Mean Effective Gain of Compact WLAN Genetic Printed Dipole Antennas in Indoor-Outdoor Scenarios

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Abstract. Two dual-printed dipole antennas for WLAN applications operating in the 802.11 a/b/g (2.4-2.5 GHz and 4.9-5.875 GHz) frequency bands are presented. Genetic Algorithm optimization (GA) is applied first, to a classical dual band printed dipole antenna schema. Later on, a pre-fractal technique is proposed on the larger strip and electromagnetic parameters are re-optimized to achieve a more compact radiator. Frequency performance of both antennas is introduced showing a $VSWR < 1.5$ for a input impedance of 50 Ohms. Finally, the mean effective gain (MEG) is worked out considering several scenarios. Results for both antennas for typical indoor and outdoor environments are given using the statistical angle of arrival behavior of such environments.

Index terms - WLAN, printed dipole antennas, genetic algorithms, Mean Effective Gain.

1 Introduction

In the last few years, the development of wireless local area networks (WLANs) was one of the main research focus in the information and communications field. Therefore, a strong effort in antenna design to provide wireless coverage with low cost has been a key factor to accomplish the WLAN development.

In this paper, a radiating element is designed to adopt the standard printed circuit board (PCB) substrate and production technology. The uniqueness of the design comes from an evolving optimization procedure applied to a classical dual printed dipole antenna (DPDA) [1] used previously in 2 and 3G base station systems combined with a pre-fractal topology [2] to reduce the size. Additionally, since the antenna is oriented to be used in a mobile device, a traditional approach to evaluate the electromagnetic performances is not enough to predict the overall behavior in a wireless scenario. The Mean Effective Gain (MEG) [3], is a recently defined parameter to include the mobile channel characteristics (those referred to spatial and polarization properties). This parameter is computed for the radiating elements placed in typical scenarios: indoor and indoor-outdoor urban.

In section II, the antenna geometries and design outlines are presented, showing the evolution of the GA applied. In section III, classical electromagnetic parameters (S-parameters, Gain) coming from the optimization are showed. In section IV, MEG results are presented. Finally, a conclusion is provided.

2 Dual Printed Dipole Antenna (DPDA) Designs with GA

2.1 Antenna Geometries of PDA

Fig.1 shows a schematic drawing of the antennas showing the genes involved in the genetic optimization. In the classical DPDA, two printed strip dipoles of different lengths, with the arms printed on opposite sides of an electrically thin dielectric substrate are connected through a parallel stripline (PS). In the case of the pre-fractal printed dipole antenna (PF-DPDA), the first iteration of a fractal tree is applied to the longer element so that the size can be reduced. In order to achieve an optimal dual-frequency radiator, the line polarity between the radiating elements must be inverted. The antennas were designed on a dielectric substrate of height $h = 1.6\text{mm}$, relative permittivity $\epsilon = 4.5$ and loss tangent $\tan(\delta) = 0.02$.

Fig. 1. Return Losses of DPDA and PF-DPDA

2.2 Evolutive Optimization (GA) Results

A genetic optimization method was applied for each geometry (DPDA PF-DPDA). Six and eight genes are codified using 30 bits in a binary codification, respectively. A simple GA with typical parameters $p_{cross} = 0.65$, $p_{mut} = 0.01$, size population of 30 individuals was let to evolve during 150 generations in DPDA and 100 generations in PF-DPDA. The *Fitness function* was:

$$F = |R_{in}(\omega_1) - 50| + |R_{in}(\omega_2) - 50| + |R_{in}(\omega_1) - R_{in}(\omega_2)| + |X_{in}(\omega_1)| + |X_{in}(\omega_2)| \quad (1)$$

Table 1. Optimum chromosomes found by GA simple

Gene	DPDA(mm)	PF-DPDA(mm)
L1	45.054	26.2694
L2	19.3643	21.3248
D	12.5259	13.2189
W1	5.5733	5.9203
W2	2.7896	2.5660
WP	2.9568	2.5019
L3	—	14.8525
α	—	30.9282

Fig. 2. Gain Pattern of PF-PDA Antenna

where $Z_{in}(\omega_i) = R_{in}(\omega_i) + jX_{in}(\omega_i)$ is the antenna input impedance at ω_i frequency.

With this fitness function, a resonant 50Ω input impedance at both frequencies is looked for. The frequencies chosen for WLAN were 2.45 and 5.4 GHz. The antenna parameters were obtained from a standard MoM simulation program. Table 1 shows the optimized parameters for each antenna and Fig. 2 the fitness function convergence towards the optimum.

As observed, computing the Size Reduction as

$$\text{size reduction} = \frac{L_1^{DPDA} - L_1^{PFDPDA} - L_3/2 \cos(\alpha)}{L_1^{DPDA}} \quad (2)$$

a 27.55% of compactness is achieved thanks to the pre-fractal method.

3 Classical Performances for the Radiating Configurations

The classical analysis of antennas comprises, among others, these main quantities: the S-parameters, impedance bandwidth and the gain radiation pattern.

Fig. 3. Return Losses of DPDA and PF-DPDA

Fig. 4. Return Losses of DPDA and PF-DPDA

Fig. 5. Gain Pattern of PF-DPDA Antenna

Fig. 6. Gain Pattern of PF-DPDA Antenna

The S_{11} is plotted in Fig.3-4. Considering a $|Γ| < -15dB$ as bandwidth criteria, it is obvious that the antennas are radiating in the whole WLAN frequencies specified.

Regarding the pattern, Fig.5-6 represents the E and H plane cuts. It is observed that the antennas have almost an omnidirectional diagram in the lower band while in the upper band the pattern is more directive. Table 2 summarizes the classical performances.

Table 2. Antenna main traditional parameters

Parameter	DPDA	PF-DPDA
Bandwidth WLAN 1 (MHz)	220	360
Bandwidth WLAN 2 (MHz)	900	1455
Directivity WLAN 1 (dBi)	1.73	1.71
Directivity WLAN 2 (dBi)	4.6	3.38
Gain WLAN 1 (dBi)	0.54	0.67
Gain WLAN 2 (dBi)	1.11	0.52

4 Effective Gain Analysis in WLAN Environments

4.1 Method of Analysis

As mentioned, the MEG is a statistical measurement of the antenna performance in a multipath environment. The mean power received from the antenna can be obtained from the radiation patterns and the statistics of the channel using this concept. The MEG of an antenna, which is defined as the ratio of the mean received to the mean incident power at the antenna, can be calculated from [4],

$$MEG = \oint \left[\frac{\Gamma}{1+\Gamma} P_{\theta}(\Omega) G_{\theta}(\Omega) + \frac{1}{1+\Gamma} P_{\phi}(\Omega) G_{\phi}(\Omega) \right] d\Omega \quad (3)$$

where G_{θ} and G_{ϕ} are the θ and ϕ polarized components of the antenna power gain pattern, Ω is the solid angle (θ, ϕ), P_{θ} and P_{ϕ} are the θ and ϕ components of the angular density functions of the incoming plane waves. Γ is the crosspolarization power ratio, defined as the ratio of the mean received power in the vertical polarization to the mean received power in the horizontal polarization. The crosspolarization power ratio (Γ or also known as XPD) varies considerably, depending on the surrounding environment. Thus, these values must be concreted according to the mobile application of interest.

4.2 Incident Wave Statistics for WLAN Environments

As a result of the large amount of interest in the wireless channel, several probability density functions have been proposed [5], [6], [7], validated through measurements. First results were related to the temporal properties of the propagation environment, and finally, a focus in the angular power distribution motivated

by the emerging MIMO systems has brought several models for the incident wave statistics. In the case of the XPR, it is shown that its value is between 0 dB and 9 dB in most cases, although in some environments can achieve 11 dB.

When a WLAN indoor environment it is considered, two possible scenarios may be of interest:

Indoor Environment

The antenna is assumed to be working inside a building. Measurements [8] have shown that the power azimuth spectrum P_ϕ is best modeled by a Laplacian function for both polarization. A Gaussian function for the elevation is assumed. Therefore, for the DPDA and PF-DPDA antennas:

$$P_\phi(\theta, \phi) = A_\phi e^{-\left|\frac{\sqrt{2}\phi}{\sigma}\right|} e^{-(\theta - [\pi/2 - m_H])^2 / 2\sigma_H^2}, 0 \leq \theta \leq \pi, 0 \leq \phi \leq 2\pi \quad (4)$$

$$P_\theta(\theta, \phi) = A_\theta e^{-\left|\frac{\sqrt{2}\phi}{\sigma}\right|} e^{-(\theta - [\pi/2 - m_V])^2 / 2\sigma_V^2}, 0 \leq \theta \leq \pi, 0 \leq \phi \leq 2\pi \quad (5)$$

For these pdfs, suitable statistic moments will be $\sigma = 24^\circ$, $\sigma_H = 9^\circ$, $\sigma_V = 11^\circ$ and $m_V = 4^\circ$, $m_V = 2^\circ$. MEG will be study for XPRs between 0 and 11, although measurements point out values around 7 dB.

Indoor-Outdoor Environment

The antenna is assumed to be working outside a building, but close to the point access system. This corresponds to traditional gaussian pdfs in elevation and uniform distribution in azimuth. Therefore, for the DPDA and PF-DPDA antennas:

$$P_\phi(\theta, \phi) = A_\phi e^{-(\theta - [\pi/2 - m_H])^2 / 2\sigma_H^2}, 0 \leq \theta \leq \pi, 0 \leq \phi \leq 2\pi \quad (6)$$

$$P_\theta(\theta, \phi) = A_\theta e^{-(\theta - [\pi/2 - m_V])^2 / 2\sigma_V^2}, 0 \leq \theta \leq \pi, 0 \leq \phi \leq 2\pi \quad (7)$$

In both cases, A_θ and A_ϕ are constants that must fulfill:

$$\int_0^{2\pi} \int_0^\pi P_\theta(\theta, \phi) \sin \theta d\theta d\phi = \int_0^{2\pi} \int_0^\pi P_\phi(\theta, \phi) \sin \theta d\theta d\phi = 1 \quad (8)$$

For these pdfs, suitable statistic moments will be $\sigma_H = 8^\circ$, $\sigma_V = 15^\circ$ and $m_V = 1^\circ$, $m_V = 2^\circ$. MEG will be study for XPRs between 0 and 11, although measurements point out values around 11 dB.

4.3 Results

Fig. 7 shows results for MEG in indoor-outdoor environment, for both frequency bands. As expected, if XPR increases, the MEG is improving approaching to theoretical Gain.

As seen, the antenna performance is worse at the higher frequency than at lower, and the antennas have almost the same MEG, with slightly differences. Fig 8 presents the results for the PF-DPDA in both environments. It is revealed that, in the case of the indoor environment, the MEG is slightly worse. As the Laplacian distribution is sharper than the uniform in the center, the indoor MEG is lower compared to the outdoor MEG.

Fig. 7. MEG in indoor-outdoor environment

Fig. 8. MEG in indoor-outdoor environment

5 Conclusion

This paper shows a novel genetically pre-fractal printed dipole antenna for WLAN frequency bands. The antenna is analyzed in classical terms showing good performances in both bands. Additionally, the Mean Effective Gain is

obtained two typical scenarios, revealing an identical performance in the compacted antenna and the standard.

Acknowledgement

This work has been funded by the Ministry of Education and Science and the European funds of regional development (FEDER) under the project TEC 2004-04529/TCM and the European Union through the Program Marco under the project PULSERS PHASE-2 (Pervasive Ultra-wideband Low Spectral Energy Radio Systems PHASE 2).

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