	1.463	1.574	1.702	1.807	2.068	2.156	3.362	3.377
	85	1.076	1.215	1.320	1.464	1.681	1.821	2.606	2.643
1.40	0	3.398-01	3.398-01	3.588-01	3.588-01	3.873-01	3.873-01	4.616-01	4.616-01
	15	3.358	3.359	3.551	3.552	3.842	3.842	4.603	4.603
	30	3.228	3.234	3.432	3.436	3.740	3.742	4.561	4.561
	40	3.078	3.089	3.292	3.301	3.619	3.624	4.509	4.509
	50	2.857	2.877	3.085	3.101	3.436	3.446	4.424	4.425
	60	2.539	2.573	2.781	2.809	3.158	3.176	4.281	4.283
	70	2.085	2.146	2.333	2.386	2.726	2.764	4.011	4.015
	75	1.797	1.879	2.042	2.116	2.428	2.485	3.769	3.776
	80	1.469	1.579	1.707	1.811	2.072	2.159	3.365	3.380
	85	1.080	1.219	1.325	1.468	1.684	1.824	2.610	2.646
6.40	0	3.418-01	3.418-01	3.602-01	3.602-01	3.881-01	3.881-01	4.621-01	4.621-01
	15	3.378	3.379	3.566	3.566	3.850	3.850	4.608	4.608
	30	3.250	3.255	3.447	3.451	3.749	3.751	4.567	4.567
	40	3.101	3.111	3.309	3.317	3.629	3.633	4.515	4.515
	50	2.882	2.901	3.104	3.119	3.447	3.456	4.431	4.432
	60	2.567	2.600	2.801	2.829	3.170	3.188	4.290	4.292
	70	2.117	2.176	2.357	2.408	2.740	2.777	4.023	4.027
	75	1.831	1.912	2.068	2.140	2.444	2.498	3.783	3.791
	80	1.506	1.615	1.735	1.838	2.088	2.174	3.384	3.398
	85	1.123	1.262	1.358	1.501	1.703	1.840	2.635	2.671

(mb)	θ	$\lambda = 3300.0 \text{ \AA}$		$\lambda = 3400.0 \text{ \AA}$		$\lambda = 3600.0 \text{ \AA}$		$\lambda = 4950.0 \text{ \AA}$	
18.4	0	3.467-01	3.467-01	3.637-01	3.637-01	3.900-01	3.900-01	4.633-01	4.633-01
	15	3.429	3.430	3.602	3.602	3.870	3.870	4.621	4.621
	30	3.304	3.309	3.486	3.490	3.770	3.772	4.581	4.581
	40	3.159	3.169	3.351	3.358	3.652	3.656	4.531	4.531
	50	2.947	2.964	3.150	3.164	3.473	3.481	4.450	4.451
	60	2.639	2.670	2.854	2.879	3.200	3.216	4.313	4.315
	70	2.200	2.256	2.418	2.466	2.775	2.808	4.054	4.057
	75	1.922	1.999	2.134	2.202	2.481	2.532	3.821	3.827
	80	1.608	1.715	1.809	1.909	2.128	2.209	3.433	3.445
	85	1.249	1.390	1.452	1.592	1.749	1.881	2.703	2.736
32.8	0	3.515-01	3.515-01	3.673-01	3.673-01	3.921-01	3.921-01	4.645-01	4.645-01
	15	3.478	3.479	3.638	3.639	3.892	3.892	4.633	4.633
	30	3.357	3.361	3.526	3.528	3.794	3.796	4.594	4.594
	40	3.216	3.224	3.394	3.400	3.678	3.681	4.546	4.546
	50	3.009	3.024	3.197	3.209	3.502	3.509	4.467	4.468
	60	2.709	2.737	2.907	2.929	3.233	3.247	4.335	4.336
	70	2.279	2.332	2.479	2.522	2.813	2.843	4.083	4.086
	75	2.008	2.081	2.199	2.263	2.522	2.568	3.857	3.862
	80	1.704	1.807	1.882	1.976	2.171	2.247	3.479	3.489
	85	1.368	1.508	1.540	1.677	1.797	1.922	2.765	2.795
56.0	0	3.576-01	3.576-01	3.721-01	3.721-01	3.954-01	3.954-01	4.659-01	4.659-01
	15	3.540	3.541	3.687	3.688	3.925	3.925	4.648	4.648
	30	3.424	3.427	3.579	3.581	3.830	3.831	4.611	4.611
	40	3.288	3.295	3.451	3.455	3.717	3.719	4.564	4.564
	50	3.088	3.101	3.261	3.269	3.546	3.550	4.489	4.489
	60	2.797	2.821	2.978	2.996	3.283	3.293	4.362	4.362
	70	2.379	2.425	2.559	2.597	2.870	2.895	4.120	4.121
	75	2.115	2.181	2.285	2.341	2.582	2.621	3.901	3.904
	80	1.822	1.917	1.974	2.060	2.234	2.301	3.535	3.542
	85	1.511	1.646	1.650	1.779	1.864	1.979	2.838	2.864
132	0	3.725-01	3.725-01	3.848-01	3.848-01	4.052-01	4.052-01	4.694-01	4.694-01
	15	3.692	3.692	3.818	3.818	4.025	4.025	4.684	4.684
	30	3.587	3.587	3.719	3.719	3.939	3.938	4.650	4.650
	40	3.464	3.465	3.603	3.603	3.836	3.834	4.609	4.608
	50	3.280	3.284	3.428	3.429	3.678	3.676	4.541	4.539
	60	3.010	3.019	3.165	3.170	3.433	3.433	4.426	4.424
	70	2.613	2.638	2.767	2.785	3.042	3.050	4.205	4.202
	75	2.359	2.399	2.502	2.533	2.762	2.781	4.004	4.001
	80	2.075	2.141	2.197	2.253	2.418	2.457	3.662	3.661
	85	1.790	1.893	1.887	1.983	2.048	2.130	2.994	3.005
370	0	4.116-01	4.116-01	4.199-01	4.199-01	4.338-01	4.338-01	4.784-01	4.784-01
	15	4.093	4.092	4.178	4.177	4.320	4.318	4.777	4.777
	30	4.018	4.011	4.108	4.102	4.259	4.253	4.754	4.752
	40	3.927	3.916	4.023	4.012	4.185	4.175	4.724	4.722
	50	3.788	3.772	3.892	3.875	4.068	4.052	4.676	4.672
	60	3.574	3.551	3.686	3.663	3.880	3.857	4.593	4.587
	70	3.234	3.208	3.351	3.322	3.560	3.530	4.431	4.420
	75	2.995	2.972	3.107	3.078	3.312	3.280	4.278	4.264
	80	2.707	2.693	2.799	2.779	2.976	2.947	4.007	3.988
	85	2.408	2.421	2.466	2.472	2.568	2.562	3.417	3.393

Parameters for computing the reflected component of the Upward Radiation

press. level (mb)	θ	$\lambda = 5350.0 \text{ \AA}$		$\lambda = 5750.0 \text{ \AA}$		$\lambda = 6150.0 \text{ \AA}$		$\lambda = 6550.0 \text{ \AA}$	
		I_e^*/I_g	I_r^*/I_g	I_e^*/I_g	I_r^*/I_g	I_e^*/I_g	I_r^*/I_g	I_e^*/I_g	I_r^*/I_g
0	0	4.625-01	4.625-01	4.611-01	4.611-01	4.665-01	4.665-01	4.784-01	4.784-01
	15	4.612	4.612	4.598	4.598	4.654	4.654	4.777	4.777
	30	4.570	4.570	4.554	4.554	4.616	4.616	4.752	4.752
	40	4.518	4.518	4.499	4.500	4.568	4.569	4.720	4.721
	50	4.433	4.434	4.410	4.412	4.490	4.491	4.669	4.670
	60	4.288	4.290	4.258	4.260	4.356	4.358	4.580	4.581
	70	4.009	4.013	3.962	3.966	4.093	4.096	4.401	4.403
	75	3.753	3.760	3.688	3.694	3.845	3.849	4.229	4.231
	80	3.310	3.322	3.207	3.216	3.400	3.407	3.909	3.912
	85	2.400	2.426	2.186	2.204	2.403	2.416	3.124	3.131
0.18	0	4.625-01	4.625-01	4.611-01	4.611-01	4.665-01	4.665-01	4.784-01	4.784-01
	15	4.612	4.612	4.598	4.598	4.654	4.654	4.777	4.777
	30	4.570	4.571	4.554	4.555	4.616	4.616	4.752	4.752
	40	4.518	4.519	4.499	4.500	4.568	4.569	4.721	4.721
	50	4.433	4.434	4.410	4.412	4.490	4.491	4.669	4.670
	60	4.288	4.290	4.258	4.260	4.356	4.358	4.580	4.581
	70	4.009	4.014	3.962	3.966	4.093	4.096	4.401	4.403
	75	3.753	3.760	3.688	3.694	3.845	3.850	4.229	4.231
	80	3.311	3.322	3.207	3.217	3.401	3.407	3.909	3.912
	85	2.401	2.426	2.187	2.205	2.404	2.417	3.124	3.132
1.40	0	4.626-01	4.626-01	4.613-01	4.613-01	4.667-01	4.667-01	4.785-01	4.785-01
	15	4.614	4.614	4.600	4.600	4.656	4.656	4.778	4.778
	30	4.572	4.572	4.557	4.557	4.618	4.618	4.753	4.753
	40	4.520	4.520	4.502	4.503	4.571	4.571	4.722	4.722
	50	4.435	4.436	4.414	4.415	4.493	4.494	4.671	4.671
	60	4.291	4.293	4.262	4.264	4.360	4.362	4.582	4.583
	70	4.013	4.017	3.968	3.972	4.098	4.101	4.404	4.406
	75	3.758	3.764	3.695	3.701	3.852	3.856	4.233	4.235
	80	3.316	3.328	3.216	3.225	3.409	3.415	3.914	3.917
	85	2.408	2.433	2.197	2.215	2.415	2.428	3.132	3.140
6.40	0	4.638-01	4.638-01	4.631-01	4.631-01	4.684-01	4.684-01	4.795-01	4.795-01
	15	4.626	4.626	4.619	4.619	4.673	4.674	4.788	4.788
	30	4.585	4.585	4.577	4.577	4.637	4.638	4.764	4.764
	40	4.534	4.535	4.525	4.526	4.592	4.593	4.734	4.734
	50	4.452	4.453	4.440	4.441	4.519	4.520	4.685	4.685
	60	4.312	4.314	4.295	4.297	4.392	4.393	4.600	4.600
	70	4.042	4.046	4.012	4.016	4.141	4.144	4.429	4.431
	75	3.793	3.800	3.750	3.755	3.905	3.909	4.265	4.267
	80	3.363	3.373	3.287	3.296	3.479	3.486	3.957	3.961
	85	2.473	2.497	2.292	2.310	2.514	2.526	3.201	3.208

(mb)	θ	$\lambda = 5350.0 \text{ \AA}$		$\lambda = 5750.0 \text{ \AA}$		$\lambda = 6150.0 \text{ \AA}$		$\lambda = 6550.0 \text{ \AA}$	
18.4	0	4.668-01	4.668-01	4.678-01	4.678-01	4.729-01	4.729-01	4.819-01	4.819-01
	15	4.656	4.657	4.667	4.667	4.719	4.720	4.813	4.813
	30	4.619	4.619	4.630	4.631	4.688	4.689	4.792	4.792
	40	4.573	4.573	4.585	4.586	4.649	4.650	4.765	4.766
	50	4.497	4.498	4.510	4.512	4.586	4.586	4.722	4.722
	60	4.368	4.370	4.382	4.384	4.475	4.477	4.647	4.647
	70	4.118	4.122	4.132	4.136	4.257	4.260	4.495	4.496
	75	3.888	3.893	3.898	3.903	4.050	4.054	4.349	4.350
	80	3.487	3.497	3.481	3.490	3.673	3.679	4.074	4.077
	85	2.651	2.674	2.565	2.582	2.796	2.808	3.389	3.395
32.8	0	4.693-01	4.693-01	4.716-01	4.716-01	4.765-01	4.765-01	4.839-01	4.839-01
	15	4.682	4.682	4.707	4.707	4.757	4.757	4.833	4.833
	30	4.648	4.648	4.674	4.675	4.730	4.730	4.814	4.815
	40	4.605	4.605	4.634	4.635	4.696	4.696	4.791	4.791
	50	4.535	4.536	4.568	4.569	4.640	4.641	4.752	4.753
	60	4.415	4.416	4.454	4.456	4.544	4.545	4.685	4.686
	70	4.183	4.186	4.232	4.235	4.353	4.355	4.550	4.551
	75	3.968	3.973	4.022	4.027	4.170	4.174	4.418	4.419
	80	3.593	3.602	3.646	3.654	3.836	3.841	4.171	4.173
	85	2.806	2.828	2.806	2.823	3.043	3.055	3.548	3.554
56.0	0	4.719-01	4.719-01	4.754-01	4.754-01	4.800-01	4.800-01	4.858-01	4.858-01
	15	4.709	4.709	4.746	4.746	4.793	4.793	4.854	4.854
	30	4.678	4.678	4.718	4.718	4.770	4.770	4.837	4.837
	40	4.638	4.639	4.683	4.683	4.741	4.741	4.816	4.817
	50	4.574	4.575	4.625	4.626	4.694	4.694	4.783	4.783
	60	4.464	4.465	4.526	4.528	4.611	4.612	4.723	4.724
	70	4.251	4.252	4.332	4.334	4.448	4.449	4.604	4.604
	75	4.052	4.056	4.147	4.151	4.290	4.293	4.488	4.489
	80	3.705	3.711	3.815	3.821	4.000	4.004	4.268	4.270
	85	2.970	2.989	3.061	3.076	3.302	3.312	3.712	3.716
132	0	4.759-01	4.759-01	4.802-01	4.802-01	4.843-01	4.843-01	4.884-01	4.884-01
	15	4.751	4.751	4.796	4.796	4.838	4.838	4.880	4.880
	30	4.724	4.724	4.773	4.773	4.820	4.820	4.867	4.867
	40	4.690	4.690	4.745	4.745	4.797	4.797	4.850	4.850
	50	4.635	4.635	4.699	4.699	4.760	4.760	4.822	4.822
	60	4.541	4.540	4.619	4.619	4.695	4.695	4.774	4.773
	70	4.356	4.355	4.460	4.461	4.565	4.565	4.675	4.675
	75	4.183	4.182	4.309	4.310	4.439	4.440	4.579	4.579
	80	3.876	3.876	4.034	4.036	4.205	4.206	4.397	4.397
	85	3.212	3.220	3.394	3.401	3.629	3.634	3.927	3.928
370	0	4.833-01	4.833-01	4.867-01	4.867-01	4.895-01	4.895-01	4.921-01	4.921-01
	15	4.828	4.827	4.862	4.862	4.892	4.892	4.918	4.918
	30	4.809	4.808	4.847	4.847	4.880	4.879	4.909	4.909
	40	4.786	4.784	4.828	4.827	4.864	4.864	4.898	4.897
	50	4.747	4.745	4.797	4.796	4.840	4.839	4.879	4.878
	60	4.681	4.677	4.742	4.740	4.796	4.794	4.845	4.844
	70	4.549	4.542	4.633	4.629	4.707	4.705	4.778	4.776
	75	4.422	4.413	4.526	4.521	4.621	4.617	4.710	4.708
	80	4.189	4.177	4.327	4.320	4.455	4.450	4.580	4.577
	85	3.642	3.625	3.830	3.820	4.025	4.018	4.231	4.225